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EXPERIMENTAL WAKE SURVEY BEHIND A 120°-INCLUDED-ANGLE CONE AT ANGLES OF ATTACK OF 0° AND 5°, MACH NUMBERS FROM 1.60 TO 3.95, AND LONGITUDINAL STATIONS VARYING FROM 1.0 TO 8.39 BODY DIAMETERS

by Clarence A. Brown, Jr., James F. Campbell, and Dorothy H. Tudor

Langley Research Center
Hampton, Va. 23365

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16. Abstract

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SUMMARY

An investigation was conducted to obtain flow properties in the wake of a 120°-included-angle cone at Mach numbers from 1.60 to 3.95 and at angles of attack of 0° and 5°. The wake flow properties were calculated from total and static pressures measured with a pressure rake at longitudinal stations varying from 1.0 to 8.39 body diameters and lateral stations varying from -0.42 to 3.0 body diameters. These measurements showed a consistent trend throughout the range of Mach numbers and longitudinal distances and an increase in dynamic pressure with increasing downstream position.

INTRODUCTION

Investigations have shown that many parameters affect the drag and stability characteristics of decelerator systems. Recently, attention has been given to landing an unmanned instrumented payload on the planet Mars. Consideration of the thin atmosphere associated with Mars has resulted in entry designs that have a low ballistic coefficient and utilize a parachute for landing. Many designs have indicated that the parachute would be deployed behind a blunt body at speeds from high subsonic to high supersonic. Because of the complexity of the flow field generated by a blunt body, it is desirable to obtain experimentally the flow characteristics of this region. Results of several investigations to define the flow field behind blunt bodies can be found in references 1 to 4.

An investigation was conducted to obtain flow properties in the wake of a 120°-included-angle cone at Mach numbers from 1.60 to 3.95 and at angles of attack of 0° and 5°. The wake flow properties were calculated from total and static pressures measured with a pressure rake at longitudinal stations varying 1.0 to 8.39 body diameters and lateral stations varying from -0.42 to 3.0 body diameters. Free-stream Reynolds number

was 1.65×10^6 per foot $\left(5.42 \times 10^6\right.$ per meter$\left.\right)$ for most of the study. To evaluate the effect of a reduced Reynolds number, one set of data was taken at a Reynolds number of 1.0×10^6 per foot $\left(3.28 \times 10^6\right.$ per meter$\left.\right)$.

In addition to the 120°-included-angle cone, a model of the entry vehicle used in the SPED-II decelerator program was also tested to determine the center-line wake for longitudinal stations varying from 1.0 to 8.39 body diameters. This configuration was of interest because the configuration is a hollow cone with a small-diameter center body. The effect of the hollow cone on the wake of the SPED-II vehicle is of interest to the decelerator program.

Tests have been made at Mach numbers from 1.60 to 3.95 on four different configurations, two 120°-included-angle cones, a 140°-included-angle cone, and the Viking entry body. This report covers data for the two 120°-included-angle cones and is intended to make these data without analysis available to interested persons.

SYMBOLS

D	cone base diameter, 4.80 inches (12.19 cm)
M_l	local Mach number
M_∞	free-stream Mach number
p_l	local static pressure, psf (N/m²)
p_∞	free-stream static pressure, psf (N/m²)
$p_{t,\infty}$	free-stream total pressure, psf (N/m²)
q_l	local dynamic pressure, psf (N/m²)
q_∞	free-stream dynamic pressure, psf (N/m²)
R	Reynolds number
T_o	stagnation temperature
V_l	local velocity
V_∞	free-stream velocity

x	longitudinal distance downstream from model base, inches (centimeters)
y	lateral distance measured from model-rake plane, inches (centimeters)
z	vertical distance measured in model-rake plane at zero angle of attack of model, inches (centimeters)
α	angle of attack of model center line, degrees

APPARATUS

Wind Tunnel

The tests were conducted in both the low and the high Mach number test sections of the Langley Unitary Plan wind tunnel (ref. 5). The test section is of the variable-pressure, continuous-flow type. Each of the test sections is approximately 4 feet (1.2 meters) square and 7 feet (2.1 meters) long. The nozzles leading to each test section are of the asymmetric sliding-block type. Use of these nozzles permits a continuous variation of Mach number from approximately 1.5 to 2.9 in the low Mach number test section and from approximately 2.3 to 4.7 in the high Mach number test section.

Models and Instrumentation

A sketch of the models used in the test program is shown in figure 1. The 120°-included-angle cone (fig. 1(a)) was constructed of polished aluminum and had a base diameter of 4.80 inches (12.19 cm). The entry vehicle used on the SPED-II decelerator program was also of interest, and limited tests were performed on this vehicle. The SPED-II vehicle was a 120°-included-angle hollow cone with a spherical radius at the apex (fig. 1(b)) and a small-diameter center body. It was constructed of polished aluminum and had a base diameter of 4.80 inches (12.19 cm).

The cone models were supported in the test section by a horizontal cantilevered strut (fig. 2) having a sharp leading edge with a maximum cross-sectional thickness of about 0.375 inch (0.953 cm). The use of the horizontal cantilevered strut eliminated the possibility of obtaining schlieren photographs during the tests.

A pressure rake, illustrated in figure 3, was used to perform the wake survey behind the bodies. The rake was 10.0 inches (25.40 cm) high and was composed of 41 total-pressure tubes 0.25 inch (0.64 cm) apart and 21 static-pressure tubes 0.50 inch (1.27 cm) apart. The rake was connected to a sting, which in turn was attached to a standard support system. The pressures were recorded by using three 48-channel

pressure-scanning valves. Two gages used to record total pressure had a maximum range of 7.50 psia ($51.7\ kN/m^2$). The gage used to record the static pressure had a maximum range of 3.00 psia ($20.68\ kN/m^2$).

TESTS AND ACCURACY

The tests were performed at Mach numbers of 1.60, 2.30, 2.96, and 3.95. The Reynolds number was 1.65×10^6 per foot $\left(5.42 \times 10^6 \text{ per meter}\right)$ for both configurations except for one test at a Mach number of 2.30 for the 120°-included-angle cone. During this test the Reynolds number was reduced to 1.0×10^6 per foot $\left(3.28 \times 10^6 \text{ per meter}\right)$. The stagnation dewpoint was maintained at -30° F (239° K) in order to avoid condensation effects. The test conditions for each configuration were as follows:

M_∞	T_o, $^{\circ}F$	T_o, $^{\circ}K$	$p_{t,\infty}$, psf	$p_{t,\infty}$, N/m^2	q_∞, psf	q_∞, N/m^2
120° cone; $\alpha = 0^{\circ}$; $R = 1.65 \times 10^6$ per foot $\left(5.42 \times 10^6 \text{ per meter}\right)$						
1.60	150	339	942.6	45 131.93	397.41	19 028.09
2.30	150	339	1268.3	60 726.53	375.60	17 983.32
2.96	150	339	1790.5	85 729.60	317.49	15 201.50
3.95	175	353	3190.1	152 742.81	245.34	11 746.94
120° cone; $\alpha = 0^{\circ}$; $R = 1.0 \times 10^6$ per foot $\left(3.28 \times 10^6 \text{ per meter}\right)$						
2.30	150	339	769.6	36 848.65	227.91	10 912.39
120° cone; $\alpha = 5^{\circ}$; $R = 1.65 \times 10^6$ per foot $\left(5.42 \times 10^6 \text{ per meter}\right)$						
1.60	150	339	943.0	45 151.08	397.57	19 035.75
2.30	150	339	1263.5	60 496.71	374.15	17 914.40
2.96	150	339	1793.0	85 849.30	317.92	15 222.09
3.95	175	353	3187.9	152 637.47	245.19	11 739.76
SPED-II vehicle; $\alpha = 0^{\circ}$; $R = 1.65 \times 10^6$ per foot $\left(5.42 \times 10^6 \text{ per meter}\right)$						
1.60	150	339	945.6	45 275.57	398.67	19 088.42

The pressures in the wake of the cones were measured by means of electrically actuated pressure-scanning valves that record essentially instantaneous values. The rake was mounted vertically in the tunnel and was positioned in a longitudinal direction measured from the base of the cone. The rake was moved in a lateral direction (y-direction) at three selected longitudinal stations. At the remaining longitudinal stations, the rake was not traversed in a lateral direction. A schematic representation of the lateral and longitudinal stations is presented in figure 4. Accuracy of the pressure-scanning valves

is within 1 percent of the full scale of the gage and includes all errors of linearity, hysteresis, and repeatability. The free-stream stagnation pressure was measured with a precision mercury manometer, the accuracy of which is ±0.50 psf (±23.94 N/m^2).

The accuracy of the individual quantities is estimated to be within the following limits:

$p_{t,\infty}$	±11.0 psf (526.68 N/m^2)
p_1	±7.0 psf (335.16 N/m^2)
x	0.01 inch (0.0254 cm)
y	0.01 inch (0.0254 cm)
M_∞ at 1.60	±0.01
M_∞ at 2.30	±0.015
M_∞ at 2.96	±0.02
M_∞ at 3.95	±0.05

TABULATION OF EXPERIMENTAL DATA

Flow properties calculated from measured total and static pressures in the wake of the 120°-included-angle cone and the SPED-II vehicle are presented in tables 1 to 10. The tabulations consist of the local flow properties of Mach number, velocity, and static and dynamic pressures, each of which has been nondimensionalized by its respective free-stream value. The data are identified by the geometric information necessary to determine the longitudinal and lateral position in the flow field aft of the cone. The appropriate normal-shock expressions and isentropic-flow relations were used in conjunction with the measured total and static pressures to obtain the desired flow properties.

The pressure rake is designed with a displacement of about 0.50 inch (1.27 cm) between the total- and static-pressure tubes. In order to obtain static- and total-pressure data at identical locations, two sets of data were obtained. The data were taken at identical longitudinal and lateral positions by moving the sting to account for the offset between the total and static tubes.

PRESENTATION OF DATA

The flow properties calculated from the measured total and static pressures in the wake of the 120°-included-angle cone and for the SPED-II vehicle are presented in figures 5 to 14 and tables 1 to 10 for Mach numbers of 1.60, 2.30, 2.96, and 3.95 and for cone angles of attack of 0° and 5°. These data consist of ratios of local to free-stream conditions of Mach number, velocity, and static and dynamic pressures and are presented as a function of vertical distance z/D measured from the model-rake center line in the model-rake plane.

Presented in figure 5 and table 1 are plots and tabulated flow data ratios for a Mach number of 1.60, a cone angle of attack of 0°, x/D distances (longitudinal) varying from 1.0 to 8.39 at a y/D distance (lateral) of zero, and three selected x/D distances (x/D = 2.5, 5.0, and 8.39) at y/D distances varying from -0.42 to 3.0. Figure 6 and table 2 present plots and tabulated flow data ratios for a Mach number of 2.30 for the same cone angle of attack and x/D and y/D distances as figure 5 and table 1.

Figure 7 and table 3 present plots and tabulated flow data ratios for a Mach number of 2.30 at a Reynolds number of 1.0×10^6 per foot $(3.28 \times 10^6$ per meter). With the exception of figure 7 and table 3, all flow data ratios presented in this paper are for a Reynolds number of 1.65×10^6 per foot $(5.42 \times 10^6$ per meter) based on the base diameter. Comparison of figure 7 with figure 6 shows the effect of reducing the Reynolds number from 1.65×10^6 per foot $(5.42 \times 10^6$ per meter) to 1.0×10^6 per foot $(3.28 \times 10^6$ per meter). The flow data ratios are presented for a cone angle of attack of 0°, x/D distances varying from 1.0 to 8.39, and a y/D distance of zero. For the low Reynolds number test, the measuring rake was moved downstream from the 120° cone and measured the flow conditions at the model center line.

Figures 8 and 9 and tables 4 and 5 present plots and tabulated flow data ratios for Mach numbers of 2.96 and 3.95. These data are presented for the same x/D and y/D distances and cone angle of attack as those for figures 5 and 6 and tables 1 and 2 for Mach numbers of 1.60 and 2.30.

Figures 10, 11, 12, and 13 and tables 6, 7, 8, and 9 present plots and tabulated flow data ratios for Mach numbers of 1.60, 2.30, 2.96, and 3.95, a cone angle of attack of 5°, and varying x/D distances. During these tests, no attempt was made to traverse the pressure rake in a lateral direction (y/D); therefore, the data presented are model center-line data at various x/D distances.

Figure 14 and table 10 present plots and tabulated flow data ratios for the SPED-II vehicle at a Mach number of 1.60, cone angle of attack of 0°, x/D distances varying from 1.0 to 8.39, and y/D distance of zero. These data were obtained to determine the effect of a hollow cone configuration, similar to the SPED-II, on parachute performance behind a blunt body.

Although the purpose of this paper is not to analyze these data, several points deserve emphasis. The consistent trends established by the static- and dynamic-pressure data throughout the range of Mach numbers and x/D distances result in well-defined data curves across the wake and are particularly important in the wake recompression region where large pressure gradients are predominant. It is believed that these consistent trends, along with the demonstrated repeatability of the data at all test conditions, make the present data a reliable information source for defining the wake structure and flow properties aft of a 120° cone.

Comparison of figures 5, 6, 8, and 9 shows that for an x/D of 1.0 to 4.0, the dynamic-pressure ratio q_l/q_∞ was greater for the higher Mach number; however, for x/D distances of 4.0 or greater, the q_l/q_∞ ratio becomes greater for the lower Mach numbers tested.

Comparison of figures 10, 11, 12, and 13 indicates that when the cone is placed at 5° angle of attack, the wake at the model-rake center line decreases (approaches free-stream conditions) as the x/D distance is increased, much in the same manner as when the model was at zero angle of attack. More noticeable is the offset of the wake in the model-rake plane due to the cone angle of attack.

Comparison of figures 6 and 7 shows very little effect in the various ratios due to reducing the Reynolds number from 1.65×10^6 per foot $\left(5.42 \times 10^6 \text{ per meter}\right)$ to 1.0×10^6 per foot $\left(3.28 \times 10^6 \text{ per meter}\right)$ for the Mach number tested.

The use of a hollow 120° cone appears to have little effect on the wake conditions. Comparison of figures 5 and 14 shows the wake to be nearly identical with only slight variations for any of the plotted ratios.

The rake used during the investigation covered a z/D distance of ±1.04 body diameters from the wake (or body) center line. As would be expected, the closer the survey rake is to the base of the body, the larger variation in pressure is noted for all Mach numbers. Also for all Mach numbers and all x/D distances of the tests, the dynamic-pressure ratio approached free-stream conditions at the outer edges of the wake. However, some pressure loss is shown in that free-stream conditions are not quite obtained within the distance traversed by the survey rake. The exception to this observation is when the survey rake is placed at a large y/D distance and therefore measures the free-stream conditions of the tunnel.

One of the more important parameters for a decelerator system behind a blunt body is the available dynamic pressure. The test data indicate that decelerator systems imbedded in the wake of a blunt body should be positioned in such a way that the q_l/q_∞ ratio is not degraded in a manner to make the decelerator system ineffective. Examination of these data indicates that an x/D distance on the order of 4 or greater should be used to decrease the loss of dynamic pressure within the wake of a blunt body.

CONCLUDING REMARKS

An investigation was conducted to obtain flow properties in the wake of a 120°-included-angle cone at Mach numbers from 1.60 to 3.95 and at angles of attack of 0° and 5°. The wake flow properties were calculated from total and static pressures measured with a pressure rake at longitudinal stations varying from 1.0 to 8.39 body

diameters and lateral stations varying from -0.42 to 3.0 body diameters. These measurements showed a consistent trend throughout the range of Mach numbers and longitudinal distances and an increase in dynamic pressure with increasing downstream position.

Langley Research Center,
National Aeronautics and Space Administration,
Hampton, Va., October 22, 1970.

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TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 221.91 psf (10625.00 N/m^2);
q_∞ = 397.66 psf (19040.00 N/m^2);
$p_{t,\infty}$ = 943.20 psf (45160.66 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7844	.9049	1.0741	1.0472
.988	.7616	.9087	1.0924	1.0583
.936	.7388	.8859	1.0951	1.0599
.884	.7116	.8838	1.1144	1.0714
.832	.6844	.8733	1.1296	1.0802
.780	.6681	.8494	1.1275	1.0790
.728	.6518	.8371	1.1332	1.0823
.676	.6171	.8295	1.1594	1.0972
.624	.5823	.6872	1.0863	1.0546
.572	.5769	.1619	.5297	.6090
.520	.5714	.0285	.2235	.2714
.468	.5704	.0058	.1009	.1237
.416	.5693	.0004	.0261	.0320
.364	.5682	0.0000	0.0000	0.0000
.312	.5671	0.0000	0.0000	0.0000
.260	.5671	0.0000	0.0000	0.0000
.208	.5671	0.0000	0.0000	0.0000
.156	.5671	0.0000	0.0000	0.0000
.104	.5671	0.0000	0.0000	0.0000
.052	.5660	0.0000	0.0000	0.0000
0.000	.5671	0.0000	0.0000	0.0000
-.052	.5660	0.0000	0.0000	0.0000
-.104	.5649	.0001	.0154	.0190
-.156	.5660	0.0000	0.0000	0.0000
-.208	.5671	0.0000	0.0000	0.0000
-.260	.5671	.0020	.0586	.0720
-.312	.5671	.0020	.0586	.0720
-.364	.5671	.0050	.0935	.1147
-.416	.5671	.0050	.0935	.1147
-.468	.5693	.0068	.1089	.1335
-.520	.5714	.0232	.2014	.2451
-.572	.5725	.1849	.5683	.6473
-.624	.5736	.6962	1.1017	1.0639
-.676	.6095	.8334	1.1694	1.1028
-.728	.6453	.8509	1.1483	1.0909
-.780	.6714	.8516	1.1262	1.0783
-.832	.6975	.8689	1.1161	1.0724
-.884	.7235	.8812	1.1036	1.0650
-.936	.7496	.8902	1.0898	1.0567
-.988	.7779	.9072	1.0799	1.0508
-1.040	.8061	.9074	1.0610	1.0391

(b) $x/D = 1.5$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 221.95 psf (10627.25 N/m^2);
q_∞ = 397.74 psf (10944.04 N/m^2);
$p_{t,\infty}$ = 943.40 psf (45170.24 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9124	.9313	1.0103	1.0068
.988	.8896	.9202	1.0171	1.0112
.936	.8668	.9091	1.0241	1.0158
.884	.8201	.9037	1.0498	1.0321
.832	.7734	.9016	1.0797	1.0506
.780	.7277	.8859	1.1033	1.0648
.728	.6821	.8701	1.1294	1.0802
.676	.6495	.8589	1.1499	1.0919
.624	.6169	.8492	1.1732	1.1049
.572	.5952	.6398	1.0368	1.0239
.520	.5735	.3078	.7326	.7979
.468	.5746	.1079	.4334	.5090
.416	.5757	.0263	.2136	.2596
.364	.5757	.0058	.1004	.1231
.312	.5757	.0028	.0697	.0856
.260	.5778	0.0000	0.0000	0.0000
.208	.5800	0.0000	0.0000	0.0000
.156	.5833	0.0000	0.0000	0.0000
.104	.5854	0.0000	0.0000	0.0000
.052	.5822	0.0000	0.0000	0.0000
0.000	.5909	0.0000	0.0000	0.0000
-.052	.5876	0.0000	0.0000	0.0000
-.104	.5844	0.0000	0.0000	0.0000
-.156	.5789	0.0000	0.0000	0.0000
-.208	.5735	.0010	.0415	.0511
-.260	.5735	.0010	.0415	.0511
-.312	.5735	.0070	.1104	.1354
-.364	.5757	.0088	.1235	.1513
-.416	.5778	.0336	.2413	.2923
-.468	.5811	.1148	.4444	.5207
-.520	.5844	.3072	.7251	.7914
-.572	.6083	.7043	1.0761	1.0484
-.624	.6322	.8501	1.1596	1.0973
-.676	.6832	.8633	1.1241	1.0771
-.728	.7343	.8715	1.0894	1.0565
-.780	.7810	.8853	1.0647	1.0414
-.832	.8277	.8957	1.0403	1.0261
-.884	.8559	.9059	1.0288	1.0188
-.936	.8841	.9145	1.0170	1.0111
-.988	.8635	.9330	1.0395	1.0256
-1.040	.8429	.9432	1.0578	1.0371

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0.0$; $\alpha = 0^\circ$;

$p_\infty = 221.95$ psf (10627.25 N/m^2);
$q_\infty = 397.74$ psf (19044.04 N/m^2);
$p_{t,\infty} = 943.40$ psf (45170.24 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7386	.9079	1.1087	1.0680
.988	.7266	.9049	1.1159	1.0723
.936	.7147	.8952	1.1192	1.0742
.884	.6941	.8870	1.1305	1.0808
.832	.6734	.8887	1.1488	1.0912
.780	.6702	.8826	1.1476	1.0906
.728	.6669	.8732	1.1443	1.0887
.676	.6767	.8716	1.1349	1.0833
.624	.6865	.8833	1.1343	1.0830
.572	.6962	.8733	1.1200	1.0747
.520	.7060	.8019	1.0657	1.0420
.468	.7071	.4445	.7929	.8480
.416	.7082	.2546	.5996	.6776
.364	.7093	.1274	.4238	.4986
.312	.7104	.0574	.2842	.3424
.260	.7136	.0218	.1749	.2135
.208	.7169	0.0000	0.0000	0.0000
.156	.7212	0.0000	0.0000	0.0000
.104	.7245	0.0000	0.0000	0.0000
.052	.7169	0.0000	0.0000	0.0000
0.000	.7321	0.0000	0.0000	0.0000
-.052	.7245	0.0000	0.0000	0.0000
-.104	.7169	0.0000	0.0000	0.0000
-.156	.7125	0.0000	0.0000	0.0000
-.208	.7082	.0020	.0529	.0650
-.260	.7006	.0181	.1606	.1961
-.312	.6930	.0642	.3043	.3657
-.364	.6995	.1129	.4018	.4748
-.416	.7060	.2739	.6229	.6996
-.468	.7028	.5594	.8922	.9247
-.520	.6995	.8067	1.0739	1.0471
-.572	.6865	.8705	1.1261	1.0782
-.624	.6734	.8743	1.1394	1.0859
-.676	.6723	.8728	1.1394	1.0859
-.728	.6713	.8730	1.1404	1.0865
-.780	.6854	.8724	1.1282	1.0794
-.832	.6995	.8783	1.1206	1.0750
-.884	.7093	.8834	1.1160	1.0723
-.936	.7190	.9018	1.1199	1.0746
-.988	.7397	.9000	1.1031	1.0647
-1.040	.7603	.9066	1.0919	1.0580

(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^\circ$;

$p_\infty = 221.20$ psf (10591.21 N/m^2);
$q_\infty = 396.39$ psf (18979.44 N/m^2);
$p_{t,\infty} = 940.20$ psf (45017.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1294	1.0134	.9473	.9642
.988	1.1359	1.0089	.9424	.9608
.936	1.1424	1.0111	.9407	.9596
.884	1.1446	1.0073	.9381	.9578
.832	1.1468	1.0052	.9362	.9564
.780	1.1294	1.0168	.9489	.9653
.728	1.1119	1.0216	.9585	.9720
.676	1.1065	1.0124	.9566	.9706
.624	1.1010	1.0151	.9602	.9731
.572	1.1054	1.0143	.9579	.9716
.520	1.1097	1.0085	.9533	.9684
.468	1.1087	1.0137	.9562	.9704
.416	1.1076	1.0139	.9568	.9708
.364	1.1043	1.0145	.9585	.9720
.312	1.1010	1.0083	.9570	.9709
.260	1.0792	1.0172	.9709	.9804
.208	1.0574	1.0177	.9810	.9873
.156	1.1119	1.0081	.9522	.9676
.104	1.0901	1.0102	.9627	.9748
.052	1.0879	1.0123	.9646	.9762
0.000	1.1228	1.0010	.9442	.9620
-.052	1.1206	1.0055	.9472	.9642
-.104	1.1185	1.0042	.9475	.9644
-.156	1.1239	1.0066	.9464	.9636
-.208	1.1294	1.0039	.9428	.9611
-.260	1.1272	1.0077	.9455	.9630
-.312	1.1250	1.0098	.9474	.9643
-.364	1.1305	1.0139	.9470	.9640
-.416	1.1359	1.0078	.9419	.9605
-.468	1.1370	1.0161	.9453	.9628
-.520	1.1381	1.0125	.9432	.9614
-.572	1.1403	1.0121	.9421	.9606
-.624	1.1424	1.0033	.9371	.9571
-.676	1.1435	1.0115	.9405	.9595
-.728	1.1446	1.0080	.9384	.9580
-.780	1.1501	1.0070	.9357	.9561
-.832	1.1555	1.0094	.9346	.9553
-.884	1.1566	1.0075	.9333	.9544
-.936	1.1577	1.0107	.9343	.9551
-.988	1.1566	1.0075	.9333	.9544
-1.040	1.1555	1.0094	.9346	.9553

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^\circ$;

p_∞ = 221.06 psf (10584.45 N/m^2)
q_∞ = 396.14 psf (18967.33 N/m^2)
$p_{t,\infty}$ = 939.60 psf (44988.29 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8957	.9743	1.0430	1.0278
.988	.9000	.9837	1.0454	1.0294
.936	.9044	.9678	1.0345	1.0224
.884	.9000	.9803	1.0436	1.0282
.832	.8957	.9693	1.0403	1.0261
.780	.8946	.9561	1.0338	1.0220
.728	.8935	.9562	1.0345	1.0224
.676	.8771	.9557	1.0438	1.0283
.624	.8607	.9601	1.0562	1.0361
.572	.8596	.9553	1.0542	1.0349
.520	.8585	.9622	1.0586	1.0376
.468	.8596	.9553	1.0542	1.0349
.416	.8607	.9585	1.0552	1.0355
.364	.8531	.9564	1.0588	1.0378
.312	.8454	.9526	1.0615	1.0394
.260	.8138	.9563	1.0840	1.0533
.208	.7821	.9616	1.1088	1.0681
.156	.8432	.9497	1.0612	1.0393
.104	.8116	.9634	1.0895	1.0566
.052	.8072	.9557	1.0881	1.0557
0.000	.8411	.9634	1.0703	1.0449
-.052	.8367	.9495	1.0653	1.0418
-.104	.8323	.9620	1.0751	1.0478
-.156	.8389	.9509	1.0647	1.0414
-.208	.8454	.9514	1.0608	1.0390
-.260	.8454	.9514	1.0608	1.0390
-.312	.8454	.9514	1.0608	1.0390
-.364	.8509	.9522	1.0578	1.0371
-.416	.8564	.9529	1.0549	1.0353
-.468	.8585	.9526	1.0533	1.0343
-.520	.8607	.9555	1.0536	1.0345
-.572	.8629	.9568	1.0530	1.0341
-.624	.8651	.9699	1.0588	1.0378
-.676	.8826	.9585	1.0422	1.0273
-.728	.9000	.9673	1.0367	1.0238
-.780	.9033	.9617	1.0318	1.0207
-.832	.9066	.9679	1.0332	1.0216
-.884	.9110	.9839	1.0393	1.0255
-.936	.9153	.9714	1.0302	1.0197
-.988	.9208	.9873	1.0355	1.0230
-1.040	.9263	.9763	1.0266	1.0174

(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^\circ$;

p_∞ = 221.11 psf (10586.70 N/m^2);
q_∞ = 396.23 psf (18971.37 N/m^2);
$p_{t,\infty}$ = 939.80 psf (44997.87 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7948	.9513	1.0940	1.0593
.988	.7970	.9392	1.0856	1.0542
.936	.7992	.9472	1.0887	1.0561
.884	.7948	.9312	1.0824	1.0523
.832	.7905	.9303	1.0848	1.0537
.780	.7905	.9253	1.0819	1.0520
.728	.7905	.9236	1.0809	1.0514
.676	.7752	.9228	1.0911	1.0575
.624	.7599	.9237	1.1025	1.0644
.572	.7555	.9227	1.1051	1.0659
.520	.7512	.9218	1.1078	1.0675
.468	.7588	.9188	1.1004	1.0631
.416	.7664	.9176	1.0942	1.0594
.364	.7555	.9160	1.1011	1.0635
.312	.7446	.9162	1.1092	1.0683
.260	.7162	.9209	1.1339	1.0827
.208	.6878	.9239	1.1589	1.0970
.156	.7413	.9151	1.1110	1.0694
.104	.7129	.9197	1.1358	1.0838
.052	.7097	.9203	1.1388	1.0855
0.000	.7381	.9156	1.1138	1.0710
-.052	.7348	.9150	1.1159	1.0723
-.104	.7315	.9155	1.1187	1.0739
-.156	.7315	.9155	1.1187	1.0739
-.208	.7315	.9155	1.1187	1.0739
-.260	.7337	.9152	1.1168	1.0728
-.312	.7359	.9165	1.1160	1.0723
-.364	.7392	.9159	1.1132	1.0707
-.416	.7424	.9204	1.1134	1.0708
-.468	.7490	.9193	1.1079	1.0675
-.520	.7555	.9199	1.1034	1.0649
-.572	.7544	.9217	1.1053	1.0660
-.624	.7533	.9253	1.1082	1.0678
-.676	.7686	.9244	1.0967	1.0609
-.728	.7839	.9235	1.0854	1.0541
-.780	.7861	.9248	1.0847	1.0536
-.832	.7883	.9278	1.0849	1.0538
-.884	.7937	.9319	1.0835	1.0530
-.936	.7992	.9393	1.0841	1.0533
-.988	.8068	.9364	1.0773	1.0492
-1.040	.8145	.9535	1.0820	1.0520

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10⁶ PER FOOT (5.42 × 10⁶ PER METER) – Continued

(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^\circ$;

$p_\infty = 221.06$ psf (10584.45 N/m^2);
$q_\infty = 396.14$ psf (18967.33 N/m^2);
$p_{t,\infty} = 939.60$ psf (44988.29 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7251	.9174	1.1248	1.0775
.988	.7273	.9087	1.1178	1.0734
.936	.7295	.9084	1.1159	1.0723
.884	.7240	.9009	1.1155	1.0720
.832	.7186	.8985	1.1182	1.0736
.780	.7131	.8943	1.1199	1.0746
.728	.7076	.8952	1.1248	1.0774
.676	.7000	.8915	1.1285	1.0796
.624	.6924	.8911	1.1345	1.0831
.572	.6891	.8899	1.1364	1.0842
.520	.6858	.8905	1.1395	1.0859
.468	.6967	.8887	1.1294	1.0801
.416	.7076	.8869	1.1195	1.0744
.364	.7033	.8876	1.1234	1.0767
.312	.6989	.8900	1.1285	1.0796
.260	.7000	.8898	1.1275	1.0790
.208	.7011	.8896	1.1265	1.0784
.156	.6967	.8904	1.1305	1.0807
.104	.6978	.8935	1.1316	1.0814
.052	.6945	.8941	1.1346	1.0831
0.000	.6945	.8941	1.1346	1.0831
−.052	.6913	.8885	1.1337	1.0826
−.104	.6880	.8890	1.1367	1.0844
−.156	.6880	.8873	1.1357	1.0837
−.208	.6880	.8873	1.1357	1.0837
−.260	.6836	.8880	1.1398	1.0861
−.312	.6792	.8888	1.1439	1.0884
−.364	.6738	.8880	1.1480	1.0908
−.416	.6683	.8889	1.1533	1.0938
−.468	.6803	.8869	1.1418	1.0872
−.520	.6924	.8849	1.1306	1.0808
−.572	.6814	.8884	1.1418	1.0873
−.624	.6705	.8902	1.1522	1.0932
−.676	.6858	.8894	1.1388	1.0855
−.728	.7011	.8919	1.1279	1.0792
−.780	.7044	.8930	1.1260	1.0781
−.832	.7076	.8958	1.1251	1.0776
−.884	.7098	.9004	1.1263	1.0783
−.936	.7120	.9001	1.1243	1.0772
−.988	.7186	.9057	1.1227	1.0762
−1.040	.7251	.9063	1.1180	1.0735

(h) $x/D = 2.5$; $y/D = .83$; $\alpha = 0^\circ$;

$p_\infty = 221.08$ psf (10585.57 N/m^2);
$q_\infty = 396.18$ psf (18969.35 N/m^2);
$p_{t,\infty} = 939.70$ psf (44993.08 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7185	.9366	1.1418	1.0872
.988	.7218	.9228	1.1307	1.0809
.936	.7250	.9306	1.1329	1.0822
.884	.7294	.9148	1.1199	1.0746
.832	.7338	.9124	1.1151	1.0718
.780	.7469	.9003	1.0979	1.0616
.728	.7600	.8997	1.0881	1.0557
.676	.7392	.8999	1.1033	1.0648
.624	.7185	.9000	1.1192	1.0742
.572	.7239	.8974	1.1134	1.0708
.520	.7294	.9015	1.1117	1.0698
.468	.7501	.9014	1.0962	1.0606
.416	.7709	.9046	1.0833	1.0528
.364	.7796	.9048	1.0773	1.0491
.312	.7884	.9083	1.0734	1.0468
.260	.8222	.9060	1.0497	1.0321
.208	.8561	.9002	1.0255	1.0166
.156	.8080	.9151	1.0642	1.0411
.104	.8419	.9143	1.0422	1.0273
.052	.8320	.9194	1.0512	1.0330
0.000	.8277	.9184	1.0534	1.0344
−.052	.8178	.9141	1.0572	1.0367
−.104	.8080	.9157	1.0646	1.0413
−.156	.8026	.9100	1.0648	1.0415
−.208	.7971	.9109	1.0690	1.0441
−.260	.7785	.9039	1.0775	1.0493
−.312	.7600	.9004	1.0885	1.0559
−.364	.7392	.8971	1.1016	1.0638
−.416	.7185	.8939	1.1154	1.0720
−.468	.7141	.8879	1.1151	1.0718
−.520	.7097	.8836	1.1158	1.0722
−.572	.6868	.8874	1.1367	1.0843
−.624	.6639	.8912	1.1586	1.0968
−.676	.6759	.8892	1.1470	1.0902
−.728	.6879	.8872	1.1357	1.0837
−.780	.6890	.8871	1.1347	1.0832
−.832	.6901	.8885	1.1347	1.0832
−.884	.6912	.8917	1.1358	1.0838
−.936	.6923	.8915	1.1348	1.0833
−.988	.6977	.8973	1.1340	1.0828
−1.040	.7032	.9014	1.1322	1.0818

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(i) $x/D = 2.5$; $y/D = .63$; $\alpha = 0^\circ$;

p_∞ = 221.11 psf (10586.70 N/m²);
q_∞ = 396.23 psf (18971.37 N/m²);
$p_{t,\infty}$ = 939.80 psf (44997.87 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8210	.9358	1.0676	1.0432
.988	.8221	.9339	1.0658	1.0421
.936	.8232	.9321	1.0641	1.0410
.884	.8210	.9257	1.0619	1.0396
.832	.8189	.9278	1.0644	1.0412
.780	.8287	.9244	1.0562	1.0361
.728	.8385	.9178	1.0462	1.0298
.676	.8505	.9207	1.0405	1.0262
.624	.8625	.9288	1.0377	1.0244
.572	.8898	.9274	1.0209	1.0137
.520	.9171	.9278	1.0058	1.0038
.468	.9400	.9288	.9940	.9960
.416	.9630	.9265	.9809	.9872
.364	.9673	.9291	.9800	.9867
.312	.9717	.9300	.9783	.9855
.260	.9892	.9236	.9663	.9773
.208	1.0066	.9154	.9536	.9686
.156	.9881	.9170	.9634	.9753
.104	1.0056	.9123	.9525	.9678
.052	.9990	.9134	.9562	.9704
0.000	1.0045	.9108	.9522	.9676
-.052	.9979	.9115	.9557	.9700
-.104	.9914	.9143	.9604	.9732
-.156	.9924	.9175	.9615	.9740
-.208	.9935	.9207	.9626	.9748
-.260	.9750	.9239	.9735	.9822
-.312	.9564	.9255	.9837	.9891
-.364	.9477	.9220	.9863	.9909
-.416	.9390	.9168	.9881	.9921
-.468	.9073	.9156	1.0045	1.0030
-.520	.8756	.9143	1.0218	1.0143
-.572	.8516	.9167	1.0375	1.0243
-.624	.8276	.9208	1.0548	1.0353
-.676	.8232	.9148	1.0542	1.0349
-.728	.8189	.9189	1.0593	1.0381
-.780	.8189	.9189	1.0593	1.0381
-.832	.8189	.9189	1.0593	1.0381
-.884	.8178	.9225	1.0621	1.0398
-.936	.8167	.9277	1.0658	1.0421
-.988	.8254	.9312	1.0622	1.0398
-1.040	.8341	.9364	1.0596	1.0382

(j) $x/D = 2.5$; $y/D = .42$; $\alpha = 0^\circ$;

p_∞ = 221.01 psf (10582.20 N/m²);
q_∞ = 396.06 psf (18963.29 N/m²);
$p_{t,\infty}$ = 939.40 psf (44978.71 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7602	.9218	1.1012	1.0636
.988	.7635	.9179	1.0965	1.0608
.936	.7668	.9224	1.0968	1.0609
.884	.7755	.9159	1.0868	1.0549
.832	.7842	.9195	1.0828	1.0525
.780	.8126	.9164	1.0619	1.0397
.728	.8410	.9149	1.0430	1.0278
.676	.8673	.9205	1.0302	1.0197
.624	.8935	.9294	1.0199	1.0130
.572	.9295	.9316	1.0011	1.0007
.520	.9656	.9253	.9789	.9859
.468	.9863	.9217	.9667	.9776
.416	1.0071	.8961	.9433	.9614
.364	1.0049	.8542	.9220	.9463
.312	1.0027	.7954	.8906	.9236
.260	.9929	.6727	.8231	.8721
.208	.9830	.5621	.7562	.8178
.156	.9983	.4441	.6670	.7402
.104	.9885	.4132	.6465	.7215
.052	.9830	.4014	.6390	.7146
0.000	.9940	.3556	.5981	.6762
-.052	.9885	.3784	.6187	.6956
-.104	.9830	.4292	.6607	.7345
-.156	.9918	.5284	.7299	.7956
-.208	1.0005	.6317	.7946	.8493
-.260	.9994	.7419	.8616	.9018
-.312	.9983	.8476	.9214	.9459
-.364	.9972	.8867	.9430	.9612
-.416	.9961	.9089	.9552	.9697
-.468	.9623	.9148	.9750	.9833
-.520	.9284	.9157	.9931	.9954
-.572	.8858	.9214	1.0199	1.0130
-.624	.8432	.9203	1.0447	1.0289
-.676	.8203	.9124	1.0547	1.0352
-.728	.7974	.9129	1.0700	1.0447
-.780	.7821	.9088	1.0780	1.0496
-.832	.7668	.9097	1.0892	1.0564
-.884	.7602	.9091	1.0936	1.0590
-.936	.7537	.9136	1.1010	1.0634
-.988	.7591	.9126	1.0965	1.0607
-1.040	.7646	.9234	1.0990	1.0623

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(k) $x/D = 2.5$; $y/D = .21$; $\alpha = 0^\circ$;
p_∞ = 221.04 psf (10583.32 N/m^2);
q_∞ = 396.10 psf (18965.31 N/m^2);
$p_{t,\infty}$ = 939.50 psf (44983.50 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7157	.9064	1.1254	1.0778
.988	.7211	.8988	1.1164	1.0726
.936	.7266	.9079	1.1178	1.0734
.884	.7506	.9006	1.0954	1.0601
.832	.7746	.9100	1.0839	1.0532
.780	.8149	.9099	1.0566	1.0364
.728	.8553	.9064	1.0294	1.0192
.676	.8880	.9159	1.0156	1.0102
.624	.9207	.9237	1.0016	1.0010
.572	.9535	.9230	.9839	.9893
.520	.9862	.8987	.9546	.9693
.468	.9873	.8393	.9220	.9463
.416	.9884	.6599	.8171	.8674
.364	.9742	.4606	.6876	.7586
.312	.9600	.2854	.5453	.6246
.260	.9709	.1466	.3886	.4604
.208	.9818	.0642	.2558	.3094
.156	.9818	.0269	.1656	.2022
.104	.9928	.0030	.0554	.0680
.052	.9884	.0024	.0497	.0610
0.000	1.0037	0.0000	0.0000	0.0000
-.052	.9993	.0145	.1204	.1475
-.104	.9949	.0198	.1412	.1728
-.156	.9895	.0403	.2019	.2457
-.208	.9840	.0880	.2990	.3596
-.260	.9797	.1800	.4286	.5039
-.312	.9753	.3586	.6064	.6840
-.364	.9764	.5228	.7318	.7971
-.416	.9775	.7545	.8786	.9146
-.468	.9698	.8847	.9551	.9696
-.520	.9622	.9097	.9723	.9814
-.572	.9218	.9184	.9981	.9988
-.624	.8815	.9203	1.0218	1.0143
-.676	.8477	.9161	1.0396	1.0256
-.728	.8138	.9117	1.0584	1.0375
-.780	.7844	.9066	1.0751	1.0478
-.832	.7549	.9015	1.0928	1.0585
-.884	.7331	.8968	1.1060	1.0664
-.936	.7113	.9004	1.1251	1.0776
-.988	.7135	.9000	1.1232	1.0765
-1.040	.7157	.9114	1.1285	1.0796

(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^\circ$;
p_∞ = 221.65 psf (10612.61 N/m^2);
q_∞ = 397.19 psf (19017.80 N/m^2);
$p_{t,\infty}$ = 942.10 psf (45107.99 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6620	.8919	1.1607	1.0979
.988	.6849	.8881	1.1387	1.0855
.936	.7078	.9026	1.1293	1.0801
.884	.7296	.8990	1.1101	1.0689
.832	.7513	.9071	1.0988	1.0621
.780	.7927	.9085	1.0705	1.0450
.728	.8341	.9082	1.0435	1.0281
.676	.8766	.9193	1.0241	1.0157
.624	.9190	.9254	1.0034	1.0023
.572	.9582	.9303	.9853	.9902
.520	.9974	.9200	.9604	.9733
.468	.9963	.9068	.9540	.9689
.416	.9952	.8025	.8980	.9289
.364	.9887	.6539	.8133	.8643
.312	.9822	.4425	.6712	.7440
.260	.9876	.3193	.5686	.6476
.208	.9931	.1930	.4409	.5170
.156	.9996	.1659	.4074	.4810
.104	1.0050	.1384	.3710	.4410
.052	.9952	.0851	.2923	.3518
0.000	1.0170	.0796	.2798	.3374
-.052	1.0072	.1225	.3488	.4161
-.104	.9974	.1374	.3712	.4411
-.156	.9952	.1511	.3896	.4615
-.208	.9931	.2149	.4652	.5428
-.260	.9876	.2948	.5464	.6257
-.312	.9822	.4506	.6773	.7495
-.364	.9833	.6594	.8189	.8688
-.416	.9844	.8495	.9290	.9513
-.468	.9789	.9094	.9638	.9756
-.520	.9735	.9221	.9733	.9821
-.572	.9288	.9198	.9952	.9968
-.624	.8842	.9192	1.0196	1.0128
-.676	.8493	.9101	1.0351	1.0228
-.728	.8145	.9076	1.0556	1.0358
-.780	.7818	.8998	1.0728	1.0464
-.832	.7492	.8969	1.0942	1.0594
-.884	.7176	.8955	1.1171	1.0730
-.936	.6860	.8957	1.1427	1.0878
-.988	.6751	.8842	1.1444	1.0888
-1.040	.6642	.8960	1.1614	1.0983

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(m) $x/D = 2.5$; $y/D = -.42$; $\alpha = 0^\circ$;

p_∞ = 221.60 psf (10610.36 N/m^2);
q_∞ = 397.11 psf (19013.76 N/m^2);
$p_{t,\infty}$ = 941.90 psf (45098.42 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.5990	.8901	1.2190	1.1296
.988	.6208	.9032	1.2062	1.1228
.936	.6426	.8864	1.1745	1.1056
.884	.6175	.8705	1.1873	1.1126
.832	.5925	.8779	1.2172	1.1287
.780	.6480	.8789	1.1646	1.1001
.728	.7036	.8930	1.1266	1.0785
.676	.7406	.9069	1.1066	1.0668
.624	.7776	.9057	1.0792	1.0503
.572	.8103	.9186	1.0647	1.0414
.520	.8430	.9097	1.0388	1.0252
.468	.8593	.9170	1.0330	1.0215
.416	.8757	.9142	1.0218	1.0142
.364	.8876	.9188	1.0174	1.0114
.312	.8996	.9117	1.0067	1.0044
.260	.9236	.9159	.9959	.9973
.208	.9475	.9067	.9782	.9854
.156	.9639	.8921	.9620	.9744
.104	.9878	.8406	.9225	.9467
.052	.9726	.7300	.8563	.9054
0.000	1.0281	.6558	.7987	.8527
-.052	1.0129	.7308	.8494	.8926
-.104	.9976	.8372	.9161	.9421
-.156	.9867	.8830	.9460	.9633
-.208	.9758	.8900	.9550	.9695
-.260	.9464	.9069	.9789	.9859
-.312	.9170	.9070	.9945	.9964
-.364	.9040	.9126	1.0048	1.0032
-.416	.8909	.9082	1.0097	1.0064
-.468	.8593	.9119	1.0302	1.0197
-.520	.8277	.9106	1.0489	1.0315
-.572	.7961	.9026	1.0648	1.0414
-.624	.7646	.8979	1.0837	1.0531
-.676	.7275	.8957	1.1096	1.0686
-.728	.6905	.8869	1.1333	1.0824
-.780	.6535	.8696	1.1536	1.0940
-.832	.6164	.8657	1.1851	1.1114
-.884	.6328	.8697	1.1724	1.1044
-.936	.6491	.8920	1.1722	1.1044
-.988	.6404	.9034	1.1877	1.1128
-1.040	.6317	.8965	1.1913	1.1148

(n) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^\circ$;

p_∞ = 221.30 psf (10595.71 N/m^2);
q_∞ = 396.56 psf (18987.52 N/m^2);
$p_{t,\infty}$ = 940.60 psf (45036.17 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8087	.9451	1.0810	1.0514
.988	.8915	.9595	1.0374	1.0243
.936	.9744	.9452	.9849	.9900
.884	1.0016	.9472	.9724	.9815
.832	1.0289	.9407	.9562	.9704
.780	1.0365	.9376	.9511	.9669
.728	1.0441	.9329	.9452	.9628
.676	1.0703	.9350	.9346	.9553
.624	1.0964	.9319	.9219	.9463
.572	1.1477	.9294	.8999	.9303
.520	1.1989	.9182	.8751	.9120
.468	1.2261	.9079	.8605	.9010
.416	1.2534	.8737	.8349	.8813
.364	1.2512	.8053	.8023	.8556
.312	1.2490	.7225	.7605	.8214
.260	1.2534	.6153	.7007	.7702
.208	1.2578	.5094	.6364	.7122
.156	1.2643	.4689	.6090	.6865
.104	1.2687	.4234	.5777	.6565
.052	1.2523	.3510	.5294	.6088
0.000	1.2796	.3499	.5229	.6022
-.052	1.2632	.3876	.5539	.6332
-.104	1.2469	.4522	.6022	.6801
-.156	1.2545	.4697	.6119	.6892
-.208	1.2621	.5440	.6565	.73C7
-.260	1.2545	.6045	.6942	.7645
-.312	1.2469	.7409	.7708	.8300
-.364	1.2327	.8441	.8275	.8756
-.416	1.2185	.8948	.8569	.8983
-.468	1.1793	.9227	.8845	.9190
-.520	1.1400	.9265	.9015	.9315
-.572	1.1095	.9321	.9166	.9424
-.624	1.0790	.9258	.9263	.9494
-.676	1.0605	.9308	.9369	.9569
-.728	1.0420	.9307	.9451	.9627
-.780	1.0212	.9361	.9574	.9712
-.832	1.0005	.9347	.9665	.9775
-.884	.9569	.9457	.9941	.9961
-.936	.9133	.9432	1.0162	1.0106
-.988	.8436	.9383	1.0546	1.0351
-1.040	.7738	.9266	1.0942	1.0594

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(o) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^\circ$;
$p_\infty = 221.30$ psf (10595.71 N/m^2);
$q_\infty = 396.56$ psf (18987.52 N/m^2);
$p_{t,\infty} = 940.60$ psf (45036.17 N/m^2);

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1684	.9678	.9101	.9378
.988	1.1717	.9587	.9046	.9338
.936	1.1749	.9615	.9046	.9338
.884	1.1749	.9514	.8998	.9303
.832	1.1749	.9514	.8998	.9303
.780	1.1553	.9516	.9075	.9359
.728	1.1357	.9551	.9171	.9428
.676	1.1455	.9364	.9042	.9335
.624	1.1553	.9346	.8994	.9300
.572	1.1618	.9249	.8922	.9247
.520	1.1684	.9119	.8834	.9182
.468	1.1542	.9026	.8843	.9189
.416	1.1400	.8798	.8785	.9145
.364	1.1379	.8410	.8597	.9004
.312	1.1357	.8056	.8422	.8870
.260	1.1400	.7670	.8203	.8699
.208	1.1444	.7317	.7996	.8534
.156	1.1466	.6880	.7746	.8331
.104	1.1509	.6434	.7477	.8106
.052	1.1379	.6004	.7264	.7925
0.000	1.1575	.5817	.7089	.7774
-.052	1.1444	.6158	.7336	.7987
-.104	1.1313	.6573	.7622	.8228
-.156	1.1422	.7108	.7888	.8447
-.208	1.1531	.7466	.8047	.8575
-.260	1.1488	.7836	.8259	.8743
-.312	1.1444	.8256	.8494	.8925
-.364	1.1477	.8557	.8635	.9033
-.416	1.1509	.8909	.8798	.9155
-.468	1.1564	.9102	.8872	.9210
-.520	1.1618	.9177	.8888	.9222
-.572	1.1673	.9252	.8903	.9233
-.624	1.1727	.9259	.8885	.9220
-.676	1.1695	.9316	.8925	.9249
-.728	1.1662	.9373	.8965	.9279
-.780	1.1662	.9373	.8965	.9279
-.832	1.1662	.9492	.9022	.9320
-.884	1.1673	.9490	.9016	.9316
-.936	1.1684	.9556	.9043	.9336
-.988	1.1662	.9560	.9054	.9343
-1.040	1.1640	.9614	.9088	.9368

(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^\circ$;
$p_\infty = 221.70$ psf (10614.86 N/m^2);
$q_\infty = 397.28$ psf (19021.83 N/m^2);
$p_{t,\infty} = 942.30$ psf (45117.57 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8474	.9765	1.0735	1.0468
.988	.8550	.9668	1.0634	1.0406
.936	.8626	.9756	1.0635	1.0406
.884	.8517	.9674	1.0657	1.0421
.832	.8408	.9692	1.0736	1.0469
.780	.8212	.9692	1.0864	1.0547
.728	.8016	.9724	1.1014	1.0637
.676	.8212	.9692	1.0864	1.0547
.624	.8408	.9659	1.0718	1.0458
.572	.8408	.9642	1.0709	1.0452
.520	.8408	.9659	1.0718	1.0458
.468	.8485	.9646	1.0663	1.0424
.416	.8561	.9633	1.0608	1.0390
.364	.8495	.9644	1.0655	1.0419
.312	.8430	.9639	1.0693	1.0442
.260	.8147	.9669	1.0894	1.0565
.208	.7864	.9716	1.1116	1.0697
.156	.8430	.9622	1.0684	1.0437
.104	.8147	.9686	1.0904	1.0571
.052	.8092	.9695	1.0946	1.0596
0.000	.8430	.9689	1.0720	1.0459
-.052	.8376	.9610	1.0712	1.0454
-.104	.8321	.9619	1.0752	1.0478
-.156	.8321	.9619	1.0752	1.0478
-.208	.8321	.9619	1.0752	1.0478
-.260	.8299	.9606	1.0758	1.0483
-.312	.8278	.9626	1.0784	1.0498
-.364	.8321	.9619	1.0752	1.0478
-.416	.8365	.9612	1.0720	1.0459
-.468	.8365	.9612	1.0720	1.0459
-.520	.8365	.9612	1.0720	1.0459
-.572	.8321	.9619	1.0752	1.0478
-.624	.8278	.9626	1.0784	1.0498
-.676	.8397	.9606	1.0696	1.0444
-.728	.8517	.9586	1.0609	1.0390
-.780	.8528	.9584	1.0601	1.0386
-.832	.8539	.9633	1.0621	1.0398
-.884	.8539	.9599	1.0603	1.0387
-.936	.8539	.9766	1.0694	1.0443
-.988	.8572	.9627	1.0598	1.0384
-1.040	.8604	.9755	1.0648	1.0415

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^\circ$;

p_∞ = 221.77 psf (10618.24 N/m^2);
q_∞ = 397.41 psf (19027.89 N/m^2);
$p_{t,\infty}$ = 942.60 psf (45131.93 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0934	1.0056	.9590	.9723
.988	1.1065	1.0016	.9514	.9671
.936	1.1196	1.0010	.9455	.9630
.884	1.1065	1.0016	.9514	.9671
.832	1.0934	1.0006	.9566	.9707
.780	1.0825	1.0042	.9631	.9752
.728	1.0716	1.0078	.9697	.9797
.676	1.0880	1.0032	.9603	.9732
.624	1.1043	1.0087	.9557	.9701
.572	1.1141	1.0070	.9507	.9666
.520	1.1239	.9968	.9418	.9603
.468	1.1217	1.0006	.9444	.9622
.416	1.1196	1.0060	.9479	.9646
.364	1.1196	1.0010	.9455	.9630
.312	1.1196	.9976	.9440	.9619
.260	1.1108	1.0075	.9524	.9677
.208	1.1021	1.0041	.9545	.9692
.156	1.1337	.9967	.9376	.9574
.104	1.1250	.9983	.9420	.9605
.052	1.1217	.9989	.9437	.9617
0.000	1.1479	.9925	.9299	.9519
-.052	1.1446	.9944	.9321	.9535
-.104	1.1413	.9933	.9329	.9541
-.156	1.1413	.9984	.9353	.9558
-.208	1.1413	.9933	.9329	.9541
-.260	1.1381	.9990	.9369	.9569
-.312	1.1348	.9996	.9385	.9581
-.364	1.1381	1.0007	.9377	.9575
-.416	1.1413	.9984	.9353	.9558
-.468	1.1370	1.0076	.9414	.9601
-.520	1.1326	1.0000	.9396	.9588
-.572	1.1272	1.0043	.9439	.9618
-.624	1.1217	.9935	.9411	.9599
-.676	1.1217	.9969	.9427	.9610
-.728	1.1217	1.0019	.9451	.9627
-.780	1.1206	1.0021	.9456	.9630
-.832	1.1196	.9939	.9422	.9606
-.884	1.1174	.9976	.9449	.9625
-.936	1.1152	.9997	.9468	.9639
-.988	1.1087	1.0009	.9501	.9662
-1.040	1.1021	.9970	.9511	.9668

(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0^\circ$;

p_∞ = 221.53 psf (10606.98 N/m^2);
q_∞ = 396.98 psf (19007.70 N/m^2);
$p_{t,\infty}$ = 941.60 psf (45084.05 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1251	.9986	.9421	.9606
.988	1.1338	.9953	.9369	.9569
.936	1.1426	.9954	.9334	.9544
.884	1.1295	.9944	.9383	.9579
.832	1.1164	.9951	.9441	.9620
.780	1.1066	.9968	.9491	.9655
.728	1.0968	.9986	.9542	.9690
.676	1.1098	.9929	.9458	.9632
.624	1.1229	.9922	.9400	.9591
.572	1.1327	.9921	.9359	.9562
.520	1.1426	.9853	.9287	.9511
.468	1.1393	.9893	.9319	.9533
.416	1.1360	.9899	.9335	.9545
.364	1.1338	.9886	.9338	.9547
.312	1.1316	.9839	.9325	.9538
.260	1.1186	.9930	.9422	.9606
.208	1.1055	.9937	.9481	.9647
.156	1.1415	.9838	.9284	.9509
.104	1.1284	.9879	.9357	.9560
.052	1.1284	.9845	.9341	.9549
0.000	1.1513	.9838	.9244	.9480
-.052	1.1513	.9810	.9231	.9471
-.104	1.1513	.9810	.9231	.9471
-.156	1.1513	.9827	.9239	.9477
-.208	1.1513	.9810	.9231	.9471
-.260	1.1469	.9869	.9276	.9503
-.312	1.1426	.9876	.9297	.9518
-.364	1.1447	.9889	.9295	.9517
-.416	1.1469	.9885	.9284	.9509
-.468	1.1458	.9938	.9313	.9530
-.520	1.1447	.9889	.9295	.9517
-.572	1.1393	.9916	.9329	.9541
-.624	1.1338	.9858	.9325	.9538
-.676	1.1349	.9907	.9343	.9551
-.728	1.1360	.9922	.9346	.9553
-.780	1.1371	.9920	.9340	.9549
-.832	1.1382	.9884	.9319	.9534
-.884	1.1360	.9905	.9338	.9547
-.936	1.1338	.9926	.9356	.9560
-.988	1.1295	.9917	.9370	.9570
-1.040	1.1251	.9941	.9400	.9591

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(s) x/D = 5.0; y/D = 1.0; $\alpha = 0^\circ$;

p_∞ = 221.55 psf (10608.10 N/m^2);
q_∞ = 397.03 psf (19009.72 N/m^2);
$p_{t,\infty}$ = 941.70 psf (45088.84 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1250	.9846	.9355	.9560
.988	1.1304	.9786	.9304	.9523
.936	1.1359	.9793	.9285	.9510
.884	1.1206	.9770	.9337	.9547
.832	1.1054	.9797	.9415	.9601
.780	1.0945	.9783	.9455	.9629
.728	1.0836	.9803	.9511	.9669
.676	1.0934	.9735	.9436	.9616
.624	1.1032	.9717	.9385	.9581
.572	1.1119	.9685	.9333	.9544
.520	1.1206	.9602	.9256	.9489
.468	1.1141	.9630	.9297	.9518
.416	1.1075	.9625	.9322	.9536
.364	1.1075	.9592	.9306	.9525
.312	1.1075	.9507	.9265	.9496
.260	1.0945	.9565	.9348	.9555
.208	1.0814	.9538	.9391	.9585
.156	1.1174	.9456	.9199	.9449
.104	1.1043	.9463	.9257	.9490
.052	1.1032	.9448	.9254	.9488
0.000	1.1272	.9421	.9142	.9408
-.052	1.1261	.9415	.9144	.9409
-.104	1.1250	.9417	.9149	.9413
-.156	1.1283	.9496	.9174	.9430
-.208	1.1315	.9456	.9141	.9407
-.260	1.1261	.9533	.9201	.9450
-.312	1.1206	.9560	.9236	.9475
-.364	1.1239	.9605	.9244	.9481
-.416	1.1272	.9599	.9228	.9469
-.468	1.1283	.9681	.9263	.9494
-.520	1.1293	.9646	.9242	.9479
-.572	1.1250	.9687	.9280	.9506
-.624	1.1206	.9645	.9277	.9504
-.676	1.1217	.9693	.9296	.9517
-.728	1.1228	.9725	.9307	.9525
-.780	1.1250	.9721	.9296	.9517
-.832	1.1272	.9683	.9269	.9498
-.884	1.1283	.9715	.9279	.9506
-.936	1.1293	.9764	.9298	.9519
-.988	1.1261	.9770	.9314	.9531
-1.040	1.1228	.9776	.9331	.9542

(t) x/D = 5.0; y/D = .83; $\alpha = 0^\circ$;

p_∞ = 221.53 psf (10606.98 N/m^2);
q_∞ = 396.98 psf (19007.70 N/m^2);
$p_{t,\infty}$ = 941.60 psf (45084.05 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1279	.9818	.9330	.9541
.988	1.1334	.9758	.9279	.9505
.936	1.1388	.9765	.9260	.9492
.884	1.1236	.9742	.9311	.9528
.832	1.1084	.9735	.9372	.9571
.780	1.0964	.9740	.9425	.9609
.728	1.0844	.9745	.9480	.9647
.676	1.0942	.9660	.9396	.9588
.624	1.1040	.9659	.9354	.9558
.572	1.1127	.9593	.9285	.9510
.520	1.1214	.9509	.9209	.9455
.468	1.1138	.9506	.9238	.9477
.416	1.1062	.9435	.9236	.9475
.364	1.1040	.9355	.9205	.9453
.312	1.1018	.9207	.9141	.9407
.260	1.0877	.9131	.9162	.9422
.208	1.0735	.9123	.9219	.9462
.156	1.1084	.8924	.8973	.9285
.104	1.0942	.8984	.9061	.9349
.052	1.0898	.8890	.9032	.9327
0.000	1.1149	.8929	.8949	.9267
-.052	1.1105	.8852	.8928	.9252
-.104	1.1062	.8979	.9009	.9311
-.156	1.1127	.8984	.8985	.9294
-.208	1.1192	.9056	.8995	.9301
-.260	1.1138	.9253	.9114	.9387
-.312	1.1084	.9279	.9150	.9413
-.364	1.1149	.9369	.9167	.9425
-.416	1.1214	.9459	.9184	.9437
-.468	1.1247	.9554	.9217	.9461
-.520	1.1279	.9548	.9201	.9449
-.572	1.1247	.9588	.9233	.9473
-.624	1.1214	.9543	.9225	.9467
-.676	1.1214	.9611	.9257	.9490
-.728	1.1214	.9678	.9290	.9513
-.780	1.1225	.9676	.9284	.9509
-.832	1.1236	.9624	.9255	.9488
-.884	1.1247	.9689	.9282	.9507
-.936	1.1258	.9704	.9284	.9509
-.988	1.1225	.9710	.9301	.9521
-1.040	1.1192	.9716	.9317	.9532

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(u) $x/D = 5.0$; $y/D = .63$; $\alpha = 0^\circ$;

$p_\infty = 221.53$ psf (10606.98 N/m²);
$q_\infty = 396.98$ psf (19007.70 N/m²);
$p_{t,\infty} = 941.60$ psf (45084.05 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0996	.9721	.9402	.9592
.988	1.1040	.9663	.9355	.9560
.936	1.1084	.9655	.9333	.9544
.884	1.0942	.9630	.9381	.9578
.832	1.0800	.9621	.9438	.9618
.780	1.0692	.9607	.9479	.9646
.728	1.0583	.9576	.9513	.9670
.676	1.0692	.9489	.9421	.9606
.624	1.0800	.9470	.9364	.9565
.572	1.0855	.9342	.9277	.9504
.520	1.0909	.9197	.9182	.9436
.468	1.0800	.9065	.9161	.9421
.416	1.0692	.8747	.9045	.9337
.364	1.0648	.8484	.8926	.9250
.312	1.0604	.8255	.8823	.9174
.260	1.0506	.8086	.8773	.9137
.208	1.0408	.7748	.8628	.9027
.156	1.0648	.7395	.8334	.8801
.104	1.0550	.7380	.8364	.8825
.052	1.0496	.7305	.8343	.8808
0.000	1.0692	.7112	.8156	.8662
-.052	1.0637	.7202	.8228	.8719
-.104	1.0583	.7452	.8392	.8846
-.156	1.0681	.7690	.8485	.8919
-.208	1.0779	.7893	.8557	.8974
-.260	1.0735	.8225	.8753	.9122
-.312	1.0692	.8589	.8963	.9277
-.364	1.0768	.8829	.9055	.9345
-.416	1.0844	.9052	.9137	.9403
-.468	1.0920	.9275	.9216	.9461
-.520	1.0996	.9329	.9211	.9457
-.572	1.1018	.9443	.9258	.9490
-.624	1.1040	.9389	.9222	.9465
-.676	1.1040	.9490	.9272	.9500
-.728	1.1040	.9507	.9280	.9506
-.780	1.1051	.9539	.9291	.9514
-.832	1.1062	.9554	.9293	.9516
-.884	1.1073	.9569	.9296	.9518
-.936	1.1084	.9617	.9315	.9531
-.988	1.1062	.9621	.9326	.9539
-1.040	1.1040	.9625	.9337	.9547

(v) $x/D = 5.0$; $y/D = .42$; $\alpha = 0^\circ$;

$p_\infty = 221.48$ psf (10604.72 N/m²);
$q_\infty = 396.90$ psf (19003.67 N/m²);
$p_{t,\infty} = 941.40$ psf (45074.47 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0912	.9669	.9413	.9600
.988	1.0966	.9625	.9369	.9569
.936	1.1021	.9615	.9341	.9549
.884	1.0868	.9575	.9386	.9581
.832	1.0716	.9552	.9441	.9620
.780	1.0618	.9569	.9494	.9656
.728	1.0520	.9502	.9504	.9664
.676	1.0618	.9418	.9418	.9604
.624	1.0716	.9282	.9307	.9525
.572	1.0770	.9171	.9228	.9469
.520	1.0825	.8890	.9063	.9350
.468	1.0705	.8658	.8993	.9299
.416	1.0585	.8171	.8786	.9146
.364	1.0520	.7741	.8578	.8990
.312	1.0454	.7429	.8430	.8876
.260	1.0356	.6847	.8131	.8642
.208	1.0258	.6608	.8026	.8558
.156	1.0443	.6346	.7795	.8371
.104	1.0345	.6227	.7758	.8341
.052	1.0280	.6101	.7704	.8296
0.000	1.0432	.6087	.7638	.8242
-.052	1.0367	.6170	.7715	.8305
-.104	1.0302	.6271	.7802	.8377
-.156	1.0411	.6457	.7875	.8436
-.208	1.0520	.6884	.8089	.8609
-.260	1.0509	.7178	.8265	.8748
-.312	1.0498	.7625	.8523	.8947
-.364	1.0585	.8154	.8777	.9139
-.416	1.0672	.8477	.8913	.9240
-.468	1.0759	.8970	.9131	.9399
-.520	1.0846	.9140	.9180	.9434
-.572	1.0901	.9333	.9253	.9487
-.624	1.0955	.9289	.9208	.9455
-.676	1.0955	.9391	.9258	.9491
-.728	1.0955	.9391	.9258	.9491
-.780	1.0966	.9456	.9286	.9510
-.832	1.0977	.9488	.9297	.9518
-.884	1.0988	.9520	.9308	.9526
-.936	1.0999	.9569	.9327	.9540
-.988	1.0977	.9572	.9338	.9547
-1.040	1.0955	.9576	.9350	.9555

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(w) $x/D = 5.0$; $y/D = .21$; $\alpha = 0^\circ$;

p_∞ = 221.53 psf (10606.98 N/m^2);
q_∞ = 396.98 psf (19007.70 N/m^2);
$p_{t,\infty}$ = 941.60 psf (45084.05 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0888	.9628	.9404	.9593
.988	1.0964	.9563	.9340	.9548
.936	1.1040	.9516	.9284	.9509
.884	1.0996	.9473	.9282	.9507
.832	1.0953	.9431	.9279	.9506
.780	1.0735	.9470	.9392	.9585
.728	1.0517	.9391	.9449	.9626
.676	1.0583	.9329	.9389	.9583
.624	1.0648	.9233	.9312	.9529
.572	1.0692	.9073	.9212	.9458
.520	1.0735	.8829	.9069	.9355
.468	1.0583	.8654	.9043	.9336
.416	1.0430	.8277	.8908	.9237
.364	1.0376	.7931	.8743	.9114
.312	1.0321	.7516	.8534	.8956
.260	1.0267	.7220	.8386	.8842
.208	1.0213	.6888	.8213	.8707
.156	1.0289	.6667	.8050	.8577
.104	1.0234	.6454	.7941	.8490
.052	1.0169	.6277	.7857	.8422
0.000	1.0256	.6329	.7855	.8420
-.052	1.0191	.6353	.7896	.8453
-.104	1.0125	.6505	.8015	.8549
-.156	1.0278	.6716	.8084	.8604
-.208	1.0430	.6944	.8159	.8664
-.260	1.0430	.7442	.8447	.8889
-.312	1.0430	.7681	.8581	.8992
-.364	1.0528	.8140	.8793	.9151
-.416	1.0626	.8597	.8995	.9300
-.468	1.0724	.8901	.9111	.9385
-.520	1.0822	.9087	.9163	.9423
-.572	1.0866	.9265	.9234	.9473
-.624	1.0909	.9240	.9203	.9451
-.676	1.0898	.9360	.9268	.9497
-.728	1.0888	.9362	.9273	.9501
-.780	1.0866	.9417	.9310	.9527
-.832	1.0844	.9421	.9321	.9535
-.884	1.0855	.9470	.9340	.9549
-.936	1.0866	.9518	.9360	.9562
-.988	1.0833	.9558	.9393	.9586
-1.040	1.0800	.9564	.9410	.9598

(x) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^\circ$;

p_∞ = 221.37 psf (10599.09 N/m^2);
q_∞ = 396.69 psf (18993.57 N/m^2);
$p_{t,\infty}$ = 940.90 psf (45050.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0547	.9546	.9513	.9670
.988	1.0601	.9553	.9492	.9656
.936	1.0656	.9492	.9438	.9618
.884	1.0656	.9492	.9438	.9618
.832	1.0656	.9408	.9396	.9588
.780	1.0482	.9389	.9464	.9636
.728	1.0307	.9319	.9509	.9667
.676	1.0351	.9311	.9485	.9650
.624	1.0394	.9253	.9435	.9615
.572	1.0460	.9191	.9374	.9572
.520	1.0525	.9027	.9261	.9493
.468	1.0460	.8955	.9253	.9487
.416	1.0394	.8730	.9165	.9424
.364	1.0329	.8506	.9075	.9359
.312	1.0264	.8315	.9001	.9305
.260	1.0242	.8048	.8864	.9205
.208	1.0220	.7798	.8735	.9108
.156	1.0242	.7453	.8531	.8953
.104	1.0220	.7082	.8324	.8794
.052	1.0209	.6775	.8147	.8654
0.000	1.0220	.6653	.8068	.8592
-.052	1.0209	.6878	.8208	.8703
-.104	1.0198	.7189	.8396	.8850
-.156	1.0384	.7494	.8496	.8927
-.208	1.0569	.7698	.8534	.8956
-.260	1.0525	.8114	.8780	.9142
-.312	1.0482	.8376	.8939	.9260
-.364	1.0525	.8656	.9069	.9354
-.416	1.0569	.8851	.9151	.9414
-.468	1.0580	.9068	.9258	.9491
-.520	1.0591	.9134	.9287	.9511
-.572	1.0623	.9229	.9321	.9535
-.624	1.0656	.9223	.9303	.9523
-.676	1.0656	.9307	.9346	.9553
-.728	1.0656	.9307	.9346	.9553
-.780	1.0678	.9388	.9376	.9574
-.832	1.0700	.9384	.9365	.9566
-.884	1.0732	.9462	.9390	.9584
-.936	1.0765	.9473	.9381	.9577
-.988	1.0754	.9542	.9420	.9605
-1.040	1.0743	.9544	.9426	.9609

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(y) $x/D = 5.0$; $y/D = -.42$; $\alpha = 0^\circ$;

p_∞ = 221.37 psf (10599.09 N/m^2);
q_∞ = 396.69 psf (18993.57 N/m^2);
$p_{t,\infty}$ = 940.90 psf (45050.53 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0220	.9587	.9685	.9788
.988	1.0296	.9640	.9676	.9782
.936	1.0373	.9543	.9592	.9724
.884	1.0394	.9573	.9597	.9728
.832	1.0416	.9485	.9542	.9690
.780	1.0253	.9480	.9616	.9741
.728	1.0089	.9425	.9665	.9775
.676	1.0111	.9455	.9670	.9778
.624	1.0133	.9434	.9649	.9764
.572	1.0198	.9439	.9621	.9744
.520	1.0264	.9344	.9541	.9689
.468	1.0231	.9400	.9585	.9720
.416	1.0198	.9322	.9561	.9703
.364	1.0144	.9348	.9600	.9730
.312	1.0089	.9274	.9587	.9721
.260	.9937	.9200	.9622	.9745
.208	.9784	.9008	.9595	.9727
.156	1.0133	.8710	.9271	.9500
.104	.9980	.8265	.9100	.9377
.052	.9980	.7605	.8729	.9104
0.000	1.0177	.7244	.8437	.8882
-.052	1.0177	.7691	.8694	.9077
-.104	1.0177	.8337	.9051	.9341
-.156	1.0242	.8799	.9269	.9498
-.208	1.0307	.8956	.9321	.9536
-.260	1.0285	.9196	.9456	.9630
-.312	1.0264	.9217	.9476	.9644
-.364	1.0275	.9316	.9522	.9676
-.416	1.0285	.9314	.9516	.9672
-.468	1.0275	.9384	.9557	.9700
-.520	1.0264	.9385	.9563	.9704
-.572	1.0285	.9415	.9568	.9708
-.624	1.0307	.9361	.9530	.9682
-.676	1.0329	.9441	.9561	.9703
-.728	1.0351	.9437	.9549	.9695
-.780	1.0351	.9488	.9574	.9712
-.832	1.0351	.9454	.9557	.9700
-.884	1.0373	.9551	.9596	.9727
-.936	1.0394	.9514	.9567	.9707
-.988	1.0384	.9600	.9615	.9741
-1.040	1.0373	.9535	.9588	.9721

(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^\circ$;

p_∞ = 221.72 psf (10615.99 N/m^2);
q_∞ = 397.32 psf (19023.85 N/m^2);
$p_{t,\infty}$ = 942.40 psf (45122.36 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1242	.9619	.9250	.9485
.988	1.1329	.9620	.9215	.9460
.936	1.1416	.9554	.9148	.9412
.884	1.1209	.9592	.9250	.9485
.832	1.1002	.9629	.9355	.9559
.780	1.1056	.9535	.9286	.9511
.728	1.1111	.9475	.9234	.9474
.676	1.1067	.9415	.9223	.9466
.624	1.1024	.9170	.9121	.9392
.572	1.0555	.9154	.9313	.9529
.520	1.0087	.8935	.9412	.9599
.468	.9956	.8875	.9441	.9620
.416	.9825	.8629	.9371	.9571
.364	.9749	.8542	.9360	.9563
.312	.9673	.8387	.9312	.9529
.260	.9586	.8184	.9240	.9478
.208	.9499	.7914	.9128	.9397
.156	.9662	.7580	.8857	.9199
.104	.9575	.7325	.8747	.9117
.052	.9564	.7106	.8620	.9021
0.000	.9651	.7039	.8540	.8961
-.052	.9640	.7163	.8620	.9021
-.104	.9629	.7420	.8778	.9140
-.156	.9771	.7648	.8847	.9192
-.208	.9913	.7893	.8923	.9248
-.260	1.0196	.8180	.8957	.9273
-.312	1.0479	.8432	.8970	.9283
-.364	1.0795	.8611	.8931	.9254
-.416	1.1111	.8892	.8946	.9265
-.468	1.1231	.9073	.8988	.9296
-.520	1.1350	.9169	.8988	.9295
-.572	1.1427	.9274	.9009	.9311
-.624	1.1503	.9243	.8964	.9278
-.676	1.1459	.9352	.9034	.9329
-.728	1.1416	.9428	.9088	.9368
-.780	1.1383	.9451	.9112	.9386
-.832	1.1350	.9474	.9136	.9403
-.884	1.1307	.9515	.9174	.9430
-.936	1.1263	.9557	.9211	.9457
-.988	1.1242	.9612	.9247	.9482
-1.040	1.1220	.9565	.9233	.9473

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10⁶ PER FOOT (5.42 × 10⁶ PER METER) – Continued

(aa) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 221.72$ psf (10615.99 N/m^2);
$q_\infty = 397.32$ psf (19023.85 N/m^2);
$p_{t,\infty} = 942.40$ psf (45122.36 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0239	.9643	.9704	.9801
.988	1.0283	.9669	.9697	.9796
.936	1.0327	.9560	.9622	.9745
.884	1.0250	.9607	.9681	.9786
.832	1.0174	.9554	.9690	.9792
.780	1.0218	.9563	.9674	.9781
.728	1.0261	.9572	.9658	.9770
.676	1.0849	.9484	.9350	.9555
.624	1.1438	.9343	.9038	.9332
.572	1.1623	.9225	.8909	.9237
.520	1.1808	.9055	.8757	.9125
.468	1.1939	.8979	.8672	.9061
.416	1.2069	.8767	.8523	.8948
.364	1.2418	.8495	.8271	.8752
.312	1.2767	.8186	.8008	.8543
.260	1.2973	.8023	.7864	.8427
.208	1.3180	.7703	.7645	.8247
.156	1.2701	.7403	.7634	.8238
.104	1.2908	.7132	.7433	.8069
.052	1.2745	.7009	.7416	.8055
0.000	1.2636	.6945	.7413	.8053
-.052	1.2472	.7113	.7552	.8170
-.104	1.2309	.7357	.7731	.8318
-.156	1.2309	.7634	.7875	.8436
-.208	1.2309	.7910	.8017	.8551
-.260	1.1971	.8218	.8285	.8763
-.312	1.1634	.8522	.8559	.8975
-.364	1.1416	.8750	.8755	.9123
-.416	1.1198	.8977	.8954	.9270
-.468	1.0838	.9077	.9151	.9414
-.520	1.0479	.9159	.9349	.9555
-.572	1.0228	.9220	.9494	.9657
-.624	.9978	.9265	.9636	.9755
-.676	.9934	.9306	.9679	.9784
-.728	.9891	.9297	.9695	.9795
-.780	.9891	.9347	.9721	.9813
-.832	.9891	.9347	.9721	.9813
-.884	.9836	.9508	.9832	.9888
-.936	.9782	.9467	.9838	.9892
-.988	.9782	.9585	.9899	.9933
-1.040	.9782	.9518	.9864	.9909

(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 221.74$ psf (10617.12 N/m^2);
$q_\infty = 397.36$ psf (19025.87 N/m^2);
$p_{t,\infty} = 942.50$ psf (45127.14 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2373	.9707	.8858	.9199
.988	1.2351	.9627	.8828	.9178
.936	1.2330	.9648	.8846	.9191
.884	1.2144	.9597	.8890	.9223
.832	1.1959	.9631	.8974	.9285
.780	1.1927	.9536	.8942	.9262
.728	1.1894	.9508	.8941	.9261
.676	1.1981	.9373	.8845	.9190
.624	1.2068	.9255	.8757	.9125
.572	1.2112	.9196	.8714	.9092
.520	1.2155	.9069	.8638	.9035
.468	1.1959	.8936	.8644	.9040
.416	1.1763	.8922	.8709	.9088
.364	1.1796	.8558	.8518	.8943
.312	1.1828	.8449	.8452	.8893
.260	1.1807	.8283	.8376	.8834
.208	1.1785	.7962	.8219	.8712
.156	1.1730	.7835	.8173	.8675
.104	1.1709	.7547	.8028	.8560
.052	1.1665	.7366	.7946	.8494
0.000	1.1632	.7338	.7942	.8491
-.052	1.1589	.7330	.7953	.8499
-.104	1.1545	.7580	.8103	.8619
-.156	1.1807	.7665	.8057	.8583
-.208	1.2068	.7871	.8076	.8598
-.260	1.2035	.8187	.8248	.8734
-.312	1.2003	.8382	.8356	.8819
-.364	1.2035	.8597	.8452	.8893
-.416	1.2068	.8796	.8537	.8958
-.468	1.2155	.8916	.8564	.8979
-.520	1.2242	.9018	.8583	.8993
-.572	1.2340	.9136	.8604	.9009
-.624	1.2438	.9236	.8617	.9019
-.676	1.2384	.9298	.8665	.9055
-.728	1.2330	.9461	.8760	.9127
-.780	1.2351	.9440	.8742	.9114
-.832	1.2373	.9470	.8748	.9118
-.884	1.2449	.9473	.8723	.9099
-.936	1.2526	.9560	.8736	.9109
-.988	1.2547	.9556	.8727	.9102
-1.040	1.2569	.9637	.8756	.9124

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(cc) x/D = 8.39; y/D = 3.0; $\alpha = 0^\circ$;

p_∞ = 222.03 psf (10630.63 N/m^2);
q_∞ = 397.87 psf (19050.10 N/m^2);
$p_{t,\infty}$ = 943.70 psf (45184.60 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2665	1.0176	.8964	.9278
.988	1.2719	1.0149	.8933	.9255
.936	1.2774	1.0172	.8924	.9248
.884	1.2632	1.0165	.8970	.9283
.832	1.2491	1.0241	.9055	.9344
.780	1.2425	1.0186	.9054	.9344
.728	1.2360	1.0232	.9098	.9376
.676	1.2436	1.0150	.9034	.9329
.624	1.2513	1.0170	.9015	.9316
.572	1.2610	1.0169	.8980	.9290
.520	1.2708	1.0134	.8930	.9253
.468	1.2621	1.0167	.8975	.9286
.416	1.2534	1.0183	.9013	.9314
.364	1.2523	1.0168	.9011	.9312
.312	1.2513	1.0136	.9000	.9305
.260	1.2382	1.0211	.9081	.9363
.208	1.2251	1.0184	.9117	.9389
.156	1.2545	1.0113	.8978	.9289
.104	1.2415	1.0154	.9044	.9336
.052	1.2371	1.0094	.9033	.9328
0.000	1.2578	1.0158	.8987	.9295
-.052	1.2534	1.0064	.8961	.9276
-.104	1.2491	1.0072	.8980	.9290
-.156	1.2502	1.0087	.8983	.9292
-.208	1.2513	1.0068	.8970	.9283
-.260	1.2436	1.0116	.9019	.9318
-.312	1.2360	1.0130	.9053	.9343
-.364	1.2349	1.0132	.9058	.9346
-.416	1.2338	1.0134	.9063	.9350
-.468	1.2382	1.0194	.9073	.9358
-.520	1.2425	1.0118	.9024	.9322
-.572	1.2393	1.0141	.9046	.9338
-.624	1.2360	1.0096	.9038	.9332
-.676	1.2360	1.0130	.9053	.9343
-.728	1.2360	1.0181	.9076	.9359
-.780	1.2382	1.0126	.9043	.9336
-.832	1.2404	1.0122	.9034	.9329
-.884	1.2393	1.0107	.9031	.9327
-.936	1.2382	1.0143	.9051	.9341
-.988	1.2143	1.0153	.9144	.9409
-1.040	1.1903	1.0095	.9209	.9456

(dd) x/D = 8.39; y/D = 2.0; $\alpha = 0^\circ$;

p_∞ = 221.98 psf (10628.38 N/m^2);
q_∞ = 397.79 psf (19046.06 N/m^2);
$p_{t,\infty}$ = 943.50 psf (45175.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1632	1.0066	.9303	.9522
.988	1.1653	1.0028	.9277	.9504
.936	1.1675	1.0058	.9282	.9507
.884	1.1534	1.0050	.9334	.9545
.832	1.1392	1.0041	.9388	.9583
.780	1.1229	1.0070	.9470	.9640
.728	1.1066	1.0083	.9545	.9692
.676	1.1251	1.0050	.9451	.9627
.624	1.1436	1.0034	.9367	.9568
.572	1.1545	1.0031	.9321	.9535
.520	1.1653	.9994	.9261	.9493
.468	1.1599	1.0004	.9287	.9511
.416	1.1545	1.0031	.9321	.9535
.364	1.1512	1.0054	.9345	.9552
.312	1.1479	1.0009	.9338	.9547
.260	1.1327	1.0036	.9413	.9600
.208	1.1175	.9996	.9458	.9631
.156	1.1588	1.0006	.9292	.9515
.104	1.1436	.9983	.9343	.9551
.052	1.1414	1.0021	.9370	.9570
0.000	1.1697	.9919	.9209	.9455
-.052	1.1675	.9970	.9241	.9478
-.104	1.1653	.9957	.9244	.9480
-.156	1.1697	1.0017	.9254	.9488
-.208	1.1740	.9958	.9210	.9456
-.260	1.1675	1.0021	.9265	.9495
-.312	1.1610	1.0016	.9288	.9512
-.364	1.1588	1.0070	.9322	.9536
-.416	1.1566	1.0007	.9301	.9521
-.468	1.1588	1.0121	.9345	.9553
-.520	1.1610	1.0049	.9304	.9523
-.572	1.1577	1.0089	.9335	.9545
-.624	1.1545	.9977	.9296	.9518
-.676	1.1555	.9992	.9299	.9519
-.728	1.1566	1.0057	.9325	.9538
-.780	1.1588	1.0053	.9314	.9530
-.832	1.1610	.9982	.9272	.9501
-.884	1.1675	1.0038	.9272	.9501
-.936	1.1740	1.0026	.9241	.9478
-.988	1.1729	1.0028	.9246	.9482
-1.040	1.1719	1.0030	.9251	.9486

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^\circ$;

$p_\infty = 221.98$ psf (10628.38 N/m^2);
$q_\infty = 397.79$ psf (19046.06 N/m^2);
$p_{t,\infty} = 943.50$ psf (45175.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1253	1.0012	.9433	.9614
.988	1.1362	.9993	.9378	.9576
.936	1.1470	.9973	.9325	.9538
.884	1.1340	1.0031	.9405	.9594
.832	1.1209	.9987	.9439	.9618
.780	1.1111	1.0004	.9489	.9653
.728	1.1013	.9971	.9515	.9671
.676	1.1198	.9972	.9436	.9616
.624	1.1383	.9955	.9352	.9557
.572	1.1438	.9946	.9325	.9538
.520	1.1492	.9868	.9267	.9497
.468	1.1427	.9931	.9322	.9536
.416	1.1362	.9926	.9347	.9553
.364	1.1340	.9946	.9365	.9567
.312	1.1318	.9883	.9344	.9552
.260	1.1144	.9914	.9432	.9613
.208	1.0970	.9895	.9497	.9659
.156	1.1351	.9877	.9328	.9540
.104	1.1177	.9858	.9391	.9585
.052	1.1187	.9906	.9410	.9598
0.000	1.1383	.9820	.9288	.9512
-.052	1.1394	.9852	.9299	.9519
-.104	1.1405	.9833	.9285	.9510
-.156	1.1427	.9897	.9307	.9525
-.208	1.1449	.9842	.9272	.9500
-.260	1.1383	.9905	.9328	.9540
-.312	1.1318	.9917	.9360	.9563
-.364	1.1296	.9920	.9371	.9571
-.416	1.1275	.9874	.9358	.9561
-.468	1.1253	.9945	.9401	.9592
-.520	1.1231	.9915	.9396	.9588
-.572	1.1100	.9972	.9478	.9646
-.624	1.0970	.9895	.9497	.9659
-.676	1.0981	.9859	.9475	.9644
-.728	1.0992	.9908	.9494	.9657
-.780	1.0992	.9941	.9510	.9668
-.832	1.0992	.9891	.9486	.9651
-.884	1.1024	.9952	.9501	.9662
-.936	1.1057	.9879	.9452	.9628
-.988	1.1079	.9959	.9481	.9648
-1.040	1.1100	.9922	.9454	.9629

(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^\circ$;

$p_\infty = 222.00$ psf (10629.51 N/m^2);
$q_\infty = 397.83$ psf (19048.08 N/m^2);
$p_{t,\infty} = 943.60$ psf (45179.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2122	.9904	.9039	.9333
.988	1.2133	.9852	.9011	.9312
.936	1.2144	.9884	.9021	.9320
.884	1.1992	.9844	.9060	.9348
.832	1.1839	.9872	.9131	.9400
.780	1.1752	.9837	.9149	.9412
.728	1.1665	.9836	.9182	.9436
.676	1.1752	.9752	.9110	.9384
.624	1.1839	.9720	.9061	.9349
.572	1.1904	.9674	.9014	.9315
.520	1.1970	.9526	.8921	.9246
.468	1.1839	.9533	.8974	.9285
.416	1.1709	.9490	.9003	.9306
.364	1.1698	.9407	.8968	.9281
.312	1.1687	.9308	.8924	.9249
.260	1.1654	.9314	.8940	.9260
.208	1.1622	.9235	.8914	.9241
.156	1.1774	.9105	.8794	.9152
.104	1.1741	.9111	.8809	.9163
.052	1.1676	.9140	.8848	.9192
0.000	1.1861	.9021	.8721	.9098
-.052	1.1796	.9147	.8806	.9161
-.104	1.1730	.9159	.8836	.9184
-.156	1.1817	.9280	.8862	.9203
-.208	1.1904	.9213	.8797	.9154
-.260	1.1828	.9261	.8848	.9193
-.312	1.1752	.9463	.8974	.9285
-.364	1.1807	.9539	.8988	.9296
-.416	1.1861	.9631	.9011	.9313
-.468	1.2002	.9725	.9001	.9305
-.520	1.2144	.9716	.8945	.9264
-.572	1.2220	.9770	.8942	.9262
-.624	1.2296	.9791	.8923	.9248
-.676	1.2362	.9813	.8910	.9238
-.728	1.2427	.9903	.8927	.9251
-.780	1.2416	.9905	.8932	.9254
-.832	1.2405	.9942	.8952	.9269
-.884	1.2449	.9882	.8910	.9238
-.936	1.2492	.9960	.8929	.9252
-.988	1.2416	.9957	.8955	.9271
-1.040	1.2340	.9988	.8997	.9302

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(gg) $x/D = 8.39$; $y/D = .83$; $\alpha = 0^\circ$;

$p_\infty = 222.03$ psf (10630.63 N/m^2);
$q_\infty = 397.87$ psf (19050.10 N/m^2);
$p_{t,\infty} = 943.70$ psf (45184.60 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2099	.9819	.9009	.9311
.988	1.2077	.9773	.8995	.9301
.936	1.2056	.9793	.9013	.9314
.884	1.1881	.9775	.9070	.9355
.832	1.1707	.9823	.9160	.9420
.780	1.1631	.9753	.9157	.9418
.728	1.1555	.9699	.9162	.9421
.676	1.1642	.9632	.9096	.9374
.624	1.1729	.9532	.9015	.9315
.572	1.1805	.9399	.8923	.9248
.520	1.1881	.9351	.8871	.9210
.468	1.1740	.9140	.8823	.9174
.416	1.1599	.9081	.8848	.9193
.364	1.1588	.8828	.8728	.9103
.312	1.1577	.8711	.8675	.9063
.260	1.1577	.8728	.8683	.9069
.208	1.1577	.8592	.8615	.9018
.156	1.1696	.8450	.8500	.8930
.104	1.1696	.8296	.8422	.8870
.052	1.1653	.8322	.8451	.8892
0.000	1.1816	.8256	.8359	.8821
-.052	1.1773	.8321	.8407	.8858
-.104	1.1729	.8363	.8444	.8887
-.156	1.1849	.8409	.8424	.8872
-.208	1.1968	.8676	.8514	.8941
-.260	1.1936	.8818	.8595	.9003
-.312	1.1903	.8841	.8618	.9020
-.364	1.2056	.9000	.8640	.9037
-.416	1.2208	.9277	.8717	.9095
-.468	1.2317	.9308	.8693	.9077
-.520	1.2425	.9423	.8708	.9088
-.572	1.2447	.9504	.8738	.9110
-.624	1.2469	.9517	.8736	.9109
-.676	1.2436	.9642	.8805	.9160
-.728	1.2404	.9699	.8843	.9188
-.780	1.2360	.9707	.8862	.9203
-.832	1.2317	.9749	.8897	.9228
-.884	1.2360	.9724	.8870	.9208
-.936	1.2404	.9750	.8866	.9206
-.988	1.2425	.9729	.8848	.9193
-1.040	1.2447	.9792	.8870	.9208

(hh) $x/D = 8.39$; $y/D = .63$; $\alpha = 0^\circ$;

$p_\infty = 221.98$ psf (10628.38 N/m^2);
$q_\infty = 397.79$ psf (19046.06 N/m^2);
$p_{t,\infty} = 943.50$ psf (45175.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1993	.9781	.9031	.9327
.988	1.1960	.9719	.9015	.9315
.936	1.1928	.9759	.9045	.9337
.884	1.1764	.9704	.9082	.9364
.832	1.1601	.9700	.9144	.9409
.780	1.1514	.9666	.9162	.9422
.728	1.1427	.9614	.9172	.9429
.676	1.1536	.9476	.9063	.9350
.624	1.1645	.9354	.8963	.9277
.572	1.1721	.9086	.8805	.9160
.520	1.1797	.9038	.8753	.9122
.468	1.1645	.8846	.8716	.9094
.416	1.1492	.8654	.8678	.9065
.364	1.1514	.8344	.8513	.8940
.312	1.1536	.8101	.8380	.8837
.260	1.1547	.7911	.8277	.8757
.208	1.1557	.7806	.8218	.8711
.156	1.1688	.7591	.8059	.8585
.104	1.1699	.7503	.8008	.8544
.052	1.1699	.7486	.7999	.8537
0.000	1.1840	.7440	.7927	.8478
-.052	1.1840	.7382	.7896	.8453
-.104	1.1840	.7555	.7988	.8527
-.156	1.2058	.7632	.7956	.8501
-.208	1.2276	.7709	.7924	.8476
-.260	1.2178	.7883	.8046	.8574
-.312	1.2080	.8212	.8245	.8732
-.364	1.2134	.8304	.8273	.8754
-.416	1.2189	.8807	.8500	.8930
-.468	1.2287	.8856	.8490	.8922
-.520	1.2385	.9195	.8617	.9019
-.572	1.2363	.9182	.8618	.9020
-.624	1.2341	.9305	.8683	.9069
-.676	1.2308	.9465	.8769	.9134
-.728	1.2276	.9606	.8846	.9191
-.780	1.2232	.9581	.8850	.9194
-.832	1.2189	.9673	.8909	.9237
-.884	1.2232	.9665	.8889	.9223
-.936	1.2276	.9725	.8901	.9231
-.988	1.2276	.9708	.8893	.9226
-1.040	1.2276	.9742	.8908	.9237

TABLE 1.- VARIATION OF p_l/p_∞, q_l/q_∞, M_l/M_∞ AND V_l/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(ii) $x/D = 8.39$; $y/D = .42$; $\alpha = 0^\circ$;

p_∞ = 222.03 psf (10630.63 N/m^2);
q_∞ = 397.87 psf (19050.10 N/m^2);
$p_{t,\infty}$ = 943.70 psf (45184.60 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1944	.9724	.9023	.9321
.988	1.1944	.9640	.8984	.9292
.936	1.1944	.9657	.8992	.9298
.884	1.1748	.9591	.9036	.9330
.832	1.1552	.9627	.9129	.9398
.780	1.1476	.9523	.9109	.9384
.728	1.1400	.9486	.9122	.9393
.676	1.1487	.9319	.9007	.9309
.624	1.1574	.9252	.8941	.9261
.572	1.1650	.9001	.8790	.9149
.520	1.1726	.8800	.8663	.9054
.468	1.1574	.8608	.8624	.9025
.416	1.1422	.8365	.8558	.8974
.364	1.1476	.8168	.8436	.8881
.312	1.1531	.7782	.8215	.8708
.260	1.1607	.7595	.8089	.8609
.208	1.1683	.7443	.7982	.8522
.156	1.1781	.7337	.7891	.8450
.104	1.1857	.7148	.7764	.8346
.052	1.1813	.7122	.7765	.8346
0.000	1.2031	.7112	.7689	.8283
-.052	1.1987	.7108	.7700	.8293
-.104	1.1944	.7186	.7757	.8340
-.156	1.2107	.7274	.7751	.8335
-.208	1.2270	.7414	.7773	.8353
-.260	1.2162	.7627	.7919	.8472
-.312	1.2053	.7907	.8100	.8617
-.364	1.2096	.8105	.8185	.8685
-.416	1.2140	.8422	.8329	.8798
-.468	1.2227	.8593	.8383	.8840
-.520	1.2314	.8935	.8518	.8944
-.572	1.2325	.9086	.8586	.8996
-.624	1.2336	.9220	.8645	.9041
-.676	1.2259	.9370	.8743	.9114
-.728	1.2183	.9486	.8824	.9175
-.780	1.2129	.9547	.8872	.9210
-.832	1.2075	.9608	.8921	.9246
-.884	1.2151	.9577	.8878	.9215
-.936	1.2227	.9631	.8875	.9213
-.988	1.2227	.9648	.8883	.9218
-1.040	1.2227	.9699	.8906	.9236

(jj) $x/D = 8.39$; $y/D = .21$; $\alpha = 0^\circ$;

p_∞ = 221.86 psf (10622.75 N/m^2);
q_∞ = 397.57 psf (19035.97 N/m^2);
$p_{t,\infty}$ = 943.00 psf (45151.08 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1648	.9706	.9129	.9398
.988	1.1702	.9629	.9071	.9356
.936	1.1757	.9619	.9045	.9337
.884	1.1572	.9569	.9093	.9372
.832	1.1387	.9586	.9175	.9431
.780	1.1354	.9474	.9134	.9402
.728	1.1321	.9429	.9126	.9396
.676	1.1409	.9329	.9043	.9335
.624	1.1496	.9195	.8943	.9263
.572	1.1626	.9086	.8840	.9187
.520	1.1757	.8841	.8672	.9061
.468	1.1594	.8736	.8681	.9067
.416	1.1430	.8496	.8621	.9022
.364	1.1496	.8228	.8460	.8899
.312	1.1561	.8079	.8360	.8822
.260	1.1724	.7911	.8214	.8708
.208	1.1888	.7673	.8034	.8565
.156	1.1855	.7559	.7985	.8525
.104	1.2018	.7354	.7822	.8393
.052	1.1931	.7354	.7851	.8417
0.000	1.2149	.7153	.7673	.8271
-.052	1.2062	.7256	.7756	.8339
-.104	1.1975	.7326	.7822	.8393
-.156	1.2149	.7446	.7829	.8399
-.208	1.2323	.7549	.7827	.8397
-.260	1.2236	.7723	.7945	.8493
-.312	1.2149	.8085	.8158	.8663
-.364	1.2181	.8285	.8247	.8733
-.416	1.2214	.8535	.8359	.8821
-.468	1.2279	.8762	.8447	.8889
-.520	1.2345	.8886	.8484	.8918
-.572	1.2323	.9061	.8575	.8987
-.624	1.2301	.9184	.8641	.9037
-.676	1.2214	.9320	.8735	.9108
-.728	1.2127	.9438	.8822	.9173
-.780	1.2051	.9452	.8856	.9199
-.832	1.1975	.9517	.8915	.9242
-.884	1.2040	.9522	.8893	.9226
-.936	1.2105	.9578	.8895	.9227
-.988	1.2094	.9580	.8900	.9231
-1.040	1.2083	.9599	.8913	.9240

TABLE 1.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Concluded.

(kk) x/D = 8.39; y/D = 0; $\alpha = 0^\circ$;

p_∞ = 221.79 psf (10619.37 N/m^2);
q_∞ = 397.45 psf (19029.91 N/m^2);
$p_{t,\infty}$ = 942.70 psf (45136.72 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1676	.9681	.9106	.9381
.988	1.1698	.9609	.9063	.9350
.936	1.1720	.9605	.9053	.9343
.884	1.1546	.9570	.9104	.9380
.832	1.1371	.9601	.9189	.9441
.780	1.1306	.9512	.9172	.9429
.728	1.1241	.9490	.9188	.9441
.676	1.1349	.9386	.9094	.9372
.624	1.1458	.9281	.9000	.9304
.572	1.1556	.9161	.8904	.9234
.520	1.1654	.9025	.8800	.9156
.468	1.1513	.8932	.8808	.9163
.416	1.1371	.8874	.8834	.9182
.364	1.1491	.8750	.8726	.9101
.312	1.1611	.8438	.8525	.8949
.260	1.1840	.8274	.8360	.8822
.208	1.2068	.8075	.8180	.8681
.156	1.1850	.7878	.8153	.8660
.104	1.2079	.7574	.7918	.8471
.052	1.2036	.7375	.7828	.8398
0.000	1.2090	.7347	.7795	.8371
-.052	1.2047	.7355	.7814	.8386
-.104	1.2003	.7503	.7906	.8462
-.156	1.2199	.7653	.7921	.8473
-.208	1.2395	.7907	.7987	.8527
-.260	1.2297	.8082	.8107	.8623
-.312	1.2199	.8307	.8252	.8737
-.364	1.2221	.8508	.8344	.8809
-.416	1.2243	.8828	.8492	.8924
-.468	1.2330	.8880	.8486	.8920
-.520	1.2417	.9034	.8530	.8953
-.572	1.2428	.9100	.8557	.8973
-.624	1.2439	.9183	.8592	.9000
-.676	1.2286	.9314	.8707	.9087
-.728	1.2134	.9427	.8814	.9167
-.780	1.2112	.9431	.8824	.9175
-.832	1.2090	.9503	.8866	.9206
-.884	1.2123	.9497	.8851	.9195
-.936	1.2155	.9542	.8860	.9201
-.988	1.2101	.9552	.8885	.9219
-1.040	1.2047	.9596	.8925	.9249

(ll) x/D = 8.39; y/D = -.42; $\alpha = 0^\circ$;

p_∞ = 221.77 psf (10618.24 N/m^2);
q_∞ = 397.41 psf (19027.89 N/m^2);
$p_{t,\infty}$ = 942.60 psf (45131.93 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1577	.9751	.9177	.9433
.988	1.1621	.9692	.9133	.9401
.936	1.1664	.9701	.9120	.9391
.884	1.1512	.9678	.9169	.9427
.832	1.1360	.9706	.9243	.9480
.780	1.1284	.9652	.9249	.9484
.728	1.1207	.9666	.9287	.9511
.676	1.1382	.9567	.9168	.9426
.624	1.1556	.9518	.9076	.9359
.572	1.1708	.9473	.8995	.9301
.520	1.1860	.9361	.8884	.9219
.468	1.1806	.9371	.8909	.9238
.416	1.1751	.9381	.8935	.9256
.364	1.1893	.9270	.8829	.9178
.312	1.2034	.9243	.8764	.9130
.260	1.2132	.9089	.8655	.9048
.208	1.2230	.9036	.8596	.9003
.156	1.2089	.8466	.8369	.8829
.104	1.2187	.8105	.8155	.8661
.052	1.2143	.7683	.7954	.8500
0.000	1.2143	.7458	.7837	.8405
-.052	1.2100	.7588	.7919	.8472
-.104	1.2056	.7907	.8098	.8616
-.156	1.2296	.8152	.8142	.8651
-.208	1.2535	.8482	.8226	.8717
-.260	1.2404	.8816	.8430	.8876
-.312	1.2274	.9028	.8576	.8988
-.364	1.2296	.9143	.8623	.9024
-.416	1.2317	.9258	.8670	.9059
-.468	1.2404	.9327	.8671	.9060
-.520	1.2491	.9361	.8657	.9049
-.572	1.2470	.9399	.8682	.9068
-.624	1.2448	.9421	.8699	.9081
-.676	1.2306	.9481	.8777	.9140
-.728	1.2165	.9592	.8880	.9216
-.780	1.2067	.9593	.8916	.9243
-.832	1.1969	.9628	.8969	.9282
-.884	1.1969	.9595	.8953	.9270
-.936	1.1969	.9628	.8969	.9282
-.988	1.1926	.9636	.8989	.9296
-1.040	1.1882	.9644	.9009	.9311

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 101.18$ psf (4844.59 N/m^2);
$q_\infty = 374.67$ psf (17939.51 N/m^2);
$p_{t,\infty} = 1265.20$ psf (60578.10 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9319	.7490	.8965	.9455
.988	.8372	.7178	.9259	.9619
.936	.7424	.6935	.9665	.9833
.884	.6950	.6691	.9812	.9907
.832	.6476	.6464	.9991	.9996
.780	.6239	.6220	.9985	.9993
.728	.6002	.5976	.9978	.9989
.676	.5410	.5758	1.0317	1.0150
.624	.4818	.5627	1.0808	1.0369
.572	.4462	.5479	1.1081	1.0484
.520	.4107	.5313	1.1374	1.0602
.468	.4225	.5026	1.0906	1.0411
.416	.4344	.2393	.7423	.8463
.364	.4383	.0724	.4064	.5379
.312	.4423	.0172	.1974	.2775
.260	.4423	0.0000	0.0000	0.0000
.208	.4423	0.0000	0.0000	0.0000
.156	.4581	0.0000	0.0000	0.0000
.104	.4739	0.0000	0.0000	0.0000
.052	.4620	0.0000	0.0000	0.0000
0.000	.4502	0.0000	0.0000	0.0000
-.104	.4581	0.0000	0.0000	0.0000
-.156	.4541	0.0000	0.0000	0.0000
-.208	.4502	0.0000	0.0000	0.0000
-.260	.4581	0.0000	0.0000	0.0000
-.312	.4541	0.0000	0.0000	0.0000
-.364	.4541	.0342	.2743	.3787
-.416	.4581	.2185	.6907	.8077
-.468	.4581	.4784	1.0220	1.0105
-.520	.4581	.5221	1.0676	1.0312
-.572	.4620	.5411	1.0822	1.0375
-.624	.4660	.5600	1.0963	1.0435
-.676	.5134	.5757	1.0590	1.0274
-.728	.5607	.5985	1.0331	1.0157
-.780	.6002	.6183	1.0149	1.0072
-.832	.6397	.6451	1.0042	1.0020
-.884	.6832	.6681	.9889	.9946
-.936	.7266	.6963	.9789	.9896
-.988	.7898	.7178	.9534	.9765
-1.040	.8530	.7498	.9376	.9682

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 101.39$ psf (4854.54 N/m^2);
$q_\infty = 375.44$ psf (17976.38 N/m^2);
$p_{t,\infty} = 1267.80$ psf (60702.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7726	.7000	.9519	.9757
.988	.6938	.6781	.9886	.9944
.936	.6149	.6613	1.0370	1.0175
.884	.5834	.6410	1.0482	1.0226
.832	.5519	.6277	1.0665	1.0307
.780	.5440	.6126	1.0612	1.0284
.728	.5361	.5975	1.0557	1.0259
.676	.4967	.5882	1.0882	1.0401
.624	.4573	.5841	1.1303	1.0574
.572	.4573	.5807	1.1269	1.0560
.520	.4573	.5859	1.1319	1.0580
.468	.5322	.6082	1.0691	1.0318
.416	.6071	.6358	1.0234	1.0112
.364	.6346	.4628	.8539	.9204
.312	.6622	.2134	.5676	.7032
.260	.6741	.0672	.3158	.4309
.208	.6859	.0154	.1501	.2128
.156	.6859	.0031	.0675	.0966
.104	.6859	0.0000	0.0000	0.0000
.052	.6819	0.0000	0.0000	0.0000
0.000	.6780	0.0000	0.0000	0.0000
-.104	.6701	.0077	.1072	.1529
-.156	.6701	.0077	.1072	.1529
-.208	.6701	.0077	.1072	.1529
-.260	.6425	.0460	.2674	.3699
-.312	.6425	.1419	.4699	.6069
-.364	.5755	.3721	.8041	.8889
-.416	.6149	.6210	1.0049	1.0024
-.468	.5479	.5911	1.0386	1.0182
-.520	.4809	.5716	1.0902	1.0409
-.572	.4573	.5698	1.1163	1.0517
-.624	.4336	.5750	1.1516	1.0657
-.676	.4651	.5832	1.1197	1.0531
-.728	.4967	.5966	1.0960	1.0433
-.780	.5243	.6085	1.0773	1.0354
-.832	.5519	.6222	1.0618	1.0286
-.884	.5676	.6402	1.0620	1.0287
-.936	.5834	.6600	1.0636	1.0294
-.988	.6307	.6774	1.0364	1.0172
-1.040	.6780	.6983	1.0149	1.0071

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0.0$; $\alpha = 0^\circ$;

p_∞ = 101.42 psf (4856.08 N/m^2);
q_∞ = 375.56 psf (17982.05 N/m^2);
$p_{t,\infty}$ = 1268.20 psf (60721.74 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6855	.6732	.9910	.9956
.988	.6146	.6559	1.0331	1.0157
.936	.5437	.6454	1.0896	1.0407
.884	.5200	.6315	1.1020	1.0459
.832	.4964	.6228	1.1201	1.0533
.780	.5673	.6681	1.0852	1.0388
.728	.6382	.6802	1.0324	1.0154
.676	.6185	.6660	1.0377	1.0178
.624	.5988	.6605	1.0503	1.0235
.572	.6343	.6631	1.0225	1.0107
.520	.6697	.6744	1.0035	1.0017
.468	.7761	.7030	.9518	.9757
.416	.8825	.7281	.9083	.9522
.364	.9613	.7465	.8812	.9367
.312	1.0400	.7526	.8507	.9184
.260	1.0755	.6220	.7605	.8593
.208	1.1110	.3890	.5917	.7251
.156	1.1267	.1893	.4098	.5418
.104	1.1425	.1278	.3345	.4538
.052	1.1307	.1647	.3817	.5097
0.000	1.1188	.2029	.4259	.5596
-.104	1.1267	.1457	.3596	.4838
-.156	1.1267	.1549	.3708	.4970
-.208	1.1267	.3067	.5217	.6595
-.260	1.0006	.5751	.7581	.8577
-.312	1.0006	.7313	.8549	.9210
-.364	.9100	.7435	.9039	.9496
-.416	.8746	.7182	.9062	.9510
-.468	.7840	.6884	.9371	.9679
-.520	.6934	.6620	.9772	.9887
-.572	.6343	.6560	1.0170	1.0081
-.624	.5752	.6586	1.0701	1.0323
-.676	.6106	.6665	1.0447	1.0210
-.728	.6461	.6813	1.0269	1.0128
-.780	.5791	.6077	1.0244	1.0116
-.832	.5121	.6127	1.0938	1.0424
-.884	.5082	.6269	1.1107	1.0494
-.936	.5043	.6429	1.1291	1.0569
-.988	.5397	.6542	1.1010	1.0454
-1.040	.5752	.6708	1.0799	1.0365

(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^\circ$;

p_∞ = 101.49 psf (4859.52 N/m^2);
q_∞ = 375.83 psf (17994.81 N/m^2);
$p_{t,\infty}$ = 1269.10 psf (60764.84 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0710	.9971	.9649	.9825
.988	1.0276	1.0021	.9875	.9939
.936	.9843	1.0053	1.0106	1.0051
.884	.9961	1.0044	1.0041	1.0020
.832	1.0080	1.0035	.9978	.9989
.780	1.0040	1.0038	.9999	1.0000
.728	1.0001	1.0041	1.0020	1.0010
.676	.9961	1.0009	1.0024	1.0012
.624	.9922	1.0012	1.0045	1.0022
.572	1.0001	1.0006	1.0003	1.0001
.520	1.0080	1.0001	.9961	.9981
.468	1.0316	1.0053	.9872	.9937
.416	1.0552	1.0122	.9794	.9898
.364	1.1143	1.1122	.9991	.9995
.312	1.1733	1.1826	1.0039	1.0019
.260	1.1694	1.2316	1.0263	1.0125
.208	1.1654	1.2284	1.0267	1.0127
.156	1.2521	1.2237	.9886	.9944
.104	1.3387	1.2242	.9563	.9780
.052	1.3151	1.2207	.9635	.9817
0.000	1.2914	1.2120	.9688	.9845
-.104	1.2678	1.1871	.9676	.9839
-.156	1.1969	1.1366	.9745	.9873
-.208	1.1261	1.0913	.9844	.9923
-.260	1.1261	1.0512	.9662	.9831
-.312	1.0552	.9954	.9713	.9857
-.364	1.0473	1.0013	.9778	.9890
-.416	.9843	.9972	1.0065	1.0032
-.468	.9765	.9978	1.0109	1.0052
-.520	.9686	.9984	1.0153	1.0073
-.572	.9686	.9984	1.0153	1.0073
-.624	.9686	.9984	1.0153	1.0073
-.676	.9725	.9981	1.0131	1.0063
-.728	.9765	.9978	1.0109	1.0052
-.780	.9725	.9981	1.0131	1.0063
-.832	.9686	.9967	1.0144	1.0069
-.884	.9725	.9946	1.0113	1.0054
-.936	.9765	.9943	1.0091	1.0044
-.988	.9804	.9940	1.0069	1.0034
-1.040	.9843	.9938	1.0048	1.0023

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^\circ$;

$p_\infty = 101.47$ psf (4858.37 N/m^2);
$q_\infty = 375.74$ psf (17990.56 N/m^2);
$p_{t,\infty} = 1268.80$ psf (60750.47 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2284	1.0394	.9199	.9586
.988	1.1693	1.0369	.9417	.9704
.936	1.1103	1.0344	.9652	.9826
.884	1.1142	1.0272	.9601	.9800
.832	1.1182	1.0216	.9559	.9778
.780	1.0985	1.0179	.9626	.9813
.728	1.0788	1.0124	.9688	.9844
.676	1.0670	1.0081	.9720	.9861
.624	1.0552	1.0020	.9745	.9874
.572	1.0473	.9974	.9759	.9881
.520	1.0394	.9962	.9790	.9896
.468	1.0315	.9933	.9813	.9908
.416	1.0237	.9887	.9828	.9915
.364	1.0158	.9841	.9843	.9923
.312	1.0079	.9829	.9875	.9939
.260	1.0079	.9794	.9858	.9930
.208	1.0079	.9777	.9849	.9926
.156	1.0040	.9745	.9852	.9927
.104	1.0000	.9748	.9873	.9938
.052	1.0040	.9745	.9852	.9927
0.000	1.0079	.9742	.9831	.9917
-.104	.9922	.9713	.9894	.9948
-.156	.9961	.9728	.9882	.9942
-.208	1.0000	.9725	.9861	.9932
-.260	.9922	.9731	.9903	.9953
-.312	.9961	.9815	.9926	.9964
-.364	1.0040	.9809	.9884	.9943
-.416	.9922	.9870	.9974	.9987
-.468	1.0000	.9916	.9958	.9980
-.520	1.0079	.9963	.9942	.9972
-.572	1.0276	.9966	.9848	.9925
-.624	1.0473	1.0021	.9782	.9892
-.676	1.0630	1.0061	.9729	.9865
-.728	1.0788	1.0136	.9693	.9847
-.780	1.0748	1.0192	.9738	.9870
-.832	1.0709	1.0229	.9773	.9888
-.884	1.0985	1.0296	.9681	.9841
-.936	1.1260	1.0362	.9593	.9796
-.988	1.1457	1.0400	.9527	.9762
-1.040	1.1654	1.0455	.9471	.9732

(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^\circ$;

$p_\infty = 101.48$ psf (4858.76 N/m^2);
$q_\infty = 375.77$ psf (17991.97 N/m^2);
$p_{t,\infty} = 1268.90$ psf (60755.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9766	.9102	.9654	.9827
.988	.9175	.9042	.9927	.9964
.936	.8585	.8982	1.0229	1.0109
.884	.8506	.8901	1.0229	1.0109
.832	.8427	.8819	1.0230	1.0110
.780	.8348	.8756	1.0241	1.0115
.728	.8270	.8657	1.0232	1.0111
.676	.8073	.8585	1.0312	1.0148
.624	.7876	.8547	1.0418	1.0196
.572	.7758	.8486	1.0459	1.0215
.520	.7640	.8426	1.0502	1.0235
.468	.7482	.8402	1.0597	1.0277
.416	.7325	.8345	1.0674	1.0311
.364	.7325	.8275	1.0629	1.0291
.312	.7325	.8258	1.0618	1.0286
.260	.7325	.8205	1.0584	1.0271
.208	.7325	.8188	1.0573	1.0266
.156	.7246	.8176	1.0623	1.0289
.104	.7167	.8165	1.0673	1.0311
.052	.7206	.8110	1.0608	1.0282
0.000	.7246	.8124	1.0589	1.0274
-.104	.7167	.8132	1.0652	1.0301
-.156	.7325	.8138	1.0541	1.0252
-.208	.7482	.8144	1.0433	1.0203
-.260	.7364	.8170	1.0533	1.0249
-.312	.7521	.8210	1.0448	1.0210
-.364	.7600	.8222	1.0401	1.0189
-.416	.7561	.8277	1.0463	1.0217
-.468	.7640	.8341	1.0449	1.0211
-.520	.7718	.8388	1.0424	1.0200
-.572	.7758	.8454	1.0439	1.0206
-.624	.7797	.8521	1.0454	1.0213
-.676	.7915	.8600	1.0423	1.0199
-.728	.8033	.8678	1.0393	1.0185
-.780	.8152	.8739	1.0354	1.0167
-.832	.8270	.8817	1.0326	1.0154
-.884	.8388	.8896	1.0298	1.0142
-.936	.8506	.8992	1.0281	1.0134
-.988	.8782	.9058	1.0156	1.0075
-1.040	.9057	.9142	1.0047	1.0023

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) - Continued

(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^\circ$;

p_∞ = 101.48 psf (4858.76 N/m^2);
q_∞ = 375.77 psf (17991.97 N/m^2);
$p_{t,\infty}$ = 1268.90 psf (60755.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7796	.8031	1.0150	1.0072
.988	.7245	.7794	1.0372	1.0176
.936	.6694	.7696	1.0722	1.0332
.884	.6457	.7609	1.0855	1.0389
.832	.6221	.7522	1.0996	1.0449
.780	.6379	.7406	1.0775	1.0355
.728	.6536	.7290	1.0561	1.0261
.676	.6260	.7206	1.0729	1.0335
.624	.5985	.7139	1.0922	1.0418
.572	.5867	.7061	1.0971	1.0438
.520	.5749	.7000	1.1035	1.0465
.468	.5512	.6948	1.1227	1.0543
.416	.5276	.6896	1.1432	1.0625
.364	.5276	.6843	1.1389	1.0608
.312	.5276	.6930	1.1461	1.0636
.260	.5315	.6754	1.1272	1.0561
.208	.5355	.6716	1.1199	1.0532
.156	.5315	.6702	1.1228	1.0544
.104	.5276	.6687	1.1258	1.0556
.052	.5315	.6597	1.1141	1.0508
0.000	.5355	.6716	1.1199	1.0532
-.104	.5355	.6767	1.1241	1.0549
-.156	.5512	.6633	1.0970	1.0438
-.208	.5670	.6691	1.0864	1.0393
-.260	.5591	.6697	1.0945	1.0427
-.312	.5749	.6738	1.0826	1.0377
-.364	.5788	.6735	1.0787	1.0360
-.416	.5827	.6819	1.0818	1.0373
-.468	.5867	.6869	1.0820	1.0374
-.520	.5906	.6935	1.0836	1.0381
-.572	.5906	.7023	1.0904	1.0410
-.624	.5906	.7092	1.0958	1.0433
-.676	.5985	.7191	1.0961	1.0434
-.728	.6064	.7272	1.0951	1.0430
-.780	.6182	.7368	1.0918	1.0416
-.832	.6300	.7464	1.0885	1.0402
-.884	.6379	.7580	1.0901	1.0409
-.936	.6457	.7714	1.0930	1.0421
-.988	.6694	.7801	1.0796	1.0364
-1.040	.6930	.7905	1.0681	1.0314

(h) $x/D = 2.5$; $y/D = .83$; $\alpha = 0^\circ$;

p_∞ = 101.48 psf (4858.76 N/m^2);
q_∞ = 375.77 psf (17991.97 N/m^2);
$p_{t,\infty}$ = 1268.90 psf (60755.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7324	.7718	1.0266	1.0126
.988	.6812	.7443	1.0453	1.0213
.936	.6300	.7359	1.0808	1.0369
.884	.6064	.7254	1.0938	1.0424
.832	.5827	.7185	1.1104	1.0493
.780	.5985	.7052	1.0855	1.0389
.728	.6142	.6936	1.0626	1.0290
.676	.5906	.6866	1.0782	1.0358
.624	.5670	.6797	1.0949	1.0429
.572	.5512	.6739	1.1057	1.0474
.520	.5355	.6681	1.1170	1.0520
.468	.5158	.6626	1.1334	1.0586
.416	.4961	.6588	1.1523	1.0660
.364	.5000	.6550	1.1445	1.0630
.312	.5040	.6582	1.1428	1.0623
.260	.5119	.6507	1.1275	1.0562
.208	.5197	.6466	1.1154	1.0514
.156	.5158	.6452	1.1184	1.0526
.104	.5119	.6507	1.1275	1.0562
.052	.5197	.6345	1.1049	1.0471
0.000	.5276	.6513	1.1110	1.0496
-.104	.5197	.6464	1.1152	1.0513
-.156	.5315	.6368	1.0946	1.0428
-.208	.5434	.6517	1.0951	1.0430
-.260	.5355	.6453	1.0977	1.0441
-.312	.5473	.6444	1.0851	1.0387
-.364	.5512	.6441	1.0810	1.0370
-.416	.5512	.6493	1.0853	1.0389
-.468	.5552	.6543	1.0856	1.0390
-.520	.5591	.6592	1.0858	1.0391
-.572	.5591	.6662	1.0916	1.0415
-.624	.5591	.6731	1.0972	1.0439
-.676	.5670	.6813	1.0962	1.0434
-.728	.5749	.6911	1.0965	1.0436
-.780	.5827	.7010	1.0968	1.0437
-.832	.5906	.7091	1.0958	1.0433
-.884	.5945	.7228	1.1026	1.0461
-.936	.5985	.7364	1.1093	1.0489
-.988	.6221	.7452	1.0944	1.0427
-1.040	.6457	.7574	1.0830	1.0379

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(i) $x/D = 2.5$; $y/D = .63$; $\alpha = 0^\circ$;

$p_\infty = 101.32$ psf (4851.10 N/m^2);
$q_\infty = 375.18$ psf (17963.61 N/m^2);
$p_{t,\infty} = 1266.90$ psf (60659.50 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6945	.7307	1.0257	1.0123
.988	.6392	.7069	1.0516	1.0241
.936	.5840	.7005	1.0952	1.0430
.884	.5642	.6380	1.1043	1.0468
.832	.5445	.6825	1.1196	1.0531
.780	.5564	.6712	1.0984	1.0444
.728	.5682	.6616	1.0791	1.0362
.676	.5524	.6558	1.0896	1.0407
.624	.5366	.6518	1.1021	1.0459
.572	.5327	.6486	1.1034	1.0465
.520	.5287	.6436	1.1033	1.0464
.468	.5564	.6416	1.0739	1.0339
.416	.5840	.6674	1.0691	1.0318
.364	.7418	.7655	1.0158	1.0076
.312	.8996	.7885	.9362	.9674
.260	.9430	.7887	.9145	.9556
.208	.9865	.7889	.8943	.9442
.156	1.0062	.7874	.8846	.9386
.104	1.0259	.7859	.8752	.9331
.052	1.0299	.7856	.8734	.9321
0.000	1.0338	.7853	.8715	.9310
-.104	1.0259	.7913	.8782	.9349
-.156	1.0180	.7849	.8781	.9348
-.208	1.0101	.7855	.8818	.9370
-.260	.8286	.7940	.9789	.9896
-.312	.8207	.7841	.9775	.9889
-.364	.7813	.7556	.9835	.9919
-.416	.6313	.6533	1.0172	1.0083
-.468	.5919	.6335	1.0346	1.0164
-.520	.5524	.6364	1.0734	1.0337
-.572	.5406	.6373	1.0858	1.0391
-.624	.5287	.6417	1.1016	1.0457
-.676	.5366	.6481	1.0989	1.0446
-.728	.5445	.6545	1.0963	1.0435
-.780	.5485	.6629	1.0994	1.0448
-.832	.5524	.6713	1.1024	1.0460
-.884	.5485	.6838	1.1166	1.0519
-.936	.5445	.6981	1.1323	1.0581
-.988	.5721	.7065	1.1112	1.0497
-1.040	.5998	.7185	1.0945	1.0427

(j) $x/D = 2.5$; $y/D = .42$; $\alpha = 0^\circ$;

$p_\infty = 101.22$ psf (4846.50 N/m^2);
$q_\infty = 374.82$ psf (17946.60 N/m^2);
$p_{t,\infty} = 1265.70$ psf (60602.04 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6633	.6979	1.0258	1.0123
.988	.6081	.6846	1.0611	1.0283
.936	.5528	.6764	1.1062	1.0476
.884	.5370	.6671	1.1146	1.0510
.832	.5212	.6613	1.1264	1.0558
.780	.5370	.6532	1.1029	1.0462
.728	.5528	.6468	1.0817	1.0373
.676	.6594	.6371	.9830	.9916
.624	.7660	.7427	.9847	.9925
.572	.8963	.7975	.9433	.9712
.520	1.0266	.7893	.8769	.9341
.468	1.0503	.7893	.8669	.9282
.416	1.0740	.7874	.8563	.9218
.364	1.0779	.7871	.8545	.9208
.312	1.0819	.7851	.8519	.9191
.260	1.0858	.7830	.8492	.9175
.208	1.0898	.7827	.8475	.9165
.156	1.0977	.7768	.8413	.9126
.104	1.1056	.7745	.8370	.9099
.052	1.1095	.7707	.8334	.9077
0.000	1.1135	.7686	.8308	.9061
-.104	1.0977	.7760	.8408	.9123
-.156	1.1016	.7757	.8392	.9113
-.208	1.1056	.7772	.8384	.9109
-.260	1.0740	.7814	.8530	.9198
-.312	1.0779	.7811	.8512	.9188
-.364	1.0582	.7826	.8600	.9241
-.416	1.0503	.7832	.8636	.9262
-.468	1.0305	.7848	.8726	.9316
-.520	1.0108	.7828	.8800	.9359
-.572	.8292	.7913	.9769	.9886
-.624	.6475	.6615	1.0107	1.0052
-.676	.5923	.6324	1.0333	1.0158
-.728	.5370	.6382	1.0902	1.0409
-.780	.5370	.6435	1.0946	1.0428
-.832	.5370	.6504	1.1006	1.0453
-.884	.5251	.6600	1.1211	1.0537
-.936	.5133	.6731	1.1451	1.0632
-.988	.5370	.6836	1.1283	1.0566
-1.040	.5607	.6958	1.1140	1.0508

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(k) $x/D = 2.5$; $y/D = .21$; $\alpha = 0°$;

$p_\infty = 101.42$ psf (4856.08 N/m^2);
$q_\infty = 375.56$ psf (17982.05 N/m^2);
$p_{t,\infty} = 1268.20$ psf (60721.74 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6461	.6803	1.0262	1.0125
.988	.5909	.6687	1.0638	1.0295
.936	.5358	.6623	1.1118	1.0499
.884	.5831	.6554	1.0602	1.0279
.832	.6303	.6972	1.0517	1.0241
.780	.6894	.7294	1.0286	1.0136
.728	.7485	.7529	1.0029	1.0014
.676	.8431	.7615	.9504	.9749
.624	.9376	.7683	.9052	.9504
.572	.9928	.7710	.8813	.9367
.520	1.0479	.7720	.8583	.9231
.468	1.0716	.7772	.8516	.9190
.416	1.0952	.7753	.8414	.9127
.364	1.0952	.7718	.8395	.9115
.312	1.0952	.7701	.8385	.9109
.260	1.0913	.7336	.8199	.8992
.208	1.0873	.6656	.7824	.8744
.156	1.0991	.5539	.7099	.8225
.104	1.1110	.4591	.6429	.7693
.052	1.1070	.3898	.5934	.7266
0.000	1.1031	.3668	.5766	.7115
-.104	1.0952	.4344	.6298	.7583
-.156	1.0991	.5281	.6932	.8097
-.208	1.1031	.6406	.7621	.8604
-.260	1.0873	.7156	.8112	.8936
-.312	1.0913	.7521	.8302	.9057
-.364	1.0676	.7679	.8481	.9168
-.416	1.0794	.7705	.8449	.9148
-.468	1.0558	.7723	.8553	.9212
-.520	1.0322	.7654	.8611	.9248
-.572	.9770	.7609	.8825	.9374
-.624	.9219	.7564	.9058	.9508
-.676	.8588	.7490	.9339	.9662
-.728	.7958	.7363	.9619	.9809
-.780	.6894	.7163	1.0193	1.0092
-.832	.5831	.6562	1.0608	1.0282
-.884	.5397	.6454	1.0935	1.0423
-.936	.4964	.6590	1.1522	1.0659
-.988	.5200	.6660	1.1317	1.0579
-1.040	.5437	.6782	1.1169	1.0520

(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0°$;

$p_\infty = 101.40$ psf (4854.93 N/m^2);
$q_\infty = 375.47$ psf (17977.79 N/m^2);
$p_{t,\infty} = 1267.90$ psf (60707.38 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8195	.7451	.9535	.9766
.988	.7486	.7260	.9848	.9925
.936	.6777	.7122	1.0251	1.0120
.884	.6462	.6954	1.0374	1.0176
.832	.6146	.6838	1.0547	1.0255
.780	.6225	.6727	1.0396	1.0186
.728	.6304	.6809	1.0393	1.0185
.676	.7644	.7179	.9691	.9846
.624	.8983	.7653	.9230	.9603
.572	.9732	.7823	.8966	.9455
.520	1.0480	.7782	.8617	.9251
.468	1.0677	.7750	.8519	.9192
.416	1.0874	.7699	.8415	.9127
.364	1.0874	.7629	.8376	.9104
.312	1.0874	.7472	.8289	.9049
.260	1.0756	.6519	.7785	.8718
.208	1.0638	.5122	.6939	.8102
.156	1.0677	.3697	.5884	.7222
.104	1.0717	.3150	.5422	.6793
.052	1.0638	.3340	.5603	.6964
0.000	1.0559	.3528	.5780	.7128
-.104	1.0559	.3230	.5531	.6896
-.156	1.0677	.3382	.5628	.6988
-.208	1.0795	.4661	.6571	.7810
-.260	1.0638	.6299	.7695	.8656
-.312	1.0756	.7237	.8203	.8994
-.364	1.0638	.7579	.8441	.9144
-.416	1.0717	.7661	.8455	.9152
-.468	1.0598	.7687	.8517	.9190
-.520	1.0480	.7714	.8579	.9228
-.572	.9495	.7702	.9006	.9478
-.624	.8510	.7428	.9342	.9664
-.676	.7368	.6815	.9618	.9809
-.728	.6225	.6691	1.0367	1.0174
-.780	.6304	.6668	1.0284	1.0135
-.832	.6383	.6767	1.0296	1.0141
-.884	.6422	.6938	1.0394	1.0186
-.936	.6462	.7144	1.0515	1.0241
-.988	.6856	.7290	1.0312	1.0148
-1.040	.7250	.7470	1.0151	1.0072

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(m) $x/D = 2.5$; $y/D = -.42$; $\alpha = 0^\circ$;

p_∞ = 101.30 psf (4850.33 N/m²);
q_∞ = 375.12 psf (17960.78 N/m²);
$p_{t,\infty}$ = 1266.70 psf (60649.92 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7259	.7005	.9823	.9913
.988	.6431	.6788	1.0274	1.0130
.936	.5602	.6623	1.0873	1.0397
.884	.5405	.6446	1.0920	1.0417
.832	.5208	.6356	1.1047	1.0470
.780	.5168	.6219	1.0970	1.0438
.728	.5129	.6083	1.0890	1.0404
.676	.4655	.6013	1.1365	1.0598
.624	.4182	.5839	1.1816	1.0770
.572	.4892	.5613	1.0711	1.0327
.520	.5602	.5682	1.0071	1.0034
.468	.8009	.7681	.9793	.9898
.416	1.0416	.7498	.8484	.9170
.364	1.0495	.7491	.8449	.9149
.312	1.0573	.7730	.8550	.9211
.260	1.0652	.7654	.8477	.9166
.208	1.0731	.7613	.8423	.9132
.156	1.0850	.7569	.8352	.9089
.104	1.0968	.7559	.8302	.9057
.052	1.1007	.7521	.8266	.9034
0.000	1.1047	.6958	.7936	.8820
-.104	1.0889	.7619	.8365	.9096
-.156	1.0889	.7549	.8326	.9072
-.208	1.0889	.7567	.8336	.9078
-.260	1.0534	.7612	.8501	.9180
-.312	1.0534	.7629	.8510	.9186
-.364	.7772	.7682	.9942	.9972
-.416	1.0179	.7412	.8533	.9200
-.468	.7417	.7639	1.0148	1.0071
-.520	.4655	.5417	1.0786	1.0360
-.572	.4300	.5600	1.1411	1.0616
-.624	.3945	.5869	1.2197	1.0906
-.676	.4379	.6012	1.1717	1.0733
-.728	.4813	.6120	1.1276	1.0563
-.780	.5011	.6211	1.1133	1.0505
-.832	.5208	.6318	1.1015	1.0456
-.884	.5247	.6455	1.1091	1.0488
-.936	.5287	.6679	1.1240	1.0548
-.988	.5721	.6839	1.0934	1.0423
-1.040	.6155	.7086	1.0730	1.0336

(n) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^\circ$;

p_∞ = 101.31 psf (4850.71 N/m²);
q_∞ = 375.15 psf (17962.20 N/m²);
$p_{t,\infty}$ = 1266.80 psf (60654.71 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7415	.7193	.9850	.9926
.988	.6784	.7031	1.0181	1.0087
.936	.6153	.7043	1.0699	1.0322
.884	.7770	.7638	.9915	.9958
.832	.9387	.8145	.9315	.9649
.780	.9623	.8074	.9160	.9564
.728	.9860	.7969	.8990	.9469
.676	.9978	.7890	.8892	.9413
.624	1.0096	.7811	.8796	.9357
.572	1.0215	.7767	.8720	.9312
.520	1.0333	.7723	.8645	.9268
.468	1.0451	.7696	.8581	.9229
.416	1.0570	.7617	.8489	.9173
.364	1.0530	.7445	.8408	.9123
.312	1.0491	.7185	.8276	.9040
.260	1.0412	.6226	.7733	.8682
.208	1.0333	.5265	.7138	.8254
.156	1.0373	.4270	.6416	.7682
.104	1.0412	.3892	.6114	.7424
.052	1.0373	.3931	.6156	.7461
0.000	1.0333	.4042	.6254	.7546
-.104	1.0333	.3994	.6217	.7514
-.156	1.0412	.4094	.6270	.7559
-.208	1.0491	.4923	.6850	.8033
-.260	1.0412	.6041	.7617	.8602
-.312	1.0491	.6878	.8097	.8926
-.364	1.0373	.7361	.8424	.9133
-.416	1.0491	.7562	.8490	.9174
-.468	1.0373	.7624	.8573	.9225
-.520	1.0254	.7633	.8628	.9257
-.572	1.0175	.7692	.8694	.9297
-.624	1.0096	.7768	.8771	.9343
-.676	1.0057	.7858	.8840	.9383
-.728	1.0018	.7931	.8898	.9416
-.780	.9465	.8026	.9208	.9591
-.832	.8913	.8033	.9493	.9744
-.884	.7375	.7100	.9812	.9907
-.936	.5837	.7004	1.0954	1.0431
-.988	.6074	.7039	1.0766	1.0351
-1.040	.6310	.7196	1.0679	1.0313

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(o) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^\circ$;

p_∞ = 101.36 psf (4853.01 N/m^2);
q_∞ = 375.33 psf (17970.70 N/m^2);
$p_{t,\infty}$ = 1267.40 psf (60683.44 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1288	.8962	.8910	.9423
.988	1.0894	.8730	.8952	.9447
.936	1.0499	.8603	.9052	.9504
.884	1.0578	.8440	.8933	.9436
.832	1.0657	.8347	.8850	.9389
.780	1.0460	.8205	.8857	.9393
.728	1.0262	.8098	.8883	.9408
.676	1.0262	.7976	.8816	.9369
.624	1.0262	.7871	.8758	.9335
.572	1.0223	.7787	.8728	.9317
.520	1.0183	.7685	.8687	.9293
.468	1.0144	.7601	.8656	.9274
.416	1.0104	.7411	.8564	.9219
.364	.9986	.7124	.8446	.9147
.312	.9867	.6748	.8270	.9037
.260	.9828	.6033	.7835	.8752
.208	.9789	.5510	.7503	.8521
.156	.9828	.4980	.7118	.8239
.104	.9867	.4747	.6936	.8100
.052	.9907	.4655	.6855	.8037
0.000	.9946	.4652	.6839	.8024
−.104	.9867	.4777	.6958	.8117
−.156	.9867	.4901	.7047	.8186
−.208	.9867	.5324	.7346	.8408
−.260	.9907	.5902	.7718	.8672
−.312	.9907	.6464	.8077	.8913
−.364	.9946	.6969	.8371	.9100
−.416	.9946	.7354	.8599	.9240
−.468	.9986	.7509	.8672	.9284
−.520	1.0025	.7611	.8713	.9308
−.572	1.0065	.7730	.8764	.9338
−.624	1.0104	.7797	.8785	.9350
−.676	1.0183	.7879	.8796	.9357
−.728	1.0262	.7995	.8827	.9375
−.780	1.0223	.8103	.8903	.9419
−.832	1.0183	.8246	.8999	.9474
−.884	1.0262	.8345	.9018	.9485
−.936	1.0341	.8479	.9055	.9506
−.988	1.0381	.8598	.9101	.9531
−1.040	1.0420	.8735	.9156	.9562

(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^\circ$;

p_∞ = 101.32 psf (4851.10 N/m^2);
q_∞ = 375.18 psf (17963.61 N/m^2);
$p_{t,\infty}$ = 1266.90 psf (60659.50 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0570	.9817	.9637	.9819
.988	1.0136	.9850	.9857	.9930
.936	.9703	.9864	1.0083	1.0040
.884	.9782	.9841	1.0030	1.0015
.832	.9860	.9818	.9978	.9989
.780	.9742	.9827	1.0043	1.0021
.728	.9624	.9801	1.0091	1.0044
.676	.9545	.9772	1.0118	1.0057
.624	.9466	.9760	1.0154	1.0074
.572	.9466	.9760	1.0154	1.0074
.520	.9466	.9743	1.0145	1.0070
.468	.9387	.9748	1.0191	1.0091
.416	.9308	.9719	1.0218	1.0104
.364	.9308	.9702	1.0209	1.0100
.312	.9308	.9685	1.0200	1.0096
.260	.9269	.9687	1.0223	1.0107
.208	.9229	.9690	1.0247	1.0118
.156	.9229	.9690	1.0247	1.0118
.104	.9229	.9655	1.0228	1.0109
.052	.9269	.9653	1.0205	1.0098
0.000	.9308	.9650	1.0182	1.0087
−.104	.9150	.9620	1.0254	1.0121
−.156	.9229	.9615	1.0207	1.0099
−.208	.9308	.9626	1.0169	1.0081
−.260	.9190	.9635	1.0239	1.0114
−.312	.9269	.9629	1.0193	1.0092
−.364	.9269	.9629	1.0193	1.0092
−.416	.9229	.9632	1.0216	1.0103
−.468	.9229	.9632	1.0216	1.0103
−.520	.9229	.9667	1.0234	1.0112
−.572	.9269	.9664	1.0211	1.0101
−.624	.9308	.9679	1.0197	1.0094
−.676	.9348	.9676	1.0174	1.0083
−.728	.9387	.9708	1.0169	1.0081
−.780	.9348	.9728	1.0201	1.0096
−.832	.9308	.9731	1.0225	1.0107
−.884	.9427	.9757	1.0174	1.0083
−.936	.9545	.9783	1.0124	1.0060
−.988	.9663	.9792	1.0066	1.0032
−1.040	.9782	.9801	1.0010	1.0005

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(q) x/D = 5.0; y/D = 2.0; $\alpha = 0^o$;

p_∞ = 101.39 psf (4854.54 N/m^2);

q_∞ = 375.44 psf (17976.38 N/m^2);

$p_{t,\infty}$ = 1267.80 psf (60702.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8117	.8789	1.0406	1.0191
.988	.7723	.8644	1.0579	1.0269
.936	.7329	.8655	1.0867	1.0395
.884	.7250	.8644	1.0919	1.0416
.832	.7171	.8632	1.0971	1.0438
.780	.7289	.8606	1.0866	1.0394
.728	.7408	.8545	1.0740	1.0340
.676	.7250	.8539	1.0853	1.0388
.624	.7092	.8533	1.0969	1.0437
.572	.7053	.8519	1.0990	1.0446
.520	.7014	.8504	1.1012	1.0455
.468	.6895	.8496	1.1100	1.0492
.416	.6777	.8487	1.1190	1.0529
.364	.6777	.8469	1.1179	1.0524
.312	.6777	.8469	1.1179	1.0524
.260	.6856	.8429	1.1088	1.0487
.208	.6935	.8423	1.1021	1.0459
.156	.6895	.8409	1.1043	1.0468
.104	.6856	.8411	1.1076	1.0482
.052	.6856	.8359	1.1042	1.0468
0.000	.6856	.8394	1.1065	1.0477
-.104	.6856	.8369	1.1048	1.0470
-.156	.7014	.8357	1.0916	1.0415
-.208	.7171	.8363	1.0799	1.0365
-.260	.7014	.8375	1.0927	1.0420
-.312	.7171	.8363	1.0799	1.0365
-.364	.7132	.8366	1.0831	1.0379
-.416	.7171	.8363	1.0799	1.0365
-.468	.7132	.8384	1.0842	1.0384
-.520	.7092	.8404	1.0885	1.0402
-.572	.7053	.8407	1.0918	1.0416
-.624	.7014	.8427	1.0961	1.0434
-.676	.6974	.8448	1.1006	1.0453
-.728	.6935	.8468	1.1050	1.0471
-.780	.6974	.8482	1.1028	1.0462
-.832	.7014	.8497	1.1007	1.0453
-.884	.7053	.8511	1.0985	1.0444
-.936	.7092	.8543	1.0975	1.0440
-.988	.7171	.8555	1.0922	1.0418
-1.040	.7250	.8584	1.0881	1.0400

(r) x/D = 5.0; y/D = 1.5; $\alpha = 0^o$;

p_∞ = 101.48 psf (4858.76 N/m^2);

q_∞ = 375.77 psf (17991.97 N/m^2);

$p_{t,\infty}$ = 1268.90 psf (60755.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7874	.8719	1.0523	1.0244
.988	.8976	.9872	1.0487	1.0228
.936	1.0078	.9877	.9899	.9951
.884	1.0393	.9836	.9728	.9865
.832	1.0708	.9795	.9564	.9781
.780	1.0511	.9775	.9643	.9822
.728	1.0315	.9755	.9725	.9863
.676	1.0354	.9717	.9687	.9844
.624	1.0393	.9714	.9668	.9834
.572	1.0393	.9679	.9650	.9825
.520	1.0393	.9662	.9642	.9821
.468	1.0315	.9633	.9664	.9832
.416	1.0236	.9621	.9695	.9848
.364	1.0236	.9586	.9678	.9839
.312	1.0236	.9552	.9660	.9830
.260	1.0157	.9523	.9683	.9842
.208	1.0078	.9529	.9723	.9863
.156	1.0118	.9491	.9685	.9843
.104	1.0157	.9488	.9665	.9833
.052	1.0196	.9485	.9645	.9823
0.000	1.0236	.9482	.9625	.9812
-.104	1.0078	.9476	.9696	.9849
-.156	1.0157	.9470	.9656	.9828
-.208	1.0236	.9481	.9624	.9812
-.260	1.0078	.9493	.9705	.9854
-.312	1.0157	.9505	.9674	.9837
-.364	1.0118	.9525	.9703	.9852
-.416	1.0078	.9546	.9732	.9867
-.468	1.0039	.9548	.9753	.9877
-.520	1.0000	.9569	.9782	.9892
-.572	1.0039	.9566	.9762	.9882
-.624	1.0078	.9598	.9759	.9881
-.676	1.0078	.9615	.9768	.9885
-.728	1.0078	.9650	.9785	.9894
-.780	1.0078	.9668	.9794	.9898
-.832	1.0078	.9685	.9803	.9903
-.884	.9921	.9732	.9904	.9953
-.936	.9763	.9744	.9990	.9995
-.988	.8346	.9395	1.0610	1.0283
-1.040	.6929	.8279	1.0931	1.0421

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^\circ$;

p_∞ = 101.39 psf (4854.54 N/m²);

q_∞ = 375.44 psf (17976.38 N/m²);

$p_{t,\infty}$ = 1267.80 psf (60702.59 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0808	.9378	.9315	.9649
.988	1.0414	.9338	.9469	.9731
.936	1.0019	.9316	.9642	.9821
.884	1.0177	.9251	.9534	.9765
.832	1.0335	.9205	.9437	.9714
.780	1.0177	.9147	.9480	.9737
.728	1.0019	.9089	.9524	.9760
.676	1.0059	.9016	.9468	.9730
.624	1.0098	.8961	.9420	.9705
.572	1.0138	.8906	.9373	.9680
.520	1.0177	.8833	.9316	.9650
.468	1.0098	.8787	.9328	.9656
.416	1.0019	.8741	.9340	.9662
.364	1.0019	.8671	.9303	.9642
.312	1.0019	.8601	.9265	.9622
.260	.9980	.8569	.9266	.9623
.208	.9941	.8537	.9267	.9623
.156	.9941	.8485	.9239	.9608
.104	.9941	.8450	.9220	.9597
.052	.9980	.8447	.9200	.9586
0.000	1.0019	.8444	.9180	.9575
-.104	.9862	.8445	.9254	.9616
-.156	.9901	.8442	.9234	.9605
-.208	.9941	.8474	.9233	.9604
-.260	.9822	.8500	.9303	.9642
-.312	.9862	.8550	.9311	.9647
-.364	.9862	.8567	.9321	.9652
-.416	.9783	.8626	.9390	.9689
-.468	.9783	.8696	.9428	.9709
-.520	.9783	.8748	.9456	.9725
-.572	.9822	.8798	.9464	.9729
-.624	.9862	.8865	.9481	.9738
-.676	.9862	.8917	.9509	.9752
-.728	.9862	.8987	.9546	.9772
-.780	.9783	.9028	.9607	.9803
-.832	.9704	.9069	.9667	.9834
-.884	.9743	.9119	.9674	.9838
-.936	.9783	.9168	.9681	.9841
-.988	.9862	.9197	.9657	.9829
-1.040	.9941	.9244	.9643	.9822

(t) $x/D = 5.0$; $y/D = .83$; $\alpha = 0^\circ$;

p_∞ = 101.49 psf (4859.14 N/m²);

q_∞ = 375.80 psf (17993.39 N/m²);

$p_{t,\infty}$ = 1269.00 psf (60760.05 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0878	.9241	.9217	.9595
.988	1.0484	.9184	.9359	.9673
.936	1.0090	.9127	.9511	.9753
.884	1.0248	.9028	.9386	.9687
.832	1.0405	.8964	.9281	.9631
.780	1.0208	.8891	.9333	.9658
.728	1.0011	.8819	.9386	.9687
.676	1.0090	.8726	.9300	.9641
.624	1.0169	.8616	.9205	.9589
.572	1.0169	.8546	.9167	.9568
.520	1.0169	.8459	.9121	.9542
.468	1.0090	.8395	.9122	.9543
.416	1.0011	.8332	.9123	.9543
.364	.9972	.8265	.9104	.9533
.312	.9932	.8181	.9075	.9517
.260	.9893	.8149	.9076	.9517
.208	.9854	.8135	.9086	.9523
.156	.9893	.8097	.9047	.9501
.104	.9932	.8059	.9008	.9479
.052	.9932	.8041	.8998	.9473
0.000	.9932	.8041	.8998	.9473
-.104	.9854	.8032	.9028	.9491
-.156	.9893	.8029	.9009	.9480
-.208	.9932	.8043	.8999	.9474
-.260	.9814	.8070	.9068	.9513
-.312	.9854	.8119	.9077	.9518
-.364	.9854	.8137	.9087	.9524
-.416	.9775	.8213	.9166	.9568
-.468	.9775	.8265	.9195	.9584
-.520	.9775	.8352	.9244	.9610
-.572	.9814	.8419	.9262	.9620
-.624	.9854	.8503	.9290	.9635
-.676	.9893	.8570	.9307	.9645
-.728	.9932	.8672	.9344	.9665
-.780	.9854	.8748	.9422	.9706
-.832	.9775	.8806	.9492	.9743
-.884	.9854	.8905	.9506	.9751
-.936	.9932	.8986	.9512	.9754
-.988	.9972	.9035	.9519	.9757
-1.040	1.0011	.9102	.9535	.9766

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(u) $x/D = 5.0$; $y/D = .63$; $\alpha = 0^\circ$;

$p_\infty = 101.18$ psf (4844.59 N/m^2);

$q_\infty = 374.67$ psf (17939.51 N/m^2);

$p_{t,\infty} = 1265.20$ psf (60578.10 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1001	.9080	.9085	.9523
.988	1.0605	.8970	.9197	.9585
.936	1.0209	.8878	.9325	.9654
.884	1.0289	.8749	.9222	.9598
.832	1.0368	.8656	.9137	.9552
.780	1.0170	.8566	.9178	.9574
.728	.9972	.8441	.9200	.9587
.676	1.0012	.8333	.9123	.9544
.624	1.0051	.8225	.9046	.9501
.572	1.0051	.8120	.8988	.9468
.520	1.0051	.8050	.8949	.9446
.468	1.0012	.8001	.8940	.9440
.416	.9972	.7934	.8920	.9429
.364	.9932	.7884	.8910	.9423
.312	.9893	.7835	.8899	.9417
.260	.9853	.7803	.8899	.9417
.208	.9814	.7771	.8899	.9417
.156	.9853	.7715	.8849	.9388
.104	.9893	.7712	.8829	.9377
.052	.9932	.7692	.8800	.9360
0.000	.9972	.7671	.8771	.9342
−.104	.9814	.7693	.8854	.9391
−.156	.9853	.7690	.8834	.9379
−.208	.9893	.7704	.8825	.9374
−.260	.9774	.7713	.8883	.9408
−.312	.9814	.7763	.8894	.9414
−.364	.9814	.7780	.8904	.9420
−.416	.9735	.7839	.8974	.9460
−.468	.9735	.7892	.9004	.9477
−.520	.9735	.7927	.9024	.9488
−.572	.9774	.8011	.9053	.9505
−.624	.9814	.8096	.9083	.9521
−.676	.9853	.8198	.9121	.9543
−.728	.9893	.8317	.9169	.9569
−.780	.9893	.8405	.9217	.9596
−.832	.9893	.8510	.9275	.9627
−.884	.9932	.8612	.9312	.9647
−.936	.9972	.8731	.9357	.9672
−.988	1.0012	.8816	.9384	.9686
−1.040	1.0051	.8918	.9419	.9705

(v) $x/D = 5.0$; $y/D = .42$; $\alpha = 0^\circ$;

$p_\infty = 101.22$ psf (4846.50 N/m^2);

$q_\infty = 374.82$ psf (17946.60 N/m^2);

$p_{t,\infty} = 1265.70$ psf (60602.04 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0998	.8946	.9019	.9485
.988	1.0563	.8769	.9112	.9537
.936	1.0128	.8610	.9220	.9597
.884	1.0167	.8449	.9116	.9540
.832	1.0207	.8324	.9031	.9492
.780	1.0009	.8234	.9070	.9514
.728	.9811	.8109	.9091	.9526
.676	.9890	.7998	.8993	.9470
.624	.9969	.7922	.8914	.9426
.572	1.0009	.7849	.8855	.9392
.520	1.0049	.7811	.8816	.9369
.468	1.0167	.7749	.8730	.9318
.416	1.0286	.7722	.8665	.9280
.364	1.0286	.7687	.8645	.9268
.312	1.0286	.7600	.8596	.9238
.260	1.0326	.7474	.8508	.9185
.208	1.0365	.7366	.8430	.9137
.156	1.0523	.7143	.8239	.9017
.104	1.0682	.6920	.8049	.8894
.052	1.0682	.6832	.7997	.8860
0.000	1.0682	.6779	.7966	.8840
−.104	1.0523	.6958	.8132	.8948
−.156	1.0484	.7102	.8231	.9012
−.208	1.0444	.7246	.8329	.9074
−.260	1.0207	.7387	.8507	.9184
−.312	1.0167	.7495	.8586	.9232
−.364	1.0088	.7554	.8653	.9273
−.416	.9890	.7640	.8789	.9353
−.468	.9811	.7681	.8848	.9387
−.520	.9732	.7687	.8887	.9410
−.572	.9732	.7722	.8908	.9422
−.624	.9732	.7792	.8948	.9445
−.676	.9772	.7859	.8968	.9456
−.728	.9811	.7979	.9018	.9485
−.780	.9811	.8084	.9077	.9518
−.832	.9811	.8207	.9146	.9556
−.884	.9890	.8341	.9183	.9577
−.936	.9969	.8492	.9229	.9602
−.988	1.0009	.8629	.9285	.9633
−1.040	1.0049	.8767	.9340	.9663

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(w) $x/D = 5.0$; $y/D = .21$; $\alpha = 0^\circ$;
$p_\infty = 101.30$ psf (4850.33 N/m^2);
$q_\infty = 375.12$ psf (17960.78 N/m^2);
$p_{t,\infty} = 1266.70$ psf (60649.92 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0831	.8860	.9044	.9500
.988	1.0555	.8654	.9055	.9506
.936	1.0278	.8553	.9122	.9543
.884	1.0436	.8471	.9010	.9480
.832	1.0594	.8372	.8889	.9411
.780	1.0436	.8384	.8963	.9454
.728	1.0278	.8361	.9019	.9486
.676	1.0713	.8188	.8743	.9326
.624	1.1147	.8154	.8553	.9212
.572	1.1345	.8087	.8443	.9145
.520	1.1543	.7984	.8317	.9066
.468	1.1661	.7887	.8224	.9007
.416	1.1780	.7738	.8105	.8930
.364	1.1582	.7420	.8004	.8865
.312	1.1385	.7033	.7860	.8768
.260	1.1306	.6425	.7539	.8547
.208	1.1227	.5940	.7274	.8355
.156	1.1227	.5517	.7010	.8157
.104	1.1227	.5199	.6805	.7998
.052	1.1227	.5022	.6688	.7905
0.000	1.1227	.4969	.6653	.7876
-.104	1.1147	.5084	.6754	.7957
-.156	1.1108	.5336	.6931	.8096
-.208	1.1068	.5764	.7216	.8313
-.260	1.1029	.6261	.7534	.8543
-.312	1.0989	.6739	.7831	.8749
-.364	1.0831	.7209	.8158	.8965
-.416	1.0910	.7589	.8340	.9081
-.468	1.0752	.7759	.8495	.9177
-.520	1.0594	.7859	.8613	.9249
-.572	1.0515	.7795	.8610	.9247
-.624	1.0436	.7854	.8675	.9286
-.676	1.0238	.7974	.8825	.9374
-.728	1.0041	.8007	.8930	.9435
-.780	.9922	.8051	.9008	.9479
-.832	.9803	.8130	.9107	.9535
-.884	.9803	.8235	.9165	.9567
-.936	.9803	.8375	.9243	.9610
-.988	.9843	.8460	.9271	.9625
-1.040	.9883	.8579	.9317	.9650

(x) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^\circ$;
$p_\infty = 101.29$ psf (4849.95 N/m^2);
$q_\infty = 375.09$ psf (17959.36 N/m^2);
$p_{t,\infty} = 1266.60$ psf (60645.13 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2396	.9328	.8675	.9285
.988	1.2199	.9168	.8669	.9282
.936	1.2001	.9026	.8672	.9284
.884	1.2080	.8863	.8565	.9220
.832	1.2159	.8752	.8484	.9170
.780	1.1843	.8654	.8548	.9209
.728	1.1528	.8573	.8624	.9255
.676	1.1765	.8397	.8448	.9148
.624	1.2001	.8274	.8303	.9058
.572	1.2001	.8169	.8250	.9024
.520	1.2001	.8081	.8206	.8996
.468	1.2001	.7923	.8125	.8944
.416	1.2001	.7660	.7989	.8855
.364	1.1804	.7307	.7868	.8774
.312	1.1607	.6955	.7741	.8687
.260	1.1528	.6363	.7430	.8469
.208	1.1449	.6000	.7239	.8330
.156	1.1449	.5665	.7034	.8176
.104	1.1449	.5471	.6913	.8082
.052	1.1488	.5326	.6809	.8001
0.000	1.1528	.5234	.6738	.7945
-.104	1.1449	.5556	.6966	.8123
-.156	1.1409	.5683	.7058	.8193
-.208	1.1370	.5916	.7213	.8310
-.260	1.1370	.6251	.7415	.8458
-.312	1.1330	.6677	.7677	.8643
-.364	1.1370	.7132	.7920	.8809
-.416	1.1291	.7595	.8202	.8993
-.468	1.1330	.7802	.8298	.9055
-.520	1.1370	.7975	.8375	.9103
-.572	1.1488	.8088	.8391	.9113
-.624	1.1607	.8185	.8397	.9117
-.676	1.1646	.8269	.8426	.9135
-.728	1.1686	.8389	.8473	.9163
-.780	1.1528	.8489	.8581	.9229
-.832	1.1370	.8606	.8700	.9301
-.884	1.1330	.8697	.8761	.9337
-.936	1.1291	.8735	.8796	.9357
-.988	1.1054	.8788	.8916	.9427
-1.040	1.0817	.8806	.9023	.9488

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(y) $x/D = 5.0$; $y/D = -.42$; $\alpha = 0°$;

p_∞ = 101.25 psf (4847.65 N/m^2);

q_∞ = 374.91 psf (17950.85 N/m^2);

$p_{t,\infty}$ = 1266.00 psf (60616.41 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2890	.9417	.8547	.9209
.988	1.2416	.9279	.8645	.9268
.936	1.1941	.9141	.8749	.9330
.884	1.1941	.8931	.8648	.9270
.832	1.1941	.8791	.8580	.9229
.780	1.1586	.8643	.8637	.9263
.728	1.1230	.8496	.8698	.9299
.676	1.1467	.8285	.8500	.9180
.624	1.1704	.8091	.8314	.9065
.572	1.1704	.7933	.8233	.9013
.520	1.1704	.7793	.8160	.8966
.468	1.1744	.7737	.8117	.8939
.416	1.1783	.7822	.8147	.8958
.364	1.1625	.7939	.8264	.9033
.312	1.1467	.7934	.8318	.9067
.260	1.1388	.7905	.8332	.9076
.208	1.1309	.7859	.8336	.9079
.156	1.1348	.7803	.8292	.9051
.104	1.1388	.7660	.8202	.8993
.052	1.1427	.7324	.8006	.8866
0.000	1.1467	.7092	.7865	.8772
−.104	1.1309	.7545	.8168	.8972
−.156	1.1269	.7759	.8298	.9054
−.208	1.1230	.7797	.8333	.9076
−.260	1.1230	.7850	.8361	.9094
−.312	1.1190	.7870	.8386	.9110
−.364	1.1230	.7902	.8389	.9111
−.416	1.1151	.7873	.8403	.9120
−.468	1.1190	.7712	.8302	.9057
−.520	1.1230	.7727	.8295	.9052
−.572	1.1348	.7875	.8331	.9075
−.624	1.1467	.8042	.8374	.9102
−.676	1.1546	.8194	.8424	.9133
−.728	1.1625	.8380	.8491	.9174
−.780	1.1586	.8541	.8586	.9233
−.832	1.1546	.8737	.8699	.9300
−.884	1.1704	.8866	.8703	.9303
−.936	1.1862	.9011	.8716	.9310
−.988	1.1941	.9163	.8760	.9336
−1.040	1.2020	.9315	.8803	.9361

(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0°$;

p_∞ = 101.17 psf (4844.21 N/m^2);

q_∞ = 374.64 psf (17938.09 N/m^2);

$p_{t,\infty}$ = 1265.10 psf (60573.31 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2027	.8983	.8642	.9266
.988	1.1592	.8859	.8742	.9325
.936	1.1157	.8717	.8839	.9382
.884	1.1196	.8591	.8760	.9336
.832	1.1236	.8483	.8689	.9294
.780	1.0959	.8382	.8746	.9328
.728	1.0682	.8281	.8805	.9362
.676	1.0880	.8161	.8661	.9277
.624	1.1078	.8058	.8529	.9197
.572	1.1078	.7988	.8491	.9175
.520	1.1078	.7918	.8454	.9152
.468	1.1157	.7754	.8336	.9079
.416	1.1236	.7555	.8200	.8992
.364	1.1117	.7301	.8104	.8930
.312	1.0999	.7064	.8014	.8871
.260	1.0999	.6713	.7813	.8736
.208	1.0999	.6485	.7678	.8644
.156	1.0999	.6238	.7531	.8541
.104	1.0999	.5992	.7381	.8433
.052	1.1117	.5806	.7226	.8320
0.000	1.1236	.5672	.7105	.8229
−.104	1.1157	.5888	.7265	.8348
−.156	1.1038	.6110	.7440	.8476
−.208	1.0920	.6402	.7657	.8629
−.260	1.0999	.6624	.7761	.8701
−.312	1.0880	.6863	.7942	.8824
−.364	1.0880	.7144	.8103	.8930
−.416	1.0840	.7446	.8288	.9048
−.468	1.0840	.7639	.8395	.9115
−.520	1.0840	.7797	.8481	.9168
−.572	1.0880	.7900	.8521	.9193
−.624	1.0920	.7984	.8551	.9211
−.676	1.0999	.8084	.8573	.9224
−.728	1.1078	.8165	.8585	.9232
−.780	1.1038	.8274	.8658	.9275
−.832	1.0999	.8382	.8730	.9318
−.884	1.1117	.8513	.8751	.9331
−.936	1.1236	.8644	.8771	.9343
−.988	1.1315	.8761	.8799	.9359
−1.040	1.1394	.8913	.8844	.9385

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(aa) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 101.33$ psf (4851.86 N/m^2);

$q_\infty = 375.24$ psf (17966.45 N/m^2);

$p_{t,\infty} = 1267.10$ psf (60669.07 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1139	.8737	.8856	.9392
.988	1.0705	.8578	.8952	.9447
.936	1.0270	.8472	.9082	.9521
.884	1.0349	.8326	.8969	.9457
.832	1.0428	.8250	.8895	.9414
.780	1.0152	.8149	.8960	.9452
.728	.9875	.8065	.9037	.9496
.676	1.0073	.7963	.8891	.9412
.624	1.0270	.7860	.8748	.9329
.572	1.0270	.7773	.8700	.9300
.520	1.0270	.7686	.8651	.9271
.468	1.0270	.7563	.8581	.9230
.416	1.0270	.7406	.8492	.9175
.364	1.0231	.7216	.8399	.9117
.312	1.0191	.7080	.8335	.9078
.260	1.0191	.6834	.8189	.8985
.208	1.0191	.6659	.8084	.8917
.156	1.0231	.6411	.7916	.8806
.104	1.0270	.6215	.7779	.8713
.052	1.0349	.6015	.7624	.8606
0.000	1.0428	.5886	.7513	.8528
-.104	1.0349	.6048	.7645	.8621
-.156	1.0310	.6227	.7772	.8709
-.208	1.0270	.6494	.7952	.8830
-.260	1.0270	.6617	.8027	.8880
-.312	1.0231	.6778	.8140	.8953
-.364	1.0231	.7059	.8306	.9060
-.416	1.0191	.7272	.8447	.9148
-.468	1.0191	.7430	.8539	.9204
-.520	1.0191	.7588	.8629	.9258
-.572	1.0231	.7708	.8680	.9288
-.624	1.0270	.7792	.8710	.9307
-.676	1.0310	.7877	.8741	.9325
-.728	1.0349	.7961	.8771	.9342
-.780	1.0310	.8034	.8828	.9376
-.832	1.0270	.8160	.8914	.9425
-.884	1.0310	.8262	.8952	.9447
-.936	1.0349	.8381	.8999	.9474
-.988	1.0428	.8463	.9009	.9479
-1.040	1.0507	.8597	.9045	.9500

(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 101.25$ psf (4848.03 N/m^2);

$q_\infty = 374.94$ psf (17952.27 N/m^2);

$p_{t,\infty} = 1266.10$ psf (60621.19 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0438	.8606	.9080	.9520
.988	1.0043	.8392	.9141	.9554
.936	.9647	.8282	.9265	.9622
.884	.9687	.8157	.9176	.9573
.832	.9726	.8066	.9107	.9535
.780	.9529	.7994	.9159	.9564
.728	.9331	.7922	.9214	.9594
.676	.9489	.7805	.9069	.9514
.624	.9647	.7723	.8947	.9445
.572	.9647	.7635	.8896	.9415
.520	.9647	.7548	.8845	.9386
.468	.9647	.7426	.8773	.9344
.416	.9647	.7286	.8690	.9295
.364	.9608	.7114	.8605	.9244
.312	.9568	.6994	.8550	.9210
.260	.9568	.6784	.8420	.9131
.208	.9568	.6609	.8311	.9063
.156	.9608	.6413	.8170	.8973
.104	.9647	.6252	.8050	.8895
.052	.9726	.6088	.7912	.8803
0.000	.9805	.5994	.7819	.8740
-.104	.9647	.6047	.7917	.8807
-.156	.9687	.6185	.7990	.8856
-.208	.9726	.6375	.8096	.8925
-.260	.9647	.6539	.8233	.9013
-.312	.9687	.6695	.8313	.9064
-.364	.9687	.6888	.8432	.9138
-.416	.9647	.7137	.8601	.9241
-.468	.9647	.7277	.8685	.9292
-.520	.9647	.7400	.8758	.9335
-.572	.9647	.7505	.8820	.9371
-.624	.9647	.7593	.8872	.9401
-.676	.9687	.7695	.8913	.9425
-.728	.9726	.7798	.8954	.9448
-.780	.9687	.7871	.9014	.9483
-.832	.9647	.7979	.9094	.9528
-.884	.9687	.8064	.9124	.9544
-.936	.9726	.8183	.9173	.9571
-.988	.9805	.8283	.9191	.9581
-1.040	.9884	.8399	.9218	.9596

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(cc) x/D = 8.39; y/D = 3.0; $\alpha = 0^\circ$;
p_∞ = 101.39 psf (4854.54 N/m^2);
q_∞ = 375.44 psf (17976.38 N/m^2);
$p_{t,\infty}$ = 1267.80 psf (60702.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0817	.9978	.9604	.9802
.988	1.0423	1.0007	.9799	.9901
.936	1.0028	1.0037	1.0005	1.0002
.884	1.0107	1.0014	.9954	.9977
.832	1.0186	1.0008	.9912	.9957
.780	.9949	1.0025	1.0038	1.0019
.728	.9712	1.0026	1.0160	1.0077
.676	.9830	.9999	1.0086	1.0041
.624	.9949	.9991	1.0021	1.0010
.572	.9988	.9988	1.0000	1.0000
.520	1.0028	1.0002	.9987	.9994
.468	1.0028	1.0002	.9987	.9994
.416	1.0028	1.0019	.9996	.9998
.364	1.0028	1.0019	.9996	.9998
.312	1.0028	1.0019	.9996	.9998
.260	1.0028	1.0019	.9996	.9998
.208	1.0028	1.0037	1.0005	1.0002
.156	1.0028	1.0019	.9996	.9998
.104	1.0028	1.0019	.9996	.9998
.052	1.0067	1.0017	.9975	.9988
0.000	1.0107	1.0031	.9962	.9982
-.104	1.0028	1.0003	.9988	.9994
-.156	1.0067	1.0000	.9967	.9984
-.208	1.0107	.9997	.9946	.9973
-.260	.9949	1.0009	1.0030	1.0015
-.312	.9988	1.0006	1.0009	1.0004
-.364	.9988	1.0006	1.0009	1.0004
-.416	.9870	.9997	1.0064	1.0031
-.468	.9870	.9997	1.0064	1.0031
-.520	.9870	.9997	1.0064	1.0031
-.572	.9909	.9994	1.0043	1.0021
-.624	.9949	.9991	1.0021	1.0010
-.676	.9988	.9988	1.0000	1.0000
-.728	1.0028	1.0003	.9988	.9994
-.780	.9988	1.0006	1.0009	1.0004
-.832	.9949	1.0009	1.0030	1.0015
-.884	.9988	1.0006	1.0009	1.0004
-.936	1.0028	1.0003	.9988	.9994
-.988	1.0107	.9997	.9946	.9973
-1.040	1.0186	.9991	.9904	.9953

(dd) x/D = 8.39; y/D = 2.0; $\alpha = 0^\circ$;
p_∞ = 101.37 psf (4853.78 N/m^2);
q_∞ = 375.39 psf (17973.54 N/m^2);
$p_{t,\infty}$ = 1267.60 psf (60693.02 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2086	1.0371	.9263	.9621
.988	1.1691	1.0401	.9432	.9712
.936	1.1296	1.0413	.9601	.9800
.884	1.1375	1.0390	.9557	.9777
.832	1.1454	1.0384	.9521	.9759
.780	1.1099	1.0393	.9677	.9839
.728	1.0743	1.0402	.9840	.9921
.676	1.0980	1.0367	.9717	.9859
.624	1.1217	1.0332	.9597	.9798
.572	1.1217	1.0315	.9589	.9794
.520	1.1217	1.0315	.9589	.9794
.468	1.1178	1.0300	.9599	.9799
.416	1.1138	1.0286	.9610	.9805
.364	1.1138	1.0268	.9602	.9800
.312	1.1138	1.0268	.9602	.9800
.260	1.1099	1.0271	.9620	.9810
.208	1.1059	1.0292	.9647	.9824
.156	1.1138	1.0286	.9610	.9805
.104	1.1217	1.0280	.9573	.9786
.052	1.1217	1.0280	.9573	.9786
0.000	1.1217	1.0280	.9573	.9786
-.104	1.1059	1.0241	.9623	.9811
-.156	1.1059	1.0241	.9623	.9811
-.208	1.1059	1.0259	.9631	.9816
-.260	1.0980	1.0282	.9677	.9839
-.312	1.0980	1.0300	.9685	.9843
-.364	1.0980	1.0300	.9685	.9843
-.416	1.0901	1.0323	.9731	.9867
-.468	1.0901	1.0323	.9731	.9867
-.520	1.0901	1.0341	.9740	.9871
-.572	1.1020	1.0332	.9683	.9842
-.624	1.1138	1.0323	.9627	.9813
-.676	1.1178	1.0320	.9609	.9804
-.728	1.1217	1.0334	.9598	.9799
-.780	1.1138	1.0340	.9635	.9818
-.832	1.1059	1.0364	.9681	.9841
-.884	1.1178	1.0372	.9633	.9817
-.936	1.1296	1.0398	.9594	.9797
-.988	1.1375	1.0410	.9566	.9782
-1.040	1.1454	1.0404	.9531	.9763

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(ee) x/D = 8.39; y/D = 1.5; $\alpha = 0^o$;

p_∞ = 101.34 psf (4852.25 N/m^2);

q_∞ = 375.27 psf (17967.87 N/m^2);

$p_{t,\infty}$ = 1267.20 psf (60673.86 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1774	1.0014	.9223	.9599
.988	1.1339	1.0047	.9413	.9702
.936	1.0904	1.0028	.9590	.9794
.884	1.0984	1.0004	.9544	.9770
.832	1.1063	.9963	.9490	.9742
.780	1.0746	.9970	.9632	.9816
.728	1.0430	.9959	.9771	.9887
.676	1.0628	.9909	.9656	.9828
.624	1.0825	.9894	.9560	.9779
.572	1.0865	.9856	.9524	.9760
.520	1.0904	.9836	.9497	.9746
.468	1.0865	.9821	.9508	.9751
.416	1.0825	.9789	.9509	.9752
.364	1.0825	.9772	.9501	.9748
.312	1.0825	.9755	.9492	.9743
.260	1.0825	.9755	.9492	.9743
.208	1.0825	.9737	.9484	.9739
.156	1.0825	.9720	.9475	.9735
.104	1.0825	.9702	.9467	.9730
.052	1.0904	.9714	.9438	.9715
0.000	1.0984	.9708	.9401	.9695
-.104	1.0825	.9667	.9450	.9721
-.156	1.0786	.9670	.9469	.9731
-.208	1.0746	.9691	.9496	.9745
-.260	1.0707	.9694	.9515	.9755
-.312	1.0667	.9697	.9534	.9765
-.364	1.0667	.9714	.9543	.9770
-.416	1.0588	.9755	.9598	.9799
-.468	1.0588	.9790	.9616	.9808
-.520	1.0588	.9808	.9624	.9812
-.572	1.0707	.9816	.9575	.9787
-.624	1.0825	.9842	.9535	.9766
-.676	1.0865	.9857	.9525	.9760
-.728	1.0904	.9906	.9531	.9764
-.780	1.0865	.9944	.9567	.9782
-.832	1.0825	.9965	.9594	.9797
-.884	1.0944	1.0008	.9563	.9780
-.936	1.1063	1.0052	.9532	.9764
-.988	1.1181	1.0061	.9486	.9740
-1.040	1.1300	1.0087	.9448	.9720

(ff) x/D = 8.39; y/D = 1.0; $\alpha = 0^o$;

p_∞ = 101.40 psf (4854.93 N/m^2);

q_∞ = 375.47 psf (17977.79 N/m^2);

$p_{t,\infty}$ = 1267.90 psf (60707.38 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1290	.9452	.9150	.9559
.988	1.0895	.9395	.9286	.9633
.936	1.0501	.9355	.9439	.9715
.884	1.0540	.9265	.9375	.9681
.832	1.0580	.9209	.9330	.9657
.780	1.0303	.9160	.9429	.9710
.728	1.0027	.9077	.9514	.9755
.676	1.0264	.8989	.9358	.9672
.624	1.0501	.8901	.9207	.9590
.572	1.0501	.8832	.9171	.9570
.520	1.0501	.8779	.9144	.9555
.468	1.0501	.8692	.9098	.9530
.416	1.0501	.8657	.9080	.9520
.364	1.0461	.8608	.9071	.9515
.312	1.0422	.8541	.9053	.9504
.260	1.0422	.8471	.9016	.9484
.208	1.0422	.8454	.9006	.9478
.156	1.0461	.8416	.8969	.9457
.104	1.0501	.8395	.8941	.9441
.052	1.0501	.8378	.8932	.9436
0.000	1.0501	.8360	.8923	.9431
-.104	1.0422	.8317	.8933	.9437
-.156	1.0422	.8317	.8933	.9437
-.208	1.0422	.8317	.8933	.9437
-.260	1.0343	.8340	.8980	.9463
-.312	1.0343	.8410	.9018	.9485
-.364	1.0343	.8445	.9036	.9495
-.416	1.0264	.8504	.9102	.9532
-.468	1.0264	.8556	.9130	.9548
-.520	1.0264	.8644	.9177	.9574
-.572	1.0343	.8708	.9176	.9573
-.624	1.0422	.8789	.9183	.9577
-.676	1.0461	.8873	.9210	.9592
-.728	1.0501	.8975	.9245	.9611
-.780	1.0461	.9048	.9300	.9641
-.832	1.0422	.9086	.9337	.9661
-.884	1.0501	.9168	.9344	.9664
-.936	1.0580	.9266	.9359	.9673
-.988	1.0659	.9348	.9365	.9676
-1.040	1.0738	.9412	.9362	.9674

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(gg) $x/D = 8.39$; $y/D = .83$; $\alpha = 0^\circ$;
$p_\infty = 101.35$ psf (4852.63 N/m^2);
$q_\infty = 375.30$ psf (17969.29 N/m^2);
$p_{t,\infty} = 1267.30$ psf (60678.65 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1141	.9188	.9081	.9520
.988	1.0746	.9131	.9218	.9596
.936	1.0351	.9056	.9354	.9670
.884	1.0390	.8948	.9280	.9630
.832	1.0430	.8875	.9225	.9600
.780	1.0153	.8809	.9315	.9649
.728	.9876	.8708	.9390	.9689
.676	1.0074	.8588	.9233	.9605
.624	1.0272	.8486	.9089	.9525
.572	1.0272	.8399	.9043	.9499
.520	1.0272	.8329	.9005	.9477
.468	1.0272	.8277	.8977	.9461
.416	1.0272	.8207	.8939	.9440
.364	1.0272	.8154	.8910	.9423
.312	1.0272	.8102	.8881	.9407
.260	1.0232	.8035	.8862	.9395
.208	1.0193	.8003	.8861	.9395
.156	1.0232	.7948	.8813	.9367
.104	1.0272	.7910	.8775	.9345
.052	1.0272	.7857	.8746	.9328
0.000	1.0272	.7857	.8746	.9328
-.104	1.0193	.7830	.8765	.9339
-.156	1.0232	.7845	.8756	.9334
-.208	1.0272	.7859	.8747	.9328
-.260	1.0153	.7921	.8833	.9378
-.312	1.0193	.7970	.8843	.9384
-.364	1.0193	.8005	.8862	.9396
-.416	1.0114	.8064	.8929	.9434
-.468	1.0114	.8134	.8968	.9456
-.520	1.0114	.8204	.9007	.9478
-.572	1.0193	.8268	.9006	.9478
-.624	1.0272	.8332	.9006	.9478
-.676	1.0272	.8437	.9063	.9510
-.728	1.0272	.8524	.9110	.9536
-.780	1.0272	.8629	.9166	.9567
-.832	1.0272	.8717	.9212	.9593
-.884	1.0311	.8836	.9257	.9618
-.936	1.0351	.8938	.9293	.9637
-.988	1.0469	.9016	.9280	.9630
-1.040	1.0588	.9112	.9277	.9628

(hh) $x/D = 8.39$; $y/D = .63$; $\alpha = 0^\circ$;
$p_\infty = 101.39$ psf (4854.54 N/m^2);
$q_\infty = 375.44$ psf (17976.38 N/m^2);
$p_{t,\infty} = 1267.80$ psf (60702.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0899	.8923	.9048	.9502
.988	1.0504	.8779	.9142	.9554
.936	1.0110	.8687	.9270	.9624
.884	1.0149	.8562	.9185	.9578
.832	1.0188	.8471	.9118	.9541
.780	.9952	.8385	.9179	.9575
.728	.9715	.8263	.9223	.9599
.676	.9873	.8164	.9094	.9527
.624	1.0031	.8047	.8957	.9450
.572	1.0031	.7960	.8908	.9422
.520	1.0031	.7907	.8879	.9405
.468	1.0070	.7852	.8830	.9377
.416	1.0110	.7762	.8762	.9337
.364	1.0070	.7642	.8712	.9307
.312	1.0031	.7523	.8660	.9277
.260	.9991	.7387	.8598	.9240
.208	.9952	.7302	.8566	.9220
.156	.9991	.7177	.8475	.9165
.104	1.0031	.7034	.8374	.9102
.052	1.0031	.6981	.8343	.9083
0.000	1.0031	.6946	.8322	.9069
-.104	.9952	.6917	.8337	.9079
-.156	.9991	.6967	.8350	.9087
-.208	1.0031	.7086	.8405	.9122
-.260	.9952	.7180	.8494	.9176
-.312	.9991	.7300	.8548	.9209
-.364	.9991	.7405	.8609	.9246
-.416	.9952	.7565	.8719	.9312
-.468	.9952	.7688	.8789	.9353
-.520	.9952	.7775	.8839	.9382
-.572	.9991	.7842	.8860	.9394
-.624	1.0031	.7909	.8880	.9406
-.676	1.0031	.7997	.8929	.9434
-.728	1.0031	.8102	.8987	.9467
-.780	1.0031	.8189	.9036	.9495
-.832	1.0031	.8277	.9084	.9522
-.884	1.0070	.8413	.9141	.9553
-.936	1.0110	.8533	.9187	.9579
-.988	1.0188	.8632	.9204	.9589
-1.040	1.0267	.8766	.9240	.9608

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120^o-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(ii) $x/D = 8.39$; $y/D = .42$; $\alpha = 0^o$;

$p_\infty = 101.30$ psf (4850.33 N/m^2);

$q_\infty = 375.12$ psf (17960.78 N/m^2);

$p_{t,\infty} = 1266.70$ psf (60649.92 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0669	.8775	.9069	.9514
.988	1.0274	.8613	.9156	.9562
.936	.9878	.8503	.9278	.9629
.884	.9878	.8398	.9220	.9597
.832	.9878	.8258	.9143	.9555
.780	.9681	.8134	.9166	.9568
.728	.9483	.8009	.9190	.9581
.676	.9681	.7889	.9027	.9490
.624	.9878	.7752	.8859	.9394
.572	.9878	.7682	.8818	.9370
.520	.9878	.7577	.8758	.9335
.468	.9878	.7455	.8687	.9293
.416	.9878	.7280	.8585	.9231
.364	.9839	.7073	.8479	.9167
.312	.9799	.6884	.8381	.9107
.260	.9760	.6589	.8217	.9003
.208	.9720	.6417	.8125	.8944
.156	.9760	.6169	.7950	.8829
.104	.9799	.6008	.7830	.8748
.052	.9878	.5949	.7760	.8701
0.000	.9957	.5907	.7702	.8661
-.104	.9799	.5900	.7759	.8700
-.156	.9799	.5970	.7805	.8731
-.208	.9799	.6128	.7908	.8801
-.260	.9760	.6307	.8039	.8888
-.312	.9760	.6483	.8150	.8960
-.364	.9760	.6746	.8314	.9064
-.416	.9720	.6995	.8483	.9169
-.468	.9720	.7222	.8620	.9253
-.520	.9720	.7398	.8724	.9315
-.572	.9720	.7520	.8796	.9357
-.624	.9720	.7608	.8847	.9387
-.676	.9760	.7727	.8898	.9416
-.728	.9799	.7847	.8949	.9445
-.780	.9760	.7955	.9028	.9491
-.832	.9720	.8063	.9108	.9535
-.884	.9760	.8200	.9166	.9568
-.936	.9799	.8372	.9243	.9610
-.988	.9878	.8471	.9260	.9619
-1.040	.9957	.8587	.9287	.9634

(jj) $x/D = 8.39$; $y/D = .21$; $\alpha = 0^o$;

$p_\infty = 101.35$ psf (4852.63 N/m^2);

$q_\infty = 375.30$ psf (17969.29 N/m^2);

$p_{t,\infty} = 1267.30$ psf (60678.65 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0493	.8618	.9063	.9510
.988	1.0098	.8421	.9132	.9549
.936	.9704	.8347	.9274	.9627
.884	.9704	.8189	.9187	.9579
.832	.9704	.8102	.9138	.9552
.780	.9506	.8012	.9181	.9576
.728	.9309	.7922	.9225	.9600
.676	.9467	.7788	.9070	.9514
.624	.9625	.7689	.8938	.9439
.572	.9625	.7584	.8877	.9404
.520	.9625	.7444	.8794	.9356
.468	.9625	.7269	.8690	.9295
.416	.9625	.7059	.8564	.9219
.364	.9625	.6831	.8425	.9134
.312	.9625	.6639	.8305	.9059
.260	.9585	.6344	.8135	.8951
.208	.9546	.6154	.8029	.8881
.156	.9585	.5941	.7873	.8777
.104	.9625	.5850	.7796	.8725
.052	.9704	.5738	.7690	.8652
0.000	.9782	.5661	.7607	.8595
-.104	.9704	.5692	.7659	.8631
-.156	.9704	.5763	.7706	.8664
-.208	.9704	.5903	.7800	.8728
-.260	.9664	.6012	.7887	.8787
-.312	.9664	.6188	.8002	.8863
-.364	.9664	.6469	.8181	.8980
-.416	.9625	.6735	.8365	.9096
-.468	.9625	.7015	.8537	.9203
-.520	.9625	.7225	.8664	.9279
-.572	.9625	.7383	.8758	.9335
-.624	.9625	.7540	.8851	.9389
-.676	.9664	.7660	.8903	.9419
-.728	.9704	.7762	.8944	.9443
-.780	.9664	.7852	.9014	.9483
-.832	.9625	.7960	.9094	.9528
-.884	.9664	.8062	.9134	.9550
-.936	.9704	.8182	.9182	.9577
-.988	.9782	.8298	.9210	.9592
-1.040	.9861	.8415	.9237	.9607

TABLE 2.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Concluded.

(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 101.37$ psf (4853.40 N/m^2);

$q_\infty = 375.36$ psf (17972.12 N/m^2);

$p_{t,\infty} = 1267.50$ psf (60688.23 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0257	.8565	.9138	.9552
.988	.9863	.8333	.9192	.9582
.936	.9468	.8223	.9319	.9651
.884	.9508	.8115	.9239	.9608
.832	.9547	.8025	.9168	.9569
.780	.9350	.7935	.9213	.9593
.728	.9152	.7863	.9269	.9624
.676	.9310	.7746	.9121	.9543
.624	.9468	.7664	.8997	.9473
.572	.9468	.7577	.8946	.9444
.520	.9468	.7490	.8894	.9414
.468	.9468	.7385	.8831	.9378
.416	.9468	.7245	.8747	.9329
.364	.9429	.7073	.8661	.9277
.312	.9389	.6953	.8606	.9244
.260	.9389	.6709	.8453	.9151
.208	.9389	.6568	.8364	.9096
.156	.9429	.6373	.8221	.9006
.104	.9468	.6229	.8111	.8935
.052	.9547	.6083	.7982	.8850
0.000	.9626	.5971	.7876	.8779
-.104	.9468	.6034	.7983	.8851
-.156	.9508	.6136	.8034	.8884
-.208	.9547	.6362	.8163	.8968
-.260	.9468	.6491	.8280	.9043
-.312	.9508	.6646	.8361	.9094
-.364	.9508	.6821	.8470	.9162
-.416	.9468	.7052	.8630	.9259
-.468	.9468	.7192	.8716	.9310
-.520	.9468	.7333	.8800	.9360
-.572	.9468	.7455	.8874	.9402
-.624	.9468	.7543	.8926	.9432
-.676	.9468	.7613	.8967	.9456
-.728	.9468	.7718	.9029	.9491
-.780	.9468	.7806	.9080	.9520
-.832	.9468	.7893	.9130	.9548
-.884	.9508	.7978	.9160	.9564
-.936	.9547	.8097	.9209	.9591
-.988	.9626	.8214	.9237	.9607
-1.040	.9705	.8313	.9255	.9616

(ll) $x/D = 8.39$; $y/D = -.42$; $\alpha = 0^\circ$;

$p_\infty = 101.41$ psf (4855.31 N/m^2);

$q_\infty = 375.50$ psf (17979.21 N/m^2);

$p_{t,\infty} = 1268.00$ psf (60712.17 N/m^2);

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9856	.8528	.9302	.9642
.988	.9462	.8297	.9364	.9675
.936	.9067	.8204	.9512	.9754
.884	.9067	.8065	.9431	.9711
.832	.9067	.7943	.9359	.9673
.780	.8910	.7815	.9366	.9676
.728	.8752	.7670	.9362	.9674
.676	.8870	.7505	.9198	.9585
.624	.8989	.7356	.9046	.9501
.572	.9028	.7231	.8950	.9446
.520	.9067	.7158	.8885	.9409
.468	.9028	.7248	.8960	.9452
.416	.8989	.7356	.9046	.9501
.364	.8989	.7408	.9079	.9519
.312	.8989	.7408	.9079	.9519
.260	.8989	.7356	.9046	.9501
.208	.8989	.7339	.9036	.9495
.156	.8989	.7269	.8993	.9470
.104	.8989	.7164	.8928	.9433
.052	.9028	.6882	.8731	.9319
0.000	.9067	.6687	.8587	.9233
-.104	.8910	.6855	.8772	.9343
-.156	.9028	.7091	.8863	.9396
-.208	.9146	.7239	.8897	.9416
-.260	.8989	.7287	.9004	.9477
-.312	.9107	.7330	.8971	.9458
-.364	.9067	.7368	.9014	.9483
-.416	.9067	.7368	.9014	.9483
-.468	.9028	.7371	.9036	.9495
-.520	.8989	.7252	.8982	.9464
-.572	.8989	.7147	.8917	.9427
-.624	.8989	.7199	.8949	.9446
-.676	.8989	.7339	.9036	.9495
-.728	.8989	.7514	.9143	.9555
-.780	.8989	.7671	.9238	.9607
-.832	.8989	.7828	.9332	.9658
-.884	.9028	.7930	.9372	.9680
-.936	.9067	.8084	.9442	.9717
-.988	.9146	.8201	.9469	.9731
-1.040	.9225	.8352	.9515	.9755

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.0×10^6 PER FOOT (3.28×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.35$ psf (2937.31 N/m^2);
$q_\infty = 227.17$ psf (10876.86 N/m^2);
$p_{t,\infty} = 767.10$ psf (36728.95 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0169	.7443	.8555	.9214
.988	.8735	.7063	.8992	.9470
.936	.7301	.6854	.9690	.9845
.884	.6975	.6591	.9721	.9861
.832	.6649	.6385	.9799	.9901
.780	.6323	.6150	.9862	.9932
.728	.5997	.5915	.9932	.9967
.676	.5345	.5705	1.0331	1.0157
.624	.4693	.5551	1.0876	1.0398
.572	.4367	.5403	1.1122	1.0501
.520	.4041	.5225	1.1371	1.0600
.468	.4041	.4938	1.1053	1.0472
.416	.4041	.3037	.8669	.9282
.364	.4172	.1062	.5046	.6425
.312	.4302	.0244	.2382	.3319
.260	.4302	0.0000	0.0000	0.0000
.208	.4302	0.0000	0.0000	0.0000
.156	.4498	0.0000	0.0000	0.0000
.104	.4693	0.0000	0.0000	0.0000
.052	.4563	0.0000	0.0000	0.0000
0.000	.4433	0.0000	0.0000	0.0000
−.104	.4433	0.0000	0.0000	0.0000
−.156	.4433	0.0000	0.0000	0.0000
−.208	.4433	0.0000	0.0000	0.0000
−.260	.4433	0.0000	0.0000	0.0000
−.312	.4433	0.0000	0.0000	0.0000
−.364	.4433	.0480	.3289	.4470
−.416	.4433	.2673	.7765	.8704
−.468	.4433	.4730	1.0330	1.0156
−.520	.4433	.5106	1.0732	1.0337
−.572	.4498	.5303	1.0858	1.0391
−.624	.4563	.5529	1.1008	1.0454
−.676	.5084	.5722	1.0609	1.0282
−.728	.5606	.5944	1.0297	1.0141
−.780	.5997	.6146	1.0124	1.0059
−.832	.6388	.6377	.9991	.9996
−.884	.6779	.6608	.9873	.9938
−.936	.7170	.6897	.9808	.9905
−.988	.7887	.7133	.9510	.9752
−1.040	.8604	.7455	.9308	.9645

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.38$ psf (2938.84 N/m^2);
$q_\infty = 227.29$ psf (10882.53 N/m^2);
$p_{t,\infty} = 767.50$ psf (36748.10 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8609	.6895	.8949	.9446
.988	.7370	.6701	.9535	.9766
.936	.6131	.6535	1.0324	1.0154
.884	.6001	.6343	1.0282	1.0134
.832	.5870	.6180	1.0261	1.0124
.780	.5609	.6027	1.0366	1.0173
.728	.5348	.5903	1.0505	1.0236
.676	.4892	.5821	1.0909	1.0412
.624	.4435	.5740	1.1376	1.0603
.572	.4370	.5716	1.1437	1.0626
.520	.4305	.5778	1.1585	1.0684
.468	.5479	.6468	1.0865	1.0394
.416	.6653	.6582	.9947	.9974
.364	.6979	.5867	.9169	.9569
.312	.7305	.3409	.6832	.8019
.260	.7566	.1317	.4172	.5500
.208	.7827	.0345	.2099	.2943
.156	.7827	.0048	.0787	.1125
.104	.7827	0.0000	0.0000	0.0000
.052	.7696	.0031	.0636	.0911
0.000	.7566	.0066	.0932	.1332
−.104	.7696	.0040	.0725	.1037
−.156	.7631	.0005	.0265	.0380
−.208	.7566	.0075	.0995	.1421
−.260	.7305	.0893	.3497	.4720
−.312	.7240	.2369	.5720	.7072
−.364	.6131	.5120	.9139	.9552
−.416	.6914	.6421	.9637	.9819
−.468	.5805	.6157	1.0299	1.0142
−.520	.4696	.5632	1.0951	1.0430
−.572	.4435	.5622	1.1259	1.0556
−.624	.4174	.5699	1.1684	1.0721
−.676	.4566	.5757	1.1229	1.0544
−.728	.4957	.5873	1.0885	1.0402
−.780	.5218	.5998	1.0722	1.0332
−.832	.5479	.6152	1.0597	1.0277
−.884	.5609	.6345	1.0635	1.0294
−.936	.5740	.6508	1.0649	1.0300
−.988	.6196	.6706	1.0403	1.0190
−1.040	.6653	.6903	1.0186	1.0089

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.0×10^6 PER FOOT (3.28×10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0°$;

$p_\infty = 61.35$ psf (2937.69 N/m^2);
$q_\infty = 227.20$ psf (10878.27 N/m^2);
$p_{t,\infty} = 767.20$ psf (36733.73 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7819	.6678	.9242	.9609
.988	.6711	.6502	.9843	.9923
.936	.5604	.6440	1.0721	1.0331
.884	.5669	.6320	1.0559	1.0260
.832	.5734	.6258	1.0447	1.0210
.780	.6255	.6968	1.0555	1.0258
.728	.6776	.6728	.9964	.9983
.676	.6320	.6560	1.0188	1.0090
.624	.5864	.6450	1.0488	1.0228
.572	.6255	.6450	1.0154	1.0074
.520	.6646	.6709	1.0047	1.0023
.468	.8014	.7183	.9467	.9730
.416	.9383	.7396	.8878	.9405
.364	1.0100	.7572	.8659	.9276
.312	1.0816	.7603	.8384	.9108
.260	1.1012	.6545	.7709	.8666
.208	1.1207	.4721	.6490	.7744
.156	1.1403	.2785	.4942	.6320
.104	1.1598	.2048	.4203	.5534
.052	1.1598	.2117	.4272	.5611
0.000	1.1598	.2284	.4438	.5791
-.104	1.1468	.2181	.4361	.5708
-.156	1.1468	.2476	.4646	.6014
-.208	1.1468	.4065	.5954	.7284
-.260	1.0425	.6355	.7807	.8733
-.312	1.0425	.7372	.8409	.9124
-.364	.9122	.7559	.9103	.9533
-.416	.9383	.7307	.8825	.9374
-.468	.8080	.7001	.9309	.9646
-.520	.6776	.6492	.9788	.9895
-.572	.6190	.6333	1.0115	1.0055
-.624	.5604	.6434	1.0716	1.0329
-.676	.6125	.6569	1.0356	1.0169
-.728	.6646	.6762	1.0087	1.0042
-.780	.5995	.6752	1.0613	1.0284
-.832	.5343	.6222	1.0792	1.0362
-.884	.5213	.6261	1.0959	1.0433
-.936	.5082	.6415	1.1235	1.0546
-.988	.5408	.6507	1.0969	1.0437
-1.040	.5734	.6656	1.0774	1.0355

(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 0°$;

$p_\infty = 61.37$ psf (2938.46 N/m^2);
$q_\infty = 227.26$ psf (10881.11 N/m^2);
$p_{t,\infty} = 767.40$ psf (36743.31 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9389	.7451	.8908	.9422
.988	.8151	.7228	.9417	.9704
.936	.6912	.7119	1.0149	1.0072
.884	.6781	.6927	1.0107	1.0052
.832	.6651	.6764	1.0085	1.0041
.780	.6390	.6640	1.0193	1.0093
.728	.6129	.6688	1.0446	1.0209
.676	.7890	.7450	.9717	.9859
.624	.9650	.7835	.9011	.9481
.572	1.0172	.7853	.8787	.9352
.520	1.0694	.7813	.8548	.9209
.468	1.0824	.7745	.8459	.9155
.416	1.0954	.7706	.8387	.9110
.364	1.0889	.7595	.8352	.9088
.312	1.0824	.7369	.8251	.9025
.260	1.0694	.6452	.7768	.8706
.208	1.0563	.5359	.7122	.8242
.156	1.0628	.4153	.6251	.7543
.104	1.0694	.3584	.5789	.7136
.052	1.0694	.3464	.5692	.7047
0.000	1.0694	.3434	.5667	.7024
-.104	1.0563	.3701	.5919	.7253
-.156	1.0694	.3897	.6037	.7357
-.208	1.0824	.4889	.6721	.7931
-.260	1.0694	.6273	.7659	.8631
-.312	1.0824	.7077	.8086	.8918
-.364	1.0759	.7489	.8343	.9083
-.416	1.0824	.7600	.8379	.9105
-.468	1.0759	.7663	.8439	.9143
-.520	1.0694	.7668	.8468	.9160
-.572	.9976	.7723	.8799	.9359
-.624	.9259	.7604	.9063	.9510
-.676	.7694	.6826	.9419	.9705
-.728	.6129	.6538	1.0328	1.0156
-.780	.6260	.6557	1.0235	1.0112
-.832	.6390	.6721	1.0256	1.0122
-.884	.6455	.6919	1.0353	1.0167
-.936	.6520	.7116	1.0447	1.0210
-.988	.6977	.7284	1.0218	1.0104
-1.040	.7433	.7482	1.0033	1.0016

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.0×10^6 PER FOOT (3.28×10^6 PER METER) – Continued

(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.33$ psf (2936.54 N/m^2);
$q_\infty = 227.11$ psf (10874.02 N/m^2);
$p_{t,\infty} = 766.90$ psf (36719.37 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8476	.7143	.9180	.9575
.988	.7303	.6972	.9771	.9887
.936	.6129	.6973	1.0666	1.0308
.884	.7955	.8219	1.0165	1.0079
.832	.9780	.8197	.9155	.9562
.780	.9650	.8092	.9157	.9563
.728	.9519	.7987	.9160	.9564
.676	.9780	.7909	.8993	.9470
.624	1.0041	.7831	.8831	.9378
.572	1.0171	.7792	.8753	.9332
.520	1.0302	.7753	.8675	.9286
.468	1.0432	.7686	.8583	.9231
.416	1.0563	.7589	.8476	.9165
.364	1.0497	.7420	.8408	.9123
.312	1.0432	.7107	.8254	.9027
.260	1.0367	.6273	.7779	.8713
.208	1.0302	.5494	.7303	.8377
.156	1.0367	.4614	.6671	.7891
.104	1.0432	.4256	.6387	.7658
.052	1.0367	.4086	.6278	.7566
0.000	1.0302	.3974	.6211	.7508
-.104	1.0302	.4397	.6533	.7779
-.156	1.0367	.4567	.6638	.7864
-.208	1.0432	.5235	.7084	.8213
-.260	1.0367	.6114	.7680	.8645
-.312	1.0432	.6806	.8077	.8913
-.364	1.0302	.7309	.8423	.9133
-.416	1.0432	.7502	.8480	.9168
-.468	1.0302	.7599	.8588	.9234
-.520	1.0171	.7638	.8665	.9280
-.572	1.0106	.7672	.8713	.9308
-.624	1.0041	.7764	.8793	.9355
-.676	1.0041	.7821	.8826	.9375
-.728	1.0041	.7908	.8875	.9403
-.780	.9845	.7981	.9004	.9477
-.832	.9650	.8054	.9136	.9551
-.884	.7759	.7445	.9796	.9899
-.936	.5868	.6951	1.0884	1.0401
-.988	.6129	.7018	1.0701	1.0323
-1.040	.6390	.7143	1.0573	1.0267

(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.39$ psf (2939.22 N/m^2);
$q_\infty = 227.32$ psf (10883.95 N/m^2);
$p_{t,\infty} = 767.60$ psf (36752.89 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2247	.8923	.8536	.9202
.988	1.1400	.8671	.8721	.9313
.936	1.0553	.8563	.9008	.9479
.884	1.0553	.8419	.8932	.9436
.832	1.0553	.8332	.8886	.9409
.780	1.0227	.8213	.8961	.9453
.728	.9902	.8094	.9041	.9498
.676	1.0032	.7968	.8912	.9425
.624	1.0162	.7872	.8801	.9360
.572	1.0162	.7756	.8736	.9322
.520	1.0162	.7670	.8688	.9293
.468	1.0097	.7559	.8653	.9272
.416	1.0032	.7391	.8584	.9231
.364	.9967	.7079	.8428	.9135
.312	.9902	.6737	.8249	.9023
.260	.9836	.6106	.7879	.8781
.208	.9771	.5648	.7603	.8591
.156	.9836	.5149	.7235	.8327
.104	.9902	.4911	.7042	.8182
.052	.9967	.4731	.6889	.8064
0.000	1.0032	.4608	.6778	.7976
-.104	.9902	.4930	.7056	.8192
-.156	.9902	.5105	.7180	.8286
-.208	.9902	.5513	.7462	.8492
-.260	.9902	.5979	.7771	.8708
-.312	.9902	.6472	.8085	.8918
-.364	.9967	.6960	.8357	.9091
-.416	.9902	.7313	.8594	.9237
-.468	.9967	.7453	.8647	.9269
-.520	1.0032	.7563	.8683	.9290
-.572	1.0032	.7650	.8733	.9320
-.624	1.0032	.7766	.8798	.9359
-.676	1.0097	.7848	.8816	.9369
-.728	1.0162	.7930	.8834	.9379
-.780	1.0162	.8045	.8898	.9416
-.832	1.0162	.8132	.8946	.9444
-.884	1.0227	.8272	.8993	.9471
-.936	1.0292	.8411	.9040	.9497
-.988	1.0358	.8522	.9071	.9515
-1.040	1.0423	.8633	.9101	.9531

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.0×10^6 PER FOOT (3.28×10^6 PER METER) – Continued

(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.45$ psf (2942.29 N/m^2);
$q_\infty = 227.55$ psf (10895.29 N/m^2);
$p_{t,\infty} = 768.40$ psf (36791.19 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3403	.9169	.8271	.9037
.988	1.2623	.9028	.8457	.9154
.936	1.1842	.8945	.8691	.9295
.884	1.1842	.8772	.8607	.9245
.832	1.1842	.8685	.8564	.9219
.780	1.1582	.8561	.8598	.9239
.728	1.1321	.8495	.8662	.9278
.676	1.1582	.8359	.8496	.9177
.624	1.1842	.8252	.8348	.9086
.572	1.1842	.8166	.8304	.9058
.520	1.1842	.8050	.8245	.9021
.468	1.1907	.7901	.8146	.8957
.416	1.1972	.7665	.8001	.8863
.364	1.1777	.7362	.7907	.8800
.312	1.1582	.7002	.7775	.8711
.260	1.1517	.6515	.7521	.8534
.208	1.1452	.6172	.7341	.8405
.156	1.1452	.5794	.7113	.8236
.104	1.1452	.5532	.6951	.8111
.052	1.1517	.5352	.6817	.8007
0.000	1.1582	.5230	.6720	.7930
−.104	1.1452	.5583	.6983	.8136
−.156	1.1452	.5759	.7091	.8219
−.208	1.1452	.6050	.7269	.8351
−.260	1.1386	.6434	.7517	.8531
−.312	1.1386	.6782	.7718	.8672
−.364	1.1452	.7184	.7920	.8809
−.416	1.1321	.7571	.8178	.8978
−.468	1.1386	.7769	.8260	.9030
−.520	1.1452	.7937	.8325	.9072
−.572	1.1517	.8048	.8360	.9093
−.624	1.1582	.8159	.8393	.9114
−.676	1.1647	.8240	.8412	.9125
−.728	1.1712	.8351	.8444	.9146
−.780	1.1647	.8414	.8500	.9180
−.832	1.1582	.8535	.8584	.9231
−.884	1.1647	.8703	.8645	.9268
−.936	1.1712	.8814	.8675	.9286
−.988	1.1582	.8882	.8757	.9334
−1.040	1.1452	.9037	.8883	.9408

(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.40$ psf (2939.99 N/m^2);
$q_\infty = 227.38$ psf (10886.78 N/m^2);
$p_{t,\infty} = 767.80$ psf (36762.46 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2895	.8888	.8302	.9057
.988	1.2048	.8753	.8523	.9194
.936	1.1202	.8645	.8785	.9351
.884	1.1202	.8501	.8712	.9307
.832	1.1202	.8415	.8667	.9281
.780	1.0876	.8324	.8749	.9329
.728	1.0550	.8263	.8850	.9389
.676	1.0811	.8128	.8671	.9283
.624	1.1071	.8021	.8512	.9187
.572	1.1071	.7935	.8466	.9159
.520	1.1071	.7848	.8419	.9130
.468	1.1071	.7733	.8357	.9092
.416	1.1071	.7560	.8263	.9032
.364	1.1006	.7305	.8147	.8958
.312	1.0941	.7079	.8044	.8891
.260	1.0941	.6732	.7844	.8758
.208	1.0941	.6530	.7725	.8677
.156	1.0941	.6211	.7535	.8544
.104	1.0941	.5979	.7393	.8442
.052	1.1071	.5766	.7216	.8313
0.000	1.1202	.5639	.7095	.8222
−.104	1.1071	.5883	.7289	.8367
−.156	1.1006	.6092	.7440	.8476
−.208	1.0941	.6388	.7641	.8618
−.260	1.0941	.6621	.7779	.8714
−.312	1.0876	.6858	.7941	.8823
−.364	1.0876	.7148	.8107	.8932
−.416	1.0811	.7444	.8298	.9054
−.468	1.0811	.7617	.8394	.9115
−.520	1.0811	.7733	.8458	.9154
−.572	1.0876	.7844	.8493	.9175
−.624	1.0941	.7926	.8511	.9187
−.676	1.1006	.8008	.8530	.9198
−.728	1.1071	.8119	.8563	.9219
−.780	1.1006	.8210	.8637	.9263
−.832	1.0941	.8302	.8711	.9307
−.884	1.1071	.8437	.8730	.9318
−.936	1.1202	.8572	.8748	.9329
−.988	1.1267	.8711	.8793	.9355
−1.040	1.1332	.8880	.8852	.9390

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.0×10^6 PER FOOT (3.28×10^6 PER METER) – Continued

(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.50$ psf (2944.58 N/m^2);
$q_\infty = 227.73$ psf (10903.80 N/m^2);
$p_{t,\infty} = 769.00$ psf (36819.92 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1979	.8697	.8520	.9192
.988	1.1133	.8503	.8739	.9324
.936	1.0287	.8424	.9049	.9503
.884	1.0287	.8280	.8972	.9459
.832	1.0287	.8194	.8925	.9432
.780	1.0026	.8098	.8987	.9467
.728	.9766	.8032	.9069	.9514
.676	.9961	.7931	.8923	.9431
.624	1.0156	.7829	.8780	.9348
.572	1.0156	.7772	.8748	.9329
.520	1.0156	.7685	.8699	.9300
.468	1.0156	.7570	.8633	.9261
.416	1.0156	.7397	.8534	.9201
.364	1.0156	.7195	.8417	.9129
.312	1.0156	.7051	.8332	.9076
.260	1.0156	.6792	.8177	.8978
.208	1.0156	.6618	.8072	.8910
.156	1.0156	.6387	.7930	.8816
.104	1.0156	.6156	.7785	.8718
.052	1.0287	.5972	.7619	.8603
0.000	1.0417	.5817	.7473	.8499
-.104	1.0417	.5984	.7579	.8575
-.156	1.0352	.6164	.7716	.8671
-.208	1.0287	.6459	.7924	.8811
-.260	1.0287	.6662	.8047	.8893
-.312	1.0221	.6812	.8163	.8969
-.364	1.0221	.7043	.8301	.9056
-.416	1.0156	.7280	.8466	.9159
-.468	1.0156	.7453	.8567	.9221
-.520	1.0156	.7569	.8633	.9260
-.572	1.0156	.7685	.8698	.9300
-.624	1.0156	.7742	.8731	.9319
-.676	1.0221	.7824	.8749	.9330
-.728	1.0287	.7906	.8767	.9340
-.780	1.0221	.7998	.8845	.9386
-.832	1.0156	.8089	.8924	.9432
-.884	1.0287	.8224	.8941	.9441
-.936	1.0417	.8329	.8942	.9442
-.988	1.0482	.8440	.8973	.9459
-1.040	1.0547	.8550	.9004	.9477

(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.44$ psf (2941.90 N/m^2);
$q_\infty = 227.52$ psf (10893.87 N/m^2);
$p_{t,\infty} = 768.30$ psf (36786.40 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1321	.8555	.8693	.9296
.988	1.0475	.8303	.8903	.9419
.936	.9630	.8252	.9257	.9617
.884	.9630	.8108	.9176	.9573
.832	.9630	.8022	.9127	.9546
.780	.9434	.7921	.9163	.9566
.728	.9239	.7850	.9217	.9596
.676	.9434	.7748	.9063	.9510
.624	.9630	.7676	.8928	.9434
.572	.9630	.7589	.8878	.9405
.520	.9630	.7532	.8844	.9385
.468	.9630	.7416	.8776	.9345
.416	.9630	.7244	.8673	.9285
.364	.9565	.7104	.8618	.9252
.312	.9499	.6994	.8581	.9229
.260	.9499	.6763	.8438	.9142
.208	.9499	.6561	.8311	.9062
.156	.9499	.6330	.8163	.8968
.104	.9499	.6186	.8069	.8908
.052	.9630	.6002	.7895	.8792
0.000	.9760	.5905	.7778	.8713
-.104	.9630	.6025	.7910	.8802
-.156	.9630	.6141	.7985	.8852
-.208	.9630	.6344	.8116	.8938
-.260	.9630	.6517	.8227	.9009
-.312	.9630	.6691	.8336	.9078
-.364	.9565	.6870	.8475	.9165
-.416	.9630	.7097	.8585	.9231
-.468	.9565	.7246	.8704	.9303
-.520	.9499	.7396	.8824	.9373
-.572	.9565	.7478	.8842	.9384
-.624	.9630	.7588	.8877	.9404
-.676	.9630	.7675	.8928	.9433
-.728	.9630	.7733	.8961	.9453
-.780	.9630	.7791	.8995	.9472
-.832	.9630	.7877	.9045	.9500
-.884	.9630	.8022	.9127	.9546
-.936	.9630	.8109	.9176	.9573
-.988	.9760	.8243	.9190	.9581
-1.040	.9890	.8349	.9188	.9580

TABLE 3.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.0×10^6 PER FOOT (3.28×10^6 PER METER) – Concluded.

(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 61.59$ psf (2949.18 N/m^2);
$q_\infty = 228.09$ psf (10920.81 N/m^2);
$p_{t,\infty} = 770.20$ psf (36877.37 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1167	.8457	.8703	.9302
.988	1.0323	.8234	.8931	.9436
.936	.9479	.8155	.9276	.9628
.884	.9479	.8011	.9193	.9583
.832	.9479	.7954	.9160	.9564
.780	.9284	.7854	.9198	.9585
.728	.9089	.7783	.9253	.9615
.676	.9219	.7686	.9131	.9548
.624	.9349	.7619	.9028	.9490
.572	.9349	.7533	.8976	.9461
.520	.9349	.7447	.8925	.9432
.468	.9349	.7332	.8856	.9392
.416	.9349	.7217	.8786	.9351
.364	.9349	.7044	.8680	.9289
.312	.9349	.6929	.8609	.9246
.260	.9349	.6699	.8465	.9158
.208	.9349	.6526	.8355	.9090
.156	.9349	.6325	.8225	.9008
.104	.9349	.6152	.8112	.8935
.052	.9414	.5974	.7966	.8839
0.000	.9479	.5882	.7877	.8780
-.104	.9479	.5983	.7945	.8826
-.156	.9479	.6041	.7983	.8851
-.208	.9479	.6272	.8135	.8950
-.260	.9479	.6474	.8265	.9033
-.312	.9479	.6619	.8356	.9091
-.364	.9414	.6797	.8497	.9178
-.416	.9479	.6994	.8590	.9235
-.468	.9414	.7143	.8711	.9307
-.520	.9349	.7292	.8832	.9378
-.572	.9349	.7407	.8901	.9418
-.624	.9349	.7465	.8936	.9438
-.676	.9349	.7551	.8987	.9467
-.728	.9349	.7666	.9056	.9506
-.780	.9349	.7724	.9090	.9525
-.832	.9349	.7810	.9140	.9553
-.884	.9414	.7921	.9173	.9571
-.936	.9479	.8031	.9205	.9589
-.988	.9544	.8112	.9220	.9597
-1.040	.9609	.8280	.9283	.9632

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 51.80$ psf (2480.27 N/m^2);
$q_\infty = 317.71$ psf (15211.82 N/m^2);
$p_{t,\infty} = 1791.80$ psf (85791.85 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0081	.6956	.8306	.9272
.988	.9156	.6481	.8413	.9325
.936	.8232	.6130	.8630	.9430
.884	.7677	.5763	.8665	.9446
.832	.7122	.5520	.8804	.9511
.780	.6567	.5256	.8946	.9575
.728	.6012	.5053	.9168	.9672
.676	.5596	.4845	.9305	.9730
.624	.5179	.4677	.9503	.9811
.572	.4532	.4520	.9987	.9995
.520	.3885	.4322	1.0547	1.0189
.468	.3561	.4130	1.0769	1.0260
.416	.3237	.3876	1.0942	1.0313
.364	.3700	.2104	.7541	.8854
.312	.4162	.0745	.4232	.6125
.260	.4301	.0123	.1692	.2740
.208	.4440	.0032	.0853	.1406
.156	.4532	0.0000	0.0000	0.0000
.104	.4624	0.0000	0.0000	0.0000
.052	.4486	0.0000	0.0000	0.0000
0.000	.4347	.0010	.0480	.0795
-.104	.4440	.0032	.0853	.1406
-.156	.4393	.0040	.0949	.1562
-.208	.4347	.0047	.1037	.1705
-.260	.4116	.0082	.1411	.2301
-.312	.4070	.0410	.3176	.4857
-.364	.4393	.1471	.5786	.7620
-.416	.3792	.3811	1.0025	1.0009
-.468	.4116	.4126	1.0013	1.0005
-.520	.4440	.4339	.9886	.9958
-.572	.4578	.4559	.9979	.9992
-.624	.4717	.4739	1.0023	1.0008
-.676	.5364	.4896	.9553	.9831
-.728	.6012	.5094	.9205	.9688
-.780	.6567	.5297	.8981	.9591
-.832	.7122	.5561	.8837	.9526
-.884	.7677	.5846	.8726	.9475
-.936	.8232	.6213	.8688	.9457
-.988	.9295	.6516	.8373	.9305
-1.040	1.0359	.7005	.8223	.9229

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 51.76$ psf (2478.48 N/m^2);
$q_\infty = 317.48$ psf (15200.79 N/m^2);
$p_{t,\infty} = 1790.50$ psf (85729.60 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9807	.6065	.7864	.9038
.988	.8188	.5766	.8391	.9314
.936	.6569	.5548	.9190	.9682
.884	.6199	.5317	.9261	.9712
.832	.5829	.5168	.9416	.9776
.780	.5505	.5017	.9547	.9828
.728	.5181	.4887	.9712	.9892
.676	.4996	.4771	.9773	.9916
.624	.4811	.4676	.9859	.9948
.572	.4348	.4593	1.0278	1.0098
.520	.3886	.4510	1.0774	1.0261
.468	.3840	.4409	1.0716	1.0243
.416	.3793	.4452	1.0834	1.0280
.364	.5551	.5592	1.0037	1.0013
.312	.7309	.5701	.8832	.9524
.260	.8558	.4448	.7209	.8652
.208	.9807	.2135	.4666	.6586
.156	1.0131	.0640	.2513	.3956
.104	1.0455	.0181	.1317	.2153
.052	1.0270	.0503	.2213	.3524
0.000	1.0085	.0787	.2793	.4346
-.104	1.0270	.0344	.1830	.2951
-.156	1.0038	.0502	.2236	.3557
-.208	.9807	.1706	.4171	.6058
-.260	.7263	.4403	.7786	.8995
-.312	.7031	.5610	.8933	.9569
-.364	.7124	.5421	.8723	.9474
-.416	.4256	.4371	1.0134	1.0048
-.468	.4348	.4367	1.0021	1.0008
-.520	.4441	.4486	1.0051	1.0018
-.572	.4395	.4591	1.0221	1.0079
-.624	.4348	.4676	1.0370	1.0130
-.676	.4765	.4761	.9996	.9999
-.728	.5181	.4887	.9712	.9892
-.780	.5505	.4997	.9527	.9820
-.832	.5829	.5168	.9416	.9776
-.884	.6014	.5346	.9428	.9780
-.936	.6199	.5585	.9492	.9806
-.988	.6800	.5806	.9240	.9703
-1.040	.7401	.6110	.9086	.9637

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 51.78$ psf (2479.17 N/m^2);
$q_\infty = 317.56$ psf (15205.03 N/m^2);
$p_{t,\infty} = 1791.00$ psf (85753.54 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8519	.5722	.8196	.9215
.988	.7176	.5534	.8782	.9501
.936	.5834	.5366	.9591	.9845
.884	.5602	.5212	.9645	.9867
.832	.5371	.5098	.9743	.9904
.780	.5185	.5003	.9823	.9935
.728	.5000	.4929	.9929	.9974
.676	.5972	.5093	.9234	.9700
.624	.6945	.5585	.8968	.9585
.572	.6389	.5445	.9232	.9699
.520	.5834	.5263	.9499	.9809
.468	.7130	.5103	.8460	.9348
.416	.8426	.5994	.8434	.9335
.364	1.0139	.6577	.8054	.9141
.312	1.1852	.6706	.7522	.8843
.260	1.2361	.6642	.7330	.8727
.208	1.2871	.5792	.6708	.8322
.156	1.2963	.4148	.5657	.7512
.104	1.3056	.3181	.4936	.6855
.052	1.3010	.3057	.4847	.6768
0.000	1.2963	.3144	.4924	.6844
-.104	1.3056	.3311	.5036	.6952
-.156	1.3195	.4121	.5589	.7454
-.208	1.3334	.5715	.6547	.8208
-.260	1.0185	.6769	.8152	.9192
-.312	1.0324	.6762	.8093	.9162
-.364	.9861	.6494	.8115	.9173
-.416	.7315	.5369	.8568	.9400
-.468	.6852	.5080	.8611	.9421
-.520	.6389	.5266	.9078	.9634
-.572	.6482	.5468	.9185	.9679
-.624	.6574	.5649	.9270	.9715
-.676	.5834	.4795	.9067	.9628
-.728	.5093	.4869	.9778	.9917
-.780	.5232	.4945	.9722	.9896
-.832	.5371	.5063	.9709	.9891
-.884	.5371	.5186	.9827	.9936
-.936	.5371	.5351	.9982	.9993
-.988	.5787	.5519	.9765	.9913
-1.040	.6204	.5748	.9626	.9859

(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^o$;

$p_\infty = 51.78$ psf (2479.03 N/m^2);
$q_\infty = 317.55$ psf (15204.18 N/m^2);
$p_{t,\infty} = 1790.90$ psf (85748.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1025	1.0061	.9553	.9830
.988	1.0376	1.0151	.9891	.9960
.936	.9728	1.0138	1.0209	1.0074
.884	.9681	1.0181	1.0255	1.0090
.832	.9635	1.0183	1.0280	1.0099
.780	.9681	1.0181	1.0255	1.0090
.728	.9728	1.0138	1.0209	1.0074
.676	.9728	1.0138	1.0209	1.0074
.624	.9728	1.0138	1.0209	1.0074
.572	.9774	1.0136	1.0183	1.0066
.520	.9820	1.0175	1.0179	1.0064
.468	.9774	1.0177	1.0204	1.0073
.416	.9728	1.0179	1.0229	1.0082
.364	.9728	1.0179	1.0229	1.0082
.312	.9728	1.0179	1.0229	1.0082
.260	.9728	1.0179	1.0229	1.0082
.208	.9728	1.0179	1.0229	1.0082
.156	.9728	1.0179	1.0229	1.0082
.104	.9728	1.0179	1.0229	1.0082
.052	.9774	1.0136	1.0183	1.0066
0.000	.9820	1.0134	1.0158	1.0057
-.104	.9635	1.0092	1.0234	1.0083
-.156	.9728	1.0088	1.0183	1.0065
-.208	.9820	1.0084	1.0133	1.0048
-.260	.9589	1.0094	1.0260	1.0092
-.312	.9681	1.0090	1.0209	1.0074
-.364	.9635	1.0071	1.0224	1.0080
-.416	.9542	1.0055	1.0265	1.0094
-.468	.9496	1.0057	1.0291	1.0103
-.520	.9450	1.0058	1.0317	1.0112
-.572	.9542	1.0055	1.0265	1.0094
-.624	.9635	1.0051	1.0213	1.0076
-.676	.9635	1.0071	1.0224	1.0080
-.728	.9635	1.0071	1.0224	1.0080
-.780	.9589	1.0073	1.0250	1.0089
-.832	.9542	1.0075	1.0275	1.0097
-.884	.9589	1.0073	1.0250	1.0089
-.936	.9635	1.0071	1.0224	1.0080
-.988	.9728	1.0067	1.0173	1.0062
-1.040	.9820	1.0043	1.0113	1.0040

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^\circ$;

p_∞ = 51.79 psf (2479.58 N/m^2);
q_∞ = 317.62 psf (15207.58 N/m^2);
$p_{t,\infty}$ = 1791.30 psf (85767.91 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.5910	1.2526	.8873	.9543
.988	1.5077	1.2419	.9076	.9632
.936	1.4245	1.2290	.9289	.9723
.884	1.4060	1.2175	.9306	.9730
.832	1.3875	1.2121	.9347	.9747
.780	1.3736	1.2004	.9348	.9748
.728	1.3597	1.1886	.9350	.9748
.676	1.3459	1.1789	.9359	.9752
.624	1.3320	1.1713	.9377	.9760
.572	1.3366	1.1629	.9327	.9739
.520	1.3412	1.1585	.9294	.9725
.468	1.3320	1.1507	.9295	.9726
.416	1.3227	1.1429	.9295	.9726
.364	1.3089	1.1373	.9322	.9737
.312	1.2950	1.1317	.9348	.9748
.260	1.2765	1.1284	.9402	.9770
.208	1.2580	1.1251	.9457	.9792
.156	1.2672	1.1206	.9404	.9770
.104	1.2765	1.1181	.9359	.9752
.052	1.2765	1.1181	.9359	.9752
0.000	1.2765	1.1161	.9351	.9749
-.104	1.2580	1.1120	.9402	.9770
-.156	1.2580	1.1161	.9419	.9777
-.208	1.2580	1.1182	.9428	.9780
-.260	1.2256	1.1237	.9575	.9839
-.312	1.2256	1.1299	.9602	.9850
-.364	1.2302	1.1297	.9583	.9842
-.416	1.1932	1.1416	.9781	.9919
-.468	1.1979	1.1517	.9805	.9928
-.520	1.2025	1.1577	.9812	.9930
-.572	1.2626	1.1612	.9590	.9845
-.624	1.3227	1.1669	.9392	.9766
-.676	1.3551	1.1737	.9307	.9731
-.728	1.3875	1.1867	.9248	.9706
-.780	1.3644	1.2001	.9379	.9760
-.832	1.3412	1.2073	.9488	.9804
-.884	1.3921	1.2257	.9383	.9762
-.936	1.4430	1.2358	.9254	.9709
-.988	1.4754	1.2489	.9200	.9686
-1.040	1.5077	1.2598	.9141	.9661

(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^\circ$;

p_∞ = 51.78 psf (2479.44 N/m^2);
q_∞ = 317.60 psf (15206.73 N/m^2);
$p_{t,\infty}$ = 1791.20 psf (85763.12 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2121	.9933	.9053	.9622
.988	1.1196	.9767	.9340	.9745
.936	1.0270	.9643	.9690	.9884
.884	1.0085	.9466	.9688	.9883
.832	.9900	.9350	.9718	.9895
.780	.9715	.9194	.9728	.9898
.728	.9530	.9037	.9738	.9902
.676	.9345	.8921	.9771	.9915
.624	.9160	.8785	.9793	.9923
.572	.9021	.8688	.9814	.9931
.520	.8882	.8591	.9835	.9939
.468	.8744	.8494	.9856	.9947
.416	.8605	.8398	.9879	.9955
.364	.8512	.8278	.9861	.9949
.312	.8420	.8220	.9881	.9956
.260	.8374	.8160	.9872	.9953
.208	.8327	.8121	.9876	.9954
.156	.8235	.8084	.9908	.9966
.104	.8142	.8047	.9941	.9979
.052	.8188	.8024	.9899	.9963
0.000	.8235	.8022	.9870	.9952
-.104	.8142	.8015	.9922	.9971
-.156	.8281	.8050	.9860	.9948
-.208	.8420	.8086	.9799	.9926
-.260	.8327	.8131	.9881	.9956
-.312	.8466	.8187	.9834	.9939
-.364	.8605	.8242	.9787	.9921
-.416	.8512	.8329	.9892	.9960
-.468	.8651	.8446	.9881	.9956
-.520	.8790	.8544	.9859	.9948
-.572	.8929	.8641	.9837	.9940
-.624	.9067	.8779	.9840	.9941
-.676	.9299	.8892	.9779	.9918
-.728	.9530	.9047	.9743	.9904
-.780	.9623	.9188	.9771	.9915
-.832	.9715	.9328	.9799	.9925
-.884	1.0085	.9518	.9715	.9893
-.936	1.0455	.9687	.9626	.9859
-.988	1.0779	.9838	.9554	.9831
-1.040	1.1103	.9989	.9485	.9803

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^\circ$;

p_∞ = 51.80 psf (2480.27 N/m^2);
q_∞ = 317.71 psf (15211.82 N/m^2);
$p_{t,\infty}$ = 1791.80 psf (85791.85 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9054	.7655	.9195	.9683
.988	.8223	.7423	.9501	.9810
.936	.7391	.7274	.9920	.9971
.884	.7160	.7078	.9943	.9979
.832	.6929	.6903	.9981	.9993
.780	.6883	.6761	.9911	.9967
.728	.6837	.6557	.9793	.9923
.676	.6606	.6423	.9861	.9949
.624	.6375	.6310	.9949	.9981
.572	.6236	.6192	.9964	.9987
.520	.6098	.6075	.9981	.9993
.468	.6190	.5968	.9819	.9933
.416	.6283	.5881	.9675	.9878
.364	.6375	.5795	.9534	.9823
.312	.6467	.5729	.9412	.9774
.260	.6929	.5647	.9028	.9611
.208	.7391	.5565	.8677	.9452
.156	.7207	.5553	.8778	.9499
.104	.7022	.5540	.8883	.9547
.052	.7253	.5468	.8683	.9455
0.000	.7484	.5499	.8572	.9403
-.104	.7391	.5516	.8639	.9434
-.156	.7391	.5516	.8639	.9434
-.208	.7391	.5537	.8655	.9442
-.260	.7391	.5599	.8704	.9465
-.312	.7391	.5640	.8736	.9480
-.364	.6883	.5683	.9087	.9637
-.416	.7391	.5785	.8847	.9531
-.468	.6883	.5890	.9250	.9707
-.520	.6375	.6015	.9713	.9893
-.572	.6375	.6118	.9796	.9925
-.624	.6375	.6242	.9895	.9961
-.676	.6421	.6384	.9971	.9989
-.728	.6467	.6547	1.0061	1.0022
-.780	.6698	.6702	1.0003	1.0001
-.832	.6929	.6837	.9933	.9975
-.884	.7068	.7078	1.0007	1.0003
-.936	.7207	.7278	1.0050	1.0018
-.988	.7576	.7427	.9901	.9964
-1.040	.7946	.7659	.9818	.9933

(h) $x/D = 2.5$; $y/D = .83$; $\alpha = 0^\circ$;

p_∞ = 51.83 psf (2481.52 N/m^2);
q_∞ = 317.87 psf (15219.46 N/m^2);
$p_{t,\infty}$ = 1792.70 psf (85834.94 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8403	.7041	.9154	.9666
.988	.7618	.6808	.9453	.9790
.936	.6834	.6636	.9855	.9946
.884	.6603	.6440	.9876	.9955
.832	.6372	.6286	.9932	.9975
.780	.6326	.6123	.9839	.9941
.728	.6279	.5940	.9726	.9898
.676	.6095	.5845	.9793	.9923
.624	.5910	.5709	.9829	.9937
.572	.5772	.5613	.9861	.9949
.520	.5633	.5536	.9914	.9968
.468	.5541	.5458	.9925	.9973
.416	.5448	.5400	.9956	.9984
.364	.5402	.5341	.9943	.9979
.312	.5356	.5322	.9968	.9988
.260	.5541	.5273	.9755	.9909
.208	.5725	.5224	.9552	.9830
.156	.5633	.5207	.9614	.9855
.104	.5541	.5191	.9679	.9880
.052	.5495	.5131	.9663	.9874
0.000	.5448	.5174	.9745	.9905
-.104	.5448	.5186	.9756	.9909
-.156	.5818	.5149	.9408	.9772
-.208	.6187	.5174	.9145	.9662
-.260	.6279	.5191	.9092	.9640
-.312	.6649	.5216	.8857	.9535
-.364	.6279	.5232	.9128	.9655
-.416	.7111	.5278	.8616	.9423
-.468	.6741	.5356	.8914	.9561
-.520	.6372	.5455	.9253	.9708
-.572	.6418	.5556	.9304	.9730
-.624	.6464	.5657	.9355	.9751
-.676	.6279	.5789	.9602	.9850
-.728	.6095	.5941	.9873	.9953
-.780	.6233	.6080	.9876	.9954
-.832	.6372	.6239	.9895	.9961
-.884	.6464	.6441	.9982	.9993
-.936	.6557	.6643	1.0066	1.0024
-.988	.6880	.6815	.9953	.9983
-1.040	.7203	.7027	.9877	.9955

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(i) $x/D = 2.5$; $y/D = .63$; $\alpha = 0^\circ$;

$p_\infty = 51.82$ psf (2480.97 N/m^2);
$q_\infty = 317.79$ psf (15216.07 N/m^2);
$p_{t,\infty} = 1792.30$ psf (85815.79 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7856	.6429	.9046	.9620
.988	.7071	.6196	.9361	.9753
.936	.6285	.6045	.9807	.9929
.884	.6054	.5849	.9829	.9937
.832	.5823	.5715	.9907	.9966
.780	.5777	.5594	.9840	.9941
.728	.5730	.5452	.9754	.9908
.676	.5638	.5353	.9744	.9905
.624	.5546	.5274	.9752	.9908
.572	.5453	.5237	.9800	.9926
.520	.5361	.5179	.9830	.9937
.468	.5130	.5148	1.0018	1.0007
.416	.4899	.5117	1.0221	1.0079
.364	.5037	.5091	1.0053	1.0019
.312	.5176	.5105	.9932	.9975
.260	.5961	.5503	.9608	.9852
.208	.6747	.6436	.9767	.9913
.156	.8780	.6739	.8760	.9491
.104	1.0814	.6772	.7913	.9065
.052	1.0860	.6811	.7919	.9068
0.000	1.0906	.6809	.7901	.9059
−.104	1.0444	.6743	.8035	.9131
−.156	.9104	.6575	.8498	.9367
−.208	.7764	.5932	.8741	.9482
−.260	.8133	.5173	.7975	.9099
−.312	.6793	.4984	.8566	.9400
−.364	.6839	.4941	.8500	.9368
−.416	.5823	.5027	.9292	.9724
−.468	.5869	.5066	.9291	.9724
−.520	.5915	.5085	.9272	.9716
−.572	.5730	.5155	.9485	.9803
−.624	.5546	.5225	.9706	.9890
−.676	.5592	.5305	.9740	.9903
−.728	.5638	.5406	.9792	.9923
−.780	.5730	.5526	.9820	.9934
−.832	.5823	.5646	.9847	.9944
−.884	.5869	.5829	.9966	.9988
−.936	.5915	.6034	1.0100	1.0036
−.988	.6193	.6187	.9995	.9998
−1.040	.6470	.6401	.9947	.9981

(j) $x/D = 2.5$; $y/D = .42$; $\alpha = 0^\circ$;

$p_\infty = 51.85$ psf (2482.63 N/m^2);
$q_\infty = 318.01$ psf (15226.25 N/m^2);
$p_{t,\infty} = 1793.50$ psf (85873.24 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7391	.6034	.9035	.9615
.988	.6652	.5819	.9353	.9750
.936	.5913	.5666	.9789	.9922
.884	.5728	.5510	.9808	.9929
.832	.5543	.5415	.9884	.9957
.780	.5543	.5312	.9789	.9922
.728	.5543	.5230	.9713	.9893
.676	.5543	.5168	.9656	.9871
.624	.5543	.5127	.9617	.9856
.572	.7114	.5037	.8415	.9326
.520	.8684	.5276	.7795	.9000
.468	1.0255	.6916	.8212	.9224
.416	1.1825	.6804	.7585	.8880
.364	1.1871	.6761	.7546	.8857
.312	1.1918	.6717	.7508	.8834
.260	1.1871	.6678	.7500	.8830
.208	1.1825	.6660	.7504	.8833
.156	1.1918	.6593	.7438	.8793
.104	1.2010	.6527	.7372	.8753
.052	1.2010	.6466	.7337	.8732
0.000	1.2010	.6466	.7337	.8732
−.104	1.1825	.6502	.7415	.8779
−.156	1.1871	.6542	.7423	.8784
−.208	1.1918	.6601	.7443	.8796
−.260	1.1641	.6614	.7538	.8852
−.312	1.1687	.6674	.7557	.8863
−.364	.9008	.6794	.8685	.9456
−.416	1.1456	.6746	.7674	.8931
−.468	.8777	.6804	.8805	.9512
−.520	.6097	.5067	.9116	.9650
−.572	.5728	.5042	.9383	.9762
−.624	.5358	.5079	.9736	.9902
−.676	.5451	.5116	.9688	.9883
−.728	.5543	.5174	.9661	.9873
−.780	.5543	.5256	.9738	.9902
−.832	.5543	.5339	.9814	.9931
−.884	.5497	.5485	.9989	.9996
−.936	.5451	.5651	1.0182	1.0065
−.988	.5774	.5802	1.0024	1.0009
−1.040	.6097	.5973	.9898	.9962

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(k) $x/D = 2.5$; $y/D = .21$; $\alpha = 0^\circ$;
p_∞ = 51.79 psf (2479.58 N/m^2);
q_∞ = 317.62 psf (15207.58 N/m^2);
$p_{t,\infty}$ = 1791.30 psf (85767.91 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7306	.5777	.8893	.9551
.988	.6520	.5606	.9273	.9716
.936	.5734	.5475	.9772	.9915
.884	.5641	.5356	.9744	.9905
.832	.5549	.5277	.9752	.9908
.780	.5549	.5216	.9695	.9886
.728	.5549	.5154	.9638	.9864
.676	.6936	.5732	.9091	.9639
.624	.8323	.6557	.8876	.9544
.572	.9941	.6774	.8254	.9245
.520	1.1560	.6680	.7602	.8890
.468	1.1745	.6651	.7526	.8845
.416	1.1930	.6622	.7451	.8801
.364	1.1976	.6600	.7423	.8784
.312	1.2022	.6556	.7385	.8761
.260	1.1837	.6276	.7281	.8697
.208	1.1652	.5705	.6997	.8517
.156	1.1652	.4774	.6401	.8102
.104	1.1652	.3944	.5818	.7647
.052	1.1606	.3425	.5432	.7317
0.000	1.1560	.3239	.5293	.7192
-.104	1.1375	.3946	.5890	.7706
-.156	1.1606	.4684	.6353	.8066
-.208	1.1837	.5607	.6883	.8440
-.260	1.1513	.6264	.7376	.8756
-.312	1.1745	.6502	.7440	.8794
-.364	1.1467	.6556	.7561	.8866
-.416	1.1652	.6547	.7496	.8828
-.468	1.1375	.6560	.7594	.8885
-.520	1.1097	.6635	.7732	.8964
-.572	.9340	.6651	.8439	.9338
-.624	.7583	.5882	.8807	.9513
-.676	.6566	.5080	.8796	.9508
-.728	.5549	.5083	.9571	.9838
-.780	.5549	.5124	.9610	.9853
-.832	.5549	.5207	.9687	.9883
-.884	.5410	.5316	.9913	.9968
-.936	.5271	.5446	1.0164	1.0059
-.988	.5549	.5578	1.0027	1.0010
-1.040	.5826	.5752	.9936	.9977

(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^\circ$;
p_∞ = 51.78 psf (2479.31 N/m^2);
q_∞ = 317.58 psf (15205.88 N/m^2);
$p_{t,\infty}$ = 1791.10 psf (85758.33 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7310	.5738	.8860	.9537
.988	.6523	.5566	.9237	.9701
.936	.5737	.5477	.9771	.9915
.884	.6570	.6161	.9684	.9882
.832	.7402	.5960	.8973	.9587
.780	.7125	.5725	.8964	.9583
.728	.6847	.5531	.8988	.9594
.676	.6570	.5379	.9048	.9620
.624	.6292	.5391	.9256	.9709
.572	.9160	.6666	.8531	.9383
.520	1.2029	.6847	.7545	.8856
.468	1.2075	.6845	.7529	.8847
.416	1.2121	.6760	.7468	.8811
.364	1.2075	.6680	.7438	.8793
.312	1.2029	.6579	.7395	.8767
.260	1.1890	.6110	.7168	.8627
.208	1.1751	.5413	.6787	.8376
.156	1.1751	.4460	.6160	.7921
.104	1.1751	.3899	.5760	.7599
.052	1.1890	.3704	.5581	.7447
0.000	1.2029	.3676	.5528	.7401
-.104	1.1844	.4113	.5893	.7708
-.156	1.1936	.4566	.6185	.7939
-.208	1.2029	.5413	.6708	.8322
-.260	1.1936	.6185	.7198	.8645
-.312	1.2029	.6512	.7358	.8744
-.364	1.1613	.6655	.7570	.8871
-.416	1.2029	.6698	.7462	.8807
-.468	1.1613	.6779	.7640	.8912
-.520	1.1196	.6736	.7756	.8978
-.572	.8559	.5613	.8098	.9164
-.624	.5922	.5275	.9438	.9784
-.676	.6431	.5397	.9161	.9669
-.728	.6940	.5582	.8968	.9585
-.780	.7171	.5716	.8928	.9567
-.832	.7402	.5912	.8937	.9571
-.884	.6385	.5668	.9422	.9778
-.936	.5367	.5423	1.0052	1.0019
-.988	.5598	.5537	.9945	.9980
-1.040	.5829	.5692	.9881	.9956

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(m) $x/D = 2.5$; $y/D = -.42$; $\alpha = 0^\circ$;
$p_\infty = 51.78$ psf (2479.31 N/m^2);
$q_\infty = 317.58$ psf (15205.88 N/m^2);
$p_{t,\infty} = 1791.10$ psf (85758.33 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8800	.6538	.8619	.9425
.988	.7735	.6193	.8948	.9576
.936	.6670	.5931	.9430	.9781
.884	.6345	.5615	.9407	.9772
.832	.6021	.5423	.9490	.9806
.780	.5697	.5252	.9601	.9850
.728	.5373	.5122	.9764	.9912
.676	.5187	.4986	.9804	.9927
.624	.5002	.4850	.9846	.9943
.572	.4354	.4672	1.0359	1.0126
.520	.3705	.4432	1.0936	1.0312
.468	.5187	.4141	.8935	.9570
.416	.6670	.5539	.9113	.9649
.364	.9124	.6544	.8469	.9352
.312	1.1579	.6702	.7608	.8893
.260	1.1718	.6675	.7548	.8858
.208	1.1857	.6669	.7500	.8830
.156	1.1903	.6584	.7437	.8793
.104	1.1950	.6520	.7387	.8762
.052	1.1950	.6272	.7245	.8675
0.000	1.1950	.5776	.6953	.8487
-.104	1.1857	.6478	.7392	.8765
-.156	1.1996	.6534	.7380	.8758
-.208	1.2135	.6590	.7369	.8751
-.260	.8337	.6759	.9004	.9601
-.312	.8476	.6753	.8926	.9567
-.364	.8152	.6540	.8957	.9580
-.416	.4817	.3960	.9068	.9629
-.468	.4493	.4160	.9623	.9858
-.520	.4168	.4443	1.0324	1.0114
-.572	.4354	.4682	1.0371	1.0130
-.624	.4539	.4901	1.0392	1.0137
-.676	.5002	.5005	1.0003	1.0001
-.728	.5465	.5150	.9708	.9891
-.780	.5697	.5264	.9613	.9854
-.832	.5929	.5461	.9597	.9848
-.884	.6160	.5719	.9635	.9863
-.936	.6392	.6018	.9704	.9889
-.988	.6994	.6261	.9461	.9794
-1.040	.7596	.6606	.9326	.9738

(n) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^\circ$;
$p_\infty = 51.80$ psf (2480.41 N/m^2);
$q_\infty = 317.72$ psf (15212.67 N/m^2);
$p_{t,\infty} = 1791.90$ psf (85796.63 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8782	.6495	.8600	.9416
.988	.7858	.6247	.8916	.9562
.936	.6933	.6040	.9334	.9742
.884	.6656	.5847	.9372	.9758
.832	.6379	.5673	.9431	.9781
.780	.8644	.7181	.9115	.9649
.728	1.0909	.6977	.7998	.9111
.676	1.0909	.6833	.7915	.9066
.624	1.0909	.6730	.7855	.9033
.572	1.0862	.6650	.7824	.9016
.520	1.0816	.6569	.7793	.8999
.468	1.0724	.6470	.7768	.8984
.416	1.0631	.6392	.7754	.8977
.364	1.0585	.6291	.7709	.8951
.312	1.0539	.6148	.7638	.8911
.260	1.0446	.5719	.7399	.8769
.208	1.0354	.5227	.7105	.8587
.156	1.0400	.4626	.6669	.8294
.104	1.0446	.4230	.6363	.8074
.052	1.0539	.4018	.6175	.7931
0.000	1.0631	.3951	.6097	.7871
-.104	1.0446	.4427	.6510	.8181
-.156	1.0539	.4714	.6688	.8307
-.208	1.0631	.5248	.7026	.8535
-.260	1.0539	.5791	.7413	.8778
-.312	1.0631	.6097	.7573	.8873
-.364	1.0678	.6281	.7670	.8929
-.416	1.0631	.6366	.7738	.8968
-.468	1.0678	.6446	.7770	.8986
-.520	1.0724	.6548	.7814	.9010
-.572	1.0816	.6647	.7839	.9024
-.624	1.0909	.6746	.7864	.9038
-.676	1.0724	.6858	.7997	.9110
-.728	1.0539	.7052	.8180	.9207
-.780	.8597	.5485	.7988	.9105
-.832	.6656	.5654	.9216	.9693
-.884	.6656	.5840	.9367	.9755
-.936	.6656	.6067	.9547	.9828
-.988	.6980	.6259	.9470	.9797
-1.040	.7303	.6513	.9444	.9787

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(o) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 51.79$ psf (2479.86 N/m^2);
$q_\infty = 317.65$ psf (15209.28 N/m^2);
$p_{t,\infty} = 1791.50$ psf (85777.48 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M^1/M^∞	V_1/V_∞
1.040	1.0916	.7597	.8343	.9290
.988	1.0407	.7435	.8452	.9344
.936	.9899	.7292	.8583	.9408
.884	.9945	.7063	.8428	.9332
.832	.9991	.6917	.8321	.9279
.780	.9945	.6754	.8241	.9239
.728	.9899	.6632	.8186	.9210
.676	.9852	.6511	.8129	.9181
.624	.9806	.6430	.8098	.9164
.572	.9806	.6368	.8059	.9143
.520	.9806	.6286	.8006	.9116
.468	.9714	.6228	.8007	.9116
.416	.9621	.6129	.7982	.9102
.364	.9575	.5987	.7907	.9062
.312	.9528	.5803	.7804	.9005
.260	.9436	.5415	.7576	.8874
.208	.9343	.5068	.7365	.8749
.156	.9343	.4676	.7074	.8566
.104	.9343	.4428	.6884	.8441
.052	.9390	.4239	.6719	.8329
0.000	.9436	.4196	.6668	.8294
-.104	.9343	.4563	.6988	.8510
-.156	.9436	.4786	.7122	.8597
-.208	.9528	.5114	.7326	.8725
-.260	.9482	.5488	.7608	.8893
-.312	.9575	.5753	.7751	.8975
-.364	.9575	.5960	.7890	.9052
-.416	.9621	.6082	.7951	.9086
-.468	.9621	.6164	.8005	.9115
-.520	.9621	.6268	.8071	.9150
-.572	.9714	.6346	.8083	.9156
-.624	.9806	.6404	.8081	.9155
-.676	.9852	.6506	.8126	.9179
-.728	.9899	.6627	.8183	.9208
-.780	.9899	.6751	.8259	.9248
-.832	.9899	.6896	.8347	.9292
-.884	.9899	.7041	.8434	.9335
-.936	.9899	.7227	.8544	.9389
-.988	.9945	.7390	.8620	.9426
-1.040	.9991	.7594	.8719	.9472

(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^\circ$;

$p_\infty = 51.80$ psf (2480.00 N/m^2);
$q_\infty = 317.67$ psf (15210.12 N/m^2);
$p_{t,\infty} = 1791.60$ psf (85782.27 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3308	1.1243	.9191	.9682
.988	1.2615	1.1232	.9436	.9784
.936	1.1922	1.1201	.9693	.9885
.884	1.1876	1.1141	.9686	.9882
.832	1.1830	1.1122	.9696	.9886
.780	1.1691	1.1108	.9747	.9906
.728	1.1552	1.1073	.9790	.9922
.676	1.1599	1.1029	.9752	.9908
.624	1.1645	1.1007	.9722	.9896
.572	1.1737	1.0982	.9673	.9877
.520	1.1830	1.0958	.9624	.9858
.468	1.1737	1.0962	.9664	.9874
.416	1.1645	1.0924	.9686	.9882
.364	1.1599	1.0926	.9706	.9890
.312	1.1552	1.0928	.9726	.9898
.260	1.1506	1.0910	.9737	.9902
.208	1.1460	1.0912	.9758	.9910
.156	1.1506	1.0910	.9737	.9902
.104	1.1552	1.0908	.9717	.9894
.052	1.1552	1.0908	.9717	.9894
0.000	1.1552	1.0908	.9717	.9894
-.104	1.1460	1.0855	.9732	.9900
-.156	1.1368	1.0879	.9783	.9919
-.208	1.1275	1.0904	.9834	.9939
-.260	1.1229	1.0906	.9855	.9947
-.312	1.1136	1.0951	.9916	.9969
-.364	1.1183	1.0949	.9895	.9961
-.416	1.0998	1.0957	.9982	.9993
-.468	1.1044	1.0996	.9978	.9992
-.520	1.1090	1.1036	.9975	.9991
-.572	1.1368	1.1024	.9848	.9944
-.624	1.1645	1.1053	.9743	.9904
-.676	1.1783	1.1088	.9701	.9888
-.728	1.1922	1.1103	.9650	.9869
-.780	1.1830	1.1169	.9717	.9894
-.832	1.1737	1.1173	.9757	.9909
-.884	1.1968	1.1225	.9684	.9882
-.936	1.2199	1.1256	.9606	.9851
-.988	1.2384	1.1289	.9548	.9828
-1.040	1.2569	1.1322	.9491	.9806

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^\circ$;

$p_\infty = 51.78$ psf (2479.31 N/m^2);
$q_\infty = 317.58$ psf (15205.88 N/m^2);
$p_{t,\infty} = 1791.10$ psf (85758.33 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9244	.8786	.9749	.9907
.988	.8597	.8773	1.0102	1.0037
.936	.7950	.8719	1.0472	1.0164
.884	.7812	.8683	1.0543	1.0188
.832	.7673	.8648	1.0617	1.0211
.780	.7719	.8626	1.0571	1.0197
.728	.7765	.8562	1.0500	1.0173
.676	.7673	.8525	1.0540	1.0187
.624	.7580	.8508	1.0594	1.0204
.572	.7534	.8469	1.0602	1.0207
.520	.7488	.8450	1.0623	1.0214
.468	.7349	.8436	1.0714	1.0242
.416	.7211	.8421	1.0807	1.0272
.364	.7211	.8380	1.0780	1.0264
.312	.7211	.8339	1.0754	1.0255
.260	.7257	.8337	1.0718	1.0244
.208	.7303	.8335	1.0683	1.0233
.156	.7257	.8337	1.0718	1.0244
.104	.7211	.8318	1.0740	1.0251
.052	.7257	.8275	1.0678	1.0231
0.000	.7303	.8293	1.0656	1.0224
−.104	.7303	.8282	1.0649	1.0222
−.156	.7442	.8297	1.0559	1.0193
−.208	.7580	.8291	1.0458	1.0159
−.260	.7442	.8318	1.0572	1.0197
−.312	.7580	.8332	1.0484	1.0168
−.364	.7580	.8353	1.0497	1.0172
−.416	.7580	.8394	1.0523	1.0181
−.468	.7580	.8435	1.0549	1.0189
−.520	.7580	.8456	1.0562	1.0194
−.572	.7627	.8475	1.0541	1.0187
−.624	.7673	.8534	1.0547	1.0189
−.676	.7627	.8578	1.0605	1.0208
−.728	.7580	.8600	1.0651	1.0223
−.780	.7673	.8638	1.0610	1.0209
−.832	.7765	.8654	1.0557	1.0192
−.884	.7904	.8731	1.0510	1.0177
−.936	.8043	.8787	1.0452	1.0157
−.988	.8181	.8822	1.0384	1.0135
−1.040	.8320	.8878	1.0330	1.0116

(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0^\circ$;

$p_\infty = 51.76$ psf (2478.34 N/m^2);
$q_\infty = 317.46$ psf (15199.94 N/m^2);
$p_{t,\infty} = 1790.40$ psf (85724.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8135	.7869	.9835	.9939
.988	.7534	.7854	1.0210	1.0075
.936	.6933	.7839	1.0633	1.0217
.884	.6795	.7783	1.0703	1.0239
.832	.6656	.7748	1.0789	1.0266
.780	.6702	.7725	1.0736	1.0250
.728	.6748	.7661	1.0655	1.0224
.676	.6702	.7643	1.0679	1.0231
.624	.6656	.7624	1.0703	1.0239
.572	.7211	.7559	1.0239	1.0085
.520	.7765	.7638	.9918	.9970
.468	.8874	.9012	1.0077	1.0028
.416	.9984	.9541	.9776	.9917
.364	1.0215	.9490	.9638	.9864
.312	1.0446	.9459	.9516	.9816
.260	1.0446	.9438	.9505	.9812
.208	1.0446	.9438	.9505	.9812
.156	1.0492	.9416	.9473	.9799
.104	1.0538	.9393	.9441	.9786
.052	1.0538	.9393	.9441	.9786
0.000	1.0538	.9373	.9431	.9781
−.104	1.0354	.9341	.9498	.9809
−.156	1.0400	.9359	.9487	.9804
−.208	1.0446	.9378	.9475	.9799
−.260	.9938	.9441	.9747	.9906
−.312	.9984	.9481	.9745	.9905
−.364	.8690	.9557	1.0487	1.0169
−.416	.9522	.9562	1.0021	1.0008
−.468	.8227	.8379	1.0092	1.0033
−.520	.6933	.7568	1.0448	1.0156
−.572	.6841	.7551	1.0507	1.0175
−.624	.6748	.7576	1.0595	1.0205
−.676	.6610	.7603	1.0725	1.0246
−.728	.6471	.7650	1.0873	1.0292
−.780	.6563	.7687	1.0822	1.0277
−.832	.6656	.7724	1.0773	1.0261
−.884	.6702	.7784	1.0777	1.0263
−.936	.6748	.7865	1.0796	1.0268
−.988	.6841	.7882	1.0734	1.0249
−1.040	.6933	.7960	1.0715	1.0243

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^\circ$;

$p_\infty = 51.77$ psf (2478.75 N/m^2);
$q_\infty = 317.51$ psf (15202.48 N/m^2);
$p_{t,\infty} = 1790.70$ psf (85739.18 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1481	.9082	.8894	.9552
.988	1.0787	.8989	.9129	.9655
.936	1.0092	.8875	.9378	.9760
.884	1.0000	.8735	.9346	.9747
.832	.9907	.8615	.9325	.9738
.780	.9861	.8473	.9270	.9715
.728	.9814	.8331	.9213	.9691
.676	.9814	.8187	.9133	.9657
.624	.9814	.8063	.9064	.9627
.572	.9814	.7960	.9006	.9602
.520	.9814	.7857	.8947	.9576
.468	.9722	.7737	.8921	.9564
.416	.9629	.7659	.8918	.9563
.364	.9629	.7556	.8858	.9536
.312	.9629	.7473	.8810	.9514
.260	.9629	.7411	.8773	.9497
.208	.9629	.7370	.8749	.9486
.156	.9629	.7329	.8724	.9474
.104	.9629	.7288	.8699	.9463
.052	.9676	.7286	.8677	.9453
0.000	.9722	.7263	.8643	.9436
-.104	.9629	.7243	.8673	.9450
-.156	.9676	.7282	.8675	.9452
-.208	.9722	.7321	.8678	.9453
-.260	.9629	.7367	.8747	.9485
-.312	.9676	.7427	.8761	.9491
-.364	.9676	.7489	.8798	.9508
-.416	.9629	.7594	.8881	.9546
-.468	.9629	.7718	.8953	.9578
-.520	.9629	.7842	.9024	.9610
-.572	.9722	.7941	.9038	.9616
-.624	.9814	.8061	.9063	.9627
-.676	.9861	.8204	.9121	.9652
-.728	.9907	.8326	.9167	.9672
-.780	.9907	.8470	.9246	.9705
-.832	.9907	.8573	.9303	.9729
-.884	1.0046	.8753	.9335	.9742
-.936	1.0185	.8933	.9365	.9755
-.988	1.0370	.9028	.9331	.9741
-1.040	1.0555	.9144	.9308	.9731

(t) $x/D = 5.0$; $y/D = .83$; $\alpha = 0^\circ$;

$p_\infty = 51.78$ psf (2479.03 N/m^2);
$q_\infty = 317.55$ psf (15204.18 N/m^2);
$p_{t,\infty} = 1790.90$ psf (85748.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1210	.8691	.8805	.9512
.988	1.0515	.8536	.9010	.9604
.936	.9820	.8382	.9239	.9702
.884	.9728	.8200	.9182	.9678
.832	.9635	.8081	.9158	.9668
.780	.9635	.7916	.9064	.9627
.728	.9635	.7710	.8946	.9575
.676	.9635	.7566	.8862	.9537
.624	.9635	.7422	.8777	.9499
.572	.9635	.7298	.8703	.9465
.520	.9635	.7175	.8629	.9430
.468	.9589	.7074	.8589	.9411
.416	.9542	.6973	.8548	.9391
.364	.9542	.6891	.8498	.9367
.312	.9542	.6808	.8447	.9342
.260	.9496	.6748	.8430	.9333
.208	.9450	.6709	.8426	.9332
.156	.9496	.6666	.8378	.9308
.104	.9542	.6643	.8344	.9291
.052	.9589	.6641	.8322	.9280
0.000	.9635	.6619	.8288	.9263
-.104	.9450	.6609	.8363	.9300
-.156	.9542	.6626	.8333	.9285
-.208	.9635	.6663	.8316	.9277
-.260	.9496	.6710	.8406	.9322
-.312	.9589	.6768	.8402	.9319
-.364	.9542	.6812	.8449	.9343
-.416	.9542	.6915	.8513	.9374
-.468	.9496	.7000	.8586	.9409
-.520	.9450	.7126	.8684	.9456
-.572	.9542	.7246	.8714	.9470
-.624	.9635	.7386	.8756	.9489
-.676	.9635	.7552	.8853	.9534
-.728	.9635	.7717	.8949	.9577
-.780	.9635	.7861	.9033	.9614
-.832	.9635	.8006	.9116	.9650
-.884	.9774	.8207	.9163	.9670
-.936	.9913	.8386	.9198	.9685
-.988	1.0098	.8543	.9198	.9685
-1.040	1.0283	.8721	.9209	.9690

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(u) x/D = 5.0; y/D = .63; $\alpha = 0^\circ$;
p_∞ = 51.81 psf (2480.83 N/m^2);
q_∞ = 317.78 psf (15215.22 N/m^2);
$p_{t,\infty}$ = 1792.20 psf (85811.00 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0912	.8091	.8611	.9421
.988	1.0265	.7934	.8792	.9506
.936	.9617	.7797	.9004	.9601
.884	.9617	.7571	.8872	.9542
.832	.9617	.7427	.8788	.9504
.780	.9571	.7223	.8687	.9457
.728	.9525	.7039	.8597	.9414
.676	.9525	.6895	.8508	.9372
.624	.9525	.6751	.8419	.9328
.572	.9571	.6645	.8333	.9285
.520	.9617	.6540	.8247	.9241
.468	.9525	.6483	.8250	.9243
.416	.9432	.6404	.8240	.9238
.364	.9432	.6322	.8187	.9211
.312	.9432	.6281	.8160	.9197
.260	.9432	.6219	.8120	.9176
.208	.9432	.6177	.8093	.9161
.156	.9432	.6136	.8066	.9147
.104	.9432	.6095	.8039	.9133
.052	.9479	.6072	.8004	.9114
0.000	.9525	.6070	.7983	.9103
-.104	.9432	.6075	.8026	.9126
-.156	.9525	.6092	.7997	.9111
-.208	.9617	.6150	.7997	.9110
-.260	.9479	.6197	.8086	.9158
-.312	.9571	.6235	.8071	.9150
-.364	.9525	.6278	.8119	.9175
-.416	.9525	.6361	.8172	.9203
-.468	.9479	.6425	.8233	.9234
-.520	.9432	.6510	.8308	.9272
-.572	.9479	.6611	.8352	.9294
-.624	.9525	.6733	.8408	.9322
-.676	.9571	.6855	.8463	.9350
-.728	.9617	.7019	.8543	.9388
-.780	.9571	.7186	.8665	.9447
-.832	.9525	.7374	.8799	.9509
-.884	.9617	.7577	.8876	.9544
-.936	.9710	.7779	.8951	.9578
-.988	.9802	.7941	.9001	.9600
-1.040	.9895	.8123	.9060	.9626

(v) x/D = 5.0; y/D = .42; $\alpha = 0^\circ$;
p_∞ = 51.80 psf (2480.27 N/m^2);
q_∞ = 317.71 psf (15211.82 N/m^2);
$p_{t,\infty}$ = 1791.80 psf (85791.85 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0829	.7766	.8469	.9352
.988	1.0227	.7566	.8601	.9416
.936	.9626	.7366	.8748	.9485
.884	.9579	.7121	.8622	.9426
.832	.9533	.6979	.8556	.9395
.780	.9533	.6793	.8441	.9339
.728	.9533	.6628	.8338	.9288
.676	.9487	.6486	.8268	.9252
.624	.9441	.6364	.8211	.9223
.572	.9487	.6280	.8136	.9184
.520	.9533	.6216	.8075	.9152
.468	.9441	.6137	.8063	.9146
.416	.9348	.6080	.8065	.9147
.364	.9348	.5976	.7996	.9110
.312	.9348	.5894	.7940	.9080
.260	.9302	.5690	.7821	.9014
.208	.9255	.5485	.7699	.8945
.156	.9255	.5279	.7552	.8861
.104	.9255	.5114	.7433	.8790
.052	.9255	.5011	.7358	.8744
0.000	.9255	.4990	.7343	.8735
-.104	.9255	.5105	.7427	.8786
-.156	.9348	.5246	.7491	.8825
-.208	.9441	.5449	.7597	.8887
-.260	.9302	.5683	.7816	.9012
-.312	.9394	.5823	.7873	.9043
-.364	.9394	.5927	.7943	.9081
-.416	.9348	.6011	.8019	.9122
-.468	.9348	.6094	.8074	.9152
-.520	.9348	.6177	.8129	.9180
-.572	.9394	.6257	.8161	.9197
-.624	.9441	.6359	.8207	.9221
-.676	.9487	.6460	.8252	.9244
-.728	.9533	.6603	.8322	.9280
-.780	.9533	.6747	.8413	.9325
-.832	.9533	.6912	.8515	.9375
-.884	.9579	.7117	.8619	.9425
-.936	.9626	.7342	.8734	.9479
-.988	.9718	.7524	.8799	.9509
-1.040	.9811	.7768	.8898	.9554

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(w) $x/D = 5.0$; $y/D = .21$; $\alpha = 0^\circ$;
p_∞ = 51.86 psf (2482.90 N/m^2);
q_∞ = 318.04 psf (15227.95 N/m^2);
$p_{t,\infty}$ = 1793.70 psf (85882.82 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0895	.7582	.8342	.9290
.988	1.0249	.7364	.8476	.9356
.936	.9603	.7186	.8651	.9440
.884	.9556	.6962	.8535	.9385
.832	.9510	.6820	.8468	.9352
.780	.9464	.6678	.8400	.9319
.728	.9418	.6536	.8331	.9284
.676	.9418	.6413	.8252	.9244
.624	.9418	.6289	.8172	.9203
.572	.9418	.6207	.8118	.9175
.520	.9418	.6063	.8024	.9125
.468	.9372	.5962	.7976	.9099
.416	.9326	.5882	.7942	.9081
.364	.9279	.5760	.7879	.9046
.312	.9233	.5557	.7758	.8979
.260	.9187	.5208	.7529	.8847
.208	.9141	.4860	.7292	.8704
.156	.9187	.4507	.7005	.8521
.104	.9233	.4258	.6791	.8378
.052	.9233	.4154	.6708	.8321
0.000	.9233	.4134	.6691	.8310
-.104	.9141	.4319	.6874	.8435
-.156	.9233	.4501	.6982	.8506
-.208	.9326	.4849	.7211	.8653
-.260	.9233	.5225	.7523	.8843
-.312	.9326	.5510	.7687	.8939
-.364	.9326	.5717	.7830	.9019
-.416	.9326	.5841	.7914	.9066
-.468	.9326	.5944	.7984	.9103
-.520	.9326	.6089	.8080	.9155
-.572	.9326	.6233	.8176	.9205
-.624	.9326	.6316	.8230	.9233
-.676	.9372	.6417	.8275	.9256
-.728	.9418	.6518	.8319	.9278
-.780	.9418	.6642	.8398	.9318
-.832	.9418	.6807	.8502	.9369
-.884	.9510	.6968	.8560	.9397
-.936	.9603	.7171	.8641	.9436
-.988	.9695	.7373	.8721	.9473
-1.040	.9787	.7596	.8810	.9514

(x) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^\circ$;
p_∞ = 51.79 psf (2479.86 N/m^2);
q_∞ = 317.65 psf (15209.28 N/m^2);
$p_{t,\infty}$ = 1791.50 psf (85777.48 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0824	.7492	.8320	.9278
.988	1.0176	.7294	.8466	.9351
.936	.9528	.7096	.8630	.9430
.884	.9528	.6890	.8504	.9369
.832	.9528	.6746	.8414	.9326
.780	.9482	.6604	.8345	.9291
.728	.9436	.6482	.8288	.9263
.676	.9436	.6379	.8222	.9229
.624	.9436	.6297	.8169	.9201
.572	.9436	.6235	.8129	.9180
.520	.9436	.6173	.8088	.9159
.468	.9343	.6115	.8090	.9160
.416	.9251	.6017	.8065	.9147
.364	.9251	.5872	.7967	.9095
.312	.9251	.5687	.7840	.9025
.260	.9205	.5359	.7630	.8906
.208	.9158	.5072	.7442	.8795
.156	.9158	.4783	.7227	.8664
.104	.9158	.4535	.7037	.8543
.052	.9205	.4368	.6889	.8445
0.000	.9251	.4325	.6837	.8410
-.104	.9158	.4656	.7130	.8602
-.156	.9251	.4859	.7247	.8676
-.208	.9343	.5124	.7405	.8773
-.260	.9251	.5438	.7667	.8927
-.312	.9343	.5662	.7784	.8994
-.364	.9343	.5848	.7911	.9064
-.416	.9343	.5993	.8009	.9117
-.468	.9343	.6055	.8050	.9139
-.520	.9343	.6117	.8091	.9161
-.572	.9343	.6179	.8132	.9182
-.624	.9343	.6261	.8186	.9210
-.676	.9390	.6342	.8218	.9227
-.728	.9436	.6443	.8263	.9250
-.780	.9390	.6549	.8351	.9294
-.832	.9343	.6716	.8478	.9357
-.884	.9436	.6857	.8524	.9380
-.936	.9528	.7059	.8607	.9419
-.988	.9667	.7260	.8666	.9447
-1.040	.9806	.7502	.8746	.9485

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(y) $x/D = 5.0$; $y/D = -.42$; $\alpha = 0^\circ$;

$p_\infty = 51.79$ psf (2479.72 N/m^2);
$q_\infty = 317.63$ psf (15208.43 N/m^2);
$p_{t,\infty} = 1791.40$ psf (85772.69 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0912	.7859	.8487	.9361
.988	1.0218	.7643	.8648	.9439
.936	.9525	.7385	.8805	.9512
.884	.9432	.7121	.8689	.9458
.832	.9340	.6919	.8607	.9419
.780	.9293	.6695	.8488	.9362
.728	.9247	.6491	.8378	.9308
.676	.9155	.6289	.8288	.9263
.624	.9062	.6128	.8223	.9229
.572	.9016	.6027	.8176	.9205
.520	.8970	.5906	.8114	.9173
.468	.8924	.5764	.8037	.9132
.416	.8877	.5580	.7928	.9073
.364	.8924	.5743	.8022	.9124
.312	.8970	.5823	.8057	.9143
.260	.8970	.5782	.8029	.9128
.208	.8970	.5823	.8057	.9143
.156	.9016	.5780	.8007	.9116
.104	.9062	.5716	.7942	.9081
.052	.9108	.5549	.7805	.9006
0.000	.9155	.5341	.7638	.8911
-.104	.8970	.5679	.7957	.9089
-.156	.9062	.5737	.7956	.9089
-.208	.9155	.5774	.7942	.9081
-.260	.8970	.5761	.8014	.9120
-.312	.9062	.5778	.7985	.9104
-.364	.9062	.5778	.7985	.9104
-.416	.8970	.5555	.7869	.9041
-.468	.8970	.5741	.8000	.9112
-.520	.8970	.5906	.8115	.9173
-.572	.9016	.6028	.8177	.9205
-.624	.9062	.6192	.8266	.9251
-.676	.9155	.6373	.8344	.9291
-.728	.9247	.6555	.8420	.9328
-.780	.9293	.6781	.8542	.9388
-.832	.9340	.6965	.8635	.9433
-.884	.9432	.7209	.8742	.9483
-.936	.9525	.7432	.8833	.9525
-.988	.9663	.7653	.8899	.9554
-1.040	.9802	.7874	.8963	.9583

(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 51.78$ psf (2479.44 N/m^2);
$q_\infty = 317.60$ psf (15206.73 N/m^2);
$p_{t,\infty} = 1791.20$ psf (85763.12 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0453	.7366	.8394	.9316
.988	.9852	.7146	.8516	.9376
.936	.9251	.6946	.8665	.9447
.884	.9158	.6744	.8581	.9407
.832	.9066	.6624	.8548	.9391
.780	.9066	.6500	.8468	.9352
.728	.9066	.6377	.8387	.9312
.676	.9066	.6274	.8319	.9278
.624	.9066	.6212	.8278	.9257
.572	.9158	.6167	.8206	.9220
.520	.9251	.6142	.8148	.9191
.468	.9297	.6140	.8127	.9179
.416	.9343	.6035	.8037	.9132
.364	.9482	.5884	.7878	.9046
.312	.9621	.5775	.7748	.8973
.260	.9760	.5521	.7521	.8843
.208	.9898	.5350	.7352	.8741
.156	1.0130	.5050	.7061	.8558
.104	1.0361	.4874	.6859	.8424
.052	1.0361	.4750	.6771	.8365
0.000	1.0361	.4750	.6771	.8365
-.104	1.0268	.4946	.6940	.8479
-.156	1.0130	.5118	.7108	.8588
-.208	.9991	.5393	.7347	.8738
-.260	.9806	.5608	.7563	.8867
-.312	.9667	.5800	.7746	.8972
-.364	.9575	.5908	.7855	.9033
-.416	.9343	.6001	.8014	.9120
-.468	.9251	.6087	.8112	.9172
-.520	.9158	.6091	.8156	.9194
-.572	.9112	.6135	.8205	.9220
-.624	.9066	.6219	.8283	.9260
-.676	.9066	.6281	.8324	.9280
-.728	.9066	.6384	.8392	.9315
-.780	.9066	.6488	.8459	.9348
-.832	.9066	.6632	.8553	.9393
-.884	.9158	.6793	.8612	.9422
-.936	.9251	.7016	.8708	.9467
-.988	.9343	.7197	.8777	.9499
-1.040	.9436	.7399	.8855	.9535

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 × 10⁶ PER FOOT (5.42 × 10⁶ PER METER) – Continued

(aa) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^{\circ}$;

$p_\infty = 51.85$ psf (2482.63 N/m^2);
$q_\infty = 318.01$ psf (15226.25 N/m^2);
$p_{t,\infty} = 1793.50$ psf (85873.24 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3119	.8338	.7972	.9097
.988	1.2473	.8058	.8038	.9132
.936	1.1826	.7839	.8142	.9187
.884	1.1780	.7594	.8029	.9128
.832	1.1733	.7431	.7958	.9090
.780	1.1641	.7250	.7892	.9053
.728	1.1549	.7110	.7846	.9028
.676	1.1549	.6986	.7778	.8990
.624	1.1549	.6904	.7732	.8964
.572	1.1549	.6800	.7674	.8931
.520	1.1549	.6739	.7639	.8911
.468	1.1502	.6638	.7596	.8887
.416	1.1456	.6495	.7530	.8847
.364	1.1364	.6334	.7466	.8810
.312	1.1272	.6153	.7388	.8763
.260	1.1179	.5889	.7258	.8683
.208	1.1087	.5687	.7162	.8622
.156	1.1133	.5416	.6975	.8502
.104	1.1179	.5207	.6825	.8402
.052	1.1179	.5062	.6729	.8336
0.000	1.1179	.5000	.6688	.8307
-.104	1.1087	.5259	.6887	.8444
-.156	1.1041	.5447	.7024	.8534
-.208	1.0994	.5739	.7225	.8662
-.260	1.1041	.5985	.7363	.8747
-.312	1.0994	.6173	.7493	.8826
-.364	1.1041	.6377	.7600	.8889
-.416	1.0994	.6545	.7715	.8955
-.468	1.1041	.6646	.7758	.8979
-.520	1.1087	.6726	.7789	.8996
-.572	1.1272	.6821	.7779	.8991
-.624	1.1456	.6875	.7747	.8973
-.676	1.1549	.6974	.7771	.8986
-.728	1.1641	.7094	.7806	.9006
-.780	1.1595	.7240	.7902	.9059
-.832	1.1549	.7407	.8009	.9117
-.884	1.1687	.7607	.8068	.9148
-.936	1.1826	.7828	.8136	.9184
-.988	1.2011	.8088	.8206	.9221
-1.040	1.2195	.8389	.8294	.9265

(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^{\circ}$;

$p_\infty = 51.92$ psf (2485.81 N/m^2);
$q_\infty = 318.41$ psf (15245.78 N/m^2);
$p_{t,\infty} = 1795.80$ psf (85983.37 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2356	.7990	.8041	.9134
.988	1.1665	.7794	.8174	.9204
.936	1.0973	.7578	.8310	.9274
.884	1.0973	.7352	.8185	.9210
.832	1.0973	.7207	.8104	.9168
.780	1.0927	.7024	.8018	.9122
.728	1.0881	.6882	.7953	.9087
.676	1.0927	.6757	.7863	.9038
.624	1.0973	.6672	.7798	.9001
.572	1.0973	.6631	.7774	.8988
.520	1.0973	.6590	.7749	.8974
.468	1.0927	.6510	.7718	.8957
.416	1.0881	.6409	.7674	.8932
.364	1.0835	.6267	.7605	.8892
.312	1.0789	.6145	.7547	.8858
.260	1.0743	.5941	.7437	.8792
.208	1.0697	.5758	.7337	.8732
.156	1.0743	.5508	.7161	.8622
.104	1.0789	.5320	.7022	.8533
.052	1.0789	.5197	.6940	.8479
0.000	1.0789	.5155	.6913	.8461
-.104	1.0697	.5249	.7005	.8521
-.156	1.0697	.5455	.7141	.8609
-.208	1.0697	.5703	.7302	.8710
-.260	1.0604	.5913	.7467	.8811
-.312	1.0604	.6078	.7571	.8872
-.364	1.0650	.6241	.7655	.8920
-.416	1.0512	.6371	.7785	.8994
-.468	1.0558	.6451	.7817	.9012
-.520	1.0604	.6511	.7836	.9023
-.572	1.0697	.6569	.7837	.9023
-.624	1.0789	.6627	.7837	.9023
-.676	1.0881	.6726	.7862	.9037
-.728	1.0973	.6845	.7898	.9057
-.780	1.0881	.6973	.8005	.9115
-.832	1.0789	.7142	.8136	.9184
-.884	1.0881	.7323	.8204	.9219
-.936	1.0973	.7525	.8281	.9259
-.988	1.1112	.7725	.8338	.9288
-1.040	1.1250	.7966	.8415	.9326

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^\circ$;

$p_\infty = 51.79$ psf (2479.72 N/m²);
$q_\infty = 317.63$ psf (15208.43 N/m²);
$p_{t,\infty} = 1791.40$ psf (85772.69 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9344	.9071	.9852	.9946
.988	.8789	.9095	1.0172	1.0062
.936	.8234	.9098	1.0511	1.0177
.884	.8142	.9081	1.0561	1.0193
.832	.8049	.9085	1.0624	1.0214
.780	.8095	.9063	1.0581	1.0200
.728	.8142	.9040	1.0537	1.0186
.676	.8049	.9023	1.0588	1.0202
.624	.7957	.9027	1.0652	1.0223
.572	.7957	.9007	1.0639	1.0219
.520	.7957	.9007	1.0639	1.0219
.468	.7864	.8990	1.0692	1.0236
.416	.7772	.8974	1.0746	1.0253
.364	.7772	.8974	1.0746	1.0253
.312	.7772	.8953	1.0733	1.0249
.260	.7818	.8951	1.0700	1.0238
.208	.7864	.8949	1.0667	1.0228
.156	.7864	.8928	1.0655	1.0224
.104	.7864	.8928	1.0655	1.0224
.052	.7910	.8906	1.0611	1.0209
0.000	.7957	.8924	1.0591	1.0203
-.104	.7864	.8898	1.0637	1.0218
-.156	.8003	.8892	1.0541	1.0187
-.208	.8142	.8886	1.0447	1.0156
-.260	.7910	.8896	1.0604	1.0207
-.312	.8049	.8890	1.0509	1.0176
-.364	.8049	.8890	1.0509	1.0176
-.416	.7957	.8894	1.0572	1.0197
-.468	.7957	.8914	1.0585	1.0201
-.520	.7957	.8914	1.0585	1.0201
-.572	.7957	.8914	1.0585	1.0201
-.624	.7957	.8955	1.0609	1.0209
-.676	.7910	.8957	1.0641	1.0219
-.728	.7864	.9001	1.0698	1.0238
-.780	.7910	.8999	1.0666	1.0227
-.832	.7957	.8997	1.0633	1.0217
-.884	.8003	.8995	1.0602	1.0207
-.936	.8049	.9013	1.0582	1.0200
-.988	.8142	.9030	1.0531	1.0184
-1.040	.8234	.9026	1.0470	1.0163

(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^\circ$;

$p_\infty = 51.83$ psf (2481.66 N/m²);
$q_\infty = 317.88$ psf (15220.31 N/m²);
$p_{t,\infty} = 1792.80$ psf (85839.73 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0811	.9698	.9471	.9798
.988	1.0211	.9724	.9759	.9910
.936	.9610	.9750	1.0073	1.0026
.884	.9610	.9750	1.0073	1.0026
.832	.9610	.9750	1.0073	1.0026
.780	.9610	.9750	1.0073	1.0026
.728	.9610	.9709	1.0052	1.0019
.676	.9610	.9668	1.0030	1.0011
.624	.9610	.9668	1.0030	1.0011
.572	.9610	.9648	1.0020	1.0007
.520	.9610	.9627	1.0009	1.0003
.468	.9564	.9629	1.0034	1.0012
.416	.9518	.9610	1.0049	1.0018
.364	.9518	.9590	1.0038	1.0014
.312	.9518	.9569	1.0027	1.0010
.260	.9471	.9551	1.0042	1.0015
.208	.9425	.9573	1.0078	1.0028
.156	.9471	.9551	1.0042	1.0015
.104	.9518	.9549	1.0016	1.0006
.052	.9564	.9547	.9991	.9997
0.000	.9610	.9545	.9966	.9988
-.104	.9425	.9461	1.0019	1.0007
-.156	.9518	.9477	.9979	.9992
-.208	.9610	.9473	.9929	.9974
-.260	.9379	.9483	1.0055	1.0020
-.312	.9471	.9479	1.0004	1.0002
-.364	.9425	.9481	1.0030	1.0011
-.416	.9333	.9485	1.0081	1.0029
-.468	.9287	.9529	1.0129	1.0046
-.520	.9240	.9551	1.0167	1.0060
-.572	.9333	.9547	1.0114	1.0041
-.624	.9425	.9564	1.0073	1.0026
-.676	.9471	.9582	1.0058	1.0021
-.728	.9518	.9601	1.0044	1.0016
-.780	.9471	.9603	1.0069	1.0025
-.832	.9425	.9626	1.0106	1.0038
-.884	.9471	.9624	1.0080	1.0029
-.936	.9518	.9663	1.0076	1.0027
-.988	.9610	.9659	1.0025	1.0009
-1.040	.9702	.9655	.9975	.9991

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^o$;

$p_\infty = 51.86$ psf (2483.04 N/m^2);
$q_\infty = 318.06$ psf (15228.80 N/m^2);
$p_{t,\infty} = 1793.80$ psf (85887.61 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0713	.9336	.9335	.9742
.988	1.0113	.9362	.9622	.9858
.936	.9512	.9368	.9924	.9972
.884	.9512	.9347	.9913	.9968
.832	.9512	.9347	.9913	.9968
.780	.9512	.9306	.9891	.9960
.728	.9512	.9265	.9869	.9952
.676	.9512	.9204	.9836	.9940
.624	.9512	.9183	.9825	.9935
.572	.9559	.9140	.9779	.9918
.520	.9605	.9097	.9732	.9900
.468	.9512	.9080	.9770	.9915
.416	.9420	.9043	.9798	.9925
.364	.9420	.8982	.9765	.9912
.312	.9420	.8961	.9753	.9908
.260	.9374	.8942	.9767	.9914
.208	.9328	.8944	.9792	.9923
.156	.9374	.8901	.9745	.9905
.104	.9420	.8899	.9720	.9895
.052	.9466	.8897	.9695	.9886
0.000	.9512	.8895	.9670	.9876
-.104	.9328	.8862	.9747	.9906
-.156	.9420	.8858	.9697	.9887
-.208	.9512	.8854	.9648	.9868
-.260	.9281	.8885	.9784	.9920
-.312	.9374	.8881	.9734	.9901
-.364	.9374	.8902	.9745	.9905
-.416	.9235	.8928	.9832	.9938
-.468	.9235	.8949	.9844	.9942
-.520	.9235	.8990	.9866	.9951
-.572	.9281	.9029	.9863	.9950
-.624	.9328	.9048	.9849	.9944
-.676	.9328	.9089	.9871	.9953
-.728	.9328	.9130	.9894	.9961
-.780	.9281	.9153	.9930	.9975
-.832	.9235	.9196	.9979	.9992
-.884	.9328	.9212	.9938	.9977
-.936	.9420	.9229	.9898	.9963
-.988	.9512	.9266	.9870	.9952
-1.040	.9605	.9303	.9842	.9942

(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^o$;

$p_\infty = 51.75$ psf (2477.92 N/m^2);
$q_\infty = 317.40$ psf (15197.39 N/m^2);
$p_{t,\infty} = 1790.10$ psf (85710.45 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0647	.8721	.9050	.9621
.988	1.0323	.8838	.9253	.9708
.936	.9999	.8832	.9398	.9768
.884	1.0462	.9120	.9337	.9743
.832	1.0925	.9018	.9085	.9637
.780	1.1018	.9096	.9086	.9637
.728	1.1110	.8968	.8985	.9592
.676	1.1249	.8818	.8854	.9534
.624	1.1388	.8668	.8724	.9474
.572	1.1481	.8540	.8625	.9428
.520	1.1573	.8412	.8526	.9380
.468	1.1481	.8293	.8499	.9367
.416	1.1388	.8173	.8472	.9354
.364	1.1342	.8072	.8436	.9337
.312	1.1296	.7992	.8411	.9324
.260	1.1249	.7891	.8375	.9306
.208	1.1203	.7810	.8350	.9294
.156	1.1249	.7767	.8309	.9273
.104	1.1296	.7703	.8258	.9247
.052	1.1296	.7703	.8258	.9247
0.000	1.1296	.7703	.8258	.9247
-.104	1.1203	.7684	.8282	.9259
-.156	1.1110	.7730	.8341	.9289
-.208	1.1018	.7754	.8389	.9313
-.260	1.1018	.7816	.8423	.9330
-.312	1.0925	.7903	.8505	.9370
-.364	1.0925	.7965	.8538	.9386
-.416	1.0833	.8052	.8621	.9426
-.468	1.0833	.8176	.8688	.9457
-.520	1.0833	.8320	.8764	.9493
-.572	1.1018	.8457	.8761	.9491
-.624	1.1203	.8552	.8737	.9480
-.676	1.1110	.8721	.8860	.9537
-.728	1.1018	.8808	.8941	.9573
-.780	1.0555	.8849	.9156	.9667
-.832	1.0092	.8828	.9353	.9750
-.884	.9907	.8609	.9322	.9737
-.936	.9722	.8617	.9415	.9775
-.988	.9629	.8621	.9462	.9794
-1.040	.9536	.8645	.9521	.9818

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(gg) $x/D = 8.39$; $y/D = .83$; $\alpha = 0^\circ$;
$p_\infty = 51.82$ psf (2481.11 N/m^2);
$q_\infty = 317.81$ psf (15216.92 N/m^2);
$p_{t,\infty} = 1792.40$ psf (85820.57 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2673	.9402	.8613	.9422
.988	1.2118	.9241	.8733	.9478
.936	1.1563	.9060	.8852	.9533
.884	1.1517	.8877	.8779	.9500
.832	1.1471	.8673	.8695	.9461
.780	1.1378	.8492	.8639	.9434
.728	1.1286	.8270	.8560	.9397
.676	1.1332	.8062	.8434	.9336
.624	1.1378	.7895	.8330	.9284
.572	1.1471	.7767	.8229	.9232
.520	1.1563	.7640	.8128	.9180
.468	1.1471	.7479	.8075	.9152
.416	1.1378	.7421	.8076	.9153
.364	1.1332	.7279	.8015	.9120
.312	1.1286	.7219	.7998	.9111
.260	1.1193	.7141	.7987	.9105
.208	1.1101	.7083	.7988	.9106
.156	1.1147	.7020	.7936	.9077
.104	1.1193	.6976	.7895	.9055
.052	1.1193	.6935	.7871	.9042
0.000	1.1193	.6915	.7860	.9036
-.104	1.1101	.6956	.7916	.9067
-.156	1.1008	.6981	.7963	.9092
-.208	1.0916	.7047	.8035	.9131
-.260	1.0962	.7065	.8028	.9127
-.312	1.0869	.7131	.8100	.9165
-.364	1.0869	.7193	.8135	.9184
-.416	1.0823	.7278	.8200	.9218
-.468	1.0823	.7422	.8281	.9259
-.520	1.0823	.7526	.8339	.9288
-.572	1.1008	.7682	.8354	.9296
-.624	1.1193	.7819	.8358	.9298
-.676	1.1239	.8002	.8438	.9337
-.728	1.1286	.8207	.8527	.9381
-.780	1.1193	.8396	.8661	.9445
-.832	1.1101	.8586	.8795	.9507
-.884	1.1286	.8805	.8833	.9524
-.936	1.1471	.9003	.8859	.9536
-.988	1.1471	.9147	.8930	.9568
-1.040	1.1471	.9250	.8980	.9591

(hh) $x/D = 8.39$; $y/D = .63$; $\alpha = 0^\circ$;
$p_\infty = 51.83$ psf (2481.52 N/m^2);
$q_\infty = 317.87$ psf (15219.46 N/m^2);
$p_{t,\infty} = 1792.70$ psf (85834.94 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2851	.8805	.8278	.9257
.988	1.2204	.8607	.8398	.9318
.936	1.1557	.8368	.8509	.9372
.884	1.1510	.8143	.8411	.9324
.832	1.1464	.7939	.8322	.9280
.780	1.1418	.7715	.8220	.9228
.728	1.1372	.7511	.8127	.9179
.676	1.1372	.7325	.8026	.9126
.624	1.1372	.7202	.7958	.9089
.572	1.1418	.7076	.7872	.9043
.520	1.1464	.6950	.7786	.8995
.468	1.1418	.6849	.7745	.8972
.416	1.1372	.6727	.7691	.8941
.364	1.1279	.6608	.7654	.8920
.312	1.1187	.6488	.7616	.8898
.260	1.1094	.6348	.7564	.8868
.208	1.1002	.6228	.7524	.8844
.156	1.1048	.6144	.7457	.8804
.104	1.1094	.6018	.7365	.8749
.052	1.1048	.5978	.7356	.8743
0.000	1.1002	.5960	.7360	.8746
-.104	1.1002	.6008	.7390	.8764
-.156	1.0956	.6093	.7458	.8805
-.208	1.0909	.6219	.7550	.8860
-.260	1.0909	.6343	.7625	.8903
-.312	1.0863	.6448	.7705	.8949
-.364	1.0863	.6552	.7766	.8984
-.416	1.0817	.6657	.7845	.9028
-.468	1.0817	.6781	.7918	.9067
-.520	1.0817	.6905	.7990	.9106
-.572	1.1002	.7000	.7976	.9099
-.624	1.1187	.7136	.7987	.9105
-.676	1.1279	.7276	.8032	.9129
-.728	1.1372	.7458	.8098	.9164
-.780	1.1279	.7648	.8234	.9235
-.832	1.1187	.7858	.8381	.9309
-.884	1.1372	.8077	.8428	.9332
-.936	1.1557	.8316	.8483	.9359
-.988	1.1695	.8516	.8533	.9384
-1.040	1.1834	.8757	.8603	.9417

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(ii) x/D = 8.39; y/D = .42; $\alpha = 0^\circ$;

p_∞ = 51.85 psf (2482.63 N/m^2);
q_∞ = 318.01 psf (15226.25 N/m^2);
$p_{t,\infty}$ = 1793.50 psf (85873.24 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2640	.8409	.8156	.9195
.988	1.1995	.8170	.8253	.9245
.936	1.1349	.7911	.8349	.9293
.884	1.1303	.7625	.8213	.9224
.832	1.1256	.7400	.8108	.9170
.780	1.1210	.7217	.8024	.9125
.728	1.1164	.7034	.7938	.9078
.676	1.1210	.6909	.7850	.9031
.624	1.1256	.6804	.7774	.8988
.572	1.1303	.6678	.7687	.8938
.520	1.1349	.6552	.7598	.8888
.468	1.1256	.6412	.7547	.8858
.416	1.1164	.6272	.7495	.8827
.364	1.1072	.6091	.7417	.8780
.312	1.0980	.5889	.7324	.8723
.260	1.0933	.5644	.7185	.8637
.208	1.0887	.5460	.7082	.8571
.156	1.0933	.5272	.6944	.8482
.104	1.0980	.5146	.6846	.8416
.052	1.0933	.5087	.6821	.8399
0.000	1.0887	.5047	.6809	.8391
-.104	1.0795	.5126	.6891	.8446
-.156	1.0795	.5250	.6974	.8501
-.208	1.0795	.5436	.7096	.8581
-.260	1.0749	.5645	.7247	.8676
-.312	1.0749	.5852	.7378	.8757
-.364	1.0795	.6036	.7477	.8816
-.416	1.0703	.6246	.7639	.8911
-.468	1.0749	.6368	.7697	.8944
-.520	1.0795	.6490	.7754	.8977
-.572	1.0887	.6609	.7791	.8998
-.624	1.0980	.6729	.7829	.9019
-.676	1.1072	.6828	.7853	.9032
-.728	1.1164	.6989	.7912	.9065
-.780	1.1072	.7158	.8041	.9134
-.832	1.0980	.7348	.8181	.9207
-.884	1.1164	.7567	.8233	.9234
-.936	1.1349	.7806	.8293	.9265
-.988	1.1487	.8068	.8381	.9309
-1.040	1.1625	.8371	.8486	.9361

(jj) x/D = 8.39; y/D = .21; $\alpha = 0^\circ$;

p_∞ = 51.86 psf (2482.90 N/m^2);
q_∞ = 318.04 psf (15227.95 N/m^2);
$p_{t,\infty}$ = 1793.70 psf (85882.82 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2281	.8033	.8088	.9159
.988	1.1681	.7854	.8200	.9217
.936	1.1080	.7654	.8311	.9274
.884	1.1034	.7451	.8217	.9226
.832	1.0988	.7329	.8167	.9200
.780	1.0988	.7144	.8063	.9146
.728	1.0988	.7021	.7993	.9109
.676	1.0988	.6897	.7923	.9070
.624	1.0988	.6815	.7875	.9044
.572	1.1034	.6710	.7798	.9001
.520	1.1080	.6625	.7733	.8965
.468	1.1034	.6442	.7641	.8912
.416	1.0988	.6218	.7522	.8843
.364	1.0942	.6014	.7413	.8778
.312	1.0896	.5830	.7315	.8718
.260	1.0850	.5606	.7188	.8639
.208	1.0803	.5422	.7084	.8573
.156	1.0803	.5216	.6948	.8484
.104	1.0803	.5092	.6865	.8429
.052	1.0803	.5009	.6810	.8391
0.000	1.0803	.4989	.6795	.8382
-.104	1.0711	.5129	.6920	.8466
-.156	1.0711	.5254	.7003	.8520
-.208	1.0711	.5398	.7099	.8583
-.260	1.0665	.5607	.7251	.8678
-.312	1.0665	.5772	.7357	.8744
-.364	1.0711	.5977	.7470	.8812
-.416	1.0619	.6249	.7671	.8930
-.468	1.0665	.6412	.7754	.8977
-.520	1.0711	.6555	.7823	.9015
-.572	1.0803	.6654	.7848	.9029
-.624	1.0896	.6753	.7872	.9043
-.676	1.0942	.6854	.7914	.9066
-.728	1.0988	.6955	.7956	.9088
-.780	1.0942	.7081	.8044	.9136
-.832	1.0896	.7227	.8144	.9188
-.884	1.0942	.7390	.8218	.9227
-.936	1.0988	.7594	.8313	.9275
-.988	1.1127	.7774	.8359	.9298
-1.040	1.1265	.7994	.8424	.9330

TABLE 4.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Concluded.

(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 51.82$ psf (2481.24 N/m^2);
$q_\infty = 317.83$ psf (15217.76 N/m^2);
$p_{t,\infty} = 1792.50$ psf (85825.36 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2110	.7882	.8068	.9148
.988	1.1463	.7684	.8187	.9211
.936	1.0816	.7486	.8320	.9278
.884	1.0816	.7260	.8193	.9214
.832	1.0816	.7116	.8111	.9171
.780	1.0769	.6953	.8035	.9131
.728	1.0723	.6832	.7982	.9102
.676	1.0769	.6685	.7879	.9046
.624	1.0816	.6601	.7812	.9009
.572	1.0816	.6539	.7776	.8989
.520	1.0816	.6498	.7751	.8975
.468	1.0769	.6438	.7732	.8964
.416	1.0723	.6337	.7687	.8939
.364	1.0723	.6234	.7625	.8903
.312	1.0723	.6131	.7561	.8866
.260	1.0677	.5948	.7464	.8808
.208	1.0631	.5785	.7377	.8756
.156	1.0631	.5558	.7231	.8666
.104	1.0631	.5331	.7081	.8571
.052	1.0631	.5207	.6999	.8517
0.000	1.0631	.5145	.6957	.8490
-.104	1.0538	.5286	.7082	.8572
-.156	1.0538	.5431	.7179	.8633
-.208	1.0538	.5679	.7341	.8734
-.260	1.0492	.5888	.7491	.8825
-.312	1.0492	.6032	.7582	.8878
-.364	1.0492	.6177	.7673	.8931
-.416	1.0446	.6303	.7768	.8985
-.468	1.0446	.6365	.7806	.9006
-.520	1.0446	.6427	.7844	.9027
-.572	1.0538	.6484	.7844	.9027
-.624	1.0631	.6542	.7845	.9028
-.676	1.0677	.6643	.7888	.9051
-.728	1.0723	.6765	.7943	.9081
-.780	1.0677	.6912	.8046	.9137
-.832	1.0631	.7058	.8148	.9191
-.884	1.0723	.7219	.8205	.9220
-.936	1.0816	.7422	.8284	.9260
-.988	1.0908	.7624	.8360	.9299
-1.040	1.1000	.7847	.8446	.9341

(ll) $x/D = 8.39$; $y/D = -.42$; $\alpha = 0^\circ$;

$p_\infty = 51.84$ psf (2482.07 N/m^2);
$q_\infty = 317.94$ psf (15222.86 N/m^2);
$p_{t,\infty} = 1793.10$ psf (85854.09 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1361	.8106	.8447	.9342
.988	1.0715	.7949	.8613	.9422
.936	1.0068	.7731	.8763	.9492
.884	1.0068	.7504	.8633	.9432
.832	1.0068	.7298	.8514	.9375
.780	1.0022	.7074	.8401	.9319
.728	.9976	.6829	.8274	.9255
.676	1.0022	.6600	.8115	.9173
.624	1.0068	.6371	.7955	.9088
.572	1.0114	.6163	.7806	.9006
.520	1.0160	.6058	.7722	.8958
.468	1.0068	.6268	.7890	.9053
.416	.9976	.6499	.8071	.9150
.364	.9976	.6499	.8071	.9150
.312	.9976	.6458	.8046	.9137
.260	.9976	.6417	.8020	.9123
.208	.9976	.6417	.8020	.9123
.156	.9976	.6334	.7968	.9095
.104	.9976	.6210	.7890	.9053
.052	.9976	.5798	.7624	.8902
0.000	.9976	.5592	.7487	.8822
-.104	.9883	.5912	.7734	.8966
-.156	.9929	.6220	.7915	.9066
-.208	.9976	.6321	.7960	.9091
-.260	.9837	.6327	.8020	.9123
-.312	.9883	.6387	.8039	.9133
-.364	.9883	.6408	.8052	.9140
-.416	.9791	.6432	.8105	.9168
-.468	.9791	.6350	.8053	.9141
-.520	.9791	.6144	.7921	.9070
-.572	.9837	.6038	.7835	.9022
-.624	.9883	.6284	.7974	.9098
-.676	.9929	.6509	.8096	.9163
-.728	.9976	.6775	.8241	.9238
-.780	.9929	.6983	.8386	.9312
-.832	.9883	.7191	.8530	.9382
-.884	.9976	.7435	.8633	.9432
-.936	1.0068	.7657	.8721	.9473
-.988	1.0160	.7859	.8795	.9507
-1.040	1.0253	.8082	.8879	.9545

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 22.46$ psf (1075.43 N/m^2);
$q_\infty = 245.31$ psf (11745.56 N/m^2);
$p_{t,\infty} = 3189.70$ psf (152723.66 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.6838	.6414	.6172	.8469
.988	1.3960	.5765	.6426	.8623
.936	1.1083	.5329	.6934	.8902
.884	1.0017	.4902	.6995	.8933
.832	.8952	.4661	.7216	.9041
.780	.8312	.4437	.7306	.9084
.728	.7673	.4213	.7410	.9131
.676	.7140	.4012	.7496	.9170
.624	.6607	.3892	.7675	.9248
.572	.5968	.3774	.7952	.9361
.520	.5328	.3683	.8314	.9498
.468	.4795	.3589	.8651	.9615
.416	.4263	.3442	.8986	.9723
.364	.4476	.2984	.8165	.9443
.312	.4689	.1458	.5576	.8064
.260	.4795	.0277	.2402	.4488
.208	.4902	.0040	.0899	.1803
.156	.5009	0.0000	0.0000	0.0000
.104	.5115	0.0000	0.0000	0.0000
.052	.5009	0.0000	0.0000	0.0000
0.000	.4902	0.0000	0.0000	0.0000
-.104	.4902	.0085	.1318	.2606
-.156	.4902	.0041	.0911	.1826
-.208	.4902	0.0000	0.0000	0.0000
-.260	.5009	.0077	.1237	.2453
-.312	.5009	.0671	.3659	.6238
-.364	.5222	.2572	.7018	.8944
-.416	.5115	.3403	.8156	.9440
-.468	.5328	.3531	.8141	.9434
-.520	.5541	.3606	.8067	.9406
-.572	.5755	.3734	.8056	.9402
-.624	.5968	.3890	.8073	.9409
-.676	.6714	.4005	.7724	.9268
-.728	.7460	.4201	.7504	.9174
-.780	.8099	.4426	.7392	.9123
-.832	.8738	.4677	.7316	.9088
-.884	.9911	.4943	.7062	.8966
-.936	1.1083	.5368	.6960	.8915
-.988	1.2468	.5842	.6845	.8855
-1.040	1.3854	.6450	.6823	.8844

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 22.46$ psf (1075.56 N/m^2);
$q_\infty = 245.34$ psf (11747.04 N/m^2);
$p_{t,\infty} = 3190.10$ psf (152742.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3222	.5196	.6269	.8528
.988	1.0663	.4805	.6713	.8785
.936	.8104	.4548	.7492	.9168
.884	.7571	.4294	.7532	.9186
.832	.7037	.4174	.7701	.9259
.780	.6611	.4024	.7802	.9301
.728	.6184	.3902	.7943	.9358
.676	.5971	.3773	.7949	.9360
.624	.5758	.3725	.8044	.9397
.572	.5331	.3682	.8311	.9497
.520	.4905	.3613	.8582	.9592
.468	.4692	.3591	.8749	.9648
.416	.4478	.3596	.8961	.9715
.364	.6184	.3555	.7582	.9208
.312	.7890	.4473	.7529	.9185
.260	.9383	.4703	.7080	.8975
.208	1.0876	.4667	.6550	.8694
.156	1.1942	.3090	.5087	.7680
.104	1.3009	.1684	.3598	.6164
.052	1.3435	.1561	.3409	.5928
0.000	1.3862	.1905	.3707	.6295
-.104	1.3009	.1579	.3484	.6023
-.156	1.2156	.2554	.4584	.7231
-.208	1.1302	.4426	.6258	.8522
-.260	.9170	.4746	.7194	.9031
-.312	.8317	.4500	.7356	.9107
-.364	.8317	.3404	.6398	.8606
-.416	.5331	.3504	.8107	.9421
-.468	.5331	.3504	.8107	.9421
-.520	.5331	.3530	.8138	.9433
-.572	.5225	.3586	.8285	.9488
-.624	.5118	.3696	.8498	.9563
-.676	.5651	.3763	.8160	.9442
-.728	.6184	.3857	.7897	.9340
-.780	.6504	.3983	.7825	.9310
-.832	.6824	.4109	.7759	.9283
-.884	.7357	.4310	.7653	.9239
-.936	.7890	.4537	.7583	.9208
-.988	.8637	.4813	.7465	.9156
-1.040	.9383	.5195	.7441	.9145

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^o$;

p_∞ = 22.44 psf (1074.62 N/m^2);
q_∞ = 245.13 psf (11736.73 N/m^2);
$p_{t,\infty}$ = 3187.30 psf (152608.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1523	.4702	.6388	.8600
.988	.9283	.4464	.6935	.8902
.936	.7042	.4279	.7795	.9298
.884	.6722	.4127	.7836	.9315
.832	.6402	.4028	.7932	.9354
.780	.6188	.3953	.7993	.9377
.728	.5975	.3879	.8057	.9402
.676	.5975	.3825	.8001	.9381
.624	.5975	.3799	.7973	.9370
.572	.6615	.4476	.8226	.9466
.520	.7255	.4487	.7864	.9326
.468	.7575	.4346	.7574	.9204
.416	.7896	.4445	.7503	.9173
.364	1.0990	.5276	.6929	.8899
.312	1.4084	.5626	.6320	.8560
.260	1.4937	.5631	.6140	.8448
.208	1.5791	.5236	.5758	.8194
.156	1.5898	.4271	.5183	.7760
.104	1.6004	.3652	.4777	.7411
.052	1.6325	.3375	.4547	.7196
0.000	1.6645	.3285	.4443	.7094
-.104	1.6218	.3655	.4747	.7384
-.156	1.6538	.4184	.5030	.7633
-.208	1.6858	.5087	.5493	.8003
-.260	1.2057	.5716	.6885	.8876
-.312	1.2377	.5681	.6775	.8818
-.364	1.2590	.5195	.6424	.8621
-.416	.7896	.4295	.7376	.9116
-.468	.8109	.4290	.7273	.9068
-.520	.8322	.4418	.7286	.9074
-.572	.6935	.3731	.7334	.9097
-.624	.5548	.3738	.8208	.9459
-.676	.5655	.3735	.8127	.9429
-.728	.5762	.3813	.8135	.9432
-.780	.5975	.3888	.8066	.9406
-.832	.6188	.3963	.8002	.9381
-.884	.6402	.4091	.7994	.9378
-.936	.6615	.4246	.8012	.9385
-.988	.7042	.4423	.7925	.9351
-1.040	.7469	.4653	.7893	.9338

(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^o$;

p_∞ = 22.45 psf (1074.96 N/m^2);
q_∞ = 245.20 psf (11740.41 N/m^2);
$p_{t,\infty}$ = 3188.30 psf (152656.63 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3647	1.0015	.8567	.9587
.988	1.1727	1.0088	.9275	.9808
.936	.9808	1.0107	1.0151	1.0036
.884	.9702	1.0109	1.0208	1.0049
.832	.9595	1.0112	1.0266	1.0063
.780	.9489	1.0114	1.0324	1.0076
.728	.9382	1.0117	1.0384	1.0089
.676	.9382	1.0090	1.0371	1.0086
.624	.9382	1.0063	1.0357	1.0083
.572	.9489	1.0061	1.0297	1.0070
.520	.9595	1.0058	1.0239	1.0056
.468	.9489	1.0061	1.0297	1.0070
.416	.9382	1.0063	1.0357	1.0083
.364	.9382	1.0037	1.0343	1.0080
.312	.9382	1.0037	1.0343	1.0080
.260	.9382	1.0037	1.0343	1.0080
.208	.9382	1.0037	1.0343	1.0080
.156	.9382	1.0037	1.0343	1.0080
.104	.9382	1.0037	1.0343	1.0080
.052	.9382	1.0037	1.0343	1.0080
0.000	.9382	1.0037	1.0343	1.0080
-.104	.9382	.9980	1.0314	1.0073
-.156	.9489	.9977	1.0254	1.0060
-.208	.9595	.9975	1.0196	1.0046
-.260	.9275	.9982	1.0374	1.0087
-.312	.9382	.9980	1.0314	1.0073
-.364	.9275	.9982	1.0374	1.0087
-.416	.9169	.9958	1.0421	1.0098
-.468	.9062	.9934	1.0470	1.0108
-.520	.8956	.9936	1.0533	1.0122
-.572	.9062	.9907	1.0456	1.0105
-.624	.9169	.9905	1.0393	1.0091
-.676	.9062	.9907	1.0456	1.0105
-.728	.8956	.9910	1.0519	1.0119
-.780	.8956	.9883	1.0505	1.0116
-.832	.8956	.9856	1.0491	1.0113
-.884	.9062	.9854	1.0428	1.0099
-.936	.9169	.9851	1.0365	1.0085
-.988	.9275	.9822	1.0290	1.0068
-1.040	.9382	.9793	1.0217	1.0051

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^\circ$;

$p_\infty = 22.47$ psf (1075.83 N/m^2);
$q_\infty = 245.40$ psf (11749.98 N/m^2);
$p_{t,\infty} = 3190.90$ psf (152781.12 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.7696	1.7066	.9821	.9956
.988	1.8335	1.6731	.9553	.9886
.936	1.8975	1.6450	.9311	.9819
.884	1.8868	1.6212	.9270	.9807
.832	1.8762	1.6002	.9235	.9797
.780	1.9188	1.5778	.9068	.9748
.728	1.9614	1.5528	.8898	.9695
.676	1.9081	1.5381	.8978	.9720
.624	1.8548	1.5180	.9047	.9741
.572	1.8548	1.4994	.8991	.9724
.520	1.8548	1.4887	.8959	.9714
.468	1.8442	1.4703	.8929	.9705
.416	1.8335	1.4546	.8907	.9698
.364	1.7909	1.4422	.8974	.9719
.312	1.7482	1.4353	.9061	.9745
.260	1.7163	1.4254	.9113	.9761
.208	1.6843	1.4181	.9176	.9780
.156	1.7376	1.4142	.9022	.9734
.104	1.7909	1.4102	.8874	.9688
.052	1.7482	1.4113	.8985	.9722
0.000	1.7056	1.4096	.9091	.9755
-.104	1.7269	1.4064	.9025	.9734
-.156	1.7269	1.4144	.9050	.9742
-.208	1.7269	1.4144	.9050	.9742
-.260	1.6416	1.4271	.9324	.9822
-.312	1.6416	1.4431	.9376	.9837
-.364	1.6310	1.4434	.9407	.9846
-.416	1.5564	1.4638	.9698	.9924
-.468	1.5457	1.4827	.9794	.9949
-.520	1.5350	1.4990	.9882	.9971
-.572	1.7376	1.5048	.9306	.9817
-.624	1.9401	1.5160	.8840	.9677
-.676	1.9721	1.5339	.8819	.9670
-.728	2.0041	1.5545	.8807	.9666
-.780	1.8868	1.5759	.9139	.9769
-.832	1.7696	1.5920	.9485	.9867
-.884	1.8762	1.6322	.9327	.9823
-.936	1.9828	1.6563	.9140	.9769
-.988	1.5031	1.6916	1.0609	1.0138
-1.040	1.0234	.9780	.9776	.9944

(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^\circ$;

$p_\infty = 22.46$ psf (1075.29 N/m^2);
$q_\infty = 245.28$ psf (11744.09 N/m^2);
$p_{t,\infty} = 3189.30$ psf (152704.51 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.7487	1.1785	.8209	.9460
.988	1.5355	1.1463	.8641	.9612
.936	1.3222	1.1168	.9190	.9784
.884	1.2796	1.0858	.9212	.9790
.832	1.2369	1.0629	.9270	.9807
.780	1.2156	1.0341	.9223	.9794
.728	1.1942	1.0053	.9175	.9779
.676	1.1623	.9821	.9192	.9785
.624	1.1303	.9589	.9211	.9790
.572	1.1196	.9378	.9152	.9773
.520	1.1089	.9221	.9119	.9763
.468	1.0876	.9039	.9116	.9762
.416	1.0663	.8858	.9114	.9762
.364	1.0556	.8674	.9065	.9747
.312	1.0450	.8543	.9042	.9740
.260	1.0343	.8439	.9033	.9737
.208	1.0236	.8362	.9038	.9739
.156	1.0130	.8284	.9043	.9740
.104	1.0023	.8234	.9063	.9746
.052	1.0023	.8234	.9063	.9746
0.000	1.0023	.8207	.9049	.9742
-.104	1.0023	.8216	.9054	.9743
-.156	1.0023	.8296	.9098	.9757
-.208	1.0023	.8376	.9142	.9770
-.260	1.0023	.8430	.9171	.9778
-.312	1.0023	.8563	.9243	.9799
-.364	1.0023	.8616	.9272	.9808
-.416	1.0023	.8776	.9357	.9832
-.468	1.0023	.8963	.9456	.9860
-.520	1.0023	.9176	.9568	.9890
-.572	1.0556	.9351	.9412	.9847
-.624	1.1089	.9578	.9294	.9814
-.676	1.1516	.9781	.9216	.9791
-.728	1.1942	1.0091	.9192	.9785
-.780	1.1942	1.0331	.9301	.9816
-.832	1.1942	1.0544	.9396	.9843
-.884	1.2689	1.0927	.9280	.9810
-.936	1.3435	1.1282	.9164	.9776
-.988	1.3862	1.1539	.9124	.9764
-1.040	1.4288	1.1876	.9117	.9762

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^\circ$;
p_∞ = 22.45 psf (1075.06 N/m^2);
q_∞ = 245.23 psf (11741.51 N/m^2);
$p_{t,\infty}$ = 3188.60 psf (152670.99 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3429	.7532	.7489	.9167
.988	1.1191	.7133	.7984	.9374
.936	.8953	.6867	.8758	.9651
.884	.8633	.6529	.8696	.9630
.832	.8313	.6270	.8685	.9627
.780	.8100	.5983	.8594	.9596
.728	.7887	.5695	.8497	.9563
.676	.7674	.5514	.8476	.9556
.624	.7461	.5332	.8454	.9548
.572	.7247	.5178	.8452	.9548
.520	.7034	.5050	.8473	.9555
.468	.6714	.4924	.8564	.9586
.416	.6395	.4825	.8687	.9627
.364	.6608	.4714	.8446	.9545
.312	.6821	.4655	.8261	.9479
.260	.6928	.4573	.8125	.9428
.208	.7034	.4517	.8014	.9386
.156	.7993	.4441	.7453	.9151
.104	.8953	.4391	.7003	.8937
.052	.9166	.4332	.6875	.8871
0.000	.9379	.4327	.6792	.8827
−.104	.8953	.4348	.6969	.8919
−.156	.7887	.4400	.7469	.9158
−.208	.6821	.4453	.8080	.9411
−.260	.7887	.4480	.7537	.9188
−.312	.6821	.4559	.8176	.9448
−.364	.6928	.4610	.8158	.9441
−.416	.6821	.4720	.8318	.9500
−.468	.6928	.4824	.8344	.9509
−.520	.7034	.4955	.8393	.9527
−.572	.7034	.5088	.8505	.9566
−.624	.7034	.5248	.8638	.9611
−.676	.7247	.5456	.8677	.9624
−.728	.7461	.5691	.8734	.9643
−.780	.7674	.5900	.8768	.9654
−.832	.7887	.6162	.8839	.9677
−.884	.8207	.6474	.8882	.9690
−.936	.8526	.6813	.8939	.9708
−.988	.9059	.7094	.8849	.9680
−1.040	.9592	.7455	.8816	.9669

(h) $x/D = 2.5$; $y/D = .83$; $\alpha = 0^\circ$;
p_∞ = 22.47 psf (1075.97 N/m^2);
q_∞ = 245.43 psf (11751.45 N/m^2);
$p_{t,\infty}$ = 3191.30 psf (152800.27 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2571	.6470	.7174	.9021
.988	1.0228	.6047	.7689	.9254
.936	.7884	.5810	.8584	.9593
.884	.7671	.5522	.8484	.9559
.832	.7458	.5313	.8441	.9544
.780	.7138	.5081	.8437	.9542
.728	.6818	.4875	.8456	.9549
.676	.6712	.4718	.8384	.9524
.624	.6605	.4561	.8309	.9497
.572	.6392	.4459	.8352	.9512
.520	.6179	.4384	.8423	.9537
.468	.7245	.4252	.7661	.9242
.416	.8310	.4146	.7063	.8967
.364	.8630	.4111	.6902	.8885
.312	.8949	.4050	.6727	.8792
.260	.8843	.3999	.6725	.8791
.208	.8736	.3975	.6746	.8802
.156	.9056	.3941	.6597	.8720
.104	.9375	.3933	.6477	.8652
.052	.9375	.3879	.6433	.8626
0.000	.9375	.3879	.6433	.8626
−.104	.9162	.3911	.6534	.8685
−.156	.8843	.3919	.6658	.8754
−.208	.8523	.3927	.6788	.8825
−.260	.7777	.3945	.7123	.8996
−.312	.7458	.4007	.7330	.9095
−.364	.7351	.4036	.7410	.9131
−.416	.6392	.4139	.8047	.9398
−.468	.6286	.4195	.8169	.9445
−.520	.6179	.4304	.8346	.9510
−.572	.6179	.4411	.8449	.9546
−.624	.6179	.4544	.8576	.9590
−.676	.6392	.4672	.8549	.9581
−.728	.6605	.4854	.8572	.9589
−.780	.6818	.5009	.8571	.9588
−.832	.7031	.5190	.8592	.9595
−.884	.7351	.5476	.8631	.9609
−.936	.7671	.5788	.8687	.9627
−.988	.7990	.6074	.8719	.9638
−1.040	.8310	.6413	.8785	.9659

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(i) $x/D = 2.5$; $y/D = .63$; $\alpha = 0^{\circ}$;

p_∞ = 22.48 psf (1076.17 N/m^2);
q_∞ = 245.48 psf (11753.66 N/m^2);
$p_{t,\infty}$ = 3191.90 psf (152829.00 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1519	.5494	.6906	.8887
.988	.9386	.5174	.7424	.9138
.936	.7253	.4986	.8291	.9490
.884	.7040	.4752	.8216	.9462
.832	.6826	.4597	.8206	.9459
.780	.6506	.4445	.8266	.9481
.728	.6186	.4293	.8331	.9504
.676	.6186	.4187	.8227	.9466
.624	.6186	.4107	.8148	.9437
.572	.6080	.4056	.8168	.9445
.520	.5973	.4032	.8217	.9463
.468	.5973	.4006	.8189	.9453
.416	.5973	.3953	.8135	.9432
.364	.6080	.3923	.8033	.9393
.312	.6186	.3921	.7961	.9365
.260	.6186	.3921	.7961	.9365
.208	.6186	.3948	.7988	.9376
.156	.6720	.4014	.7729	.9271
.104	.7253	.4188	.7599	.9215
.052	.7573	.4340	.7570	.9203
0.000	.7893	.4385	.7454	.9151
-.104	.7253	.4117	.7535	.9187
-.156	.6720	.3944	.7661	.9242
-.208	.6186	.3877	.7916	.9347
-.260	.7466	.3846	.7177	.9022
-.312	.6933	.3859	.7460	.9154
-.364	.6186	.3877	.7916	.9347
-.416	.7680	.3840	.7072	.8971
-.468	.6933	.3859	.7460	.9154
-.520	.6186	.3930	.7970	.9369
-.572	.6080	.3959	.8070	.9407
-.624	.5973	.4042	.8226	.9466
-.676	.6080	.4119	.8231	.9468
-.728	.6186	.4223	.8262	.9480
-.780	.6186	.4383	.8417	.9535
-.832	.6186	.4516	.8544	.9579
-.884	.6506	.4722	.8519	.9571
-.936	.6826	.4954	.8519	.9571
-.988	.7146	.5160	.8497	.9563
-1.040	.7466	.5445	.8540	.9578

(j) $x/D = 2.5$; $y/D = .42$; $\alpha = 0^{\circ}$;

p_∞ = 22.48 psf (1076.31 N/m^2);
q_∞ = 245.51 psf (11755.14 N/m^2);
$p_{t,\infty}$ = 3192.30 psf (152848.15 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0876	.4897	.6710	.8783
.988	.8743	.4657	.7298	.9080
.936	.6611	.4495	.8246	.9474
.884	.6397	.4341	.8237	.9470
.832	.6184	.4213	.8254	.9476
.780	.6077	.4136	.8249	.9475
.728	.5971	.4032	.8218	.9463
.676	.5971	.3979	.8163	.9443
.624	.5971	.3952	.8136	.9432
.572	.5971	.3952	.8136	.9432
.520	.5971	.3952	.8136	.9432
.468	.8850	.4095	.6802	.8833
.416	1.1728	.5595	.6907	.8887
.364	1.2688	.5651	.6674	.8763
.312	1.3648	.5601	.6406	.8611
.260	1.3648	.5547	.6376	.8593
.208	1.3648	.5521	.6360	.8584
.156	1.3754	.5465	.6303	.8549
.104	1.3861	.5409	.6247	.8515
.052	1.3754	.5358	.6242	.8512
0.000	1.3648	.5361	.6267	.8528
-.104	1.3648	.5380	.6279	.8534
-.156	1.3648	.5407	.6294	.8544
-.208	1.3648	.5487	.6341	.8572
-.260	1.2155	.5524	.6741	.8800
-.312	1.2155	.5577	.6774	.8817
-.364	.9916	.5632	.7536	.9188
-.416	1.0662	.5267	.7028	.8949
-.468	.8423	.3906	.6810	.8837
-.520	.6184	.3881	.7922	.9349
-.572	.5971	.3886	.8067	.9406
-.624	.5758	.3891	.8221	.9464
-.676	.5758	.3891	.8221	.9464
-.728	.5758	.3971	.8305	.9495
-.780	.5864	.4049	.8309	.9497
-.832	.5971	.4153	.8340	.9508
-.884	.6077	.4284	.8395	.9528
-.936	.6184	.4468	.8500	.9564
-.988	.6504	.4620	.8428	.9539
-1.040	.6824	.4879	.8456	.9549

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(k) $x/D = 2.5$; $y/D = .21$; $\alpha = 0^\circ$;

$p_\infty = 22.46$ psf (1075.29 N/m^2);
$q_\infty = 245.28$ psf (11744.09 N/m^2);
$p_{t,\infty} = 3189.30$ psf (152704.51 N/m^2);

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0675	.4640	.6593	.8718
.988	.8540	.4426	.7199	.9033
.936	.6405	.4292	.8186	.9451
.884	.6298	.4135	.8102	.9420
.832	.6191	.4057	.8095	.9417
.780	.5978	.4009	.8189	.9453
.728	.5764	.3961	.8289	.9489
.676	.5978	.3929	.8107	.9422
.624	.6191	.3951	.7988	.9376
.572	.9714	.5170	.7295	.9079
.520	1.3237	.5563	.6483	.8656
.468	1.3450	.5558	.6428	.8624
.416	1.3664	.5499	.6344	.8574
.364	1.3664	.5473	.6329	.8565
.312	1.3664	.5366	.6267	.8527
.260	1.3450	.5105	.6161	.8461
.208	1.3237	.4683	.5948	.8324
.156	1.3237	.4042	.5526	.8027
.104	1.3237	.3588	.5206	.7779
.052	1.3130	.3323	.5031	.7633
0.000	1.3023	.3246	.4992	.7601
-.104	1.3023	.3607	.5263	.7824
-.156	1.3343	.4054	.5512	.8017
-.208	1.3664	.4662	.5841	.8252
-.260	1.3023	.5107	.6262	.8524
-.312	1.3343	.5340	.6326	.8563
-.364	1.2810	.5433	.6513	.8673
-.416	1.3023	.5428	.6456	.8640
-.468	1.2489	.5468	.6617	.8731
-.520	1.1956	.5508	.6787	.8825
-.572	.9074	.4161	.6772	.8817
-.624	.6191	.3884	.7921	.9349
-.676	.6085	.3887	.7993	.9377
-.728	.5978	.3889	.8066	.9406
-.780	.5978	.3916	.8094	.9417
-.832	.5978	.3996	.8176	.9448
-.884	.5978	.4103	.8285	.9488
-.936	.5978	.4237	.8419	.9536
-.988	.6298	.4389	.8348	.9511
-1.040	.6618	.4569	.8308	.9496

(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 22.48$ psf (1076.27 N/m^2);
$q_\infty = 245.50$ psf (11754.77 N/m^2);
$p_{t,\infty} = 3192.20$ psf (152843.36 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0651	.4535	.6526	.8680
.988	.8521	.4348	.7143	.9006
.936	.6390	.4213	.8120	.9426
.884	.6284	.4109	.8086	.9414
.832	.6177	.4032	.8079	.9411
.780	.6923	.4733	.8268	.9482
.728	.7669	.4528	.7684	.9252
.676	.7669	.4422	.7594	.9213
.624	.7669	.4262	.7455	.9152
.572	1.0012	.4311	.6562	.8701
.520	1.2355	.5400	.6611	.8728
.468	1.3207	.5618	.6522	.8678
.416	1.4059	.5624	.6325	.8562
.364	1.3953	.5547	.6305	.8550
.312	1.3846	.5416	.6254	.8520
.260	1.3740	.5072	.6076	.8407
.208	1.3633	.4647	.5839	.8250
.156	1.3526	.4116	.5516	.8020
.104	1.3420	.3825	.5339	.7884
.052	1.3526	.3635	.5184	.7760
0.000	1.3633	.3525	.5085	.7679
-.104	1.3420	.3910	.5398	.7930
-.156	1.3633	.4145	.5514	.8018
-.208	1.3846	.4621	.5777	.8207
-.260	1.3633	.5081	.6105	.8426
-.312	1.3846	.5369	.6227	.8503
-.364	1.2248	.5542	.6727	.8792
-.416	1.3846	.5609	.6365	.8586
-.468	1.2248	.5569	.6743	.8801
-.520	1.0651	.5021	.6866	.8866
-.572	.8947	.4156	.6815	.8840
-.624	.7243	.4251	.7661	.9242
-.676	.7669	.4374	.7552	.9195
-.728	.8095	.4523	.7475	.9161
-.780	.7136	.4520	.7959	.9364
-.832	.6177	.3983	.8030	.9392
-.884	.6177	.4036	.8083	.9413
-.936	.6177	.4143	.8189	.9453
-.988	.6390	.4298	.8201	.9457
-1.040	.6603	.4506	.8261	.9479

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(m) $x/D = 2.5$; $y/D = -.42$; $\alpha = 0^\circ$;
$p_\infty = 22.48$ psf (1076.31 N/m^2);
$q_\infty = 245.51$ psf (11755.14 N/m^2)
$p_{t,\infty} = 3192.30$ psf (152848.15 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2365	.5639	.6753	.8806
.988	1.0233	.5265	.7173	.9020
.936	.8101	.4944	.7812	.9305
.884	.7675	.4635	.7771	.9288
.832	.7249	.4432	.7819	.9308
.780	.6822	.4256	.7898	.9340
.728	.6396	.4106	.8013	.9385
.676	.6289	.4002	.7977	.9371
.624	.6183	.3925	.7968	.9368
.572	.5650	.3805	.8206	.9459
.520	.5117	.3605	.8393	.9527
.468	.5117	.3365	.8109	.9422
.416	.5117	.3179	.7882	.9333
.364	.8315	.3873	.6825	.8845
.312	1.1513	.5660	.7012	.8941
.260	1.2685	.5631	.6663	.8757
.208	1.3858	.5602	.6358	.8582
.156	1.4071	.5517	.6262	.8524
.104	1.4284	.5458	.6182	.8474
.052	1.4178	.5221	.6068	.8403
0.000	1.4071	.4716	.5790	.8216
-.104	1.4071	.5443	.6220	.8498
-.156	1.4284	.5465	.6185	.8477
-.208	1.4497	.5486	.6152	.8456
-.260	1.0127	.5620	.7450	.9149
-.312	1.0340	.5615	.7369	.9113
-.364	.9914	.2822	.5336	.7882
-.416	.6183	.3130	.7115	.8992
-.468	.5756	.3353	.7633	.9230
-.520	.5330	.3577	.8192	.9454
-.572	.5436	.3814	.8376	.9521
-.624	.5543	.3945	.8436	.9542
-.676	.5863	.4017	.8278	.9485
-.728	.6183	.4089	.8133	.9431
-.780	.6609	.4213	.7984	.9374
-.832	.7035	.4442	.7946	.9359
-.884	.7462	.4698	.7935	.9355
-.936	.7888	.5008	.7968	.9368
-.988	.8315	.5291	.7977	.9371
-1.040	.8741	.5707	.8080	.9411

(n) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^\circ$;
$p_\infty = 22.47$ psf (1075.66 N/m^2);
$q_\infty = 245.37$ psf (11748.14 N/m^2);
$p_{t,\infty} = 3190.40$ psf (152757.18 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0570	.4549	.6560	.8700
.988	.9446	.5040	.7305	.9083
.936	.8322	.4829	.7618	.9223
.884	.7872	.4587	.7633	.9230
.832	.7422	.4471	.7762	.9284
.780	.7815	.4307	.7424	.9138
.728	.8209	.5590	.8252	.9476
.676	1.0064	.5601	.7460	.9154
.624	1.1920	.5472	.6775	.8818
.572	1.2032	.5385	.6690	.8772
.520	1.2145	.5326	.6622	.8735
.468	1.2032	.5244	.6602	.8723
.416	1.1920	.5134	.6563	.8701
.364	1.1808	.5025	.6523	.8679
.312	1.1695	.4858	.6445	.8634
.260	1.1526	.4553	.6285	.8538
.208	1.1358	.4276	.6136	.8446
.156	1.1301	.3968	.5925	.8309
.104	1.1245	.3758	.5781	.8210
.052	1.1245	.3603	.5660	.8125
0.000	1.1245	.3532	.5605	.8085
-.104	1.1245	.3864	.5862	.8266
-.156	1.1470	.3999	.5905	.8295
-.208	1.1695	.4276	.6046	.8388
-.260	1.1470	.4619	.6346	.8575
-.312	1.1695	.4853	.6442	.8632
-.364	1.1751	.5035	.6546	.8692
-.416	1.1695	.5135	.6626	.8737
-.468	1.1751	.5204	.6655	.8753
-.520	1.1807	.5302	.6701	.8778
-.572	1.1976	.5368	.6695	.8775
-.624	1.2145	.5448	.6698	.8776
-.676	.9783	.5590	.7559	.9198
-.728	.7422	.4409	.7707	.9261
-.780	.7422	.4324	.7633	.9230
-.832	.7422	.4437	.7732	.9272
-.884	.7647	.4629	.7780	.9292
-.936	.7872	.4863	.7860	.9324
-.988	.7084	.5093	.8478	.9557
-1.040	.6297	.4535	.8486	.9559

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(o) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 22.46$ psf (1075.23 N/m^2);
$q_\infty = 245.27$ psf (11743.35 N/m^2);
$p_{t,\infty} = 3189.10$ psf (152694.93 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.4712	.6387	.6589	.8716
.988	1.2793	.6007	.6853	.8859
.936	1.0874	.5708	.7245	.9055
.884	1.0661	.5473	.7165	.9016
.832	1.0448	.5371	.7170	.9019
.780	1.0341	.5214	.7101	.8985
.728	1.0235	.5110	.7066	.8968
.676	1.0235	.5003	.6992	.8931
.624	1.0235	.4923	.6936	.8902
.572	1.0235	.4843	.6879	.8873
.520	1.0235	.4790	.6841	.8853
.468	1.0021	.4715	.6859	.8863
.416	.9808	.4614	.6858	.8862
.364	.9702	.4483	.6798	.8830
.312	.9595	.4325	.6714	.8785
.260	.9595	.4112	.6546	.8692
.208	.9595	.3952	.6418	.8618
.156	.9488	.3741	.6279	.8535
.104	.9382	.3610	.6203	.8488
.052	.9382	.3477	.6088	.8415
0.000	.9382	.3423	.6041	.8385
−.104	.9382	.3641	.6230	.8505
−.156	.9488	.3745	.6283	.8537
−.208	.9595	.3930	.6400	.8607
−.260	.9488	.4120	.6589	.8716
−.312	.9595	.4304	.6697	.8776
−.364	.9595	.4464	.6821	.8842
−.416	.9595	.4598	.6922	.8895
−.468	.9595	.4651	.6962	.8916
−.520	.9595	.4731	.7022	.8946
−.572	.9702	.4809	.7040	.8955
−.624	.9808	.4859	.7039	.8954
−.676	.9915	.4937	.7056	.8963
−.728	1.0021	.5041	.7092	.8981
−.780	1.0021	.5121	.7149	.9009
−.832	1.0021	.5255	.7241	.9053
−.884	1.0341	.5434	.7249	.9057
−.936	1.0661	.5693	.7307	.9084
−.988	1.0661	.5986	.7493	.9169
−1.040	1.0661	.6360	.7724	.9268

(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^\circ$;

$p_\infty = 22.47$ psf (1075.77 N/m^2);
$q_\infty = 245.39$ psf (11749.25 N/m^2);
$p_{t,\infty} = 3190.70$ psf (152771.54 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	2.0024	1.4488	.8506	.9566
.988	1.8319	1.4449	.8881	.9690
.936	1.6615	1.4410	.9313	.9819
.884	1.6402	1.4361	.9357	.9832
.832	1.6189	1.4287	.9394	.9842
.780	1.6083	1.4183	.9391	.9841
.728	1.5976	1.4105	.9396	.9843
.676	1.5976	1.3999	.9361	.9833
.624	1.5976	1.3946	.9343	.9828
.572	1.6083	1.3863	.9284	.9811
.520	1.6189	1.3861	.9253	.9802
.468	1.6189	1.3781	.9226	.9794
.416	1.6189	1.3727	.9208	.9789
.364	1.5976	1.3679	.9253	.9802
.312	1.5763	1.3658	.9308	.9818
.260	1.5550	1.3636	.9364	.9834
.208	1.5337	1.3588	.9412	.9847
.156	1.5444	1.3585	.9379	.9838
.104	1.5550	1.3556	.9337	.9826
.052	1.5444	1.3585	.9379	.9838
0.000	1.5337	1.3588	.9412	.9847
−.104	1.5337	1.3470	.9372	.9836
−.156	1.5124	1.3529	.9458	.9860
−.208	1.4911	1.3560	.9536	.9881
−.260	1.4592	1.3594	.9652	.9912
−.312	1.4379	1.3680	.9754	.9939
−.364	1.4379	1.3653	.9744	.9936
−.416	1.3846	1.3692	.9944	.9986
−.468	1.3846	1.3799	.9983	.9996
−.520	1.3846	1.3825	.9993	.9998
−.572	1.4805	1.3829	.9665	.9916
−.624	1.5763	1.3860	.9377	.9837
−.676	1.5976	1.3935	.9339	.9827
−.728	1.6189	1.3983	.9294	.9814
−.780	1.5763	1.4046	.9440	.9855
−.832	1.5337	1.4057	.9573	.9891
−.884	1.5870	1.4204	.9461	.9861
−.936	1.6402	1.4298	.9336	.9826
−.988	1.6402	1.4378	.9363	.9833
−1.040	1.6402	1.4458	.9389	.9841

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^\circ$;

p_∞ = 22.48 psf (1076.17 N/m^2);
q_∞ = 245.48 psf (11753.66 N/m^2);
$p_{t,\infty}$ = 3191.90 psf (152829.00 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3851	.9625	.8336	.9506
.988	1.1826	.9540	.8982	.9721
.936	.9802	.9482	.9836	.9959
.884	.9589	.9381	.9891	.9973
.832	.9376	.9306	.9963	.9991
.780	.9269	.9202	.9964	.9991
.728	.9163	.9098	.9965	.9991
.676	.9056	.9021	.9980	.9995
.624	.8950	.8943	.9997	.9999
.572	.8950	.8864	.9952	.9988
.520	.8950	.8784	.9907	.9977
.468	.8736	.8736	.9999	1.0000
.416	.8523	.8661	1.0080	1.0019
.364	.8523	.8607	1.0049	1.0012
.312	.8523	.8554	1.0018	1.0004
.260	.8417	.8504	1.0051	1.0012
.208	.8310	.8506	1.0117	1.0028
.156	.8310	.8479	1.0101	1.0024
.104	.8310	.8453	1.0085	1.0021
.052	.8310	.8426	1.0070	1.0017
0.000	.8310	.8426	1.0070	1.0017
-.104	.8097	.8388	1.0178	1.0042
-.156	.8310	.8409	1.0059	1.0014
-.208	.8523	.8431	.9946	.9987
-.260	.8204	.8438	1.0142	1.0034
-.312	.8417	.8487	1.0041	1.0010
-.364	.8417	.8487	1.0041	1.0010
-.416	.8310	.8542	1.0139	1.0033
-.468	.8310	.8622	1.0186	1.0044
-.520	.8310	.8676	1.0217	1.0051
-.572	.8417	.8726	1.0182	1.0043
-.624	.8523	.8804	1.0163	1.0039
-.676	.8523	.8857	1.0194	1.0046
-.728	.8523	.8964	1.0255	1.0060
-.780	.8630	.9014	1.0220	1.0052
-.832	.8736	.9065	1.0186	1.0044
-.884	.9056	.9191	1.0074	1.0018
-.936	.9376	.9317	.9968	.9992
-.988	.9589	.9391	.9897	.9975
-1.040	.9802	.9493	.9841	.9961

(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0^\circ$;

p_∞ = 22.44 psf (1074.48 N/m^2);
q_∞ = 245.10 psf (11735.25 N/m^2);
$p_{t,\infty}$ = 3186.90 psf (152589.59 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1529	.7652	.8147	.9437
.988	.9501	.7567	.8924	.9704
.936	.7473	.7482	1.0006	1.0001
.884	.7259	.7380	1.0083	1.0020
.832	.7046	.7305	1.0182	1.0043
.780	.6939	.7228	1.0206	1.0049
.728	.6832	.7123	1.0211	1.0050
.676	.6832	.7043	1.0153	1.0037
.624	.6832	.6963	1.0095	1.0023
.572	.6725	.6912	1.0138	1.0033
.520	.6619	.6835	1.0162	1.0039
.468	.6405	.6787	1.0293	1.0069
.416	.6192	.6738	1.0432	1.0100
.364	.6192	.6658	1.0370	1.0086
.312	.6192	.6632	1.0349	1.0081
.260	.6192	.6578	1.0307	1.0072
.208	.6192	.6551	1.0286	1.0067
.156	.6192	.6525	1.0265	1.0063
.104	.6192	.6498	1.0244	1.0058
.052	.6192	.6471	1.0223	1.0053
0.000	.6192	.6471	1.0223	1.0053
-.104	.6192	.6506	1.0250	1.0059
-.156	.6298	.6503	1.0161	1.0038
-.208	.6405	.6527	1.0095	1.0023
-.260	.6405	.6554	1.0115	1.0028
-.312	.6512	.6551	1.0030	1.0007
-.364	.6405	.6581	1.0136	1.0032
-.416	.6619	.6602	.9988	.9997
-.468	.6512	.6685	1.0132	1.0032
-.520	.6405	.6714	1.0238	1.0056
-.572	.6405	.6821	1.0319	1.0075
-.624	.6405	.6874	1.0360	1.0084
-.676	.6405	.6955	1.0420	1.0097
-.728	.6405	.7035	1.0480	1.0110
-.780	.6512	.7112	1.0451	1.0104
-.832	.6619	.7163	1.0403	1.0094
-.884	.6832	.7265	1.0312	1.0073
-.936	.7046	.7394	1.0244	1.0058
-.988	.7153	.7471	1.0220	1.0052
-1.040	.7259	.7576	1.0216	1.0051

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^\circ$;

$p_\infty = 22.44$ psf (1074.38 N/m^2);
$q_\infty = 245.07$ psf (11734.15 N/m^2);
$p_{t,\infty} = 3186.60$ psf (152575.23 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1320	.7614	.8201	.9457
.988	1.0679	.8375	.8856	.9682
.936	1.0038	.8177	.9025	.9735
.884	1.0145	.7881	.8814	.9669
.832	1.0252	.7666	.8647	.9614
.780	1.0145	.7402	.8542	.9579
.728	1.0038	.7138	.8433	.9541
.676	1.0038	.6925	.8306	.9495
.624	1.0038	.6712	.8177	.9448
.572	1.0038	.6525	.8063	.9405
.520	1.0038	.6366	.7963	.9366
.468	.9825	.6238	.7968	.9368
.416	.9611	.6083	.7956	.9363
.364	.9611	.5923	.7850	.9321
.312	.9611	.5816	.7779	.9291
.260	.9504	.5712	.7753	.9280
.208	.9397	.5662	.7762	.9284
.156	.9397	.5608	.7725	.9269
.104	.9397	.5555	.7688	.9253
.052	.9504	.5552	.7643	.9234
0.000	.9611	.5523	.7581	.9207
−.104	.9397	.5521	.7665	.9243
−.156	.9504	.5545	.7638	.9232
−.208	.9611	.5596	.7631	.9229
−.260	.9397	.5655	.7757	.9282
−.312	.9504	.5732	.7766	.9286
−.364	.9504	.5812	.7820	.9308
−.416	.9397	.5949	.7956	.9363
−.468	.9397	.6082	.8045	.9398
−.520	.9397	.6269	.8168	.9445
−.572	.9611	.6451	.8193	.9454
−.624	.9825	.6607	.8200	.9457
−.676	.9825	.6820	.8332	.9505
−.728	.9825	.7061	.8478	.9556
−.780	.9825	.7302	.8621	.9605
−.832	.9825	.7515	.8746	.9647
−.884	1.0145	.7775	.8754	.9649
−.936	1.0465	.8035	.8762	.9652
−.988	.8970	.8257	.9594	.9897
−1.040	.7475	.6529	.9346	.9829

(t) $x/D = 5.0$; $y/D = .83$; $\alpha = 0^\circ$;

$p_\infty = 22.43$ psf (1073.98 N/m^2);
$q_\infty = 244.98$ psf (11729.73 N/m^2);
$p_{t,\infty} = 3185.40$ psf (152517.77 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.4315	.7864	.7412	.9132
.988	1.2285	.7513	.7820	.9308
.936	1.0256	.7269	.8419	.9536
.884	1.0149	.6952	.8276	.9485
.832	1.0042	.6714	.8177	.9448
.780	.9935	.6451	.8058	.9403
.728	.9828	.6187	.7934	.9354
.676	.9721	.5976	.7840	.9316
.624	.9615	.5792	.7761	.9284
.572	.9615	.5605	.7635	.9231
.520	.9615	.5472	.7544	.9191
.468	.9508	.5368	.7514	.9178
.416	.9401	.5264	.7483	.9164
.364	.9401	.5157	.7407	.9130
.312	.9401	.5104	.7368	.9112
.260	.9294	.5027	.7354	.9106
.208	.9187	.5002	.7379	.9117
.156	.9187	.4949	.7340	.9099
.104	.9187	.4922	.7320	.9090
.052	.9294	.4920	.7276	.9069
0.000	.9401	.4917	.7232	.9049
−.104	.9187	.4913	.7313	.9087
−.156	.9294	.4937	.7288	.9075
−.208	.9401	.4934	.7245	.9055
−.260	.9187	.4993	.7372	.9114
−.312	.9294	.5044	.7367	.9112
−.364	.9294	.5071	.7386	.9121
−.416	.9187	.5154	.7490	.9167
−.468	.9187	.5261	.7567	.9201
−.520	.9187	.5394	.7663	.9242
−.572	.9294	.5526	.7711	.9263
−.624	.9401	.5683	.7775	.9290
−.676	.9508	.5868	.7856	.9323
−.728	.9615	.6106	.7969	.9368
−.780	.9615	.6320	.8108	.9422
−.832	.9615	.6561	.8261	.9479
−.884	.9935	.6847	.8302	.9494
−.936	1.0256	.7134	.8340	.9508
−.988	1.0362	.7398	.8450	.9547
−1.040	1.0469	.7690	.8571	.9588

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(u) $x/D = 5.0$; $y/D = .63$; $\alpha = 0°$;

$p_\infty = 22.46$ psf (1075.39 N/m^2);
$q_\infty = 245.30$ psf (11745.19 N/m^2);
$p_{t,\infty} = 3189.60$ psf (152718.87 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3869	.6921	.7064	.8967
.988	1.1949	.6541	.7399	.9126
.936	1.0029	.6268	.7905	.9343
.884	.9815	.5953	.7788	.9295
.832	.9602	.5718	.7717	.9265
.780	.9495	.5507	.7615	.9222
.728	.9389	.5323	.7529	.9185
.676	.9389	.5162	.7415	.9134
.624	.9389	.5029	.7319	.9089
.572	.9389	.4949	.7260	.9062
.520	.9389	.4869	.7201	.9034
.468	.9282	.4818	.7205	.9036
.416	.9175	.4741	.7188	.9028
.364	.9068	.4690	.7191	.9029
.312	.8962	.4639	.7195	.9031
.260	.8962	.4586	.7153	.9011
.208	.8962	.4532	.7111	.8990
.156	.8962	.4479	.7069	.8970
.104	.8962	.4452	.7048	.8959
.052	.8962	.4426	.7027	.8949
0.000	.8962	.4426	.7027	.8949
-.104	.8748	.4436	.7121	.8995
-.156	.8855	.4460	.7097	.8983
-.208	.8962	.4484	.7074	.8972
-.260	.8855	.4540	.7160	.9014
-.312	.8962	.4591	.7157	.9013
-.364	.8962	.4618	.7178	.9023
-.416	.8962	.4698	.7240	.9053
-.468	.8962	.4751	.7281	.9072
-.520	.8962	.4805	.7322	.9091
-.572	.9068	.4882	.7337	.9098
-.624	.9175	.4987	.7372	.9114
-.676	.9175	.5093	.7451	.9150
-.728	.9175	.5254	.7567	.9201
-.780	.9282	.5438	.7654	.9239
-.832	.9389	.5623	.7739	.9275
-.884	.9602	.5885	.7828	.9312
-.936	.9815	.6173	.7931	.9353
-.988	1.0029	.6462	.8027	.9391
-1.040	1.0242	.6804	.8150	.9438

(v) $x/D = 5.0$; $y/D = .42$; $\alpha = 0°$;

$p_\infty = 22.45$ psf (1074.99 N/m^2);
$q_\infty = 245.21$ psf (11740.78 N/m^2);
$p_{t,\infty} = 3188.40$ psf (152661.41 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3658	.6174	.6724	.8790
.988	1.1631	.5824	.7076	.8973
.936	.9603	.5607	.7641	.9233
.884	.9497	.5342	.7500	.9172
.832	.9390	.5212	.7450	.9149
.780	.9390	.5052	.7335	.9097
.728	.9390	.4918	.7237	.9051
.676	.9283	.4814	.7201	.9034
.624	.9177	.4737	.7185	.9026
.572	.9177	.4657	.7124	.8996
.520	.9177	.4604	.7083	.8976
.468	.9070	.4526	.7064	.8967
.416	.8963	.4449	.7045	.8958
.364	.8856	.4371	.7026	.8948
.312	.8750	.4267	.6984	.8927
.260	.8643	.4110	.6896	.8882
.208	.8536	.3979	.6827	.8846
.156	.8536	.3846	.6712	.8784
.104	.8536	.3739	.6618	.8732
.052	.8536	.3685	.6571	.8706
0.000	.8536	.3659	.6547	.8692
-.104	.8536	.3743	.6622	.8735
-.156	.8643	.3847	.6672	.8762
-.208	.8750	.3978	.6743	.8801
-.260	.8643	.4115	.6900	.8884
-.312	.8750	.4246	.6966	.8918
-.364	.8750	.4326	.7031	.8951
-.416	.8750	.4406	.7096	.8983
-.468	.8750	.4486	.7160	.9014
-.520	.8750	.4566	.7224	.9045
-.572	.8856	.4617	.7220	.9043
-.624	.8963	.4694	.7237	.9051
-.676	.8963	.4774	.7298	.9080
-.728	.8963	.4881	.7380	.9117
-.780	.9070	.5012	.7434	.9142
-.832	.9177	.5143	.7486	.9166
-.884	.9390	.5351	.7549	.9193
-.936	.9603	.5560	.7609	.9219
-.988	.9817	.5795	.7683	.9251
-1.040	1.0030	.6110	.7805	.9302

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(w) $x/D = 5.0$; $y/D = .21$; $\alpha = 0^\circ$;

p_∞ = 22.46 psf (1075.39 N/m^2);
q_∞ = 245.30 psf (11745.19 N/m^2);
$p_{t,\infty}$ = 3189.60 psf (152718.87 N/m^2);

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3659	.5885	.6564	.8702
.988	1.1632	.5615	.6948	.8908
.936	.9604	.5424	.7515	.9178
.884	.9497	.5186	.7390	.9122
.832	.9391	.5082	.7357	.9107
.780	.9284	.4978	.7323	.9091
.728	.9177	.4847	.7268	.9066
.676	.9071	.4716	.7211	.9039
.624	.8964	.4612	.7173	.9020
.572	.8964	.4532	.7111	.8990
.520	.8964	.4452	.7048	.8959
.468	.8857	.4348	.7006	.8938
.416	.8750	.4244	.6964	.8917
.364	.8644	.4113	.6898	.8883
.312	.8537	.3955	.6807	.8835
.260	.8430	.3718	.6641	.8745
.208	.8324	.3533	.6515	.8674
.156	.8324	.3373	.6366	.8587
.104	.8324	.3266	.6264	.8526
.052	.8324	.3213	.6213	.8494
0.000	.8324	.3186	.6187	.8478
−.104	.8324	.3293	.6290	.8541
−.156	.8430	.3370	.6323	.8561
−.208	.8537	.3555	.6453	.8638
−.260	.8430	.3744	.6665	.8758
−.312	.8537	.3955	.6807	.8835
−.364	.8537	.4142	.6966	.8918
−.416	.8537	.4249	.7055	.8963
−.468	.8537	.4329	.7121	.8995
−.520	.8537	.4436	.7208	.9037
−.572	.8644	.4513	.7226	.9046
−.624	.8750	.4618	.7264	.9064
−.676	.8857	.4695	.7281	.9072
−.728	.8964	.4826	.7337	.9098
−.780	.8964	.4906	.7398	.9126
−.832	.8964	.5039	.7498	.9171
−.884	.9177	.5168	.7504	.9173
−.936	.9391	.5376	.7566	.9201
−.988	.9604	.5557	.7607	.9219
−1.040	.9818	.5819	.7699	.9258

(x) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^\circ$;

p_∞ = 22.44 psf (1074.45 N/m^2);
q_∞ = 245.09 psf (11734.88 N/m^2);
$p_{t,\infty}$ = 3186.80 psf (152584.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3662	.5777	.6503	.8667
.988	1.1634	.5507	.6880	.8873
.936	.9606	.5289	.7420	.9136
.884	.9499	.5105	.7331	.9095
.832	.9392	.5001	.7297	.9079
.780	.9286	.4897	.7262	.9063
.728	.9179	.4766	.7206	.9036
.676	.9072	.4689	.7189	.9028
.624	.8966	.4638	.7192	.9030
.572	.8859	.4560	.7175	.9021
.520	.8752	.4483	.7157	.9013
.468	.8645	.4432	.7160	.9014
.416	.8539	.4328	.7120	.8994
.364	.8539	.4221	.7031	.8951
.312	.8539	.4088	.6919	.8894
.260	.8432	.3904	.6804	.8834
.208	.8325	.3746	.6708	.8782
.156	.8325	.3613	.6587	.8715
.104	.8325	.3506	.6489	.8659
.052	.8325	.3399	.6390	.8601
0.000	.8325	.3372	.6364	.8586
−.104	.8325	.3537	.6518	.8676
−.156	.8432	.3614	.6547	.8692
−.208	.8539	.3772	.6646	.8748
−.260	.8432	.3935	.6831	.8848
−.312	.8539	.4039	.6878	.8872
−.364	.8539	.4199	.7013	.8942
−.416	.8539	.4333	.7124	.8996
−.468	.8539	.4387	.7167	.9018
−.520	.8539	.4440	.7211	.9039
−.572	.8645	.4517	.7229	.9047
−.624	.8752	.4568	.7225	.9045
−.676	.8752	.4622	.7267	.9065
−.728	.8752	.4729	.7350	.9104
−.780	.8859	.4806	.7366	.9111
−.832	.8966	.4910	.7401	.9127
−.884	.9179	.5065	.7429	.9140
−.936	.9392	.5247	.7474	.9160
−.988	.9606	.5429	.7518	.9180
−1.040	.9819	.5718	.7631	.9229

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(y) $x/D = 5.0$; $y/D = -.42$; $\alpha = 0^\circ$;
$p_\infty = 22.45$ psf (1074.75 N/m^2);
$q_\infty = 245.16$ psf (11738.20 N/m^2);
$p_{t,\infty} = 3187.70$ psf (152627.90 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3664	.6282	.6780	.8821
.988	1.1636	.5958	.7156	.9012
.936	.9608	.5687	.7694	.9256
.884	.9501	.5396	.7537	.9188
.832	.9394	.5239	.7468	.9157
.780	.9287	.5028	.7358	.9108
.728	.9181	.4844	.7264	.9064
.676	.9074	.4713	.7207	.9037
.624	.8967	.4609	.7170	.9019
.572	.8967	.4503	.7086	.8978
.520	.8967	.4369	.6980	.8925
.468	.8860	.4238	.6916	.8892
.416	.8754	.4108	.6850	.8858
.364	.8754	.4241	.6961	.8915
.312	.8754	.4241	.6961	.8915
.260	.8647	.4244	.7006	.8938
.208	.8540	.4220	.7029	.8950
.156	.8433	.4142	.7008	.8939
.104	.8327	.4118	.7033	.8951
.052	.8327	.3958	.6895	.8881
0.000	.8327	.3798	.6754	.8807
-.104	.8327	.4123	.7037	.8953
-.156	.8433	.4120	.6990	.8930
-.208	.8540	.4171	.6989	.8929
-.260	.8433	.4200	.7057	.8964
-.312	.8540	.4225	.7033	.8952
-.364	.8433	.4174	.7035	.8953
-.416	.8540	.4091	.6921	.8895
-.468	.8433	.4174	.7035	.8953
-.520	.8327	.4337	.7217	.9041
-.572	.8433	.4467	.7278	.9071
-.624	.8540	.4572	.7317	.9088
-.676	.8647	.4703	.7375	.9115
-.728	.8754	.4833	.7431	.9141
-.780	.8754	.4994	.7553	.9195
-.832	.8754	.5207	.7713	.9264
-.884	.9074	.5386	.7705	.9260
-.936	.9394	.5646	.7752	.9280
-.988	.9608	.5907	.7841	.9317
-1.040	.9821	.6249	.7977	.9371

(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^\circ$;
$p_\infty = 22.45$ psf (1074.82 N/m^2);
$q_\infty = 245.17$ psf (11738.93 N/m^2);
$p_{t,\infty} = 3187.90$ psf (152637.47 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3026	.5503	.6500	.8665
.988	1.0997	.5259	.6915	.8892
.936	.8969	.5095	.7537	.9188
.884	.8862	.4937	.7464	.9156
.832	.8755	.4860	.7450	.9150
.780	.8755	.4753	.7368	.9112
.728	.8755	.4646	.7285	.9074
.676	.8648	.4569	.7268	.9066
.624	.8542	.4518	.7273	.9068
.572	.8435	.4467	.7277	.9070
.520	.8328	.4390	.7260	.9062
.468	.8328	.4336	.7216	.9041
.416	.8328	.4229	.7126	.8998
.364	.8328	.4123	.7036	.8953
.312	.8328	.3989	.6921	.8895
.260	.8328	.3856	.6804	.8834
.208	.8328	.3722	.6685	.8769
.156	.8221	.3591	.6609	.8727
.104	.8115	.3487	.6555	.8697
.052	.8115	.3407	.6479	.8654
0.000	.8115	.3380	.6454	.8639
-.104	.8115	.3518	.6584	.8713
-.156	.8221	.3595	.6613	.8729
-.208	.8328	.3700	.6665	.8758
-.260	.8221	.3836	.6831	.8848
-.312	.8328	.3967	.6902	.8885
-.364	.8328	.4074	.6994	.8932
-.416	.8328	.4208	.7108	.8989
-.468	.8328	.4261	.7153	.9011
-.520	.8328	.4341	.7220	.9043
-.572	.8328	.4368	.7242	.9053
-.624	.8328	.4421	.7286	.9074
-.676	.8328	.4475	.7330	.9095
-.728	.8328	.4555	.7396	.9125
-.780	.8328	.4635	.7460	.9154
-.832	.8328	.4715	.7525	.9183
-.884	.8542	.4844	.7531	.9185
-.936	.8755	.4999	.7556	.9197
-.988	.8862	.5157	.7628	.9228
-1.040	.8969	.5395	.7756	.9282

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(aa) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 22.43$ psf (1074.11 N/m^2);
$q_\infty = 245.01$ psf (11731.20 N/m^2);
$p_{t,\infty} = 3185.80$ psf (152536.93 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2604	.5484	.6596	.8720
.988	1.0682	.5238	.7002	.8936
.936	.8759	.5071	.7609	.9219
.884	.8759	.4937	.7508	.9175
.832	.8759	.4831	.7426	.9139
.780	.8652	.4753	.7412	.9132
.728	.8545	.4649	.7376	.9116
.676	.8545	.4596	.7334	.9096
.624	.8545	.4542	.7291	.9076
.572	.8438	.4492	.7296	.9079
.520	.8332	.4414	.7279	.9071
.468	.8332	.4361	.7235	.9050
.416	.8332	.4254	.7146	.9007
.364	.8332	.4147	.7055	.8963
.312	.8332	.4014	.6941	.8905
.260	.8225	.3883	.6871	.8869
.208	.8118	.3779	.6823	.8843
.156	.8118	.3645	.6701	.8778
.104	.8118	.3538	.6602	.8723
.052	.8118	.3485	.6552	.8695
0.000	.8118	.3458	.6527	.8681
-.104	.8118	.3520	.6585	.8714
-.156	.8225	.3624	.6638	.8744
-.208	.8332	.3729	.6690	.8772
-.260	.8225	.3838	.6832	.8848
-.312	.8332	.3943	.6879	.8873
-.364	.8225	.4079	.7043	.8956
-.416	.8332	.4184	.7086	.8978
-.468	.8225	.4267	.7202	.9035
-.520	.8118	.4323	.7297	.9079
-.572	.8118	.4349	.7320	.9090
-.624	.8118	.4403	.7365	.9111
-.676	.8118	.4456	.7409	.9131
-.728	.8118	.4510	.7453	.9151
-.780	.8118	.4590	.7519	.9180
-.832	.8118	.4644	.7563	.9200
-.884	.8225	.4748	.7598	.9215
-.936	.8332	.4906	.7673	.9247
-.988	.8332	.5066	.7798	.9299
-1.040	.8332	.5280	.7961	.9365

(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 22.45$ psf (1074.69 N/m^2);
$q_\infty = 245.14$ psf (11737.46 N/m^2);
$p_{t,\infty} = 3187.50$ psf (152618.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2387	.5439	.6627	.8737
.988	1.0465	.5193	.7044	.8957
.936	.8543	.5026	.7670	.9246
.884	.8436	.4868	.7597	.9214
.832	.8329	.4791	.7584	.9209
.780	.8329	.4711	.7520	.9181
.728	.8329	.4657	.7478	.9162
.676	.8436	.4601	.7385	.9120
.624	.8543	.4625	.7358	.9108
.572	.8970	.4642	.7194	.9030
.520	.9397	.4604	.7000	.8935
.468	.9717	.4677	.6937	.8903
.416	1.0038	.4696	.6840	.8852
.364	1.0251	.4690	.6764	.8812
.312	1.0465	.4632	.6653	.8752
.260	1.0465	.4471	.6537	.8686
.208	1.0465	.4391	.6478	.8653
.156	1.0572	.4201	.6304	.8550
.104	1.0678	.4092	.6190	.8480
.052	1.0678	.4012	.6129	.8442
0.000	1.0678	.3958	.6088	.8415
-.104	1.0465	.3995	.6179	.8473
-.156	1.0572	.4099	.6227	.8503
-.208	1.0678	.4230	.6294	.8544
-.260	1.0144	.4404	.6589	.8716
-.312	1.0251	.4482	.6612	.8729
-.364	.9717	.4602	.6882	.8874
-.416	.9824	.4599	.6842	.8854
-.468	.9290	.4559	.7005	.8938
-.520	.8756	.4492	.7162	.9015
-.572	.8543	.4417	.7190	.9029
-.624	.8329	.4422	.7286	.9074
-.676	.8116	.4454	.7408	.9131
-.728	.7902	.4459	.7512	.9177
-.780	.7902	.4539	.7579	.9207
-.832	.7902	.4620	.7646	.9235
-.884	.8009	.4724	.7680	.9250
-.936	.8116	.4882	.7756	.9282
-.988	.8222	.5039	.7829	.9312
-1.040	.8329	.5224	.7919	.9348

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^\circ$;

$p_\infty = 22.45$ psf (1075.06 N/m^2);
$q_\infty = 245.23$ psf (11741.51 N/m^2);
$p_{t,\infty} = 3188.60$ psf (152670.99 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3447	.9937	.8597	.9597
.988	1.1526	.9930	.9282	.9810
.936	.9605	.9922	1.0164	1.0039
.884	.9498	.9898	1.0208	1.0049
.832	.9392	.9874	1.0254	1.0060
.780	.9392	.9847	1.0240	1.0057
.728	.9392	.9821	1.0226	1.0053
.676	.9285	.9770	1.0258	1.0061
.624	.9178	.9746	1.0305	1.0071
.572	.9178	.9719	1.0291	1.0068
.520	.9178	.9666	1.0262	1.0062
.468	.9071	.9642	1.0310	1.0073
.416	.8965	.9618	1.0358	1.0083
.364	.8965	.9591	1.0343	1.0080
.312	.8965	.9564	1.0329	1.0077
.260	.8965	.9564	1.0329	1.0077
.208	.8965	.9564	1.0329	1.0077
.156	.8858	.9540	1.0378	1.0088
.104	.8751	.9543	1.0442	1.0102
.052	.8858	.9514	1.0364	1.0085
0.000	.8965	.9511	1.0300	1.0070
-.104	.8751	.9431	1.0381	1.0089
-.156	.8858	.9455	1.0332	1.0078
-.208	.8965	.9479	1.0283	1.0067
-.260	.8751	.9484	1.0410	1.0095
-.312	.8858	.9482	1.0346	1.0081
-.364	.8751	.9484	1.0410	1.0095
-.416	.8751	.9484	1.0410	1.0095
-.468	.8644	.9487	1.0476	1.0110
-.520	.8538	.9516	1.0557	1.0127
-.572	.8644	.9514	1.0491	1.0113
-.624	.8751	.9538	1.0440	1.0102
-.676	.8751	.9591	1.0469	1.0108
-.728	.8751	.9645	1.0498	1.0114
-.780	.8858	.9669	1.0448	1.0103
-.832	.8965	.9666	1.0384	1.0089
-.884	.9178	.9741	1.0302	1.0071
-.936	.9392	.9790	1.0210	1.0050
-.988	.9498	.9814	1.0165	1.0039
-1.040	.9605	.9838	1.0121	1.0029

(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^\circ$;

$p_\infty = 22.44$ psf (1074.52 N/m^2);
$q_\infty = 245.10$ psf (11735.62 N/m^2);
$p_{t,\infty} = 3187.00$ psf (152594.38 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M^1/M^∞	V_1/V_∞
1.040	1.3869	.9799	.8406	.9531
.988	1.1948	.9792	.9053	.9743
.936	1.0028	.9784	.9878	.9970
.884	1.0028	.9731	.9851	.9963
.832	1.0028	.9677	.9824	.9956
.780	.9921	.9627	.9850	.9963
.728	.9815	.9576	.9878	.9970
.676	.9708	.9498	.9891	.9973
.624	.9601	.9474	.9934	.9984
.572	.9601	.9421	.9906	.9977
.520	.9601	.9394	.9892	.9973
.468	.9601	.9368	.9878	.9970
.416	.9601	.9314	.9849	.9963
.364	.9601	.9288	.9835	.9959
.312	.9601	.9261	.9821	.9956
.260	.9495	.9237	.9863	.9966
.208	.9388	.9239	.9921	.9981
.156	.9388	.9186	.9892	.9973
.104	.9388	.9186	.9892	.9973
.052	.9388	.9159	.9878	.9970
0.000	.9388	.9159	.9878	.9970
-.104	.9175	.9132	.9977	.9994
-.156	.9388	.9154	.9874	.9969
-.208	.9601	.9149	.9761	.9940
-.260	.9175	.9185	1.0006	1.0001
-.312	.9388	.9180	.9889	.9973
-.364	.9281	.9210	.9961	.9991
-.416	.9175	.9212	1.0020	1.0005
-.468	.9068	.9241	1.0095	1.0023
-.520	.8961	.9271	1.0171	1.0041
-.572	.9175	.9292	1.0064	1.0015
-.624	.9388	.9367	.9989	.9997
-.676	.9388	.9367	.9989	.9997
-.728	.9388	.9448	1.0032	1.0008
-.780	.9388	.9474	1.0046	1.0011
-.832	.9388	.9501	1.0060	1.0014
-.884	.9601	.9549	.9973	.9993
-.936	.9815	.9598	.9889	.9973
-.988	.9921	.9649	.9862	.9966
-1.040	1.0028	.9699	.9835	.9959

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^\circ$;
$p_\infty = 22.45$ psf (1074.72 N/m^2);
$q_\infty = 245.15$ psf (11737.83 N/m^2);
$p_{t,\infty} = 3187.60$ psf (152623.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3223	.8756	.8138	.9433
.988	1.1303	.8722	.8784	.9659
.936	.9384	.8688	.9622	.9904
.884	.9277	.8584	.9619	.9903
.832	.9171	.8533	.9646	.9911
.780	.9064	.8456	.9658	.9914
.728	.8957	.8351	.9656	.9913
.676	.8957	.8271	.9609	.9901
.624	.8957	.8191	.9563	.9888
.572	.8957	.8138	.9532	.9880
.520	.8957	.8085	.9500	.9871
.468	.8851	.8007	.9511	.9875
.416	.8744	.7956	.9539	.9882
.364	.8744	.7876	.9491	.9869
.312	.8744	.7823	.9458	.9860
.260	.8744	.7769	.9426	.9851
.208	.8744	.7716	.9394	.9842
.156	.8744	.7689	.9377	.9838
.104	.8744	.7663	.9361	.9833
.052	.8744	.7636	.9345	.9828
0.000	.8744	.7636	.9345	.9828
-.104	.8531	.7596	.9436	.9854
-.156	.8744	.7618	.9334	.9825
-.208	.8957	.7640	.9235	.9797
-.260	.8531	.7677	.9486	.9868
-.312	.8744	.7725	.9399	.9844
-.364	.8744	.7725	.9399	.9844
-.416	.8531	.7757	.9535	.9881
-.468	.8531	.7837	.9585	.9894
-.520	.8531	.7890	.9617	.9903
-.572	.8531	.7970	.9666	.9916
-.624	.8531	.8051	.9714	.9928
-.676	.8531	.8104	.9747	.9937
-.728	.8531	.8184	.9795	.9949
-.780	.8638	.8235	.9764	.9941
-.832	.8744	.8286	.9734	.9934
-.884	.8957	.8361	.9661	.9915
-.936	.9171	.8463	.9606	.9900
-.988	.9171	.8516	.9636	.9908
-1.040	.9171	.8596	.9682	.9920

(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^\circ$;
$p_\infty = 22.44$ psf (1074.45 N/m^2);
$q_\infty = 245.09$ psf (11734.88 N/m^2);
$p_{t,\infty} = 3186.80$ psf (152584.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2600	.7448	.7688	.9253
.988	1.0678	.7281	.8258	.9478
.936	.8756	.7141	.9031	.9736
.884	.8756	.6955	.8912	.9700
.832	.8756	.6821	.8826	.9673
.780	.8649	.6638	.8760	.9651
.728	.8543	.6427	.8674	.9623
.676	.8543	.6267	.8565	.9587
.624	.8543	.6107	.8455	.9549
.572	.8649	.5998	.8328	.9503
.520	.8756	.5863	.8183	.9450
.468	.8649	.5732	.8141	.9434
.416	.8543	.5628	.8117	.9425
.364	.8543	.5495	.8020	.9388
.312	.8543	.5415	.7962	.9365
.260	.8436	.5338	.7954	.9362
.208	.8329	.5287	.7967	.9367
.156	.8329	.5234	.7927	.9351
.104	.8329	.5207	.7907	.9343
.052	.8436	.5151	.7814	.9306
0.000	.8543	.5149	.7763	.9285
-.104	.8329	.5145	.7859	.9324
-.156	.8436	.5142	.7808	.9303
-.208	.8543	.5166	.7777	.9290
-.260	.8329	.5198	.7900	.9341
-.312	.8436	.5249	.7888	.9336
-.364	.8436	.5276	.7908	.9344
-.416	.8329	.5385	.8041	.9396
-.468	.8329	.5466	.8101	.9419
-.520	.8329	.5599	.8199	.9456
-.572	.8329	.5706	.8277	.9485
-.624	.8329	.5866	.8393	.9527
-.676	.8329	.6000	.8488	.9560
-.728	.8329	.6187	.8619	.9605
-.780	.8329	.6321	.8711	.9635
-.832	.8329	.6481	.8821	.9671
-.884	.8436	.6666	.8889	.9693
-.936	.8543	.6850	.8955	.9713
-.988	.8543	.6984	.9042	.9740
-1.040	.8543	.7144	.9145	.9771

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(gg) $x/D = 8.39$; $y/D = .83$; $\alpha = 0^\circ$;

$p_\infty = 22.44$ psf (1074.62 N/m^2);
$q_\infty = 245.13$ psf (11736.73 N/m^2);
$p_{t,\infty} = 3187.30$ psf (152608.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2592	.6896	.7400	.9127
.988	1.0672	.6702	.7925	.9351
.936	.8751	.6508	.8624	.9606
.884	.8644	.6298	.8536	.9576
.832	.8537	.6114	.8462	.9551
.780	.8537	.5927	.8332	.9505
.728	.8537	.5714	.8181	.9449
.676	.8537	.5554	.8066	.9406
.624	.8537	.5394	.7949	.9360
.572	.8537	.5287	.7870	.9328
.520	.8537	.5180	.7790	.9296
.468	.8431	.5076	.7760	.9283
.416	.8324	.4999	.7750	.9279
.364	.8324	.4919	.7687	.9253
.312	.8324	.4866	.7646	.9235
.260	.8324	.4786	.7582	.9208
.208	.8324	.4759	.7561	.9199
.156	.8324	.4732	.7540	.9189
.104	.8324	.4706	.7519	.9180
.052	.8324	.4679	.7497	.9171
0.000	.8324	.4679	.7497	.9171
-.104	.8324	.4663	.7485	.9165
-.156	.8431	.4660	.7435	.9143
-.208	.8537	.4685	.7408	.9130
-.260	.8324	.4690	.7506	.9174
-.312	.8431	.4714	.7478	.9162
-.364	.8324	.4743	.7549	.9193
-.416	.8324	.4797	.7591	.9212
-.468	.8217	.4879	.7706	.9261
-.520	.8110	.4962	.7822	.9309
-.572	.8217	.5067	.7852	.9321
-.624	.8324	.5171	.7882	.9333
-.676	.8324	.5305	.7983	.9374
-.728	.8324	.5465	.8103	.9420
-.780	.8324	.5625	.8221	.9464
-.832	.8324	.5786	.8337	.9507
-.884	.8324	.5999	.8490	.9561
-.936	.8324	.6213	.8640	.9612
-.988	.8431	.6371	.8693	.9629
-1.040	.8537	.6582	.8780	.9658

(hh) $x/D = 8.39$; $y/D = .63$; $\alpha = 0^\circ$;

$p_\infty = 22.45$ psf (1074.72 N/m^2);
$q_\infty = 245.15$ psf (11737.83 N/m^2);
$p_{t,\infty} = 3187.60$ psf (152623.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2591	.6328	.7089	.8979
.988	1.0777	.6079	.7510	.9176
.936	.8963	.5856	.8083	.9412
.884	.8857	.5619	.7965	.9367
.832	.8750	.5462	.7901	.9341
.780	.8643	.5278	.7814	.9306
.728	.8536	.5094	.7725	.9269
.676	.8536	.4961	.7623	.9226
.624	.8536	.4881	.7562	.9199
.572	.8536	.4801	.7499	.9172
.520	.8536	.4748	.7458	.9153
.468	.8430	.4670	.7443	.9146
.416	.8323	.4620	.7450	.9150
.364	.8323	.4540	.7385	.9120
.312	.8323	.4487	.7342	.9100
.260	.8323	.4433	.7298	.9080
.208	.8323	.4380	.7254	.9059
.156	.8323	.4327	.7210	.9038
.104	.8323	.4273	.7165	.9017
.052	.8323	.4247	.7143	.9006
0.000	.8323	.4247	.7143	.9006
-.104	.8323	.4235	.7133	.9001
-.156	.8430	.4232	.7086	.8978
-.208	.8536	.4283	.7083	.8977
-.260	.8323	.4315	.7200	.9034
-.312	.8430	.4366	.7197	.9032
-.364	.8430	.4393	.7219	.9042
-.416	.8323	.4449	.7311	.9086
-.468	.8323	.4502	.7355	.9106
-.520	.8323	.4556	.7398	.9126
-.572	.8323	.4609	.7442	.9146
-.624	.8323	.4689	.7506	.9174
-.676	.8323	.4770	.7570	.9203
-.728	.8323	.4876	.7654	.9239
-.780	.8323	.4983	.7738	.9274
-.832	.8323	.5144	.7861	.9325
-.884	.8323	.5331	.8003	.9381
-.936	.8323	.5544	.8162	.9442
-.988	.8430	.5756	.8263	.9480
-1.040	.8536	.5967	.8361	.9515

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(ii) $x/D = 8.39$; $y/D = .42$; $\alpha = 0^\circ$;
$p_\infty = 22.46$ psf (1075.16 N/m^2);
$q_\infty = 245.25$ psf (11742.62 N/m^2);
$p_{t,\infty} = 3188.90$ psf (152685.35 N/m^2).

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2586	.5779	.6776	.8819
.988	1.0666	.5532	.7202	.9034
.936	.8746	.5339	.7813	.9305
.884	.8746	.5125	.7655	.9239
.832	.8746	.4992	.7555	.9196
.780	.8640	.4861	.7501	.9172
.728	.8533	.4730	.7445	.9147
.676	.8533	.4650	.7382	.9119
.624	.8533	.4570	.7318	.9089
.572	.8533	.4517	.7275	.9069
.520	.8533	.4437	.7211	.9038
.468	.8426	.4386	.7214	.9040
.416	.8320	.4308	.7196	.9032
.364	.8320	.4202	.7106	.8988
.312	.8320	.4121	.7038	.8954
.260	.8320	.3988	.6923	.8896
.208	.8320	.3881	.6830	.8847
.156	.8320	.3801	.6759	.8810
.104	.8320	.3721	.6688	.8771
.052	.8320	.3667	.6639	.8744
0.000	.8320	.3667	.6639	.8744
-.104	.8320	.3694	.6664	.8758
-.156	.8320	.3748	.6712	.8784
-.208	.8320	.3828	.6783	.8822
-.260	.8320	.3908	.6854	.8860
-.312	.8320	.4015	.6947	.8908
-.364	.8213	.4097	.7063	.8967
-.416	.8320	.4175	.7084	.8977
-.468	.8213	.4258	.7200	.9033
-.520	.8106	.4314	.7295	.9078
-.572	.8106	.4367	.7340	.9099
-.624	.8106	.4447	.7407	.9130
-.676	.8106	.4500	.7451	.9150
-.728	.8106	.4580	.7517	.9179
-.780	.8213	.4685	.7552	.9195
-.832	.8320	.4789	.7587	.9210
-.884	.8320	.4922	.7692	.9255
-.936	.8320	.5109	.7836	.9315
-.988	.8320	.5269	.7958	.9364
-1.040	.8320	.5509	.8137	.9433

(jj) $x/D = 8.39$; $y/D = 0.21$; $\alpha = 0^\circ$;
$p_\infty = 22.46$ psf (1075.43 N/m^2);
$q_\infty = 245.31$ psf (11745.56 N/m^2);
$p_{t,\infty} = 3189.70$ psf (152723.66 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2583	.5611	.6678	.8765
.988	1.0664	.5338	.7075	.8973
.936	.8744	.5171	.7690	.9254
.884	.8637	.4987	.7599	.9215
.832	.8531	.4883	.7566	.9201
.780	.8424	.4753	.7511	.9177
.728	.8318	.4649	.7476	.9161
.676	.8318	.4542	.7390	.9122
.624	.8318	.4462	.7324	.9092
.572	.8531	.4430	.7206	.9036
.520	.8744	.4398	.7092	.8981
.468	.8957	.4393	.7003	.8937
.416	.9171	.4361	.6896	.8882
.364	.9491	.4353	.6773	.8817
.312	.9810	.4292	.6614	.8730
.260	.9917	.4183	.6495	.8662
.208	1.0024	.4100	.6396	.8605
.156	1.0237	.3961	.6221	.8499
.104	1.0450	.3876	.6090	.8417
.052	1.0450	.3823	.6048	.8390
0.000	1.0450	.3823	.6048	.8390
-.104	1.0237	.3864	.6144	.8451
-.156	1.0237	.3917	.6186	.8477
-.208	1.0237	.4024	.6270	.8529
-.260	.9597	.4174	.6595	.8719
-.312	.9597	.4201	.6616	.8731
-.364	.9277	.4289	.6799	.8831
-.416	.8957	.4377	.6990	.8930
-.468	.8637	.4304	.7059	.8965
-.520	.8318	.4286	.7178	.9023
-.572	.8211	.4315	.7249	.9057
-.624	.8104	.4371	.7344	.9101
-.676	.8104	.4451	.7411	.9132
-.728	.8104	.4531	.7477	.9162
-.780	.8104	.4638	.7565	.9200
-.832	.8104	.4718	.7630	.9229
-.884	.8211	.4849	.7685	.9252
-.936	.8318	.5007	.7759	.9283
-.988	.8318	.5167	.7882	.9333
-1.040	.8318	.5407	.8063	.9405

TABLE 5.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D IN THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Concluded.

(kk) x/D = 8.39; y/D = 0; $\alpha = 0^\circ$;

p_∞ = 22.46 psf (1075.43 N/m^2);
q_∞ = 245.31 psf (11745.56 N/m^2);
$p_{t,\infty}$ = 3189.70 psf (152723.66 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2367	.5483	.6658	.8755
.988	1.0874	.5386	.7038	.8954
.936	.9382	.5396	.7584	.9209
.884	.9915	.5569	.7495	.9169
.832	1.0448	.5556	.7293	.9077
.780	1.0661	.5498	.7181	.9024
.728	1.0874	.5439	.7073	.8971
.676	1.1088	.5354	.6949	.8909
.624	1.1301	.5296	.6846	.8855
.572	1.1407	.5240	.6777	.8819
.520	1.1514	.5157	.6693	.8773
.468	1.1407	.5080	.6673	.8763
.416	1.1301	.4976	.6635	.8742
.364	1.1301	.4842	.6546	.8692
.312	1.1301	.4709	.6455	.8640
.260	1.1194	.4551	.6376	.8593
.208	1.1088	.4421	.6314	.8556
.156	1.1088	.4287	.6218	.8497
.104	1.1088	.4154	.6121	.8436
.052	1.0981	.4076	.6093	.8418
0.000	1.0874	.4026	.6084	.8413
-.104	1.0874	.4089	.6132	.8443
-.156	1.0874	.4169	.6192	.8481
-.208	1.0874	.4303	.6290	.8542
-.260	1.0768	.4439	.6421	.8619
-.312	1.0768	.4573	.6517	.8675
-.364	1.0768	.4706	.6611	.8729
-.416	1.0661	.4869	.6758	.8809
-.468	1.0661	.4950	.6814	.8839
-.520	1.0661	.5030	.6869	.8868
-.572	1.0874	.5105	.6852	.8859
-.624	1.1088	.5153	.6817	.8841
-.676	1.0981	.5209	.6887	.8877
-.728	1.0874	.5265	.6958	.8914
-.780	1.0341	.5278	.7144	.9006
-.832	.9808	.5211	.7289	.9076
-.884	.9382	.5088	.7364	.9110
-.936	.8955	.5071	.7525	.9183
-.988	.8635	.5079	.7669	.9245
-1.040	.8316	.5220	.7923	.9350

(ll) x/D = 8.39; y/D = -.42; $\alpha = 0^\circ$;

p_∞ = 22.46 psf (1075.26 N/m^2);
q_∞ = 245.27 psf (11743.72 N/m^2);
$p_{t,\infty}$ = 3189.20 psf (152699.72 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.5165	.6989	.6788	.8825
.988	1.3349	.6660	.7063	.8967
.936	1.1534	.6331	.7409	.9131
.884	1.1427	.6013	.7254	.9059
.832	1.1320	.5829	.7176	.9022
.780	1.1107	.5648	.7131	.9000
.728	1.0893	.5440	.7067	.8968
.676	1.1000	.5251	.6909	.8888
.624	1.1107	.5115	.6786	.8824
.572	1.1107	.4955	.6679	.8766
.520	1.1107	.4794	.6570	.8705
.468	1.1000	.4637	.6493	.8661
.416	1.0893	.4720	.6582	.8712
.364	1.0893	.4960	.6748	.8803
.312	1.0893	.4933	.6730	.8794
.260	1.0786	.4909	.6746	.8803
.208	1.0680	.4885	.6763	.8812
.156	1.0680	.4832	.6726	.8792
.104	1.0680	.4752	.6670	.8761
.052	1.0680	.4538	.6519	.8676
0.000	1.0680	.4325	.6364	.8586
-.104	1.0680	.4522	.6507	.8670
-.156	1.0680	.4736	.6659	.8755
-.208	1.0680	.4843	.6734	.8796
-.260	1.0466	.4848	.6806	.8835
-.312	1.0466	.4875	.6825	.8845
-.364	1.0466	.4902	.6844	.8854
-.416	1.0252	.4827	.6862	.8864
-.468	1.0252	.4613	.6708	.8782
-.520	1.0252	.4640	.6727	.8792
-.572	1.0466	.4822	.6787	.8825
-.624	1.0680	.4977	.6826	.8845
-.676	1.0786	.5134	.6899	.8884
-.728	1.0893	.5319	.6988	.8929
-.780	1.0786	.5455	.7112	.8991
-.832	1.0680	.5618	.7253	.9059
-.884	1.1000	.5851	.7293	.9077
-.936	1.1320	.6110	.7347	.9102
-.988	1.1534	.6426	.7464	.9156
-1.040	1.1747	.6768	.7590	.9211

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^\circ$;

p_∞ = 222.12 psf (10635.14 N/m^2);
q_∞ = 398.04 psf (19058.17 N/m^2);
$p_{t,\infty}$ = 944.10 psf (45203.75 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7843	.9071	1.0754	1.0480
.988	.7617	.9092	1.0925	1.0584
.936	.7391	.8881	1.0962	1.0606
.884	.7121	.8893	1.1175	1.0732
.832	.6852	.8756	1.1304	1.0807
.780	.6701	.8499	1.1262	1.0783
.728	.6550	.8376	1.1308	1.0809
.676	.6162	.8307	1.1610	1.0981
.624	.5775	.5188	.9478	.9646
.572	.5688	.1011	.4216	.4964
.520	.5602	.0211	.1941	.2364
.468	.5591	.0071	.1127	.1381
.416	.5581	.0017	.0557	.0685
.364	.5559	.0029	.0726	.0892
.312	.5538	0.0000	0.0000	0.0000
.260	.5548	0.0000	0.0000	0.0000
.208	.5559	0.0000	0.0000	0.0000
.156	.5559	0.0000	0.0000	0.0000
.104	.5570	0.0000	0.0000	0.0000
.052	.5581	0.0000	0.0000	0.0000
0.000	.5581	0.0000	0.0000	0.0000
-.052	.5591	.0057	.1011	.1239
-.104	.5602	.0051	.0956	.1172
-.156	.5624	.0039	.0836	.1026
-.208	.5645	.0027	.0696	.0855
-.260	.5656	.0051	.0950	.1166
-.312	.5667	.0045	.0893	.1095
-.364	.5688	.0033	.0764	.0938
-.416	.5710	.0021	.0610	.0750
-.468	.5742	.0122	.1455	.1779
-.520	.5775	.0759	.3625	.4314
-.572	.5915	.4634	.8851	.9195
-.624	.6055	.8316	1.1720	1.1042
-.676	.6249	.8416	1.1605	1.0979
-.728	.6443	.8565	1.1530	1.0936
-.780	.6733	.8534	1.1258	1.0780
-.832	.7024	.8700	1.1129	1.0705
-.884	.7240	.8829	1.1043	1.0654
-.936	.7455	.8859	1.0901	1.0569
-.988	.7714	.9013	1.0810	1.0514
-1.040	.7972	.9052	1.0656	1.0420

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^\circ$;

p_∞ = 221.41 psf (10601.35 N/m^2);
q_∞ = 396.77 psf (18997.61 N/m^2);
$p_{t,\infty}$ = 941.10 psf (45060.11 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9122	.9357	1.0128	1.0084
.988	.8917	.9242	1.0181	1.0119
.936	.8711	.9111	1.0227	1.0148
.884	.8225	.9078	1.0506	1.0326
.832	.7738	.9027	1.0800	1.0508
.780	.7220	.8848	1.1070	1.0670
.728	.6701	.8685	1.1385	1.0854
.676	.6366	.8508	1.1561	1.0954
.624	.6031	.7719	1.1313	1.0812
.572	.5901	.4336	.8572	.8985
.520	.5771	.1774	.5543	.6336
.468	.5761	.0526	.3021	.3631
.416	.5750	.0109	.1378	.1687
.364	.5739	.0056	.0987	.1210
.312	.5728	.0032	.0747	.0918
.260	.5761	0.0000	0.0000	0.0000
.208	.5793	0.0000	0.0000	0.0000
.156	.5815	0.0000	0.0000	0.0000
.104	.5847	0.0000	0.0000	0.0000
.052	.5804	0.0000	0.0000	0.0000
0.000	.5901	0.0000	0.0000	0.0000
-.052	.5858	0.0000	0.0000	0.0000
-.104	.5815	0.0000	0.0000	0.0000
-.156	.5836	0.0000	0.0000	0.0000
-.208	.5858	0.0000	0.0000	0.0000
-.260	.5847	.0015	.0509	.0626
-.312	.5836	.0168	.1699	.2074
-.364	.5923	.0294	.2229	.2707
-.416	.6009	.1252	.4565	.5336
-.468	.6009	.3198	.7295	.7952
-.520	.6009	.6917	1.0729	1.0464
-.572	.6290	.8538	1.1651	1.1004
-.624	.6571	.8707	1.1511	1.0925
-.676	.7036	.8729	1.1139	1.0711
-.728	.7501	.8850	1.0863	1.0546
-.780	.7944	.8941	1.0609	1.0391
-.832	.8387	.8999	1.0358	1.0233
-.884	.8592	.9113	1.0299	1.0194
-.936	.8798	.9211	1.0232	1.0152
-.988	.8463	.9400	1.0539	1.0347
-1.040	.8128	.9523	1.0824	1.0523

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(c) x/D = 2.0; y/D = 0; α = 5°;

p_∞ = 221.70 psf (10614.86 N/m²);
q_∞ = 397.28 psf (19021.83 N/m²);
$p_{t,\infty}$ = 942.30 psf (45117.57 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7318	.9084	1.1141	1.0712
.988	.7200	.9070	1.1224	1.0761
.936	.7081	.8957	1.1247	1.0774
.884	.6941	.8881	1.1312	1.0812
.832	.6800	.8871	1.1422	1.0875
.780	.6854	.8813	1.1339	1.0827
.728	.6908	.8738	1.1246	1.0774
.676	.7016	.8736	1.1159	1.0723
.624	.7124	.8752	1.1084	1.0678
.572	.7157	.7951	1.0540	1.0348
.520	.7189	.5404	.8670	.9059
.468	.7200	.2805	.6242	.7008
.416	.7210	.1107	.3918	.4639
.364	.7200	.0398	.2351	.2851
.312	.7189	.0116	.1269	.1554
.260	.7232	0.0000	0.0000	0.0000
.208	.7275	0.0000	0.0000	0.0000
.156	.7221	0.0000	0.0000	0.0000
.104	.7264	0.0000	0.0000	0.0000
.052	.7178	0.0000	0.0000	0.0000
0.000	.7254	0.0000	0.0000	0.0000
-.052	.7167	0.0000	0.0000	0.0000
-.104	.7081	.0043	.0781	.0959
-.156	.7167	.0114	.1262	.1545
-.208	.7254	.0271	.1932	.2354
-.260	.7254	.0685	.3074	.3692
-.312	.7254	.1531	.4594	.5367
-.364	.7232	.2761	.6179	.6949
-.416	.7210	.5529	.8757	.9124
-.468	.7135	.8354	1.0820	1.0520
-.520	.7059	.8713	1.1110	1.0694
-.572	.6897	.8756	1.1267	1.0786
-.624	.6736	.8799	1.1430	1.0879
-.676	.6790	.8790	1.1379	1.0850
-.728	.6843	.8782	1.1328	1.0821
-.780	.6984	.8775	1.1209	1.0752
-.832	.7124	.8851	1.1146	1.0715
-.884	.7232	.8915	1.1103	1.0690
-.936	.7340	.9062	1.1111	1.0695
-.988	.7534	.9047	1.0958	1.0603
-1.040	.7729	.9097	1.0849	1.0538

(d) x/D = 2.5; y/D = 0; α = 5°;

p_∞ = 221.91 psf (10625.00 N/m²);
q_∞ = 397.66 psf (19040.00 N/m²);
$p_{t,\infty}$ = 943.20 psf (45160.66 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6664	.8966	1.1599	1.0975
.988	.7009	.8943	1.1295	1.0802
.936	.7355	.9101	1.1124	1.0702
.884	.7743	.9102	1.0842	1.0534
.832	.8131	.9186	1.0629	1.0403
.780	.8573	.9194	1.0356	1.0231
.728	.9015	.9185	1.0094	1.0062
.676	.9296	.9236	.9968	.9979
.624	.9576	.9170	.9786	.9857
.572	.9727	.8827	.9526	.9679
.520	.9878	.8113	.9063	.9350
.468	.9738	.6296	.8041	.8570
.416	.9598	.4129	.6559	.7301
.364	.9533	.2725	.5347	.6140
.312	.9468	.1182	.3534	.4212
.260	.9544	.1042	.3305	.3955
.208	.9619	.0599	.2496	.3021
.156	.9727	.0627	.2539	.3072
.104	.9803	.0863	.2967	.3569
.052	.9867	.0694	.2652	.3204
0.000	.9986	.1326	.3644	.4336
-.052	1.0051	.1774	.4201	.4947
-.104	1.0115	.2079	.4534	.5303
-.156	1.0331	.2316	.4734	.5514
-.208	1.0547	.3404	.5682	.6472
-.260	1.0439	.5183	.7046	.7736
-.312	1.0331	.7879	.8733	.9107
-.364	1.0320	.9069	.9374	.9573
-.416	1.0309	.9254	.9475	.9643
-.468	.9964	.9316	.9669	.9777
-.520	.9619	.9293	.9829	.9886
-.572	.9145	.9293	1.0081	1.0053
-.624	.8670	.9291	1.0352	1.0229
-.676	.8401	.9139	1.0430	1.0278
-.728	.8131	.9102	1.0580	1.0373
-.780	.7775	.9062	1.0796	1.0506
-.832	.7419	.9006	1.1018	1.0639
-.884	.7160	.9000	1.1211	1.0753
-.936	.6902	.9075	1.1467	1.0901
-.988	.6848	.8936	1.1424	1.0876
-1.040	.6794	.9060	1.1548	1.0946

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 221.30$ psf (10595.71 N/m^2);
$q_\infty = 396.56$ psf (18987.52 N/m^2);
$p_{t,\infty} = 940.60$ psf (45036.17 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8973	.9479	1.0278	1.0181
.988	.9557	.9563	1.0003	1.0002
.936	1.0141	.9444	.9650	.9764
.884	1.0389	.9500	.9563	.9704
.832	1.0638	.9422	.9411	.9599
.780	1.0876	.9397	.9295	.9517
.728	1.1114	.9354	.9174	.9430
.676	1.1308	.9166	.9003	.9307
.624	1.1503	.8758	.8726	.9101
.572	1.1784	.8126	.8304	.8778
.520	1.2065	.7244	.7749	.8333
.468	1.1892	.6267	.7259	.7921
.416	1.1719	.4709	.6339	.7098
.364	1.1654	.3759	.5680	.6470
.312	1.1590	.3489	.5486	.6280
.260	1.1644	.3320	.5340	.6134
.208	1.1698	.3387	.5381	.6175
.156	1.2108	.3435	.5327	.6120
.104	1.2163	.3736	.5542	.6335
.052	1.2173	.3711	.5521	.6314
0.000	1.2627	.3998	.5627	.6418
-.052	1.2638	.4457	.5938	.6720
-.104	1.2649	.4921	.6237	.7004
-.156	1.2800	.5664	.6652	.7386
-.208	1.2952	.7159	.7435	.8071
-.260	1.2768	.8351	.8088	.8607
-.312	1.2584	.9050	.8480	.8915
-.364	1.2195	.9225	.8698	.9080
-.416	1.1806	.9281	.8866	.9206
-.468	1.1438	.9298	.9016	.9316
-.520	1.1071	.9299	.9165	.9424
-.572	1.0811	.9346	.9297	.9519
-.624	1.0552	.9342	.9409	.9597
-.676	1.0454	.9343	.9453	.9628
-.728	1.0357	.9276	.9464	.9636
-.780	1.0141	.9382	.9618	.9743
-.832	.9925	.9370	.9716	.9810
-.884	.9568	.9482	.9955	.9970
-.936	.9211	.9494	1.0152	1.0100
-.988	.8519	.9463	1.0539	1.0347
-1.040	.7827	.9380	1.0947	1.0597

(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 221.27$ psf (10594.59 N/m^2);
$q_\infty = 396.52$ psf (18985.50 N/m^2);
$p_{t,\infty} = 940.50$ psf (45031.38 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1548	.9641	.9137	.9404
.988	1.1580	.9568	.9090	.9370
.936	1.1612	.9562	.9074	.9358
.884	1.1612	.9461	.9026	.9324
.832	1.1612	.9377	.8986	.9294
.780	1.1450	.9289	.9007	.9309
.728	1.1288	.9050	.8954	.9270
.676	1.1396	.8743	.8759	.9126
.624	1.1504	.8163	.8424	.8871
.572	1.1569	.7486	.8044	.8572
.520	1.1634	.7181	.7856	.8421
.468	1.1548	.6506	.7506	.8131
.416	1.1461	.5999	.7235	.7901
.364	1.1429	.5795	.7121	.7801
.312	1.1396	.5820	.7146	.7824
.260	1.1364	.6056	.7300	.7957
.208	1.1331	.6239	.7420	.8058
.156	1.1407	.6222	.7386	.8029
.104	1.1375	.6019	.7274	.7934
.052	1.1256	.6150	.7392	.8035
0.000	1.1418	.6482	.7534	.8155
-.052	1.1299	.6953	.7845	.8411
-.104	1.1180	.7558	.8222	.8714
-.156	1.1483	.7958	.8325	.8795
-.208	1.1785	.8391	.8438	.8882
-.260	1.1731	.8858	.8690	.9074
-.312	1.1677	.9087	.8822	.9173
-.364	1.1656	.9176	.8873	.9211
-.416	1.1634	.9247	.8915	.9242
-.468	1.1666	.9274	.8916	.9243
-.520	1.1699	.9268	.8901	.9231
-.572	1.1699	.9319	.8925	.9249
-.624	1.1699	.9352	.8941	.9261
-.676	1.1688	.9354	.8946	.9265
-.728	1.1677	.9390	.8967	.9280
-.780	1.1688	.9388	.8962	.9277
-.832	1.1699	.9520	.9021	.9320
-.884	1.1710	.9518	.9016	.9316
-.936	1.1721	.9600	.9050	.9341
-.988	1.1688	.9606	.9066	.9352
-1.040	1.1656	.9646	.9097	.9375

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 221.65$ psf (10612.61 N/m^2);
$q_\infty = 397.19$ psf (19017.80 N/m^2);
$p_{t,\infty} = 942.10$ psf (45107.99 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0470	.9535	.9543	.9691
.988	1.0502	.9513	.9517	.9673
.936	1.0535	.9423	.9458	.9631
.884	1.0449	.9304	.9437	.9617
.832	1.0362	.9152	.9398	.9589
.780	1.0200	.8946	.9365	.9566
.728	1.0038	.8857	.9393	.9586
.676	1.0125	.8371	.9093	.9372
.624	1.0211	.8086	.8899	.9230
.572	1.0200	.7800	.8745	.9115
.520	1.0189	.7396	.8519	.8945
.468	1.0071	.7078	.8384	.8840
.416	.9952	.6931	.8345	.8810
.364	.9963	.6963	.8360	.8822
.312	.9974	.7131	.8456	.8896
.260	.9920	.7107	.8465	.8903
.208	.9866	.7152	.8514	.8941
.156	1.0114	.6916	.8270	.8751
.104	1.0060	.6876	.8267	.8749
.052	1.0103	.7021	.8336	.8803
0.000	1.0254	.7213	.8387	.8843
-.052	1.0297	.7593	.8587	.8997
-.104	1.0341	.7973	.8781	.9142
-.156	1.0524	.8275	.8867	.9207
-.208	1.0708	.8560	.8941	.9261
-.260	1.0654	.8854	.9117	.9389
-.312	1.0600	.8998	.9214	.9459
-.364	1.0621	.9178	.9296	.9517
-.416	1.0643	.9174	.9284	.9509
-.468	1.0632	.9310	.9357	.9561
-.520	1.0621	.9312	.9363	.9565
-.572	1.0654	.9339	.9363	.9565
-.624	1.0686	.9267	.9312	.9529
-.676	1.0675	.9352	.9360	.9563
-.728	1.0664	.9321	.9349	.9555
-.780	1.0686	.9400	.9379	.9576
-.832	1.0708	.9396	.9368	.9568
-.884	1.0729	.9509	.9414	.9601
-.936	1.0751	.9522	.9411	.9599
-.988	1.0740	.9591	.9450	.9626
-1.040	1.0729	.9543	.9431	.9613

(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 221.70$ psf (10614.86 N/m^2);
$q_\infty = 397.28$ psf (19021.83 N/m^2);
$p_{t,\infty} = 942.30$ psf (45117.57 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1180	.9560	.9247	.9483
.988	1.1213	.9521	.9215	.9460
.936	1.1245	.9414	.9150	.9413
.884	1.1159	.9329	.9144	.9408
.832	1.1072	.9194	.9112	.9386
.780	1.1007	.9004	.9044	.9336
.728	1.0943	.8594	.8862	.9203
.676	1.1105	.8277	.8633	.9032
.624	1.1266	.7787	.8314	.8786
.572	1.1040	.7661	.8330	.8799
.520	1.0813	.7433	.8291	.8768
.468	1.0360	.7300	.8394	.8848
.416	.9907	.7318	.8595	.9002
.364	.9734	.7216	.8610	.9014
.312	.9561	.7248	.8707	.9087
.260	.9497	.7362	.8804	.9160
.208	.9432	.7340	.8822	.9173
.156	.9637	.7234	.8664	.9055
.104	.9572	.7280	.8721	.9098
.052	.9605	.7426	.8793	.9151
0.000	.9712	.7625	.8861	.9202
-.052	.9745	.7846	.8973	.9285
-.104	.9777	.8142	.9125	.9395
-.156	.9874	.8392	.9219	.9462
-.208	.9971	.8591	.9282	.9508
-.260	.9961	.8827	.9414	.9601
-.312	.9950	.8979	.9500	.9661
-.364	1.0382	.9152	.9389	.9583
-.416	1.0813	.9258	.9253	.9487
-.468	1.1105	.9372	.9187	.9440
-.520	1.1396	.9336	.9051	.9342
-.572	1.1364	.9392	.9091	.9371
-.624	1.1331	.9398	.9107	.9382
-.676	1.1428	.9380	.9060	.9348
-.728	1.1525	.9379	.9021	.9320
-.780	1.1439	.9462	.9095	.9373
-.832	1.1353	.9494	.9145	.9410
-.884	1.1310	.9569	.9198	.9448
-.936	1.1266	.9577	.9220	.9463
-.988	1.1256	.9646	.9257	.9490
-1.040	1.1245	.9614	.9247	.9482

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 221.86$ psf (10622.75 N/m^2);
$q_\infty = 397.57$ psf (19035.97 N/m^2);
$p_{t,\infty} = 943.00$ psf (45151.08 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0266	.9568	.9654	.9767
.988	1.0298	.9563	.9636	.9755
.936	1.0331	.9390	.9534	.9684
.884	1.0352	.9319	.9488	.9652
.832	1.0374	.9148	.9391	.9584
.780	1.0676	.8926	.9144	.9409
.728	1.0978	.8602	.8852	.9195
.676	1.1247	.8231	.8554	.8972
.624	1.1517	.7941	.8304	.8778
.572	1.1873	.7512	.7954	.8501
.520	1.2229	.7405	.7782	.8360
.468	1.2390	.7199	.7622	.8228
.416	1.2552	.7130	.7537	.8157
.364	1.2649	.7109	.7497	.8124
.312	1.2746	.7089	.7457	.8090
.260	1.2768	.7084	.7449	.8083
.208	1.2789	.7097	.7449	.8083
.156	1.2811	.7057	.7422	.8060
.104	1.2833	.7157	.7468	.8099
.052	1.2649	.7370	.7633	.8237
0.000	1.2876	.7616	.7691	.8285
-.052	1.2692	.7878	.7878	.8439
-.104	1.2509	.8205	.8099	.8616
-.156	1.2477	.8449	.8229	.8720
-.208	1.2444	.8693	.8358	.8820
-.260	1.2121	.8890	.8564	.8979
-.312	1.1797	.9119	.8792	.9151
-.364	1.1603	.9256	.8931	.9254
-.416	1.1409	.9292	.9024	.9322
-.468	1.1129	.9410	.9195	.9446
-.520	1.0848	.9343	.9281	.9506
-.572	1.0536	.9416	.9454	.9629
-.624	1.0223	.9339	.9558	.9701
-.676	1.0158	.9400	.9620	.9744
-.728	1.0093	.9362	.9631	.9751
-.780	.9996	.9462	.9729	.9818
-.832	.9899	.9412	.9751	.9833
-.884	.9867	.9551	.9839	.9892
-.936	.9835	.9507	.9832	.9888
-.988	.9813	.9594	.9888	.9925
-1.040	.9792	.9548	.9875	.9917

(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 221.67$ psf (10613.74 N/m^2);
$q_\infty = 397.24$ psf (19019.82 N/m^2);
$p_{t,\infty} = 942.20$ psf (45112.78 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2196	.9519	.8835	.9183
.988	1.2131	.9396	.8801	.9157
.936	1.2066	.9306	.8782	.9143
.884	1.2045	.9073	.8679	.9066
.832	1.2023	.8840	.8575	.8987
.780	1.1872	.8682	.8551	.8969
.728	1.1721	.8388	.8459	.8899
.676	1.1829	.8230	.8341	.8807
.624	1.1937	.7850	.8110	.8625
.572	1.1894	.7567	.7976	.8518
.520	1.1850	.7610	.8013	.8548
.468	1.1721	.7430	.7962	.8506
.416	1.1591	.7490	.8038	.8568
.364	1.1645	.7513	.8032	.8563
.312	1.1699	.7382	.7944	.8492
.260	1.1559	.7410	.8007	.8543
.208	1.1419	.7473	.8090	.8609
.156	1.1721	.7430	.7962	.8506
.104	1.1581	.7544	.8071	.8594
.052	1.1527	.7640	.8141	.8650
0.000	1.1743	.7837	.8170	.8672
-.052	1.1689	.8052	.8300	.8775
-.104	1.1635	.8283	.8438	.8882
-.156	1.1840	.8413	.8429	.8876
-.208	1.2045	.8576	.8438	.8882
-.260	1.1980	.8791	.8566	.8981
-.312	1.1915	.9006	.8694	.9077
-.364	1.2002	.9090	.8703	.9084
-.416	1.2088	.9226	.8736	.9109
-.468	1.2196	.9256	.8712	.9091
-.520	1.2304	.9236	.8664	.9055
-.572	1.2315	.9318	.8699	.9081
-.624	1.2325	.9383	.8725	.9101
-.676	1.2369	.9324	.8683	.9069
-.728	1.2412	.9401	.8703	.9084
-.780	1.2369	.9409	.8722	.9098
-.832	1.2325	.9534	.8795	.9153
-.884	1.2369	.9510	.8768	.9133
-.936	1.2412	.9586	.8788	.9148
-.988	1.2476	.9573	.8760	.9127
-1.040	1.2541	.9629	.8762	.9128

TABLE 6.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF THE WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Concluded.

(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 221.46$ psf (10603.60 N/m^2);
$q_\infty = 396.86$ psf (19001.65 N/m^2);
$p_{t,\infty} = 941.30$ psf (45069.69 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1494	.9510	.9096	.9374
.988	1.1484	.9344	.9020	.9319
.936	1.1473	.9312	.9009	.9311
.884	1.1430	.9118	.8931	.9254
.832	1.1386	.8872	.8827	.9177
.780	1.1235	.8799	.8850	.9194
.728	1.1084	.8438	.8725	.9101
.676	1.1235	.8223	.8555	.8972
.624	1.1386	.8109	.8439	.8883
.572	1.1376	.7941	.8355	.8818
.520	1.1365	.7857	.8315	.8787
.468	1.1278	.7738	.8283	.8762
.416	1.1192	.7584	.8232	.8721
.364	1.1300	.7562	.8181	.8681
.312	1.1408	.7592	.8158	.8663
.260	1.1397	.7543	.8135	.8645
.208	1.1386	.7545	.8140	.8649
.156	1.1765	.7521	.7996	.8534
.104	1.1754	.7575	.8028	.8560
.052	1.1711	.7704	.8111	.8626
0.000	1.2121	.7794	.8019	.8552
-.052	1.2078	.8002	.8140	.8649
-.104	1.2035	.8282	.8296	.8772
-.156	1.2316	.8346	.8232	.8722
-.208	1.2596	.8546	.8237	.8726
-.260	1.2478	.8756	.8377	.8835
-.312	1.2359	.8948	.8509	.8937
-.364	1.2337	.9054	.8567	.8981
-.416	1.2316	.9193	.8640	.9036
-.468	1.2380	.9231	.8635	.9033
-.520	1.2445	.9270	.8630	.9029
-.572	1.2380	.9315	.8674	.9062
-.624	1.2316	.9378	.8726	.9102
-.676	1.2305	.9363	.8723	.9099
-.728	1.2294	.9399	.8744	.9115
-.780	1.2175	.9421	.8797	.9154
-.832	1.2056	.9544	.8897	.9229
-.884	1.2067	.9542	.8893	.9225
-.936	1.2078	.9591	.8911	.9239
-.988	1.2056	.9595	.8921	.9246
-1.040	1.2035	.9649	.8954	.9271

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 101.21$ psf (4846.12 N/m^2);
$q_\infty = 374.79$ psf (17945.18 N/m^2);
$p_{t,\infty} = 1265.60$ psf (60597.25 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8790	.7441	.9201	.9587
.988	.8034	.7185	.9457	.9725
.936	.7277	.6928	.9757	.9880
.884	.6852	.6681	.9874	.9938
.832	.6427	.6469	1.0033	1.0016
.780	.6025	.6238	1.0175	1.0084
.728	.5623	.6006	1.0335	1.0159
.676	.5316	.5768	1.0416	1.0196
.624	.5009	.5599	1.0573	1.0266
.572	.4537	.5443	1.0953	1.0431
.520	.4064	.5321	1.1442	1.0628
.468	.4182	.3867	.9616	.9808
.416	.4300	.1010	.4847	.6223
.364	.4300	.0141	.1812	.2555
.312	.4300	.0020	.0676	.0967
.260	.4300	0.0000	0.0000	0.0000
.208	.4300	0.0000	0.0000	0.0000
.156	.4418	0.0000	0.0000	0.0000
.104	.4537	0.0000	0.0000	0.0000
.052	.4348	0.0000	0.0000	0.0000
0.000	.4159	0.0000	0.0000	0.0000
-.104	.4253	0.0000	0.0000	0.0000
-.156	.4300	0.0000	0.0000	0.0000
-.208	.4348	0.0000	0.0000	0.0000
-.260	.4300	0.0000	0.0000	0.0000
-.312	.4348	.0129	.1726	.2438
-.364	.4395	.0823	.4328	.5672
-.416	.4348	.3593	.9091	.9526
-.468	.4395	.5279	1.0960	1.0434
-.520	.4442	.5432	1.1059	1.0475
-.572	.4584	.5578	1.1032	1.0464
-.624	.4726	.5707	1.0990	1.0446
-.676	.5175	.5848	1.0631	1.0292
-.728	.5623	.6024	1.0350	1.0166
-.780	.6025	.6220	1.0161	1.0077
-.832	.6427	.6452	1.0019	1.0009
-.884	.6781	.6704	.9943	.9972
-.936	.7136	.7008	.9910	.9956
-.988	.7845	.7251	.9614	.9807
-1.040	.8553	.7581	.9415	.9702

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 101.41$ psf (4855.31 N/m^2);
$q_\infty = 375.50$ psf (17979.21 N/m^2);
$p_{t,\infty} = 1268.00$ psf (60712.17 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7171	.6930	.9831	.9917
.988	.6581	.6748	1.0126	1.0061
.936	.5992	.6565	1.0468	1.0219
.884	.5685	.6397	1.0608	1.0282
.832	.5378	.6246	1.0776	1.0355
.780	.5072	.6094	1.0962	1.0434
.728	.4765	.5943	1.1168	1.0519
.676	.4600	.5799	1.1228	1.0544
.624	.4435	.5776	1.1412	1.0617
.572	.4529	.5804	1.1320	1.0580
.520	.4623	.5953	1.1347	1.0591
.468	.5496	.6150	1.0578	1.0269
.416	.6369	.5528	.9316	.9650
.364	.6463	.2397	.6090	.7404
.312	.6558	.0872	.3646	.4897
.260	.6558	.0139	.1455	.2065
.208	.6558	.0015	.0481	.0689
.156	.6699	0.0000	0.0000	0.0000
.104	.6841	0.0000	0.0000	0.0000
.052	.6558	.0078	.1089	.1553
0.000	.6275	.0120	.1386	.1968
-.104	.6746	.0121	.1338	.1902
-.156	.6864	.0181	.1625	.2299
-.208	.6982	.0672	.3102	.4239
-.260	.6534	.1940	.5449	.6819
-.312	.6652	.4039	.7792	.8723
-.364	.5779	.6094	1.0269	1.0128
-.416	.6322	.6280	.9967	.9984
-.468	.5449	.6066	1.0551	1.0257
-.520	.4576	.5765	1.1224	1.0542
-.572	.4505	.5840	1.1385	1.0606
-.624	.4435	.5915	1.1549	1.0670
-.676	.4741	.5979	1.1230	1.0544
-.728	.5048	.6061	1.0958	1.0433
-.780	.5307	.6181	1.0792	1.0362
-.832	.5567	.6301	1.0639	1.0296
-.884	.5661	.6468	1.0689	1.0318
-.936	.5756	.6687	1.0779	1.0357
-.988	.6227	.6844	1.0483	1.0226
-1.040	.6699	.7070	1.0273	1.0130

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 5^o$;

$p_\infty = 101.22$ psf (4846.50 N/m^2);
$q_\infty = 374.82$ psf (17946.60 N/m^2);
$p_{t,\infty} = 1265.70$ psf (60602.04 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6237	.6612	1.0296	1.0141
.988	.5765	.6490	1.0611	1.0283
.936	.5292	.6386	1.0985	1.0444
.884	.5080	.6227	1.1072	1.0480
.832	.4867	.6121	1.1214	1.0538
.780	.4985	.6060	1.1026	1.0461
.728	.5103	.6835	1.1573	1.0679
.676	.5812	.6679	1.0720	1.0331
.624	.6521	.6766	1.0186	1.0089
.572	.7088	.6880	.9852	.9927
.520	.7655	.7029	.9583	.9791
.468	.8458	.7248	.9257	.9617
.416	.9261	.7361	.8915	.9426
.364	.9498	.7378	.8814	.9368
.312	.9734	.7010	.8486	.9172
.260	.9805	.5374	.7403	.8450
.208	.9876	.3650	.6079	.7395
.156	1.0348	.2164	.4573	.5936
.104	1.0821	.2340	.4650	.6018
.052	1.0632	.3436	.5685	.7040
0.000	1.0443	.4046	.6224	.7520
-.104	1.1388	.5772	.7119	.8240
-.156	1.1577	.7023	.7788	.8720
-.208	1.1766	.7744	.8113	.8936
-.260	.9805	.7861	.8954	.9449
-.312	.9994	.7777	.8821	.9372
-.364	.8883	.7600	.9249	.9613
-.416	.8222	.7056	.9264	.9621
-.468	.7111	.6512	.9569	.9784
-.520	.6001	.6334	1.0273	1.0130
-.572	.5930	.6426	1.0410	1.0193
-.624	.5859	.6623	1.0632	1.0292
-.676	.6379	.6759	1.0293	1.0139
-.728	.6899	.6947	1.0035	1.0017
-.780	.6119	.6395	1.0223	1.0106
-.832	.5340	.6278	1.0843	1.0384
-.884	.5221	.6391	1.1063	1.0477
-.9[illegible]	.5103	.6556	1.1335	1.0586
-	.5410	.6656	1.1091	1.0488
	.5718	.6807	1.0912	1.0413

(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^o$;

$p_\infty = 101.33$ psf (4851.48 N/m^2);
$q_\infty = 375.21$ psf (17965.03 N/m^2);
$p_{t,\infty} = 1267.00$ psf (60664.29 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7497	.7417	.9947	.9974
.988	.7096	.7221	1.0087	1.0042
.936	.6696	.7059	1.0268	1.0128
.884	.6460	.6868	1.0311	1.0148
.832	.6224	.6816	1.0464	1.0218
.780	.6955	.7005	1.0036	1.0017
.728	.7686	.7299	.9745	.9874
.676	.8534	.7653	.9470	.9731
.624	.9383	.7728	.9075	.9517
.572	.9855	.7780	.8885	.9409
.520	1.0326	.7761	.8669	.9282
.468	1.0373	.7670	.8599	.9240
.416	1.0421	.7509	.8489	.9173
.364	1.0255	.7259	.8413	.9127
.312	1.0090	.6835	.8230	.9012
.260	.9973	.5794	.7622	.8605
.208	.9855	.4748	.6941	.8104
.156	1.0138	.3837	.6152	.7458
.104	1.0421	.4007	.6201	.7500
.052	1.0491	.4570	.6600	.7834
0.000	1.0562	.5411	.7158	.8269
-.104	1.0845	.6951	.8006	.8866
-.156	1.0986	.7307	.8155	.8963
-.208	1.1128	.7593	.8261	.9031
-.260	1.0892	.7594	.8350	.9087
-.312	1.1033	.7618	.8309	.9062
-.364	1.0986	.7657	.8348	.9086
-.416	1.0939	.7731	.8407	.9122
-.468	1.0892	.7769	.8446	.9147
-.520	1.0845	.7808	.8485	.9171
-.572	.9336	.7959	.9233	.9604
-.624	.7827	.7288	.9650	.9825
-.676	.6955	.6500	.9667	.9834
-.728	.6083	.6635	1.0444	1.0208
-.780	.6342	.6755	1.0320	1.0152
-.832	.6601	.6909	1.0231	1.0110
-.884	.6648	.7115	1.0345	1.0163
-.936	.6696	.7320	1.0456	1.0214
-.988	.7096	.7482	1.0268	1.0128
-1.040	.7497	.7696	1.0132	1.0063

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 101.13$ psf (4842.29 N/m^2);
$q_\infty = 374.50$ psf (17931.00 N/m^2);
$p_{t,\infty} = 1264.60$ psf (60549.37 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6897	.7093	1.0141	1.0068
.988	.7181	.7107	.9949	.9975
.936	.7464	.7679	1.0143	1.0069
.884	.8456	.8059	.9762	.9882
.832	.9448	.8054	.9233	.9604
.780	.9637	.8005	.9114	.9539
.728	.9826	.7885	.8958	.9451
.676	.9826	.7815	.8918	.9428
.624	.9826	.7745	.8878	.9405
.572	.9897	.7670	.8803	.9361
.520	.9968	.7612	.8739	.9324
.468	1.0015	.7521	.8666	.9280
.416	1.0062	.7342	.8542	.9206
.364	.9968	.7017	.8390	.9112
.312	.9873	.6569	.8157	.8964
.260	.9826	.5765	.7660	.8631
.208	.9779	.5082	.7209	.8307
.156	1.0015	.4586	.6767	.7967
.104	1.0251	.4743	.6802	.7995
.052	1.0299	.5110	.7044	.8183
0.000	1.0346	.5864	.7528	.8539
-.104	1.0393	.7089	.8259	.9030
-.156	1.0488	.7257	.8318	.9067
-.208	1.0582	.7424	.8376	.9104
-.260	1.0369	.7459	.8481	.9168
-.312	1.0464	.7504	.8468	.9160
-.364	1.0417	.7525	.8499	.9180
-.416	1.0346	.7600	.8571	.9223
-.468	1.0299	.7622	.8603	.9242
-.520	1.0251	.7695	.8664	.9279
-.572	1.0180	.7736	.8717	.9311
-.624	1.0110	.7829	.8800	.9359
-.676	1.0157	.7895	.8816	.9369
-.728	1.0204	.8014	.8862	.9396
-.780	.9377	.8182	.9341	.9663
-.832	.8551	.8244	.9819	.9911
-.884	.7228	.6877	.9754	.9878
-.936	.5905	.7114	1.0976	1.0440
-.988	.6212	.7214	1.0776	1.0355
-1.040	.6519	.7383	1.0642	1.0297

(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 101.05$ psf (4838.08 N/m^2);
$q_\infty = 374.17$ psf (17915.41 N/m^2);
$p_{t,\infty} = 1263.50$ psf (60496.71 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0731	.8769	.9040	.9497
.988	1.0518	.8592	.9038	.9496
.936	1.0305	.8486	.9075	.9517
.884	1.0282	.8348	.9011	.9481
.832	1.0258	.8245	.8965	.9455
.780	1.0234	.8124	.8910	.9423
.728	1.0211	.8021	.8863	.9396
.676	1.0116	.7906	.8840	.9383
.624	1.0022	.7825	.8837	.9381
.572	.9998	.7705	.8779	.9347
.520	.9974	.7566	.8710	.9306
.468	.9903	.7344	.8612	.9248
.416	.9832	.7052	.8469	.9161
.364	.9714	.6710	.8311	.9063
.312	.9596	.6316	.8113	.8936
.260	.9549	.5846	.7824	.8744
.208	.9502	.5551	.7643	.8620
.156	.9667	.5361	.7447	.8481
.104	.9832	.5418	.7423	.8464
.052	.9832	.5647	.7579	.8575
0.000	.9832	.6104	.7879	.8782
-.104	.9785	.6985	.8449	.9149
-.156	.9880	.7153	.8509	.9186
-.208	.9974	.7251	.8526	.9196
-.260	.9880	.7346	.8623	.9255
-.312	.9974	.7391	.8608	.9246
-.364	1.0022	.7458	.8627	.9257
-.416	.9974	.7531	.8690	.9294
-.468	1.0022	.7598	.8707	.9305
-.520	1.0069	.7682	.8735	.9321
-.572	1.0092	.7750	.8763	.9338
-.624	1.0116	.7853	.8811	.9366
-.676	1.0187	.7935	.8826	.9375
-.728	1.0258	.8052	.8860	.9394
-.780	1.0234	.8142	.8919	.9429
-.832	1.0211	.8318	.9026	.9489
-.884	1.0282	.8453	.9067	.9513
-.936	1.0352	.8588	.9108	.9535
-.988	1.0400	.8706	.9150	.9559
-1.040	1.0447	.8860	.9209	.9591

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – *Continued*

(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 101.24$ psf (4847.27 N/m^2);
$q_\infty = 374.88$ psf (17949.44 N/m^2);
$p_{t,\infty} = 1265.90$ psf (60611.62 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1646	.8900	.8742	.9326
.988	1.1363	.8782	.8792	.9355
.936	1.1080	.8682	.8852	.9390
.884	1.1033	.8546	.8801	.9360
.832	1.0986	.8462	.8777	.9346
.780	1.1033	.8354	.8702	.9302
.728	1.1080	.8228	.8617	.9251
.676	1.0986	.8130	.8603	.9242
.624	1.0891	.8033	.8588	.9234
.572	1.0915	.7926	.8522	.9193
.520	1.0938	.7819	.8455	.9152
.468	1.1033	.7655	.8330	.9074
.416	1.1127	.7455	.8185	.8983
.364	1.1033	.7252	.8108	.8933
.312	1.0938	.7050	.8028	.8880
.260	1.0868	.6828	.7926	.8813
.208	1.0797	.6693	.7873	.8778
.156	1.0915	.6473	.7701	.8660
.104	1.1033	.6323	.7571	.8569
.052	1.1056	.6234	.7509	.8525
0.000	1.1080	.6355	.7573	.8571
-.104	1.0891	.6931	.7977	.8847
-.156	1.0844	.7215	.8157	.8964
-.208	1.0797	.7463	.8314	.9065
-.260	1.0844	.7565	.8352	.9088
-.312	1.0797	.7638	.8411	.9125
-.364	1.0821	.7706	.8439	.9143
-.416	1.0797	.7778	.8488	.9172
-.468	1.0821	.7829	.8506	.9184
-.520	1.0844	.7897	.8533	.9200
-.572	1.0915	.7961	.8540	.9205
-.624	1.0986	.8026	.8547	.9209
-.676	1.1056	.8107	.8563	.9219
-.728	1.1127	.8224	.8597	.9239
-.780	1.1080	.8350	.8681	.9289
-.832	1.1033	.8476	.8765	.9339
-.884	1.1103	.8610	.8806	.9363
-.936	1.1174	.8762	.8855	.9392
-.988	1.1292	.8893	.8874	.9403
-1.040	1.1410	.9076	.8919	.9428

(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 101.31$ psf (4850.71 N/m^2);
$q_\infty = 375.15$ psf (17962.20 N/m^2);
$p_{t,\infty} = 1266.80$ psf (60654.71 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1371	.9086	.8939	.9440
.988	1.1465	.9026	.8873	.9402
.936	1.1560	.8897	.8773	.9344
.884	1.1677	.8818	.8690	.9294
.832	1.1795	.8721	.8599	.9240
.780	1.1913	.8589	.8491	.9175
.728	1.2031	.8475	.8393	.9114
.676	1.1890	.8364	.8387	.9110
.624	1.1748	.8252	.8381	.9107
.572	1.1748	.8112	.8310	.9062
.520	1.1748	.7885	.8192	.8987
.468	1.1701	.7626	.8073	.8910
.416	1.1654	.7332	.7932	.8817
.364	1.1489	.7012	.7812	.8736
.312	1.1324	.6744	.7717	.8671
.260	1.1206	.6402	.7559	.8561
.208	1.1088	.6201	.7478	.8504
.156	1.1276	.6045	.7322	.8390
.104	1.1465	.5959	.7209	.8307
.052	1.1465	.6029	.7252	.8339
0.000	1.1465	.6311	.7419	.8461
-.104	1.1371	.7126	.7917	.8806
-.156	1.1324	.7428	.8099	.8927
-.208	1.1276	.7607	.8213	.9001
-.260	1.1300	.7692	.8251	.9024
-.312	1.1253	.7766	.8308	.9060
-.364	1.1276	.7817	.8326	.9072
-.416	1.1229	.7908	.8392	.9113
-.468	1.1253	.7959	.8410	.9124
-.520	1.1276	.8027	.8437	.9141
-.572	1.1324	.8111	.8463	.9157
-.624	1.1371	.8194	.8489	.9173
-.676	1.1371	.8299	.8543	.9206
-.728	1.1371	.8387	.8588	.9234
-.780	1.1135	.8475	.8724	.9315
-.832	1.0899	.8563	.8864	.9397
-.884	1.0734	.8610	.8956	.9450
-.936	1.0569	.8676	.9060	.9509
-.988	1.0356	.8727	.9179	.9575
-1.040	1.0144	.8760	.9293	.9637

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 101.34$ psf (4852.25 N/m^2);
$q_\infty = 375.27$ psf (17967.87 N/m^2);
$p_{t,\infty} = 1267.20$ psf (60673.86 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0711	.8637	.8980	.9463
.988	1.0499	.8549	.9024	.9488
.936	1.0286	.8443	.9060	.9508
.884	1.0263	.8323	.9005	.9478
.832	1.0239	.8255	.8979	.9463
.780	1.0263	.8148	.8910	.9423
.728	1.0286	.8059	.8851	.9389
.676	1.0239	.7958	.8816	.9369
.624	1.0192	.7874	.8790	.9354
.572	1.0216	.7785	.8730	.9318
.520	1.0239	.7696	.8670	.9283
.468	1.0286	.7535	.8559	.9216
.416	1.0334	.7392	.8458	.9154
.364	1.0263	.7275	.8420	.9130
.312	1.0192	.7176	.8391	.9113
.260	1.0145	.6935	.8268	.9035
.208	1.0098	.6833	.8226	.9009
.156	1.0192	.6616	.8057	.8899
.104	1.0286	.6451	.7919	.8808
.052	1.0310	.6344	.7844	.8758
0.000	1.0334	.6412	.7877	.8780
-.104	1.0192	.6861	.8205	.8995
-.156	1.0216	.7087	.8329	.9074
-.208	1.0239	.7294	.8440	.9143
-.260	1.0168	.7387	.8523	.9194
-.312	1.0192	.7473	.8563	.9218
-.364	1.0216	.7506	.8572	.9224
-.416	1.0145	.7581	.8645	.9268
-.468	1.0168	.7649	.8673	.9285
-.520	1.0192	.7717	.8702	.9302
-.572	1.0216	.7768	.8720	.9312
-.624	1.0239	.7818	.8738	.9323
-.676	1.0286	.7902	.8765	.9339
-.728	1.0334	.8021	.8810	.9365
-.780	1.0286	.8112	.8880	.9406
-.832	1.0239	.8255	.8979	.9463
-.884	1.0286	.8373	.9022	.9487
-.936	1.0334	.8509	.9074	.9517
-.988	1.0428	.8624	.9094	.9528
-1.040	1.0522	.8774	.9131	.9548

(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 101.41$ psf (4855.31 N/m^2);
$q_\infty = 375.50$ psf (17979.21 N/m^2);
$p_{t,\infty} = 1268.00$ psf (60712.17 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0080	.8505	.9186	.9578
.988	.9868	.8347	.9197	.9585
.936	.9656	.8259	.9248	.9613
.884	.9633	.8138	.9192	.9582
.832	.9609	.8071	.9165	.9567
.780	.9633	.7982	.9103	.9532
.728	.9656	.7875	.9031	.9492
.676	.9633	.7790	.8993	.9470
.624	.9609	.7704	.8954	.9449
.572	.9633	.7615	.8891	.9413
.520	.9656	.7526	.8829	.9376
.468	.9680	.7402	.8745	.9327
.416	.9703	.7296	.8671	.9283
.364	.9656	.7177	.8621	.9254
.312	.9609	.7076	.8581	.9230
.260	.9586	.6921	.8497	.9178
.208	.9562	.6801	.8433	.9139
.156	.9609	.6622	.8302	.9057
.104	.9656	.6496	.8202	.8993
.052	.9703	.6370	.8102	.8929
0.000	.9750	.6436	.8125	.8944
-.104	.9609	.6762	.8389	.9111
-.156	.9680	.6914	.8451	.9150
-.208	.9750	.7100	.8533	.9200
-.260	.9609	.7216	.8666	.9280
-.312	.9680	.7280	.8672	.9284
-.364	.9703	.7331	.8692	.9296
-.416	.9609	.7373	.8760	.9336
-.468	.9633	.7441	.8789	.9353
-.520	.9656	.7509	.8818	.9370
-.572	.9656	.7561	.8849	.9388
-.624	.9656	.7631	.8890	.9412
-.676	.9703	.7732	.8927	.9433
-.728	.9750	.7833	.8963	.9454
-.780	.9727	.7922	.9025	.9489
-.832	.9703	.8063	.9116	.9540
-.884	.9727	.8166	.9163	.9566
-.936	.9750	.8304	.9228	.9602
-.988	.9798	.8405	.9262	.9620
-1.040	.9845	.8541	.9314	.9648

TABLE 7.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.30 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Concluded.

(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^{\circ}$;

$p_\infty = 101.28$ psf (4849.18 N/m^2);
$q_\infty = 375.03$ psf (17956.53 N/m^2);
$p_{t,\infty} = 1266.40$ psf (60635.56 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9821	.8467	.9285	.9633
.988	.9608	.8291	.9289	.9635
.936	.9396	.8185	.9333	.9659
.884	.9396	.8080	.9274	.9627
.832	.9396	.7993	.9223	.9599
.780	.9396	.7906	.9173	.9571
.728	.9396	.7819	.9122	.9543
.676	.9396	.7731	.9071	.9515
.624	.9396	.7644	.9020	.9486
.572	.9396	.7557	.8968	.9457
.520	.9396	.7452	.8906	.9421
.468	.9419	.7345	.8831	.9377
.416	.9443	.7239	.8755	.9333
.364	.9396	.7120	.8705	.9304
.312	.9349	.7036	.8676	.9286
.260	.9349	.6862	.8567	.9221
.208	.9349	.6757	.8502	.9181
.156	.9372	.6580	.8379	.9105
.104	.9396	.6473	.8300	.9056
.052	.9443	.6365	.8210	.8998
0.000	.9490	.6396	.8209	.8998
-.104	.9349	.6730	.8485	.9171
-.156	.9419	.6865	.8537	.9202
-.208	.9490	.7034	.8609	.9246
-.260	.9372	.7148	.8733	.9320
-.312	.9443	.7213	.8740	.9324
-.364	.9443	.7265	.8771	.9343
-.416	.9396	.7339	.8838	.9381
-.468	.9396	.7391	.8869	.9400
-.520	.9396	.7444	.8901	.9418
-.572	.9396	.7514	.8942	.9442
-.624	.9396	.7566	.8974	.9460
-.676	.9419	.7634	.9003	.9476
-.728	.9443	.7755	.9062	.9510
-.780	.9419	.7861	.9136	.9551
-.832	.9396	.7968	.9209	.9591
-.884	.9419	.8088	.9267	.9623
-.936	.9443	.8226	.9334	.9659
-.988	.9514	.8343	.9365	.9676
-1.040	.9585	.8460	.9395	.9692

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^\circ$;

p_∞ = 51.80 psf (2480.00 N/m^2);
q_∞ = 317.67 psf (15210.12 N/m^2);
$p_{t,\infty}$ = 1791.60 psf (85782.27 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1448	.6891	.7758	.8979
.988	.9878	.6426	.8066	.9147
.936	.8309	.6044	.8529	.9382
.884	.7616	.5725	.8670	.9449
.832	.6924	.5489	.8903	.9556
.780	.6416	.5244	.9040	.9617
.728	.5909	.5040	.9236	.9701
.676	.5585	.4849	.9317	.9735
.624	.5262	.4678	.9429	.9781
.572	.4478	.4507	1.0033	1.0012
.520	.3693	.4294	1.0784	1.0265
.468	.3370	.4041	1.0952	1.0316
.416	.3047	.3563	1.0814	1.0274
.364	.3554	.1381	.6234	.7977
.312	.4062	.0433	.3266	.4974
.260	.4108	.0148	.1896	.3051
.208	.4154	.0108	.1614	.2618
.156	.4247	.0060	.1187	.1946
.104	.4339	.0046	.1025	.1686
.052	.4247	.0060	.1187	.1946
0.000	.4154	.0038	.0960	.1580
-.104	.4247	.0024	.0748	.1234
-.156	.4201	.0031	.0860	.1417
-.208	.4154	.0038	.0960	.1580
-.260	.4016	.0308	.2770	.4314
-.312	.3970	.1153	.5390	.7279
-.364	.4293	.2872	.8179	.9207
-.416	.3785	.4106	1.0415	1.0145
-.468	.4108	.4256	1.0178	1.0064
-.520	.4431	.4406	.9972	.9990
-.572	.4570	.4564	.9994	.9998
-.624	.4708	.4723	1.0015	1.0006
-.676	.5355	.4859	.9526	.9820
-.728	.6001	.5057	.9180	.9677
-.780	.6555	.5258	.8957	.9580
-.832	.7109	.5563	.8846	.9530
-.884	.7663	.5867	.8750	.9486
-.936	.8217	.6274	.8738	.9481
-.988	.9186	.6622	.8490	.9363
-1.040	1.0155	.7113	.8369	.9303

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^\circ$;

p_∞ = 51.81 psf (2480.55 N/m^2);
q_∞ = 317.74 psf (15213.52 N/m^2);
$p_{t,\infty}$ = 1792.00 psf (85801.42 N/m^2);

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8769	.5940	.8230	.9233
.988	.7522	.5625	.8647	.9438
.936	.6276	.5413	.9287	.9722
.884	.5907	.5224	.9404	.9770
.832	.5538	.5055	.9554	.9831
.780	.5215	.4884	.9678	.9879
.728	.4892	.4775	.9880	.9956
.676	.4707	.4619	.9906	.9965
.624	.4523	.4565	1.0047	1.0017
.572	.4154	.4520	1.0432	1.0151
.520	.3784	.4454	1.0848	1.0285
.468	.3554	.4361	1.1078	1.0354
.416	.3323	.4309	1.1388	1.0444
.364	.5630	.5503	.9886	.9958
.312	.7938	.5792	.8542	.9388
.260	.8261	.4400	.7298	.8708
.208	.8584	.2357	.5240	.7143
.156	.8953	.0942	.3243	.4944
.104	.9322	.0696	.2732	.4263
.052	.9415	.1848	.4431	.6340
0.000	.9507	.2539	.5168	.7076
-.104	1.1353	.3050	.5183	.7090
-.156	.9922	.4818	.6968	.8497
-.208	.8492	.6137	.8501	.9368
-.260	.8445	.5420	.8011	.9118
-.312	.7015	.5114	.8538	.9386
-.364	.6461	.5076	.8864	.9538
-.416	.5538	.4542	.9056	.9624
-.468	.4984	.4484	.9485	.9803
-.520	.4430	.4528	1.0110	1.0040
-.572	.4338	.4532	1.0221	1.0079
-.624	.4246	.4618	1.0430	1.0150
-.676	.4661	.4703	1.0045	1.0016
-.728	.5077	.4829	.9753	.9908
-.780	.5400	.4979	.9603	.9850
-.832	.5723	.5129	.9467	.9796
-.884	.5953	.5345	.9475	.9799
-.936	.6184	.5643	.9552	.9830
-.988	.6830	.5881	.9280	.9719
-1.040	.7476	.6223	.9123	.9653

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.76$ psf (2478.20 N/m^2);
$q_\infty = 317.44$ psf (15199.09 N/m^2);
$p_{t,\infty} = 1790.30$ psf (85720.03 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7576	.5567	.8572	.9403
.988	.6606	.5383	.9027	.9611
.936	.5636	.5261	.9662	.9873
.884	.5451	.5126	.9697	.9887
.832	.5266	.4990	.9734	.9901
.780	.5035	.4897	.9862	.9949
.728	.4804	.4845	1.0043	1.0015
.676	.4850	.4761	.9908	.9966
.624	.4897	.5724	1.0812	1.0274
.572	.5728	.5545	.9839	.9941
.520	.6560	.5447	.9113	.9648
.468	.8500	.6061	.8444	.9340
.416	1.0440	.6509	.7896	.9056
.364	1.0717	.6517	.7798	.9002
.312	1.0994	.6340	.7594	.8885
.260	1.0902	.5644	.7195	.8643
.208	1.0809	.4823	.6679	.8302
.156	1.1502	.3629	.5617	.7478
.104	1.2195	.3323	.5220	.7125
.052	1.2334	.3983	.5683	.7534
0.000	1.2472	.4889	.6261	.7997
-.104	1.3766	.6460	.6851	.8419
-.156	1.4043	.6757	.6937	.8476
-.208	1.4320	.6847	.6915	.8462
-.260	.9886	.7069	.8456	.9346
-.312	1.0163	.6995	.8296	.9267
-.364	1.0440	.6447	.7859	.9035
-.416	.6005	.5122	.9235	.9701
-.468	.6282	.5171	.9073	.9631
-.520	.6560	.5303	.8991	.9596
-.572	.6652	.5484	.9080	.9634
-.624	.6744	.5644	.9148	.9664
-.676	.5959	.4836	.9009	.9603
-.728	.5174	.4912	.9743	.9904
-.780	.5266	.4990	.9734	.9901
-.832	.5359	.5109	.9764	.9912
-.884	.5359	.5253	.9901	.9964
-.936	.5359	.5438	1.0074	1.0027
-.988	.5820	.5644	.9847	.9944
-1.040	.6282	.5911	.9700	.9888

(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.80$ psf (2480.27 N/m^2);
$q_\infty = 317.71$ psf (15211.82 N/m^2);
$p_{t,\infty} = 1791.80$ psf (85791.85 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7200	.5531	.8764	.9493
.988	.6369	.5403	.9210	.9690
.936	.5539	.5316	.9797	.9925
.884	.6369	.5854	.9587	.9844
.832	.7200	.5900	.9052	.9622
.780	.6969	.5746	.9080	.9634
.728	.6739	.5592	.9110	.9647
.676	.8031	.6069	.8693	.9460
.624	.9323	.6586	.8405	.9321
.572	1.0246	.6627	.8042	.9135
.520	1.1170	.6648	.7715	.8954
.468	1.1354	.6742	.7706	.8949
.416	1.1539	.6610	.7569	.8870
.364	1.1262	.6315	.7488	.8823
.312	1.0985	.5957	.7364	.8748
.260	1.0708	.5373	.7084	.8573
.208	1.0431	.4830	.6805	.8388
.156	1.0846	.4274	.6277	.8010
.104	1.1262	.4234	.6131	.7898
.052	1.1308	.4521	.6323	.8044
0.000	1.1354	.5096	.6699	.8315
-.104	1.1816	.6160	.7220	.8659
-.156	1.2047	.6335	.7252	.8679
-.208	1.2277	.6428	.7236	.8669
-.260	1.1954	.6504	.7376	.8756
-.312	1.2185	.6556	.7335	.8730
-.364	1.2047	.6603	.7404	.8772
-.416	1.2093	.6663	.7423	.8784
-.468	1.1954	.6752	.7515	.8839
-.520	1.1816	.6881	.7631	.8907
-.572	.8954	.5177	.7604	.8891
-.624	.6092	.5325	.9349	.9748
-.676	.6508	.5471	.9169	.9673
-.728	.6923	.5618	.9008	.9603
-.780	.7154	.5793	.8998	.9599
-.832	.7385	.5988	.9005	.9601
-.884	.6323	.6219	.9917	.9970
-.936	.5262	.5587	1.0305	1.0108
-.988	.5539	.5698	1.0143	1.0051
-1.040	.5816	.5892	1.0065	1.0024

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) - Continued

(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.77$ psf (2478.75 N/m^2);
$q_\infty = 317.51$ psf (15202.48 N/m^2);
$p_{t,\infty} = 1790.70$ psf (85739.18 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8867	.6344	.8458	.9347
.988	.7897	.6120	.8803	.9511
.936	.6928	.5977	.9289	.9723
.884	.7897	.6181	.8847	.9531
.832	.8867	.6816	.8767	.9494
.780	.9745	.6962	.8453	.9345
.728	1.0622	.6923	.8073	.9151
.676	1.0576	.6781	.8008	.9116
.624	1.0530	.6701	.7977	.9100
.572	1.0484	.6601	.7935	.9077
.520	1.0438	.6500	.7891	.9053
.468	1.0207	.6366	.7898	.9057
.416	.9976	.6151	.7852	.9032
.364	.9929	.5885	.7699	.8945
.312	.9883	.5579	.7513	.8838
.260	.9791	.5151	.7253	.8680
.208	.9699	.4846	.7069	.8563
.156	.9929	.4547	.6767	.8362
.104	1.0160	.4537	.6682	.8303
.052	1.0160	.4701	.6802	.8386
0.000	1.0160	.5093	.7080	.8570
-.104	1.0438	.5856	.7490	.8824
-.156	1.0622	.5992	.7511	.8836
-.208	1.0807	.6086	.7505	.8833
-.260	1.0530	.6161	.7649	.8917
-.312	1.0715	.6194	.7603	.8890
-.364	1.0761	.6253	.7623	.8902
-.416	1.0622	.6322	.7714	.8954
-.468	1.0668	.6381	.7734	.8965
-.520	1.0715	.6441	.7753	.8976
-.572	1.0853	.6579	.7786	.8995
-.624	1.0992	.6738	.7829	.9019
-.676	1.0992	.6882	.7913	.9065
-.728	1.0992	.7129	.8053	.9141
-.780	.8867	.5782	.8075	.9152
-.832	.6743	.5835	.9302	.9729
-.884	.6697	.6022	.9483	.9803
-.936	.6650	.6271	.9710	.9892
-.988	.7066	.6479	.9576	.9839
-1.040	.7482	.6749	.9498	.9808

(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.84$ psf (2481.94 N/m^2);
$q_\infty = 317.92$ psf (15222.01 N/m^2);
$p_{t,\infty} = 1793.00$ psf (85849.30 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0793	.7296	.8222	.9229
.988	1.0240	.7197	.8384	.9311
.936	.9686	.7099	.8561	.9397
.884	.9686	.6914	.8449	.9343
.832	.9686	.6832	.8399	.9318
.780	.9686	.6730	.8335	.9286
.728	.9686	.6607	.8259	.9248
.676	.9640	.6506	.8215	.9225
.624	.9594	.6405	.8171	.9202
.572	.9548	.6325	.8139	.9186
.520	.9502	.6204	.8081	.9155
.468	.9409	.6065	.8028	.9127
.416	.9317	.5843	.7919	.9068
.364	.9225	.5622	.7806	.9006
.312	.9133	.5379	.7675	.8932
.260	.9087	.5135	.7517	.8840
.208	.9040	.4993	.7432	.8789
.156	.9179	.4822	.7248	.8677
.104	.9317	.4754	.7143	.8611
.052	.9317	.4816	.7190	.8640
0.000	.9317	.5022	.7341	.8734
-.104	.9409	.5517	.7657	.8922
-.156	.9548	.5716	.7738	.8968
-.208	.9686	.5813	.7747	.8973
-.260	.9548	.5922	.7876	.9045
-.312	.9686	.5957	.7842	.9026
-.364	.9732	.6016	.7863	.9037
-.416	.9686	.6060	.7909	.9063
-.468	.9732	.6119	.7929	.9074
-.520	.9778	.6179	.7949	.9085
-.572	.9824	.6279	.7995	.9109
-.624	.9871	.6380	.8040	.9133
-.676	.9917	.6522	.8110	.9170
-.728	.9963	.6664	.8178	.9206
-.780	.9963	.6849	.8291	.9264
-.832	.9963	.7054	.8414	.9326
-.884	.9963	.7259	.8536	.9385
-.936	.9963	.7485	.8668	.9448
-.988	1.0055	.7666	.8731	.9478
-1.040	1.0147	.7908	.8828	.9522

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.85$ psf (2482.63 N/m^2);
$q_\infty = 318.01$ psf (15226.25 N/m^2);
$p_{t,\infty} = 1793.50$ psf (85873.24 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0788	.7262	.8205	.9220
.988	1.0142	.7105	.8370	.9304
.936	.9497	.6929	.8542	.9388
.884	.9451	.6808	.8487	.9362
.832	.9405	.6687	.8432	.9334
.780	.9358	.6586	.8389	.9313
.728	.9312	.6485	.8345	.9291
.676	.9312	.6362	.8266	.9251
.624	.9312	.6280	.8212	.9224
.572	.9266	.6200	.8180	.9207
.520	.9220	.6079	.8120	.9176
.468	.9174	.5896	.8017	.9121
.416	.9128	.5713	.7911	.9064
.364	.9082	.5530	.7803	.9004
.312	.9036	.5368	.7708	.8950
.260	.8990	.5206	.7610	.8894
.208	.8944	.5105	.7555	.8862
.156	.9082	.4955	.7386	.8762
.104	.9220	.4887	.7280	.8697
.052	.9220	.4928	.7311	.8715
0.000	.9220	.5072	.7417	.8780
-.104	.9220	.5462	.7697	.8944
-.156	.9358	.5621	.7750	.8974
-.208	.9497	.5758	.7787	.8995
-.260	.9312	.5828	.7911	.9064
-.312	.9451	.5883	.7890	.9053
-.364	.9451	.5945	.7931	.9075
-.416	.9405	.5988	.7980	.9101
-.468	.9405	.6029	.8007	.9116
-.520	.9405	.6070	.8034	.9130
-.572	.9405	.6153	.8088	.9159
-.624	.9405	.6235	.8142	.9187
-.676	.9405	.6358	.8222	.9229
-.728	.9405	.6502	.8315	.9276
-.780	.9405	.6666	.8419	.9328
-.832	.9405	.6851	.8535	.9385
-.884	.9451	.7054	.8639	.9435
-.936	.9497	.7278	.8754	.9488
-.988	.9635	.7497	.8821	.9519
-1.040	.9773	.7758	.8909	.9559

(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.80$ psf (2480.14 N/m^2);
$q_\infty = 317.69$ psf (15210.97 N/m^2);
$p_{t,\infty} = 1791.70$ psf (85787.06 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0522	.7158	.8248	.9242
.988	.9829	.6983	.8429	.9333
.936	.9137	.6829	.8645	.9437
.884	.9091	.6708	.8590	.9411
.832	.9045	.6586	.8533	.9384
.780	.9045	.6463	.8453	.9345
.728	.9045	.6340	.8372	.9305
.676	.8999	.6239	.8327	.9282
.624	.8953	.6159	.8294	.9266
.572	.8953	.6056	.8225	.9230
.520	.8953	.5933	.8141	.9187
.468	.8953	.5768	.8027	.9127
.416	.8953	.5624	.7926	.9072
.364	.9045	.5497	.7796	.9000
.312	.9137	.5349	.7651	.8918
.260	.9183	.5305	.7601	.8889
.208	.9229	.5262	.7551	.8860
.156	.9506	.5147	.7358	.8744
.104	.9783	.5154	.7259	.8683
.052	.9783	.5216	.7302	.8710
0.000	.9783	.5299	.7359	.8745
-.104	.9691	.5632	.7624	.8902
-.156	.9645	.5778	.7740	.8969
-.208	.9599	.5821	.7783	.8996
-.260	.9460	.5869	.7876	.9045
-.312	.9414	.5891	.7911	.9064
-.364	.9368	.5894	.7932	.9075
-.416	.9229	.5961	.8037	.9132
-.468	.9183	.5963	.8058	.9143
-.520	.9137	.6007	.8108	.9169
-.572	.9091	.6070	.8172	.9203
-.624	.9045	.6155	.8249	.9243
-.676	.9091	.6255	.8295	.9266
-.728	.9137	.6418	.8381	.9309
-.780	.9137	.6582	.8488	.9362
-.832	.9137	.6767	.8606	.9419
-.884	.9183	.6991	.8725	.9475
-.936	.9229	.7215	.8842	.9528
-.988	.9368	.7435	.8909	.9559
-1.040	.9506	.7675	.8985	.9593

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.82$ psf (2480.97 N/m^2);
$q_\infty = 317.79$ psf (15216.07 N/m^2);
$p_{t,\infty} = 1792.30$ psf (85815.79 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3283	.8143	.7830	.9019
.988	1.2591	.7947	.7945	.9082
.936	1.1899	.7773	.8082	.9156
.884	1.1853	.7610	.8013	.9119
.832	1.1807	.7469	.7953	.9087
.780	1.1715	.7329	.7910	.9063
.728	1.1623	.7148	.7842	.9026
.676	1.1484	.7010	.7813	.9010
.624	1.1346	.6872	.7783	.8993
.572	1.1346	.6749	.7713	.8953
.520	1.1346	.6605	.7630	.8906
.468	1.1300	.6463	.7563	.8867
.416	1.1254	.6321	.7495	.8827
.364	1.1161	.6222	.7467	.8810
.312	1.1069	.6083	.7413	.8778
.260	1.0977	.5963	.7371	.8752
.208	1.0885	.5865	.7340	.8734
.156	1.1069	.5691	.7171	.8628
.104	1.1254	.5580	.7042	.8545
.052	1.1207	.5541	.7031	.8539
0.000	1.1161	.5605	.7086	.8574
-.104	1.1254	.5937	.7264	.8686
-.156	1.1254	.6123	.7376	.8756
-.208	1.1254	.6246	.7450	.8800
-.260	1.1161	.6354	.7545	.8856
-.312	1.1161	.6436	.7594	.8885
-.364	1.1207	.6454	.7589	.8882
-.416	1.1069	.6502	.7664	.8926
-.468	1.1115	.6582	.7695	.8943
-.520	1.1161	.6621	.7702	.8947
-.572	1.1254	.6720	.7728	.8962
-.624	1.1346	.6839	.7764	.8982
-.676	1.1484	.6977	.7795	.9000
-.728	1.1623	.7136	.7836	.9022
-.780	1.1530	.7346	.7982	.9102
-.832	1.1438	.7597	.8150	.9191
-.884	1.1623	.7836	.8211	.9223
-.936	1.1807	.8177	.8322	.9280
-.988	1.2038	.8434	.8371	.9304
-1.040	1.2268	.8733	.8437	.9337

(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.83$ psf (2481.52 N/m^2);
$q_\infty = 317.87$ psf (15219.46 N/m^2);
$p_{t,\infty} = 1792.70$ psf (85834.94 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2361	.7803	.7945	.9083
.988	1.1669	.7628	.8085	.9158
.936	1.0977	.7475	.8252	.9244
.884	1.0931	.7292	.8168	.9201
.832	1.0885	.7191	.8128	.9180
.780	1.0885	.7068	.8058	.9143
.728	1.0885	.6965	.8000	.9112
.676	1.0839	.6844	.7947	.9083
.624	1.0792	.6764	.7917	.9067
.572	1.0839	.6701	.7863	.9037
.520	1.0885	.6596	.7784	.8994
.468	1.0839	.6516	.7753	.8976
.416	1.0792	.6436	.7722	.8959
.364	1.0792	.6333	.7660	.8923
.312	1.0792	.6251	.7610	.8895
.260	1.0700	.6111	.7557	.8864
.208	1.0608	.6013	.7529	.8847
.156	1.0700	.5844	.7390	.8764
.104	1.0792	.5675	.7252	.8679
.052	1.0792	.5572	.7186	.8638
0.000	1.0792	.5572	.7186	.8638
-.104	1.0700	.5789	.7356	.8743
-.156	1.0700	.5933	.7447	.8798
-.208	1.0700	.6077	.7536	.8851
-.260	1.0654	.6162	.7605	.8891
-.312	1.0654	.6203	.7630	.8906
-.364	1.0654	.6203	.7630	.8906
-.416	1.0608	.6267	.7686	.8938
-.468	1.0608	.6349	.7736	.8967
-.520	1.0608	.6431	.7786	.8995
-.572	1.0700	.6530	.7812	.9009
-.624	1.0792	.6649	.7849	.9030
-.676	1.0885	.6789	.7897	.9056
-.728	1.0977	.6949	.7957	.9089
-.780	1.0931	.7116	.8068	.9149
-.832	1.0885	.7303	.8191	.9213
-.884	1.0931	.7526	.8298	.9267
-.936	1.0977	.7812	.8436	.9336
-.988	1.1115	.8011	.8490	.9363
-1.040	1.1254	.8293	.8584	.9408

TABLE 8.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 2.96 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) - Concluded.

(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 51.82$ psf (2481.38 N/m^2);
$q_\infty = 317.85$ psf (15218.61 N/m^2);
$p_{t,\infty} = 1792.60$ psf (85830.15 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2068	.7714	.7995	.9109
.988	1.1423	.7558	.8134	.9183
.936	1.0779	.7402	.8287	.9262
.884	1.0733	.7260	.8225	.9230
.832	1.0686	.7139	.8173	.9204
.780	1.0686	.7016	.8103	.9167
.728	1.0686	.6893	.8031	.9129
.676	1.0640	.6792	.7990	.9106
.624	1.0594	.6732	.7972	.9097
.572	1.0640	.6669	.7917	.9067
.520	1.0686	.6585	.7850	.9030
.468	1.0686	.6502	.7800	.9003
.416	1.0686	.6420	.7751	.8975
.364	1.0686	.6338	.7701	.8947
.312	1.0686	.6256	.7651	.8918
.260	1.0594	.6137	.7611	.8895
.208	1.0502	.6038	.7583	.8878
.156	1.0548	.5851	.7448	.8799
.104	1.0594	.5705	.7338	.8733
.052	1.0594	.5582	.7259	.8683
0.000	1.0594	.5561	.7245	.8675
-.104	1.0502	.5778	.7417	.8781
-.156	1.0502	.5901	.7496	.8828
-.208	1.0502	.6025	.7574	.8874
-.260	1.0456	.6089	.7631	.8907
-.312	1.0456	.6089	.7631	.8907
-.364	1.0456	.6150	.7669	.8929
-.416	1.0410	.6194	.7713	.8954
-.468	1.0410	.6255	.7752	.8975
-.520	1.0410	.6379	.7828	.9018
-.572	1.0502	.6477	.7853	.9032
-.624	1.0594	.6576	.7879	.9046
-.676	1.0686	.6716	.7927	.9073
-.728	1.0779	.6876	.7987	.9105
-.780	1.0733	.7043	.8101	.9166
-.832	1.0686	.7230	.8225	.9230
-.884	1.0733	.7454	.8334	.9285
-.936	1.0779	.7719	.8462	.9349
-.988	1.0871	.7940	.8547	.9390
-1.040	1.0963	.8183	.8640	.9435

TABLE 9.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 22.43$ psf (1073.74 N/m^2);
$q_\infty = 244.93$ psf (11727.15 N/m^2);
$p_{t,\infty} = 3184.70$ psf (152484.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.7272	.6441	.6107	.8427
.988	1.4180	.5852	.6424	.8621
.936	1.1088	.5476	.7027	.8949
.884	1.0022	.5050	.7098	.8984
.832	.8956	.4703	.7247	.9056
.780	.8103	.4405	.7373	.9114
.728	.7250	.4213	.7623	.9225
.676	.6823	.4063	.7717	.9265
.624	.6397	.3914	.7822	.9309
.572	.5757	.3823	.8149	.9437
.520	.5118	.3732	.8540	.9578
.468	.4584	.3585	.8844	.9678
.416	.4051	.3385	.9141	.9770
.364	.4371	.2660	.7801	.9300
.312	.4691	.0785	.4090	.6729
.260	.4691	.0140	.1726	.3352
.208	.4691	.0056	.1097	.2185
.156	.4904	.0038	.0885	.1775
.104	.5118	.0020	.0621	.1254
.052	.4904	.0083	.1300	.2571
0.000	.4691	.0140	.1726	.3352
-.104	.4904	.0083	.1304	.2579
-.156	.4904	.0039	.0891	.1786
-.208	.4904	.0083	.1304	.2579
-.260	.5011	.0530	.3253	.5725
-.312	.5011	.2275	.6737	.8798
-.364	.5118	.3204	.7913	.9346
-.416	.5118	.3417	.8171	.9446
-.468	.5224	.3468	.8147	.9437
-.520	.5331	.3572	.8185	.9451
-.572	.5544	.3700	.8169	.9445
-.624	.5757	.3828	.8154	.9439
-.676	.6504	.3969	.7812	.9305
-.728	.7250	.4164	.7579	.9206
-.780	.7996	.4386	.7406	.9130
-.832	.8742	.4634	.7280	.9072
-.884	.9595	.4959	.7189	.9028
-.936	1.0448	.5391	.7183	.9025
-.988	1.1834	.5890	.7055	.8962
-1.040	1.3220	.6655	.7095	.8982

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 22.42$ psf (1073.71 N/m^2);
$q_\infty = 244.92$ psf (11726.78 N/m^2);
$p_{t,\infty} = 3184.60$ psf (152479.47 N/m^2);

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3641	.5200	.6174	.8470
.988	1.0870	.4843	.6675	.8764
.936	.8099	.4618	.7551	.9194
.884	.7460	.4341	.7628	.9228
.832	.6820	.4170	.7819	.9308
.780	.6394	.3994	.7903	.9342
.728	.5968	.3925	.8109	.9422
.676	.5755	.3823	.8151	.9438
.624	.5542	.3749	.8225	.9466
.572	.5222	.3703	.8421	.9537
.520	.4902	.3658	.8638	.9611
.468	.4582	.3612	.8878	.9689
.416	.4263	.3593	.9181	.9781
.364	.6074	.3603	.7701	.9259
.312	.7886	.4782	.7787	.9295
.260	.9058	.4781	.7265	.9064
.208	1.0231	.3953	.6216	.8496
.156	1.0444	.2212	.4602	.7249
.104	1.0657	.1396	.3620	.6191
.052	1.1510	.2183	.4355	.7007
0.000	1.2362	.3499	.5320	.7870
-.104	1.4707	.4918	.5783	.8212
-.156	1.2362	.5404	.6612	.8729
-.208	1.0018	.5088	.7127	.8998
-.260	1.0018	.4395	.6624	.8735
-.312	.7673	.4346	.7526	.9183
-.364	.7673	.4346	.7526	.9183
-.416	.5328	.3576	.8192	.9454
-.468	.5328	.3549	.8161	.9442
-.520	.5328	.3523	.8131	.9431
-.572	.5222	.3552	.8247	.9474
-.624	.5115	.3608	.8398	.9528
-.676	.5542	.3704	.8176	.9447
-.728	.5968	.3827	.8008	.9383
-.780	.6394	.3950	.7860	.9324
-.832	.6820	.4126	.7778	.9291
-.884	.7247	.4329	.7729	.9271
-.936	.7673	.4612	.7753	.9280
-.988	.8419	.4914	.7640	.9233
-1.040	.9165	.5376	.7659	.9241

TABLE 9.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 5^{\circ}$;

p_∞ = 22.45 psf (1074.82 N/m^2);
q_∞ = 245.17 psf (11738.93 N/m^2);
$p_{t,\infty}$ = 3187.90 psf (152637.47 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1716	.4604	.6268	.8528
.988	.9160	.4374	.6911	.8889
.936	.6604	.4224	.7998	.9379
.884	.6284	.4099	.8076	.9410
.832	.5964	.4000	.8189	.9453
.780	.5751	.3952	.8289	.9489
.728	.5538	.3878	.8367	.9518
.676	.5538	.3851	.8339	.9507
.624	.5538	.3824	.8310	.9497
.572	.6391	.3804	.7715	.9265
.520	.7243	.4607	.7975	.9371
.468	.9053	.4696	.7202	.9034
.416	1.0864	.5263	.6960	.8915
.364	1.2248	.5628	.6778	.8820
.312	1.3633	.5514	.6359	.8583
.260	1.3527	.5011	.6086	.8414
.208	1.3420	.4454	.5761	.8196
.156	1.4166	.3582	.5028	.7631
.104	1.4911	.3348	.4739	.7376
.052	1.5231	.3741	.4956	.7569
0.000	1.5550	.4373	.5303	.7856
-.104	1.7254	.5509	.5650	.8118
-.156	1.7574	.5714	.5702	.8155
-.208	1.7893	.5866	.5726	.8172
-.260	1.2355	.6004	.6971	.8920
-.312	1.2675	.5677	.6693	.8773
-.364	1.2888	.4553	.5944	.8321
-.416	.7456	.4208	.7513	.9177
-.468	.7669	.4256	.7450	.9149
-.520	.7882	.4357	.7435	.9143
-.572	.6604	.4574	.8323	.9502
-.624	.5325	.3754	.8396	.9528
-.676	.5538	.3749	.8227	.9467
-.728	.5751	.3797	.8125	.9428
-.780	.5858	.3874	.8133	.9431
-.832	.5964	.4005	.8194	.9454
-.884	.6178	.4159	.8205	.9459
-.936	.6391	.4367	.8266	.9481
-.988	.6817	.4569	.8187	.9452
-1.040	.7243	.4905	.8229	.9467

(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^{\circ}$;

p_∞ = 22.43 psf (1074.11 N/m^2);
q_∞ = 245.01 psf (11731.20 N/m^2);
$p_{t,\infty}$ = 3185.80 psf (152536.93 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0863	.4362	.6336	.8569
.988	.8520	.4207	.7027	.8948
.936	.6177	.4157	.8204	.9458
.884	.6071	.4080	.8198	.9456
.832	.5964	.4029	.8219	.9464
.780	.6603	.4041	.7822	.9309
.728	.7242	.4637	.8001	.9381
.676	.7668	.4573	.7722	.9268
.624	.8094	.4935	.7808	.9303
.572	1.0011	.5473	.7394	.9124
.520	1.1929	.5506	.6794	.8828
.468	1.2568	.5517	.6626	.8737
.416	1.3207	.5528	.6470	.8648
.364	1.3100	.5398	.6419	.8618
.312	1.2994	.5028	.6220	.8499
.260	1.2568	.4585	.6040	.8385
.208	1.2142	.4170	.5860	.8265
.156	1.2461	.3789	.5514	.8018
.104	1.2781	.3807	.5458	.7976
.052	1.2887	.3938	.5528	.8028
0.000	1.2994	.4282	.5740	.8182
-.104	1.3633	.4970	.6038	.8383
-.156	1.3952	.5149	.6075	.8407
-.208	1.4272	.5248	.6064	.8400
-.260	1.3739	.5341	.6235	.8508
-.312	1.4059	.5386	.6190	.8480
-.364	1.2035	.5490	.6754	.8807
-.416	1.3846	.5525	.6317	.8558
-.468	1.1822	.5629	.6900	.8884
-.520	.9798	.4425	.6720	.8789
-.572	.8414	.4113	.6991	.8931
-.624	.7029	.4226	.7754	.9281
-.676	.7455	.4349	.7638	.9232
-.728	.7881	.4499	.7555	.9196
-.780	.6923	.4735	.8270	.9482
-.832	.5964	.4039	.8229	.9467
-.884	.5964	.4119	.8310	.9497
-.936	.5964	.4278	.8470	.9554
-.988	.6284	.4457	.8422	.9537
-1.040	.6603	.4716	.8451	.9547

TABLE 9.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 22.45$ psf (1074.86 N/m^2);
$q_\infty = 245.18$ psf (11739.30 N/m^2);
$p_{t,\infty} = 3188.00$ psf (152642.26 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0438	.4321	.6434	.8627
.988	.9053	.4462	.7020	.8945
.936	.7668	.4814	.7924	.9350
.884	.7668	.4655	.7791	.9296
.832	.7668	.4628	.7769	.9287
.780	.9053	.5286	.7642	.9233
.728	1.0438	.5386	.7183	.9025
.676	1.0864	.5508	.7121	.8995
.624	1.1290	.5524	.6995	.8933
.572	1.1503	.5439	.6877	.8872
.520	1.1716	.5354	.6760	.8810
.468	1.1503	.5227	.6741	.8800
.416	1.1290	.5019	.6667	.8760
.364	1.1183	.4782	.6539	.8688
.312	1.1077	.4518	.6387	.8599
.260	1.0864	.4177	.6201	.8487
.208	1.0651	.3969	.6105	.8426
.156	1.0757	.3834	.5970	.8338
.104	1.0864	.3778	.5897	.8290
.052	1.0970	.3828	.5907	.8297
0.000	1.1077	.4039	.6038	.8383
-.104	1.1290	.4566	.6360	.8583
-.156	1.1609	.4718	.6375	.8592
-.208	1.1929	.4817	.6354	.8580
-.260	1.1503	.4907	.6532	.8684
-.312	1.1822	.4979	.6490	.8660
-.364	1.1822	.5006	.6507	.8670
-.416	1.1716	.5062	.6573	.8707
-.468	1.1716	.5141	.6625	.8736
-.520	1.1716	.5248	.6693	.8774
-.572	1.1822	.5325	.6711	.8784
-.624	1.1929	.5429	.6746	.8803
-.676	.9585	.5646	.7675	.9248
-.728	.7242	.4319	.7723	.9268
-.780	.7242	.4373	.7770	.9288
-.832	.7242	.4532	.7911	.9345
-.884	.7455	.4766	.7996	.9379
-.936	.7668	.5027	.8097	.9418
-.988	.6923	.5338	.8781	.9658
-1.040	.6177	.4771	.8788	.9660

(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 22.43$ psf (1073.84 N/m^2);
$q_\infty = 244.95$ psf (11728.26 N/m^2);
$p_{t,\infty} = 3185.00$ psf (152498.62 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.4695	.6052	.6417	.8617
.988	1.2566	.5785	.6785	.8823
.936	1.0436	.5624	.7341	.9100
.884	1.0329	.5414	.7240	.9052
.832	1.0223	.5310	.7207	.9037
.780	1.0116	.5206	.7174	.9021
.728	1.0010	.5129	.7158	.9013
.676	.9903	.5052	.7142	.9006
.624	.9797	.4975	.7126	.8998
.572	.9797	.4895	.7069	.8969
.520	.9797	.4789	.6991	.8931
.468	.9584	.4661	.6974	.8922
.416	.9371	.4480	.6914	.8891
.364	.9371	.4293	.6769	.8815
.312	.9371	.4107	.6620	.8734
.260	.9264	.3923	.6508	.8670
.208	.9158	.3846	.6481	.8654
.156	.9264	.3737	.6351	.8578
.104	.9371	.3708	.6290	.8541
.052	.9371	.3708	.6290	.8541
0.000	.9371	.3788	.6358	.8582
-.104	.9371	.4090	.6607	.8726
-.156	.9584	.4218	.6634	.8741
-.208	.9797	.4320	.6640	.8745
-.260	.9584	.4405	.6779	.8820
-.312	.9797	.4453	.6742	.8800
-.364	.9797	.4506	.6782	.8822
-.416	.9797	.4560	.6822	.8843
-.468	.9797	.4613	.6862	.8864
-.520	.9797	.4693	.6921	.8895
-.572	.9903	.4770	.6940	.8905
-.624	1.0010	.4821	.6940	.8904
-.676	1.0010	.4928	.7016	.8943
-.728	1.0010	.5061	.7111	.8990
-.780	1.0010	.5194	.7204	.9035
-.832	1.0010	.5381	.7332	.9096
-.884	1.0436	.5637	.7350	.9104
-.936	1.0862	.5973	.7416	.9134
-.988	1.0862	.6320	.7628	.9228
-1.040	1.0862	.6746	.7881	.9333

TABLE 9.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 5^\circ$;

p_∞ = 22.43 psf (1073.81 N/m²);
q_∞ = 244.94 psf (11727.89 N/m²);
$p_{t,\infty}$ = 3184.90 psf (152493.83 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.3640	.5573	.6392	.8602
.988	1.1508	.5386	.6841	.8853
.936	.9377	.5252	.7484	.9164
.884	.9271	.5095	.7413	.9133
.832	.9164	.5017	.7399	.9127
.780	.8951	.4916	.7411	.9132
.728	.8738	.4815	.7423	.9137
.676	.8738	.4735	.7361	.9109
.624	.8738	.4655	.7299	.9080
.572	.8631	.4578	.7283	.9073
.520	.8525	.4474	.7245	.9055
.468	.8418	.4344	.7183	.9025
.416	.8312	.4187	.7097	.8984
.364	.8205	.4030	.7008	.8939
.312	.8099	.3926	.6963	.8916
.260	.8099	.3793	.6844	.8854
.208	.8099	.3740	.6795	.8829
.156	.8099	.3687	.6747	.8803
.104	.8099	.3633	.6698	.8776
.052	.8205	.3631	.6652	.8751
0.000	.8312	.3681	.6655	.8753
-.104	.8312	.3903	.6853	.8859
-.156	.8525	.4005	.6854	.8860
-.208	.8738	.4106	.6855	.8861
-.260	.8525	.4191	.7012	.8941
-.312	.8738	.4240	.6966	.8918
-.364	.8631	.4269	.7033	.8951
-.416	.8738	.4346	.7053	.8961
-.468	.8631	.4349	.7098	.8984
-.520	.8525	.4431	.7210	.9038
-.572	.8631	.4482	.7206	.9036
-.624	.8738	.4533	.7203	.9035
-.676	.8844	.4610	.7220	.9043
-.728	.8951	.4714	.7257	.9061
-.780	.8951	.4848	.7359	.9108
-.832	.8951	.5008	.7480	.9163
-.884	.9164	.5189	.7525	.9183
-.936	.9377	.5450	.7624	.9226
-.988	.9590	.5712	.7717	.9266
-1.040	.9803	.6053	.7858	.9324

(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^\circ$;

p_∞ = 22.45 psf (1074.99 N/m²);
q_∞ = 245.21 psf (11740.78 N/m²);
$p_{t,\infty}$ = 3188.40 psf (152661.41 N/m²)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2986	.5343	.6414	.8616
.988	1.0857	.5183	.6909	.8889
.936	.8728	.5102	.7645	.9235
.884	.8728	.4969	.7545	.9192
.832	.8728	.4889	.7485	.9165
.780	.8622	.4812	.7471	.9159
.728	.8515	.4735	.7457	.9153
.676	.8409	.4658	.7443	.9146
.624	.8303	.4581	.7428	.9140
.572	.8303	.4475	.7341	.9100
.520	.8303	.4395	.7276	.9069
.468	.8196	.4265	.7213	.9040
.416	.8090	.4134	.7149	.9009
.364	.8090	.4001	.7033	.8952
.312	.8090	.3922	.6963	.8916
.260	.7983	.3818	.6916	.8892
.208	.7877	.3767	.6916	.8892
.156	.7983	.3685	.6794	.8828
.104	.8090	.3656	.6723	.8790
.052	.8090	.3656	.6723	.8790
0.000	.8090	.3682	.6747	.8803
-.104	.8090	.3846	.6896	.8882
-.156	.8196	.3924	.6919	.8894
-.208	.8303	.4028	.6965	.8917
-.260	.8196	.4110	.7081	.8976
-.312	.8303	.4161	.7079	.8974
-.364	.8303	.4187	.7102	.8986
-.416	.8303	.4240	.7147	.9008
-.468	.8303	.4294	.7191	.9029
-.520	.8303	.4320	.7214	.9040
-.572	.8303	.4347	.7236	.9050
-.624	.8303	.4427	.7302	.9082
-.676	.8303	.4480	.7346	.9102
-.728	.8303	.4586	.7432	.9141
-.780	.8409	.4690	.7468	.9158
-.832	.8515	.4820	.7524	.9182
-.884	.8622	.4977	.7598	.9215
-.936	.8728	.5214	.7729	.9271
-.988	.8835	.5451	.7855	.9322
-1.040	.8941	.5741	.8013	.9385

TABLE 9.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 22.43$ psf (1074.18 N/m^2);
$q_\infty = 245.03$ psf (11731.94 N/m^2);
$p_{t,\infty} = 3186.00$ psf (152546.50 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2999	.5347	.6414	.8615
.988	1.0868	.5160	.6891	.8879
.936	.8737	.5079	.7625	.9226
.884	.8630	.4949	.7572	.9204
.832	.8524	.4872	.7560	.9198
.780	.8417	.4794	.7547	.9193
.728	.8311	.4717	.7534	.9187
.676	.8417	.4661	.7442	.9146
.624	.8524	.4579	.7330	.9094
.572	.8417	.4502	.7313	.9087
.520	.8311	.4398	.7275	.9069
.468	.8204	.4268	.7212	.9039
.416	.8098	.4137	.7148	.9008
.364	.8098	.4031	.7056	.8963
.312	.8098	.3951	.6985	.8928
.260	.8098	.3871	.6914	.8891
.208	.8098	.3818	.6867	.8867
.156	.8098	.3765	.6819	.8841
.104	.8098	.3738	.6795	.8829
.052	.8098	.3712	.6770	.8816
0.000	.8098	.3738	.6795	.8829
-.104	.8098	.3849	.6895	.8881
-.156	.8204	.3927	.6918	.8893
-.208	.8311	.4031	.6964	.8917
-.260	.8204	.4086	.7058	.8964
-.312	.8311	.4164	.7078	.8974
-.364	.8204	.4193	.7149	.9009
-.416	.8311	.4217	.7123	.8996
-.468	.8204	.4273	.7217	.9041
-.520	.8098	.4302	.7289	.9075
-.572	.8098	.4329	.7311	.9086
-.624	.8098	.4382	.7356	.9107
-.676	.8098	.4435	.7401	.9127
-.728	.8098	.4515	.7467	.9157
-.780	.8098	.4595	.7533	.9186
-.832	.8098	.4728	.7641	.9233
-.884	.8311	.4882	.7665	.9243
-.936	.8524	.5117	.7748	.9278
-.988	.8524	.5303	.7888	.9336
-1.040	.8524	.5596	.8102	.9420

(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^\circ$;

$p_\infty = 22.46$ psf (1075.36 N/m^2);
$q_\infty = 245.30$ psf (11744.83 N/m^2);
$p_{t,\infty} = 3189.50$ psf (152714.08 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2769	.5267	.6422	.8620
.988	1.0641	.5107	.6928	.8898
.936	.8512	.4999	.7663	.9243
.884	.8406	.4895	.7631	.9229
.832	.8300	.4818	.7619	.9224
.780	.8193	.4741	.7607	.9219
.728	.8087	.4691	.7616	.9223
.676	.8193	.4582	.7478	.9162
.624	.8300	.4526	.7385	.9120
.572	.8300	.4447	.7319	.9090
.520	.8300	.4340	.7231	.9048
.468	.8406	.4258	.7117	.8993
.416	.8512	.4176	.7004	.8937
.364	.8619	.4173	.6958	.8914
.312	.8725	.4144	.6891	.8879
.260	.8938	.4139	.6805	.8834
.208	.9151	.4187	.6764	.8812
.156	.9470	.4152	.6621	.8734
.104	.9789	.4144	.6506	.8669
.052	.9896	.4115	.6449	.8636
0.000	1.0002	.4139	.6433	.8626
-.104	.9789	.4229	.6573	.8707
-.156	.9683	.4311	.6673	.8763
-.208	.9577	.4367	.6753	.8806
-.260	.9151	.4378	.6917	.8892
-.312	.9045	.4380	.6959	.8914
-.364	.8832	.4385	.7047	.8958
-.416	.8512	.4340	.7140	.9005
-.468	.8300	.4345	.7236	.9050
-.520	.8087	.4350	.7335	.9097
-.572	.8087	.4324	.7312	.9086
-.624	.8087	.4350	.7335	.9097
-.676	.7980	.4380	.7408	.9131
-.728	.7874	.4462	.7528	.9184
-.780	.7980	.4539	.7542	.9190
-.832	.8087	.4670	.7599	.9215
-.884	.8087	.4829	.7728	.9270
-.936	.8087	.5068	.7917	.9347
-.988	.8193	.5278	.8026	.9391
-1.040	.8300	.5568	.8191	.9453

TABLE 9.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF A 120°-INCLUDED-ANGLE CONE AT A MACH NUMBER OF 3.95 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Concluded.

(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^\circ$;

p_∞ = 22.45 psf (1075.06 N/m^2);
q_∞ = 245.23 psf (11741.51 N/m^2);
$p_{t,\infty}$ = 3188.60 psf (152670.99 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2352	.5305	.6554	.8696
.988	1.0436	.5140	.7018	.8944
.936	.8519	.5080	.7722	.9268
.884	.8625	.5051	.7652	.9238
.832	.8732	.5048	.7604	.9217
.780	.9051	.5120	.7521	.9181
.728	.9371	.5245	.7482	.9164
.676	.9797	.5209	.7292	.9077
.624	1.0223	.5225	.7149	.9009
.572	1.0649	.5135	.6944	.8907
.520	1.1074	.5018	.6731	.8794
.468	1.1074	.4911	.6659	.8755
.416	1.1074	.4752	.6550	.8694
.364	1.0968	.4648	.6510	.8671
.312	1.0861	.4571	.6487	.8653
.260	1.0649	.4496	.6498	.8664
.208	1.0436	.4449	.6529	.8682
.156	1.0542	.4366	.6436	.8628
.104	1.0649	.4310	.6362	.8585
.052	1.0649	.4284	.6343	.8573
0.000	1.0649	.4310	.6362	.8585
-.104	1.0649	.4422	.6444	.8633
-.156	1.0755	.4526	.6487	.8658
-.208	1.0861	.4630	.6529	.8682
-.260	1.0542	.4717	.6689	.8772
-.312	1.0649	.4795	.6710	.8783
-.364	1.0649	.4848	.6747	.8803
-.416	1.0436	.4906	.6857	.8861
-.468	1.0436	.4933	.6875	.8871
-.520	1.0436	.4933	.6875	.8871
-.572	1.0436	.4986	.6912	.8890
-.624	1.0436	.4986	.6912	.8890
-.676	1.0010	.4997	.7065	.8968
-.728	.9584	.5007	.7228	.9047
-.780	.8945	.4863	.7373	.9115
-.832	.8306	.4852	.7643	.9234
-.884	.8199	.4854	.7694	.9256
-.936	.8093	.5017	.7873	.9330
-.988	.8093	.5203	.8018	.9387
-1.040	.8093	.5495	.8240	.9471

TABLE 10.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF THE SPED-II VEHICLE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 221.88$ psf (10623.88 N/m^2);
$q_\infty = 397.62$ psf (19037.98 N/m^2);
$p_{t,\infty} = 943.10$ psf (45155.87 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7872	.9079	1.0739	1.0471
.988	.7656	.9098	1.0901	1.0569
.936	.7440	.8886	1.0928	1.0586
.884	.7171	.8881	1.1129	1.0705
.832	.6901	.8760	1.1266	1.0785
.780	.6783	.8515	1.1204	1.0749
.728	.6664	.8418	1.1239	1.0770
.676	.6265	.8318	1.1523	1.0932
.624	.5866	.6695	1.0683	1.0437
.572	.5812	.1629	.5294	.6087
.520	.5758	.0304	.2297	.2787
.468	.5737	.0055	.0975	.1196
.416	.5715	.0007	.0341	.0419
.364	.5704	.0013	.0471	.0578
.312	.5693	0.0000	0.0000	0.0000
.260	.5683	0.0000	0.0000	0.0000
.208	.5672	0.0000	0.0000	0.0000
.156	.5683	0.0000	0.0000	0.0000
.104	.5672	0.0000	0.0000	0.0000
.052	.5661	0.0000	0.0000	0.0000
0.000	.5672	0.0000	0.0000	0.0000
-.052	.5661	0.0000	0.0000	0.0000
-.104	.5650	0.0000	0.0000	0.0000
-.156	.5661	0.0000	0.0000	0.0000
-.208	.5672	0.0000	0.0000	0.0000
-.260	.5672	0.0000	0.0000	0.0000
-.312	.5672	0.0000	0.0000	0.0000
-.364	.5672	0.0000	0.0000	0.0000
-.416	.5672	.0020	.0595	.0730
-.468	.5704	.0091	.1265	.1549
-.520	.5737	.0248	.2077	.2526
-.572	.5790	.2174	.6128	.6901
-.624	.5844	.7169	1.1075	1.0673
-.676	.6114	.8361	1.1694	1.1028
-.728	.6384	.8548	1.1572	1.0960
-.780	.6696	.8513	1.1275	1.0791
-.832	.7009	.8693	1.1136	1.0709
-.884	.7268	.8782	1.0992	1.0624
-.936	.7527	.8887	1.0866	1.0548
-.988	.7818	.9053	1.0761	1.0484
-1.040	.8109	.9054	1.0567	1.0364

(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 0^\circ$;

$p_\infty = 221.44$ psf (10602.47 N/m^2);
$q_\infty = 396.82$ psf (18999.63 N/m^2);
$p_{t,\infty} = 941.20$ psf (45064.90 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.9031	.9390	1.0197	1.0129
.988	.8944	.9255	1.0172	1.0113
.936	.8858	.9120	1.0147	1.0096
.884	.8426	.9061	1.0370	1.0240
.832	.7994	.9051	1.0641	1.0410
.780	.7518	.8865	1.0859	1.0544
.728	.7043	.8729	1.1133	1.0707
.676	.6687	.8605	1.1344	1.0830
.624	.6330	.8465	1.1564	1.0955
.572	.6060	.6187	1.0104	1.0068
.520	.5790	.2980	.7174	.7848
.468	.5779	.1100	.4364	.5122
.416	.5768	.0301	.2286	.2774
.364	.5758	.0105	.1352	.1655
.312	.5747	.0052	.0950	.1165
.260	.5768	.0010	.0414	.0509
.208	.5790	0.0000	0.0000	0.0000
.156	.5812	0.0000	0.0000	0.0000
.104	.5833	0.0000	0.0000	0.0000
.052	.5812	0.0000	0.0000	0.0000
0.000	.5876	0.0000	0.0000	0.0000
-.052	.5855	0.0000	0.0000	0.0000
-.104	.5833	0.0000	0.0000	0.0000
-.156	.5790	0.0000	0.0000	0.0000
-.208	.5747	0.0000	0.0000	0.0000
-.260	.5747	0.0000	0.0000	0.0000
-.312	.5747	0.0000	0.0000	0.0000
-.364	.5768	.0063	.1041	.1277
-.416	.5790	.0339	.2420	.2932
-.468	.5844	.1231	.4589	.5361
-.520	.5898	.3280	.7457	.8090
-.572	.6179	.7328	1.0890	1.0563
-.624	.6460	.8505	1.1475	1.0905
-.676	.6978	.8668	1.1145	1.0715
-.728	.7497	.8780	1.0822	1.0522
-.780	.7918	.8925	1.0617	1.0395
-.832	.8339	.9019	1.0400	1.0259
-.884	.8242	.9185	1.0557	1.0358
-.936	.8145	.9351	1.0715	1.0456
-.988	.7821	.9471	1.1005	1.0631
-1.040	.7497	.9525	1.1272	1.0788

TABLE 10.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF THE SPED-II VEHICLE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER)

– Continued

(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 221.88$ psf (10623.88 N/m^2);
$q_\infty = 397.62$ psf (19037.98 N/m^2);
$p_{t,\infty} = 943.10$ psf (45155.87 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.7460	.9093	1.1040	1.0652
.988	.7331	.9081	1.1130	1.0706
.936	.7201	.8986	1.1171	1.0730
.884	.7007	.8886	1.1261	1.0782
.832	.6813	.8885	1.1419	1.0873
.780	.6813	.8802	1.1366	1.0843
.728	.6813	.8736	1.1323	1.0818
.676	.6910	.8736	1.1244	1.0772
.624	.7007	.8820	1.1219	1.0758
.572	.7050	.8746	1.1138	1.0710
.520	.7094	.7776	1.0470	1.0303
.468	.7104	.4785	.8207	.8702
.416	.7115	.2385	.5790	.6577
.364	.7094	.1190	.4096	.4833
.312	.7072	.0498	.2653	.3205
.260	.7137	.0180	.1587	.1939
.208	.7201	0.0000	0.0000	0.0000
.156	.7191	0.0000	0.0000	0.0000
.104	.7255	0.0000	0.0000	0.0000
.052	.7191	0.0000	0.0000	0.0000
0.000	.7309	0.0000	0.0000	0.0000
-.052	.7245	0.0000	0.0000	0.0000
-.104	.7180	0.0000	0.0000	0.0000
-.156	.7137	0.0000	0.0000	0.0000
-.208	.7094	.0063	.0945	.1159
-.260	.7018	.0192	.1656	.2022
-.312	.6943	.0622	.2992	.3598
-.364	.7018	.1101	.3961	.4686
-.416	.7094	.2759	.6236	.7003
-.468	.7072	.5450	.8778	.9141
-.520	.7050	.7932	1.0607	1.0389
-.572	.6910	.8731	1.1240	1.0770
-.624	.6770	.8787	1.1393	1.0858
-.676	.6792	.8751	1.1351	1.0834
-.728	.6813	.8763	1.1341	1.0829
-.780	.6943	.8742	1.1221	1.0759
-.832	.7072	.8787	1.1147	1.0715
-.884	.7169	.8837	1.1102	1.0689
-.936	.7266	.9018	1.1141	1.0712
-.988	.7460	.8986	1.0975	1.0614
-1.040	.7654	.9053	1.0875	1.0554

(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 220.61$ psf (10563.04 N/m^2);
$q_\infty = 395.34$ psf (18928.98 N/m^2);
$p_{t,\infty} = 937.70$ psf (44897.32 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.6701	.8933	1.1546	1.0945
.988	.6885	.8836	1.1329	1.0821
.936	.7069	.9005	1.1287	1.0797
.884	.7319	.8981	1.1077	1.0675
.832	.7568	.9056	1.0939	1.0592
.780	.8067	.9072	1.0605	1.0388
.728	.8566	.9038	1.0272	1.0177
.676	.8858	.9172	1.0175	1.0115
.624	.9151	.9238	1.0048	1.0031
.572	.9617	.9325	.9847	.9898
.520	1.0084	.9159	.9530	.9682
.468	1.0019	.9002	.9479	.9646
.416	.9954	.7951	.8937	.9258
.364	.9878	.6206	.7926	.8478
.312	.9802	.4327	.6645	.7379
.260	.9845	.2916	.5443	.6236
.208	.9888	.1810	.4278	.5031
.156	.9975	.1650	.4067	.4802
.104	1.0019	.1379	.3710	.4409
.052	.9932	.1002	.3176	.3808
0.000	1.0149	.1110	.3307	.3957
-.052	1.0062	.1313	.3613	.4301
-.104	.9975	.1679	.4103	.4841
-.156	.9921	.1580	.3990	.4718
-.208	.9867	.1991	.4492	.5258
-.260	.9856	.2955	.5476	.6269
-.312	.9845	.4586	.6825	.7541
-.364	.9888	.6503	.8109	.8625
-.416	.9932	.8512	.9257	.9490
-.468	.9867	.9127	.9618	.9742
-.520	.9802	.9206	.9691	.9793
-.572	.9325	.9206	.9936	.9958
-.624	.8848	.9188	1.0191	1.0125
-.676	.8566	.9086	1.0299	1.0195
-.728	.8284	.9034	1.0443	1.0287
-.780	.7937	.8960	1.0625	1.0400
-.832	.7590	.8935	1.0850	1.0538
-.884	.7232	.8928	1.1111	1.0694
-.936	.6874	.8921	1.1392	1.0858
-.988	.6820	.8830	1.1379	1.0850
-1.040	.6766	.8972	1.1515	1.0928

TABLE 10.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF THE SPED-II VEHICLE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 221.93$ psf (10626.13 N/m^2);
$q_\infty = 397.70$ psf (19042.02 N/m^2);
$p_{t,\infty} = 943.30$ psf (45165.45 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	.8170	.9490	1.0778	1.0494
.988	.9021	.9645	1.0340	1.0221
.936	.9873	.9497	.9808	.9872
.884	1.0045	.9534	.9742	.9827
.832	1.0218	.9470	.9627	.9749
.780	1.0293	.9457	.9585	.9720
.728	1.0369	.9477	.9560	.9703
.676	1.0703	.9384	.9364	.9565
.624	1.1037	.9323	.9191	.9443
.572	1.1403	.9307	.9034	.9329
.520	1.1770	.9222	.8852	.9195
.468	1.2093	.9128	.8688	.9073
.416	1.2417	.8779	.8408	.8859
.364	1.2406	.8185	.8123	.8635
.312	1.2395	.7241	.7643	.8246
.260	1.2373	.6106	.7025	.7718
.208	1.2352	.5351	.6582	.7322
.156	1.2632	.4997	.6289	.7052
.104	1.2611	.4927	.6250	.7016
.052	1.2427	.4356	.5920	.6703
0.000	1.2869	.4216	.5724	.6513
-.052	1.2686	.4527	.5974	.6754
-.104	1.2503	.4757	.6168	.6939
-.156	1.2567	.4641	.6077	.6853
-.208	1.2632	.5545	.6626	.7362
-.260	1.2524	.6396	.7146	.7824
-.312	1.2417	.7446	.7744	.8329
-.364	1.2223	.8491	.8335	.8802
-.416	1.2029	.9018	.8659	.9051
-.468	1.1694	.9249	.8893	.9226
-.520	1.1360	.9277	.9037	.9331
-.572	1.1048	.9334	.9192	.9443
-.624	1.0735	.9324	.9319	.9534
-.676	1.0627	.9343	.9376	.9574
-.728	1.0520	.9296	.9400	.9591
-.780	1.0293	.9386	.9549	.9695
-.832	1.0067	.9376	.9651	.9765
-.884	.9657	.9498	.9917	.9945
-.936	.9248	.9519	1.0146	1.0096
-.988	.8482	.9500	1.0583	1.0374
-1.040	.7717	.9364	1.1016	1.0638

(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 221.55$ psf (10608.10 N/m^2);
$q_\infty = 397.03$ psf (19009.72 N/m^2);
$p_{t,\infty} = 941.70$ psf (45088.84 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1652	.9664	.9107	.9382
.988	1.1684	.9574	.9052	.9342
.936	1.1716	.9602	.9053	.9343
.884	1.1727	.9516	.9008	.9310
.832	1.1738	.9497	.8995	.9300
.780	1.1522	.9503	.9082	.9364
.728	1.1306	.9508	.9171	.9428
.676	1.1479	.9393	.9046	.9338
.624	1.1652	.9276	.8923	.9248
.572	1.1641	.9245	.8912	.9239
.520	1.1630	.9112	.8851	.9195
.468	1.1522	.8929	.8803	.9159
.416	1.1414	.8797	.8779	.9141
.364	1.1371	.8432	.8611	.9015
.312	1.1327	.8152	.8483	.8917
.260	1.1165	.7791	.8354	.8817
.208	1.1003	.7669	.8349	.8813
.156	1.1338	.7261	.8003	.8539
.104	1.1176	.6932	.7876	.8437
.052	1.1035	.6650	.7763	.8345
0.000	1.1349	.6341	.7475	.8105
-.052	1.1208	.6651	.7703	.8296
-.104	1.1068	.7160	.8043	.8572
-.156	1.1273	.7307	.8051	.8578
-.208	1.1479	.7573	.8122	.8635
-.260	1.1435	.7853	.8287	.8765
-.312	1.1392	.8336	.8554	.8971
-.364	1.1414	.8652	.8707	.9087
-.416	1.1435	.8951	.8847	.9192
-.468	1.1511	.9122	.8902	.9232
-.520	1.1587	.9158	.8890	.9224
-.572	1.1608	.9272	.8937	.9258
-.624	1.1630	.9301	.8943	.9262
-.676	1.1630	.9301	.8943	.9262
-.728	1.1630	.9368	.8975	.9286
-.780	1.1641	.9366	.8970	.9282
-.832	1.1652	.9482	.9021	.9320
-.884	1.1652	.9465	.9013	.9314
-.936	1.1652	.9532	.9045	.9337
-.988	1.1641	.9534	.9050	.9341
-1.040	1.1630	.9586	.9079	.9362

TABLE 10.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF THE SPED-II VEHICLE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65 × 10^6 PER FOOT (5.42 × 10^6 PER METER) – Continued

(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^o$;

p_∞ = 221.60 psf (10610.36 N/m^2);
q_∞ = 397.11 psf (19013.76 N/m^2);
$p_{t,\infty}$ = 941.90 psf (45098.42 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M^1/M^∞	V_1/V_∞
1.040	1.0504	.9566	.9543	.9691
.988	1.0568	.9555	.9508	.9667
.936	1.0633	.9493	.9448	.9625
.884	1.0568	.9504	.9483	.9649
.832	1.0504	.9432	.9476	.9644
.780	1.0363	.9474	.9561	.9703
.728	1.0223	.9482	.9631	.9751
.676	1.0352	.9291	.9474	.9642
.624	1.0482	.9218	.9378	.9575
.572	1.0493	.9182	.9355	.9559
.520	1.0504	.9012	.9263	.9494
.468	1.0471	.8951	.9246	.9482
.416	1.0439	.8822	.9193	.9444
.364	1.0396	.8611	.9101	.9378
.312	1.0352	.8417	.9017	.9317
.260	1.0233	.8270	.8990	.9297
.208	1.0115	.8073	.8934	.9256
.156	1.0331	.7830	.8706	.9086
.104	1.0212	.7479	.8558	.8974
.052	1.0179	.7128	.8368	.8828
0.000	1.0309	.7035	.8261	.8744
-.052	1.0277	.7245	.8397	.8850
-.104	1.0244	.7640	.8636	.9034
-.156	1.0439	.7705	.8591	.8999
-.208	1.0633	.7988	.8667	.9057
-.260	1.0568	.8236	.8828	.9177
-.312	1.0504	.8483	.8987	.9295
-.364	1.0536	.8728	.9102	.9378
-.416	1.0568	.8873	.9163	.9422
-.468	1.0579	.9089	.9269	.9498
-.520	1.0590	.9137	.9289	.9512
-.572	1.0633	.9246	.9325	.9538
-.624	1.0677	.9222	.9294	.9516
-.676	1.0677	.9288	.9327	.9540
-.728	1.0677	.9272	.9319	.9534
-.780	1.0698	.9351	.9349	.9555
-.832	1.0720	.9347	.9338	.9547
-.884	1.0741	.9477	.9393	.9586
-.936	1.0763	.9490	.9390	.9584
-.988	1.0752	.9559	.9429	.9611
-1.040	1.0741	.9527	.9418	.9603

(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^o$;

p_∞ = 222.00 psf (10629.51 N/m^2);
q_∞ = 397.83 psf (19048.08 N/m^2);
$p_{t,\infty}$ = 943.60 psf (45179.81 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1216	.9640	.9271	.9500
.988	1.1270	.9663	.9260	.9492
.936	1.1323	.9603	.9209	.9456
.884	1.1248	.9617	.9247	.9482
.832	1.1172	.9597	.9268	.9498
.780	1.1075	.9581	.9301	.9521
.728	1.0978	.9599	.9350	.9556
.676	1.1043	.9436	.9244	.9480
.624	1.1108	.9189	.9096	.9374
.572	1.0547	.9107	.9292	.9515
.520	.9986	.9040	.9514	.9671
.468	.9932	.8899	.9465	.9637
.416	.9878	.8708	.9389	.9583
.364	.9814	.8569	.9344	.9552
.312	.9749	.8379	.9271	.9500
.260	.9673	.8309	.9268	.9498
.208	.9598	.8138	.9208	.9455
.156	.9738	.7911	.9013	.9314
.104	.9663	.7622	.8882	.9217
.052	.9641	.7424	.8775	.9138
0.000	.9727	.7307	.8667	.9057
-.052	.9706	.7438	.8754	.9123
-.104	.9684	.7694	.8913	.9241
-.156	.9824	.7953	.8997	.9302
-.208	.9965	.8061	.8994	.9300
-.260	1.0223	.8348	.9036	.9331
-.312	1.0482	.8585	.9050	.9341
-.364	1.0827	.8790	.9010	.9312
-.416	1.1172	.8944	.8947	.9266
-.468	1.1248	.9114	.9002	.9305
-.520	1.1323	.9201	.9014	.9315
-.572	1.1291	.9307	.9079	.9362
-.624	1.1259	.9313	.9095	.9373
-.676	1.1356	.9362	.9080	.9362
-.728	1.1453	.9378	.9049	.9340
-.780	1.1367	.9444	.9115	.9388
-.832	1.1280	.9459	.9157	.9418
-.884	1.1237	.9551	.9219	.9463
-.936	1.1194	.9559	.9241	.9478
-.988	1.1183	.9611	.9270	.9499
-1.040	1.1172	.9562	.9251	.9486

TABLE 10.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF THE SPED-II VEHICLE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Continued

(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^o$;

$p_\infty = 221.79$ psf (10619.37 N/m^2);
$q_\infty = 397.45$ psf (19029.91 N/m^2);
$p_{t,\infty} = 942.70$ psf (45136.72 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.0200	.9647	.9725	.9816
.988	1.0265	.9669	.9706	.9802
.936	1.0330	.9558	.9619	.9743
.884	1.0341	.9589	.9630	.9751
.832	1.0351	.9554	.9607	.9735
.780	1.0718	.9489	.9409	.9597
.728	1.1085	.9540	.9277	.9504
.676	1.1376	.9454	.9116	.9389
.624	1.1667	.9367	.8960	.9275
.572	1.1753	.9199	.8847	.9192
.520	1.1839	.9082	.8758	.9126
.468	1.1936	.8878	.8624	.9024
.416	1.2033	.8825	.8564	.8979
.364	1.2217	.8638	.8408	.8859
.312	1.2400	.8500	.8279	.8759
.260	1.2562	.8280	.8119	.8632
.208	1.2723	.8042	.7950	.8497
.156	1.2540	.7753	.7863	.8426
.104	1.2702	.7478	.7673	.8270
.052	1.2508	.7363	.7672	.8270
0.000	1.2680	.7309	.7592	.8203
-.052	1.2486	.7426	.7712	.8303
-.104	1.2292	.7689	.7909	.8464
-.156	1.2260	.7918	.8036	.8567
-.208	1.2227	.8146	.8162	.8667
-.260	1.1947	.8438	.8404	.8856
-.312	1.1667	.8627	.8599	.9005
-.364	1.1397	.8829	.8801	.9158
-.416	1.1128	.8979	.8983	.9292
-.468	1.0739	.9084	.9197	.9447
-.520	1.0351	.9137	.9395	.9588
-.572	1.0200	.9181	.9487	.9652
-.624	1.0049	.9241	.9589	.9723
-.676	1.0049	.9357	.9650	.9764
-.728	1.0049	.9324	.9632	.9752
-.780	.9974	.9421	.9719	.9811
-.832	.9898	.9367	.9728	.9818
-.884	.9845	.9493	.9820	.9880
-.936	.9791	.9469	.9835	.9890
-.988	.9769	.9573	.9899	.9933
-1.040	.9747	.9493	.9869	.9913

(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^o$;

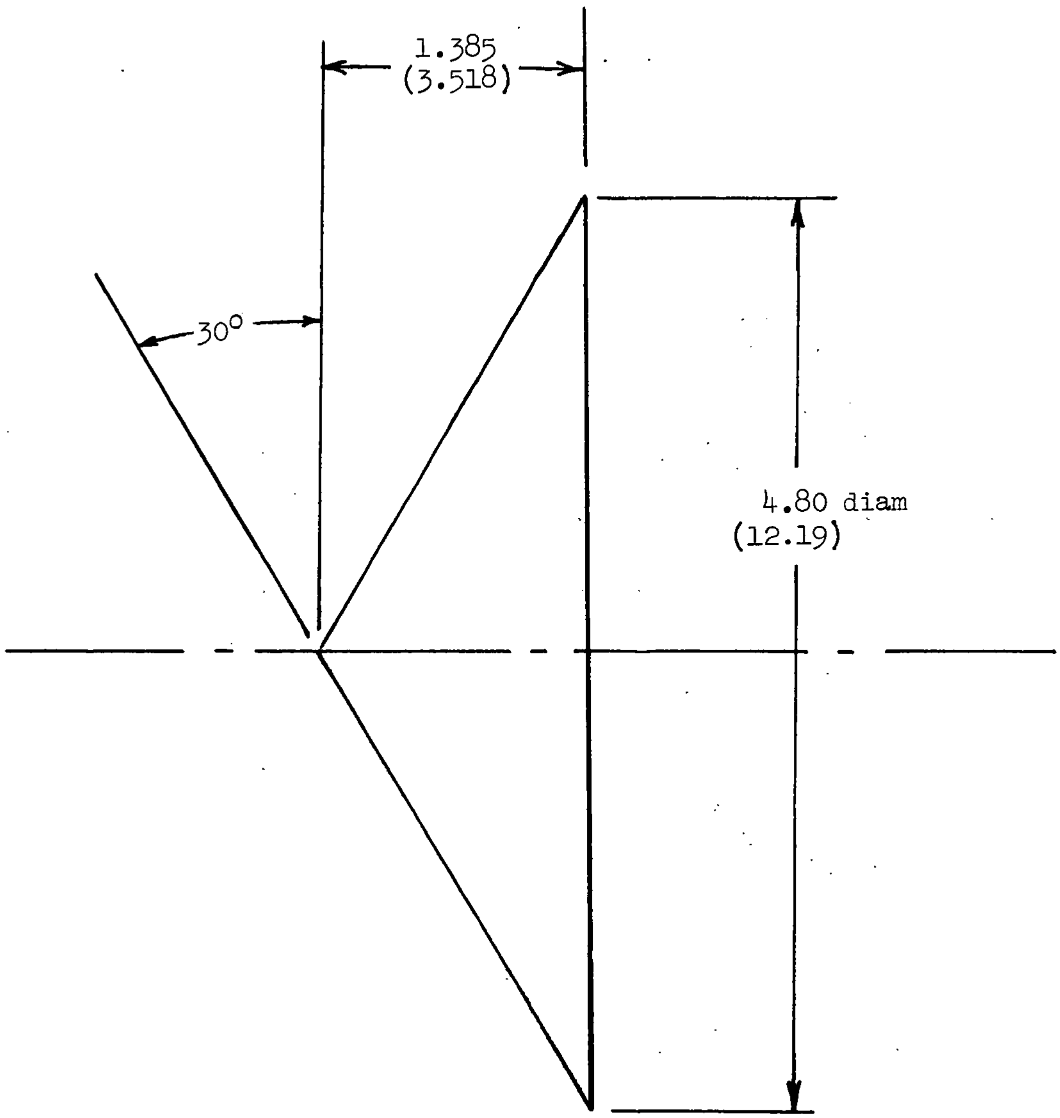
$p_\infty = 221.77$ psf (10618.24 N/m^2);
$q_\infty = 397.41$ psf (19027.89 N/m^2);
$p_{t,\infty} = 942.60$ psf (45131.93 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.2393	.9702	.8848	.9192
.988	1.2361	.9607	.8816	.9168
.936	1.2329	.9646	.8845	.9191
.884	1.2329	.9562	.8807	.9162
.832	1.2329	.9528	.8791	.9150
.780	1.2070	.9526	.8884	.9219
.728	1.1810	.9573	.9003	.9307
.676	1.2048	.9395	.8830	.9179
.624	1.2285	.9215	.8661	.9052
.572	1.2242	.9121	.8632	.9030
.520	1.2199	.9062	.8619	.9020
.468	1.2048	.8972	.8629	.9029
.416	1.1897	.8865	.8632	.9031
.364	1.1897	.8678	.8541	.8961
.312	1.1897	.8542	.8474	.8910
.260	1.1692	.8412	.8482	.8916
.208	1.1487	.8247	.8473	.8909
.156	1.1789	.7950	.8212	.8706
.104	1.1584	.7837	.8225	.8716
.052	1.1519	.7661	.8155	.8661
0.000	1.1681	.7561	.8045	.8574
-.052	1.1616	.7632	.8106	.8622
-.104	1.1551	.7832	.8234	.8724
-.156	1.1778	.7924	.8202	.8698
-.208	1.2005	.8083	.8206	.8701
-.260	1.1940	.8334	.8354	.8817
-.312	1.1875	.8549	.8485	.8918
-.364	1.1940	.8689	.8531	.8953
-.416	1.2005	.8896	.8608	.9013
-.468	1.2156	.9003	.8606	.9011
-.520	1.2307	.9092	.8595	.9003
-.572	1.2296	.9195	.8648	.9042
-.624	1.2285	.9299	.8700	.9082
-.676	1.2318	.9276	.8678	.9065
-.728	1.2350	.9404	.8726	.9102
-.780	1.2383	.9398	.8712	.9091
-.832	1.2415	.9493	.8744	.9115
-.884	1.2480	.9481	.8716	.9094
-.936	1.2545	.9587	.8742	.9113
-.988	1.2599	.9577	.8719	.9096
-1.040	1.2653	.9617	.8718	.9096

TABLE 10.- VARIATION OF p_1/p_∞, q_1/q_∞, M_1/M_∞ AND V_1/V_∞ WITH z/D AT THE CENTER OF WAKE OF THE SPED-II VEHICLE AT A MACH NUMBER OF 1.60 AND A REYNOLDS NUMBER OF 1.65×10^6 PER FOOT (5.42×10^6 PER METER) – Concluded.

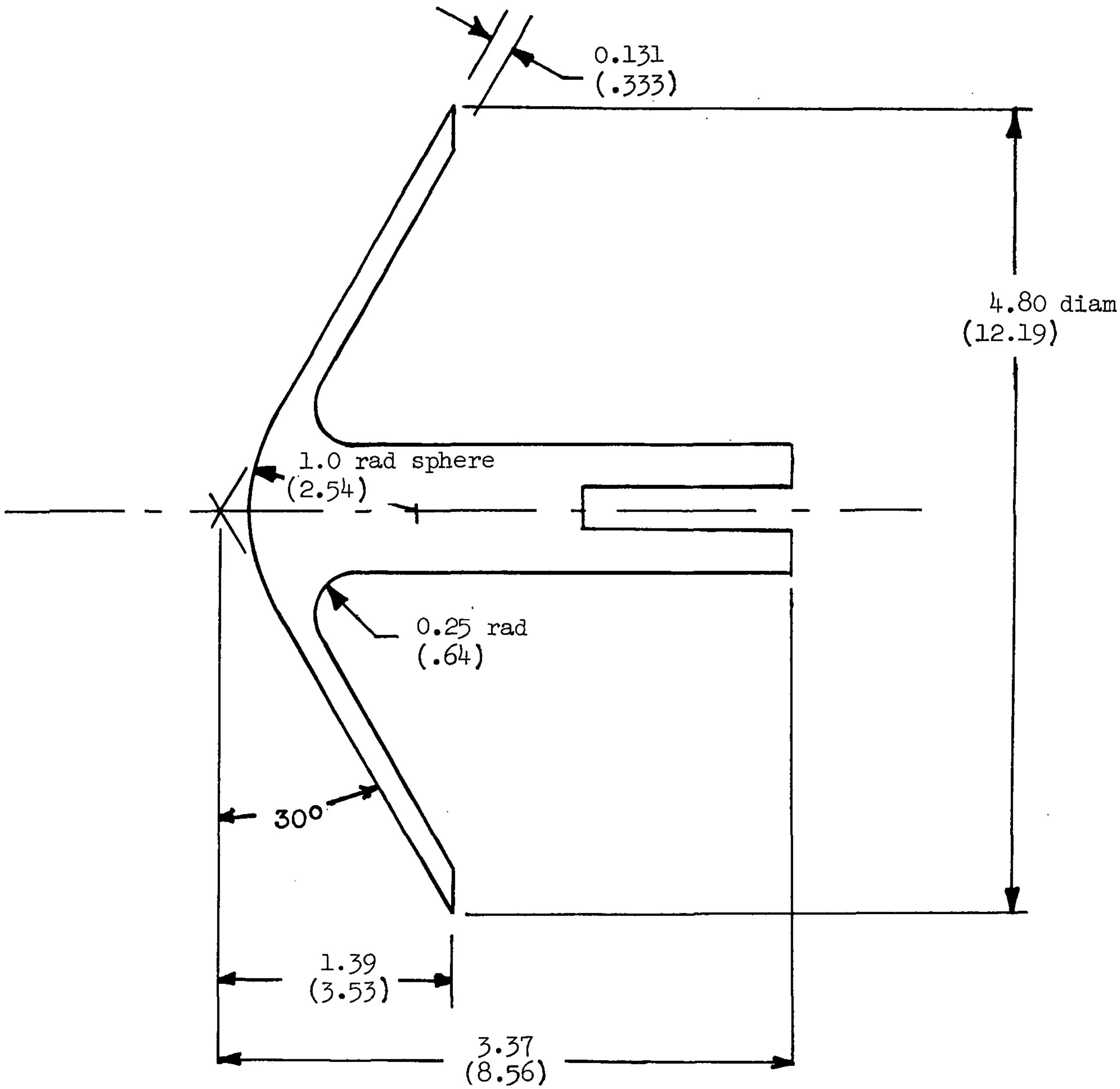
(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^\circ$;
$p_\infty = 221.93$ psf (10626.13 N/m^2);
$q_\infty = 397.70$ psf (19042.02 N/m^2);
$p_{t,\infty} = 943.30$ psf (45165.45 N/m^2)

z/D	p_1/p_∞	q_1/q_∞	M_1/M_∞	V_1/V_∞
1.040	1.1599	.9688	.9139	.9405
.988	1.1620	.9633	.9105	.9381
.936	1.1642	.9629	.9095	.9373
.884	1.1610	.9551	.9070	.9355
.832	1.1577	.9557	.9086	.9367
.780	1.1361	.9563	.9174	.9431
.728	1.1145	.9535	.9249	.9484
.676	1.1383	.9391	.9083	.9365
.624	1.1620	.9229	.8912	.9240
.572	1.1610	.9214	.8909	.9237
.520	1.1599	.9048	.8832	.9181
.468	1.1502	.8964	.8828	.9178
.416	1.1404	.8915	.8841	.9188
.364	1.1491	.8730	.8716	.9094
.312	1.1577	.8595	.8616	.9019
.260	1.1566	.8479	.8562	.8977
.208	1.1556	.8396	.8524	.8948
.156	1.1880	.8146	.8281	.8760
.104	1.1869	.7893	.8155	.8661
.052	1.1739	.7730	.8115	.8629
0.000	1.2182	.7590	.7893	.8451
-.052	1.2052	.7623	.7953	.8499
-.104	1.1923	.7837	.8107	.8623
-.156	1.2204	.7934	.8063	.8588
-.208	1.2484	.8117	.8063	.8588
-.260	1.2355	.8313	.8203	.8699
-.312	1.2225	.8508	.8342	.8808
-.364	1.2225	.8694	.8433	.8878
-.416	1.2225	.8880	.8523	.8947
-.468	1.2322	.8980	.8536	.8958
-.520	1.2420	.9045	.8534	.8956
-.572	1.2312	.9184	.8637	.9034
-.624	1.2204	.9289	.8724	.9100
-.676	1.2225	.9284	.8715	.9093
-.728	1.2247	.9348	.8737	.9109
-.780	1.2150	.9383	.8788	.9148
-.832	1.2052	.9485	.8871	.9210
-.884	1.2085	.9479	.8856	.9199
-.936	1.2117	.9540	.8873	.9211
-.988	1.2074	.9548	.8893	.9225
-1.040	1.2031	.9673	.8967	.9280



(a) 120°-included-angle cone.

Figure 1.- Sketch of models used in wake survey. Dimensions are in inches (cm).



(b) SPED-II vehicle.

Figure 1.- Concluded.

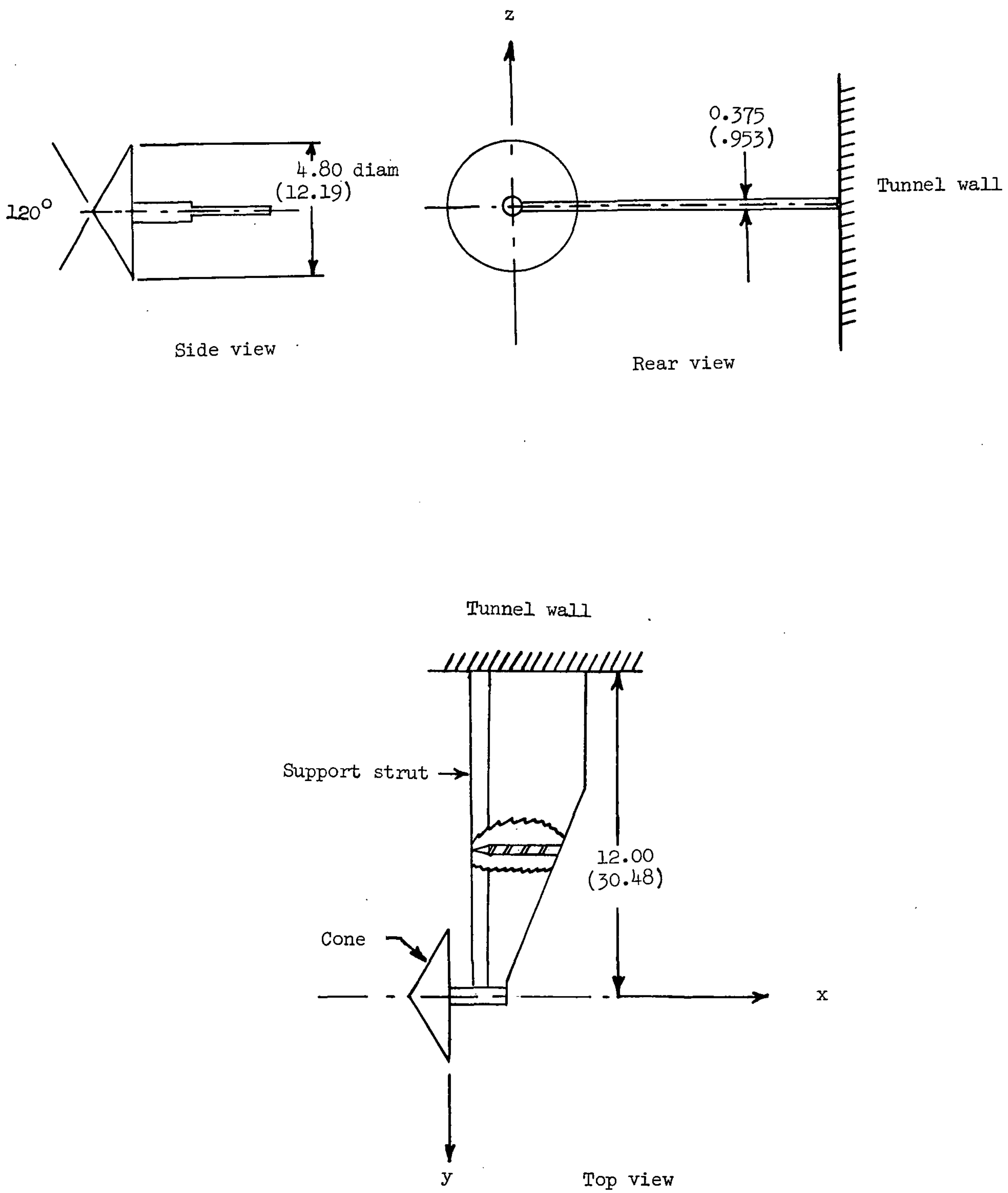


Figure 2.- Sketch of model and model support system. Dimensions are in inches (cm).

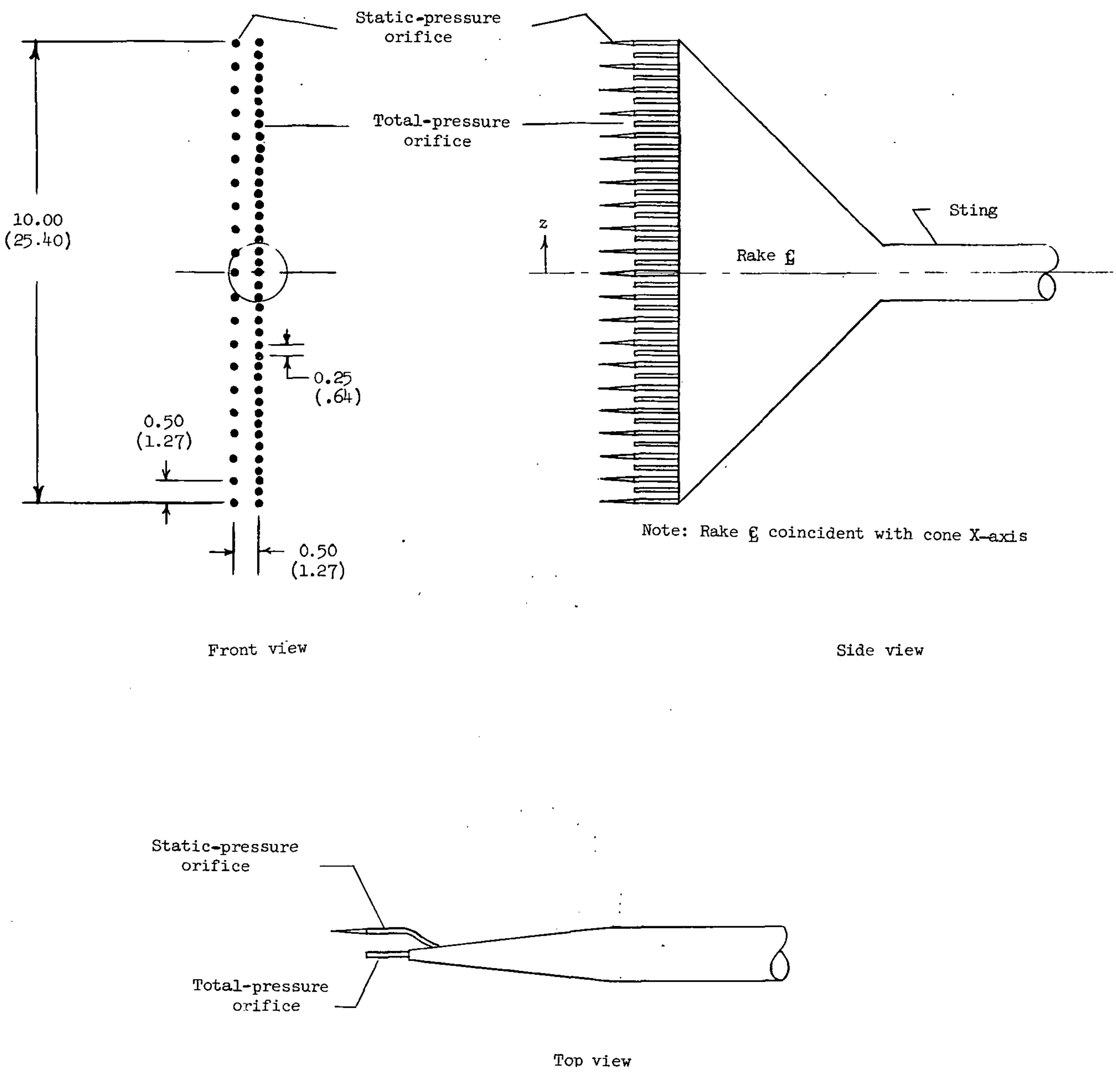


Figure 3.- Sketch of pressure rake used in wake survey. Dimensions are in inches (cm).

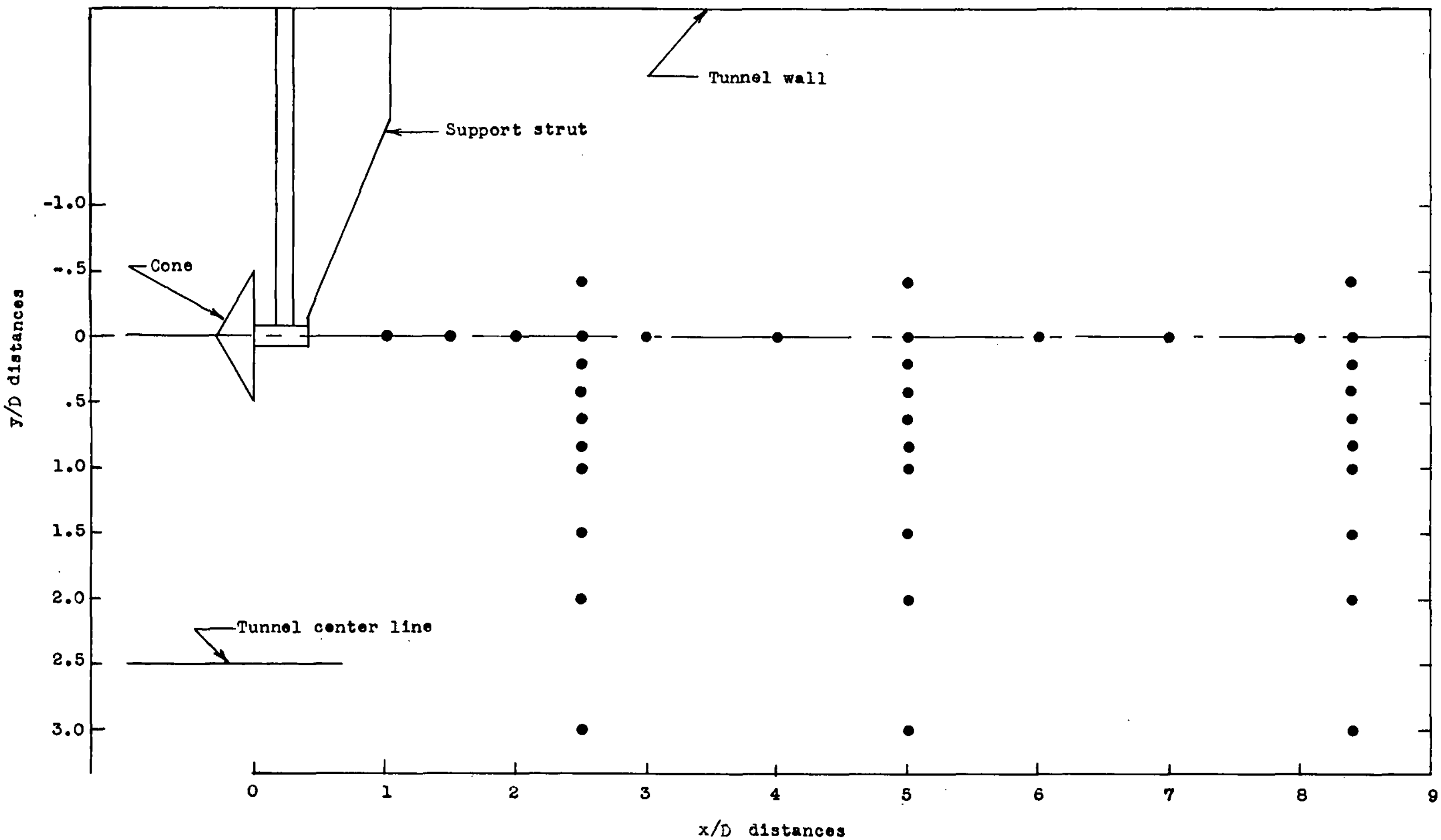
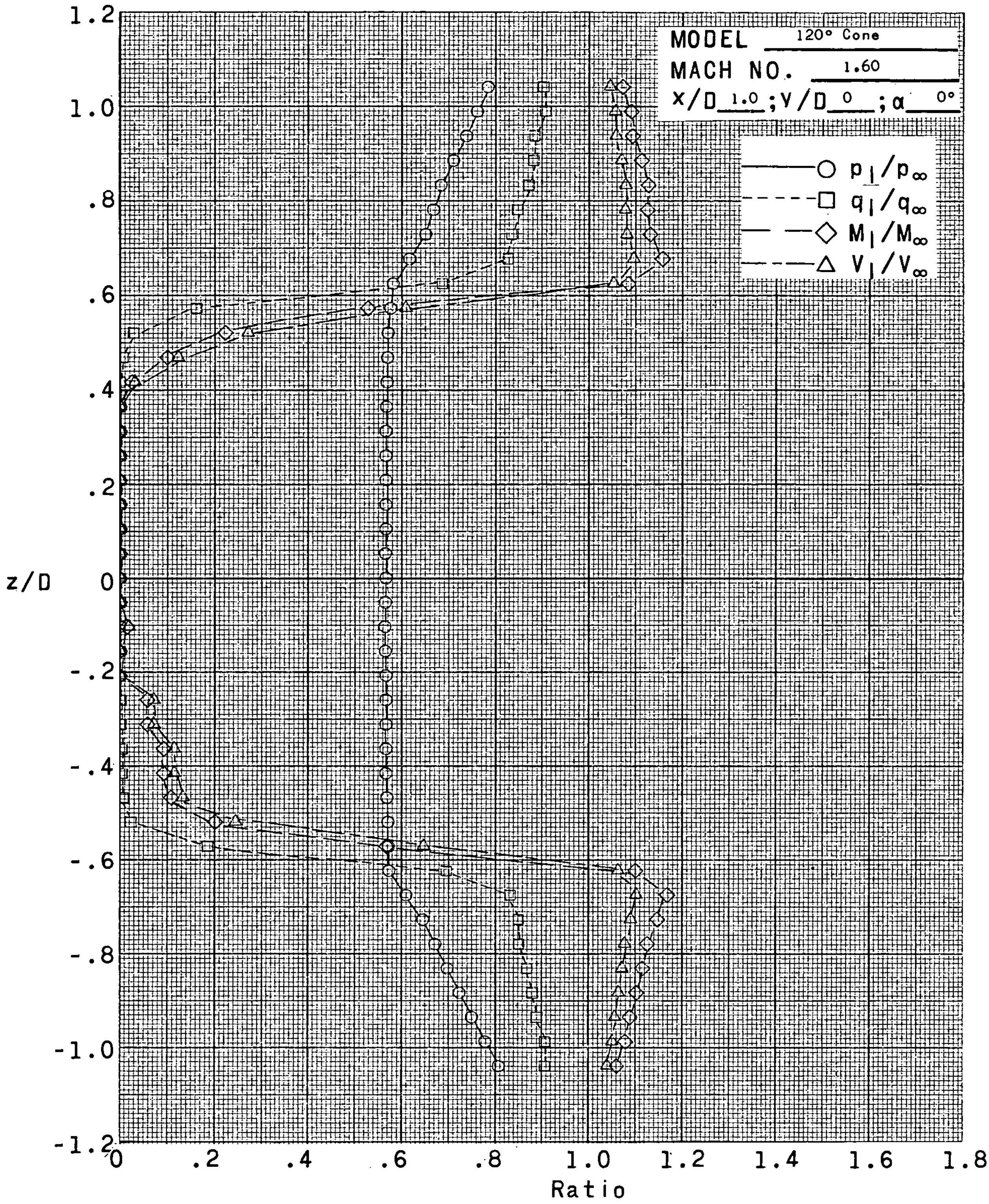
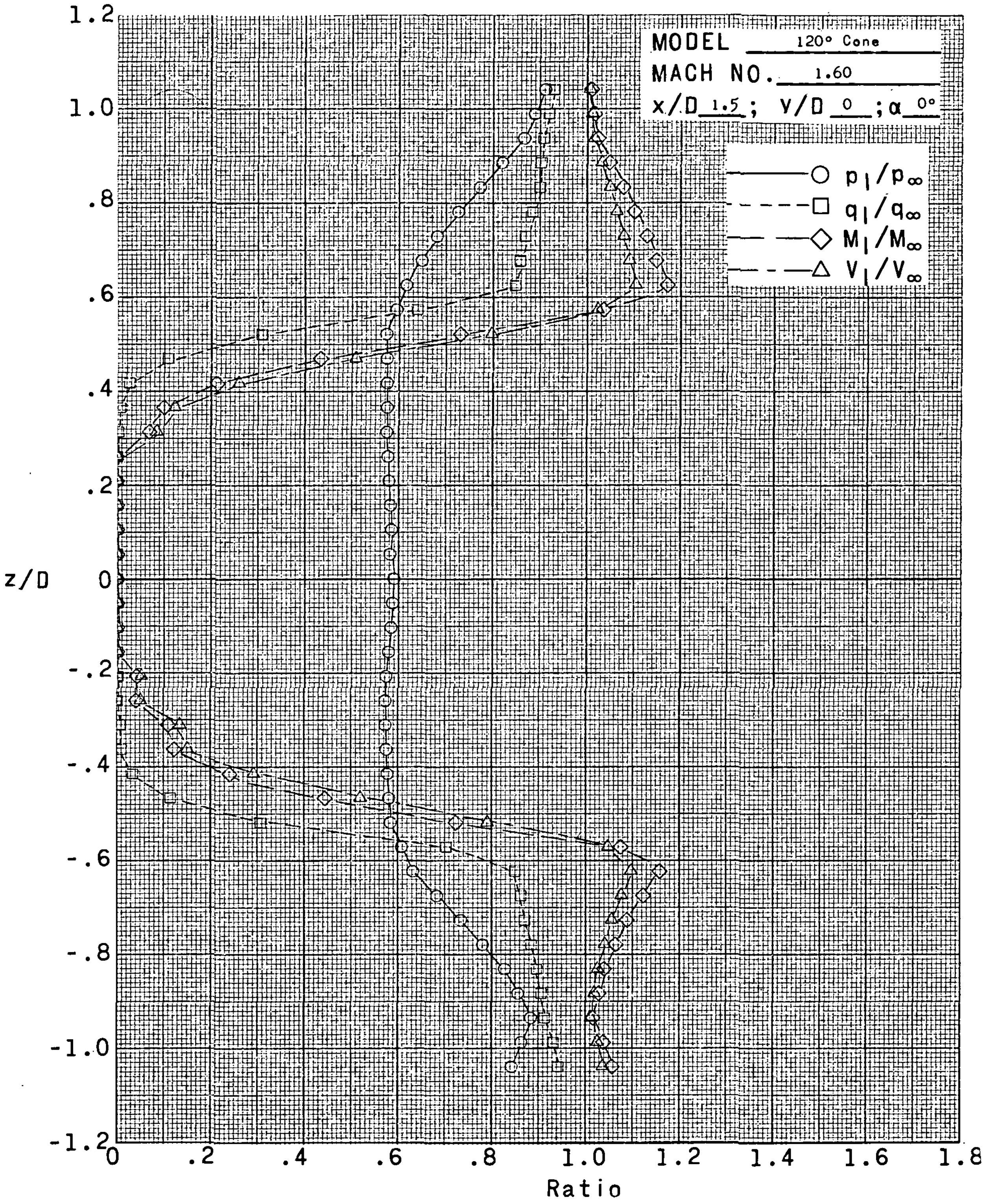


Figure 4.- Schematic representation of lateral and longitudinal stations used in wake survey.



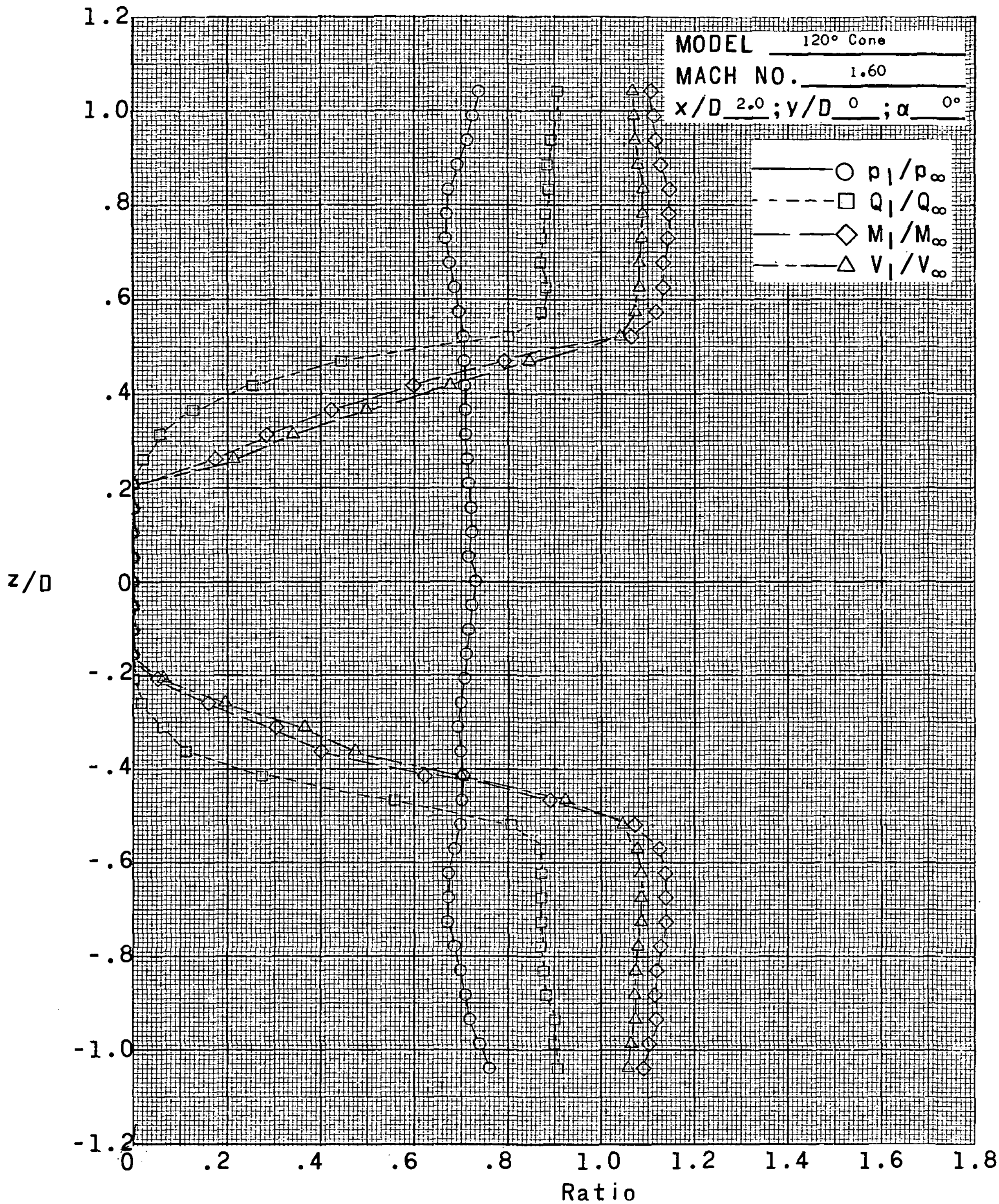
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 5.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in wake of a 120^0-included-angle cone at a Mach number of 1.60 and a Reynolds number of 1.65×10^6 per foot (5.42×10^6 per meter).



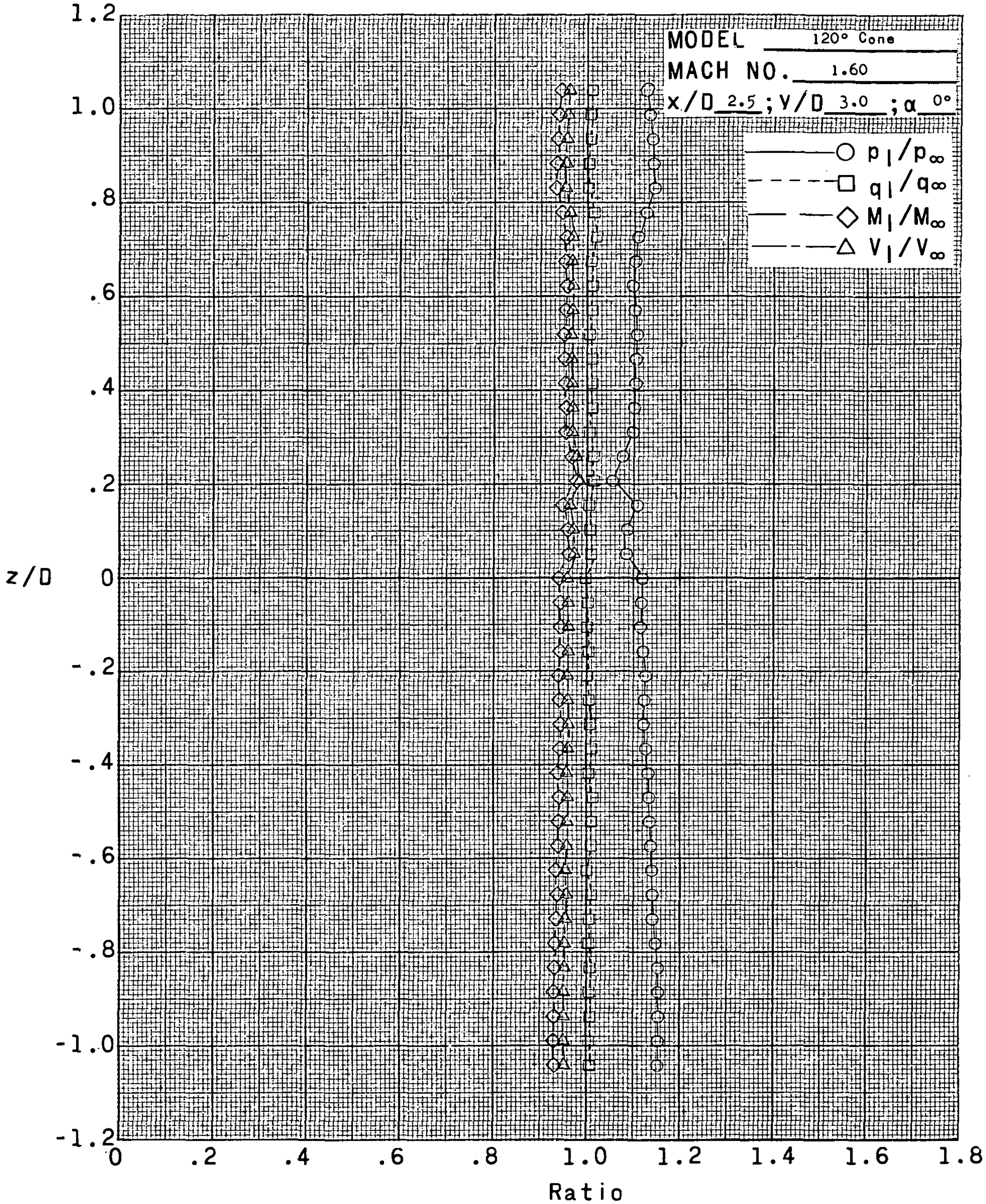
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 0^0$.

Figure 5.- Continued.



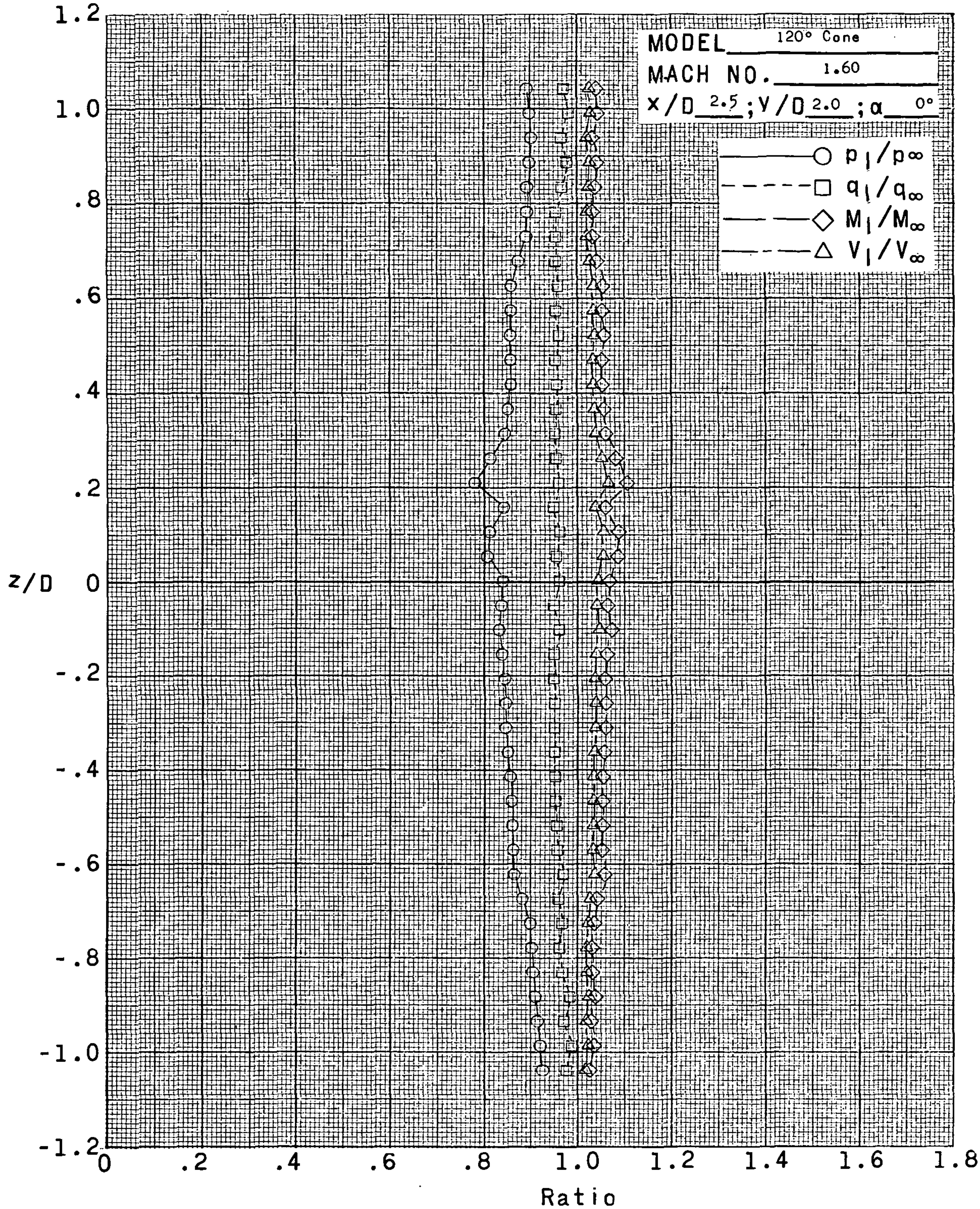
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 5.- Continued.



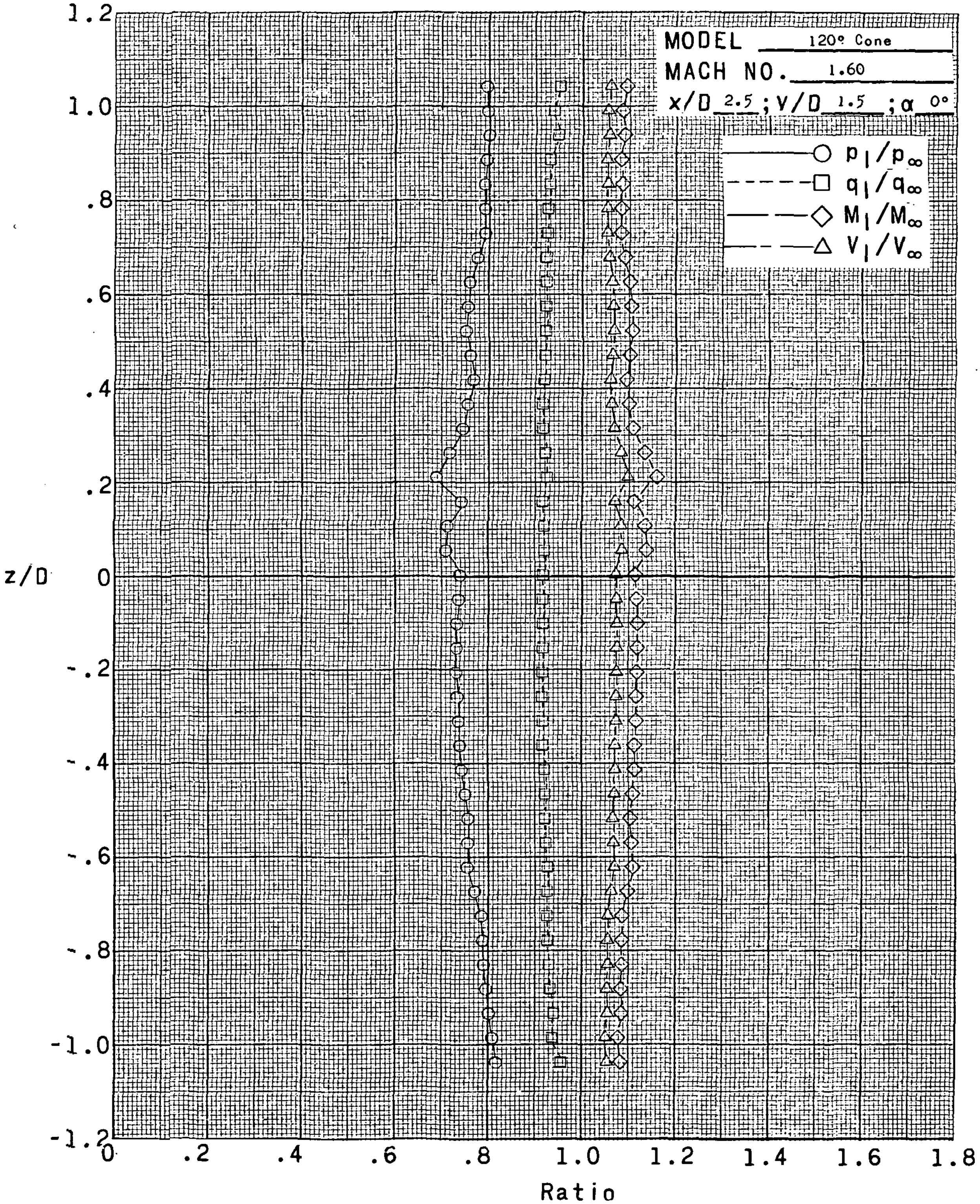
(d) x/D = 2.5; y/D = 3.0; α = 0°.

Figure 5.- Continued.



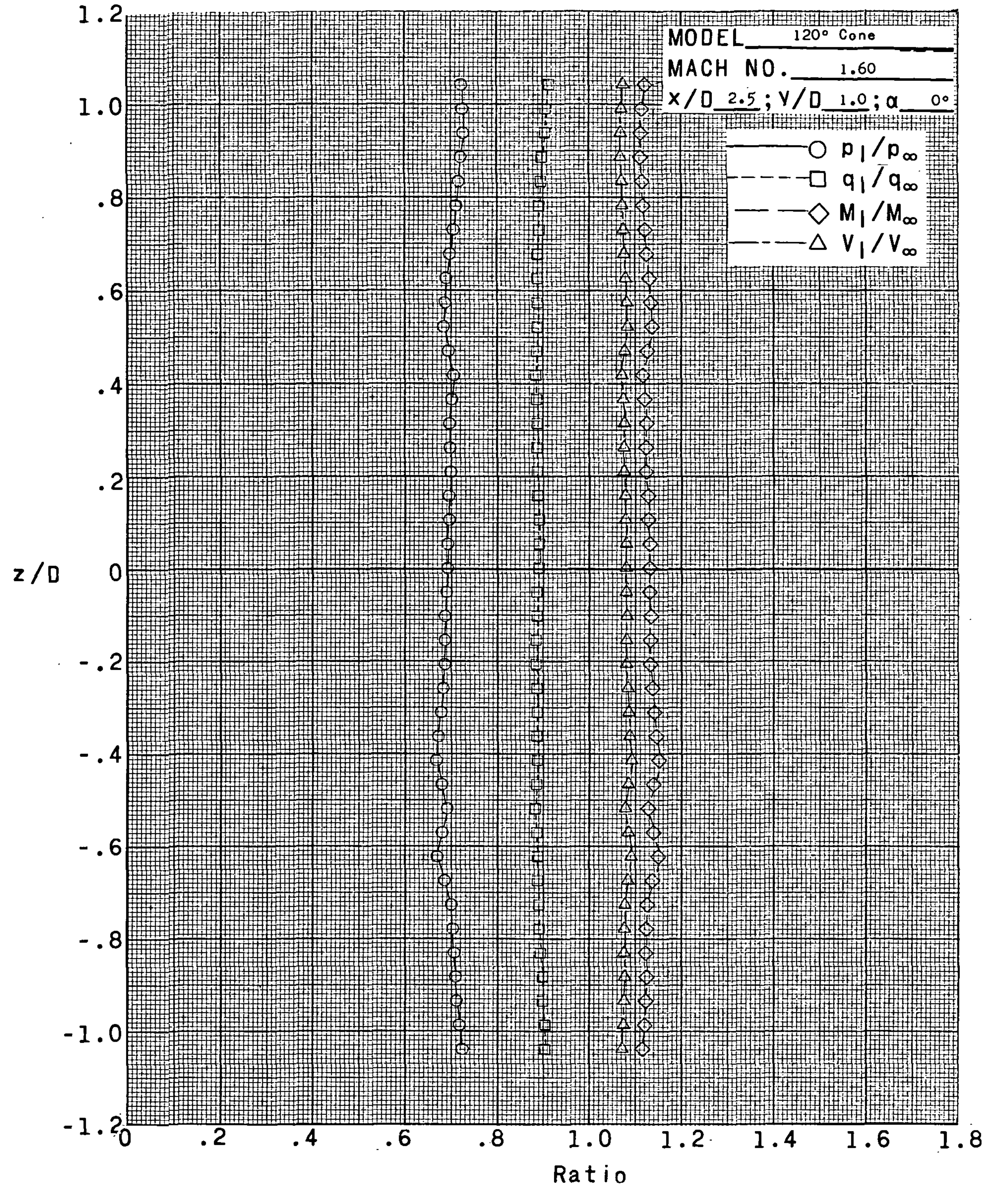
(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^{0}$.

Figure 5.- Continued.



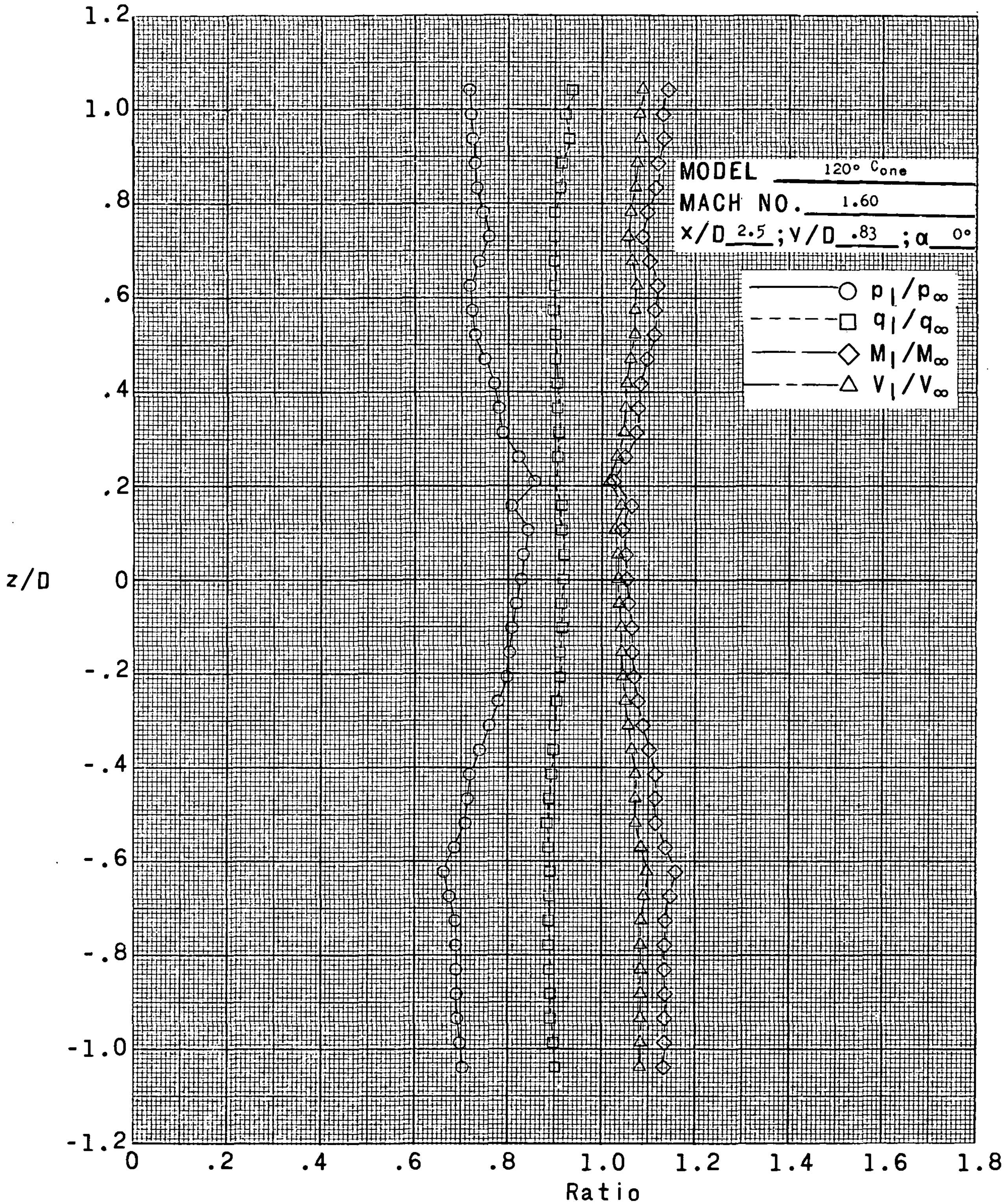
(f) x/D = 2.5; y/D = 1.5; α = 0°.

Figure 5.- Continued.



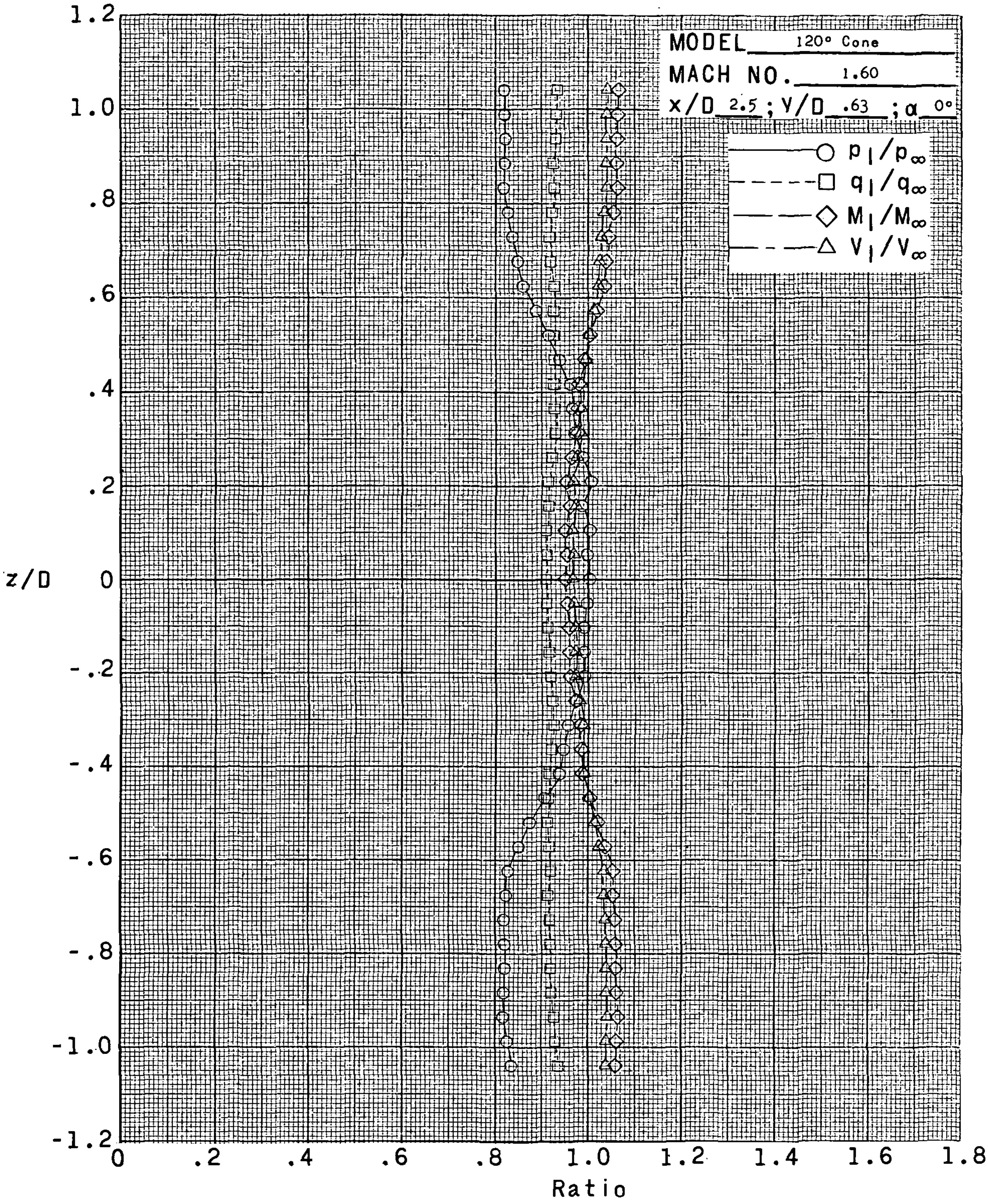
(g) x/D = 2.5; y/D = 1.0; α = 0°.

Figure 5.- Continued.



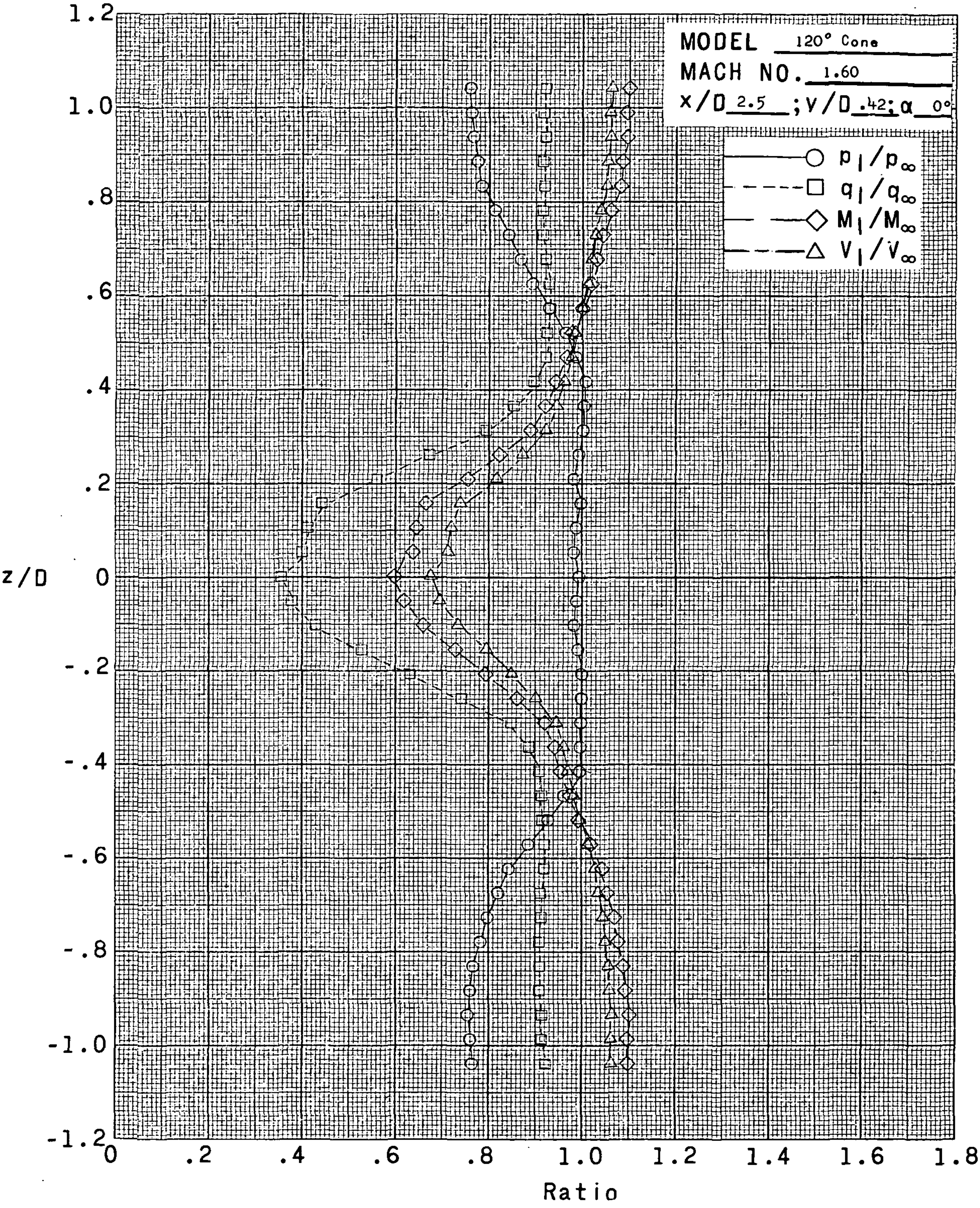
(h) $x/D = 2.5$; $y/D = 0.83$; $\alpha = 0^\circ$.

Figure 5.- Continued.



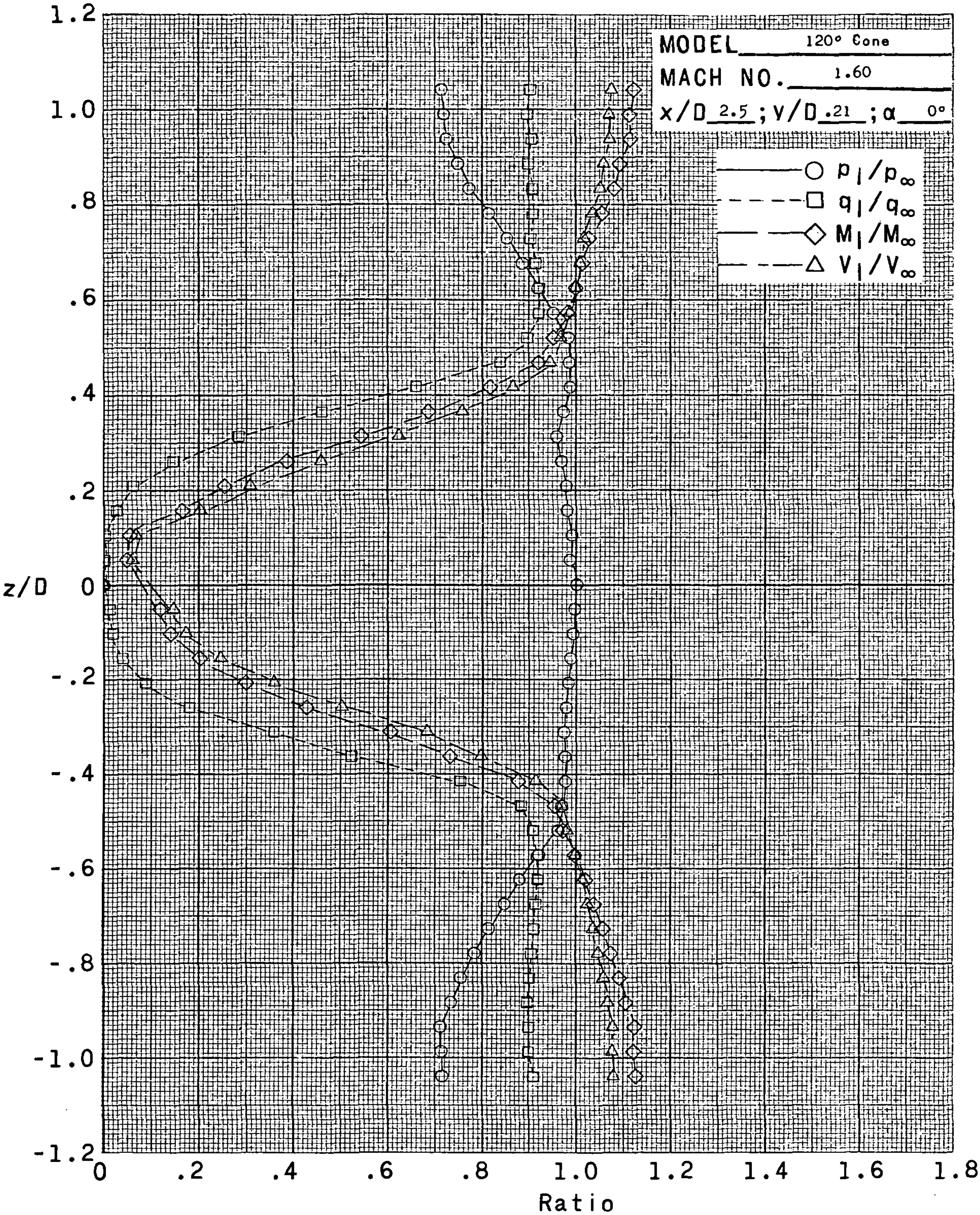
(i) $x/D = 2.5$; $y/D = 0.63$; $\alpha = 0^{0}$.

Figure 5.- Continued.



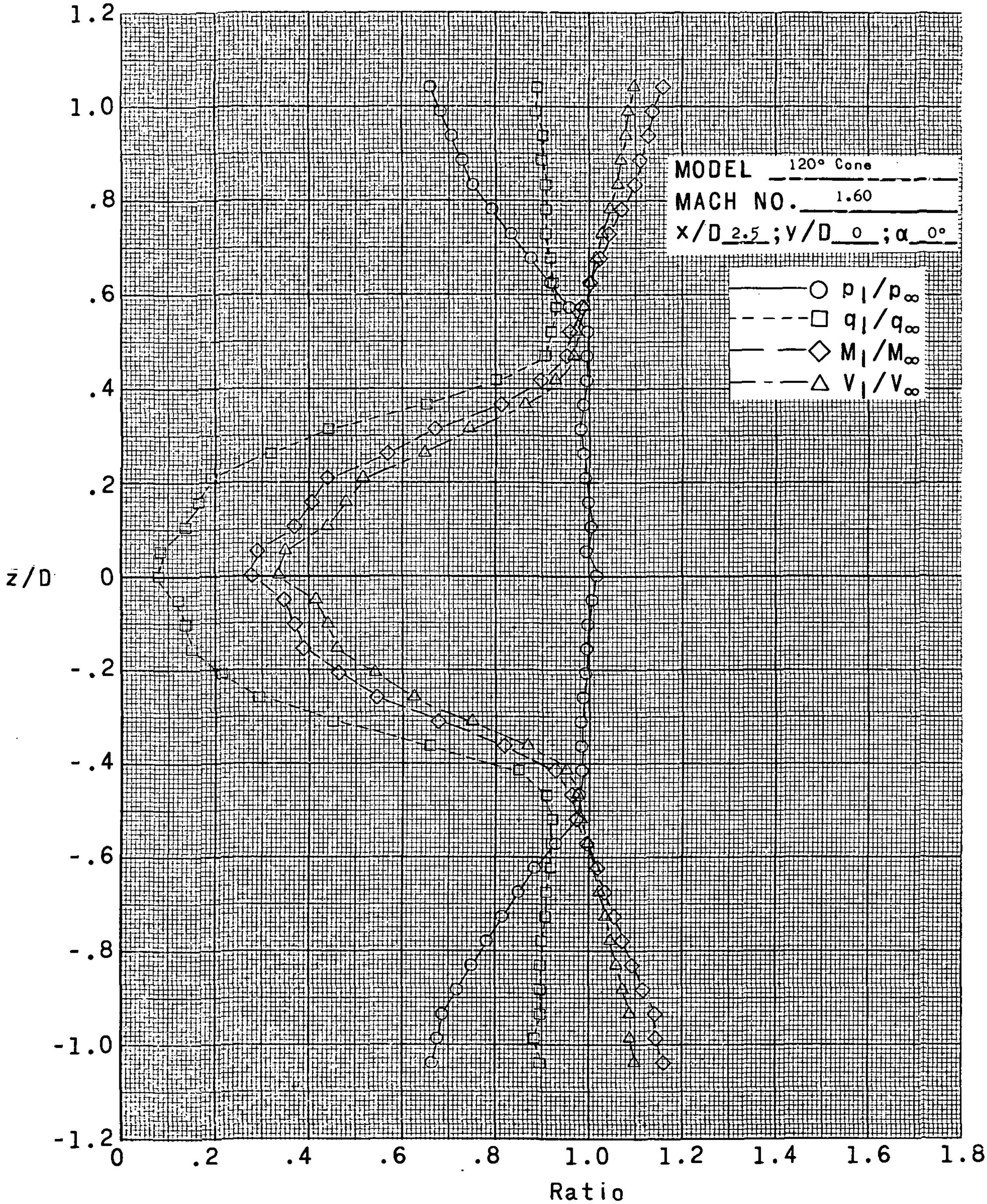
(j) $x/D = 2.5$; $y/D = 0.42$; $\alpha = 0^0$.

Figure 5.- Continued.



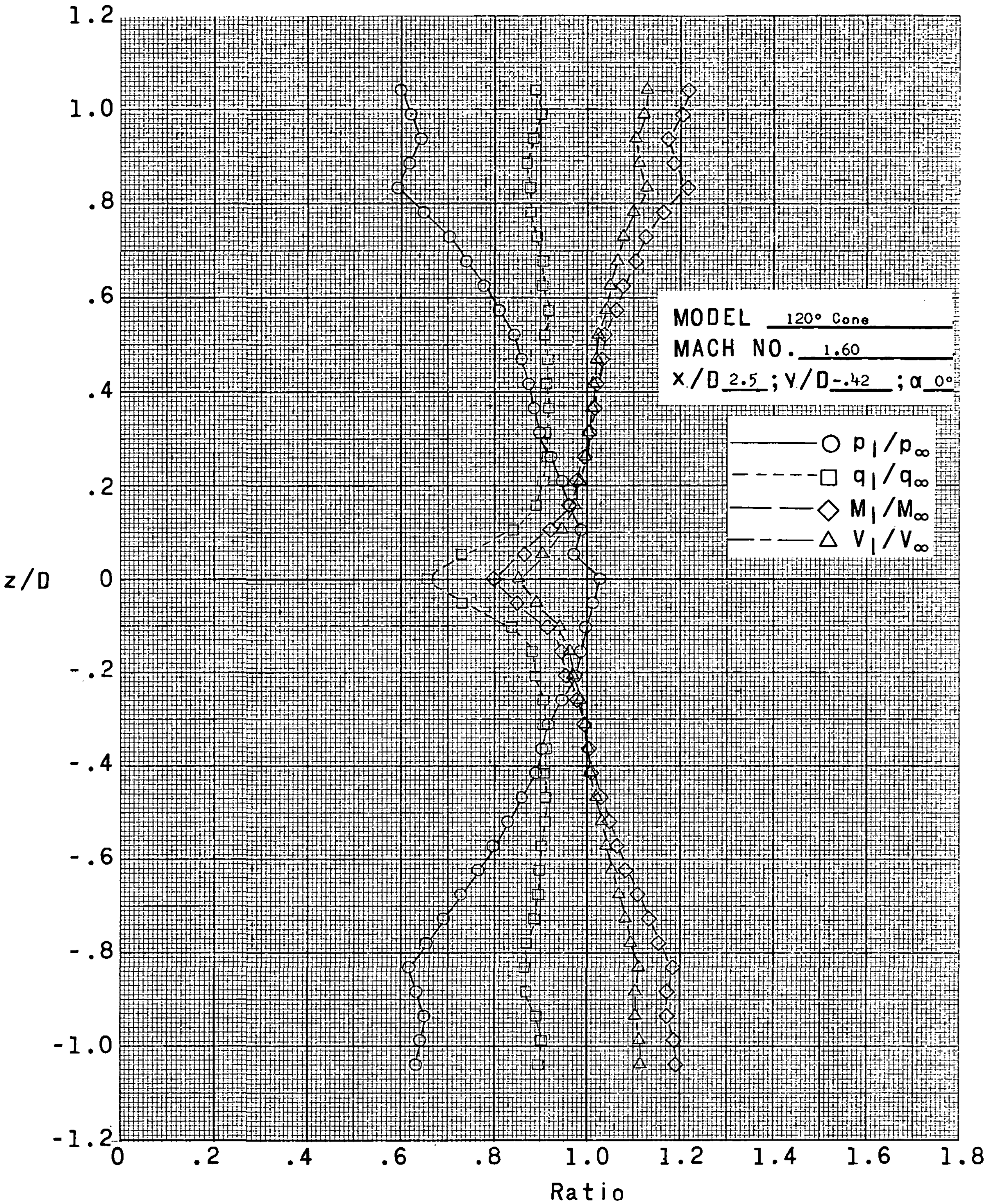
(k) x/D = 2.5; y/D = 0.21; α = 0°.

Figure 5.- Continued.



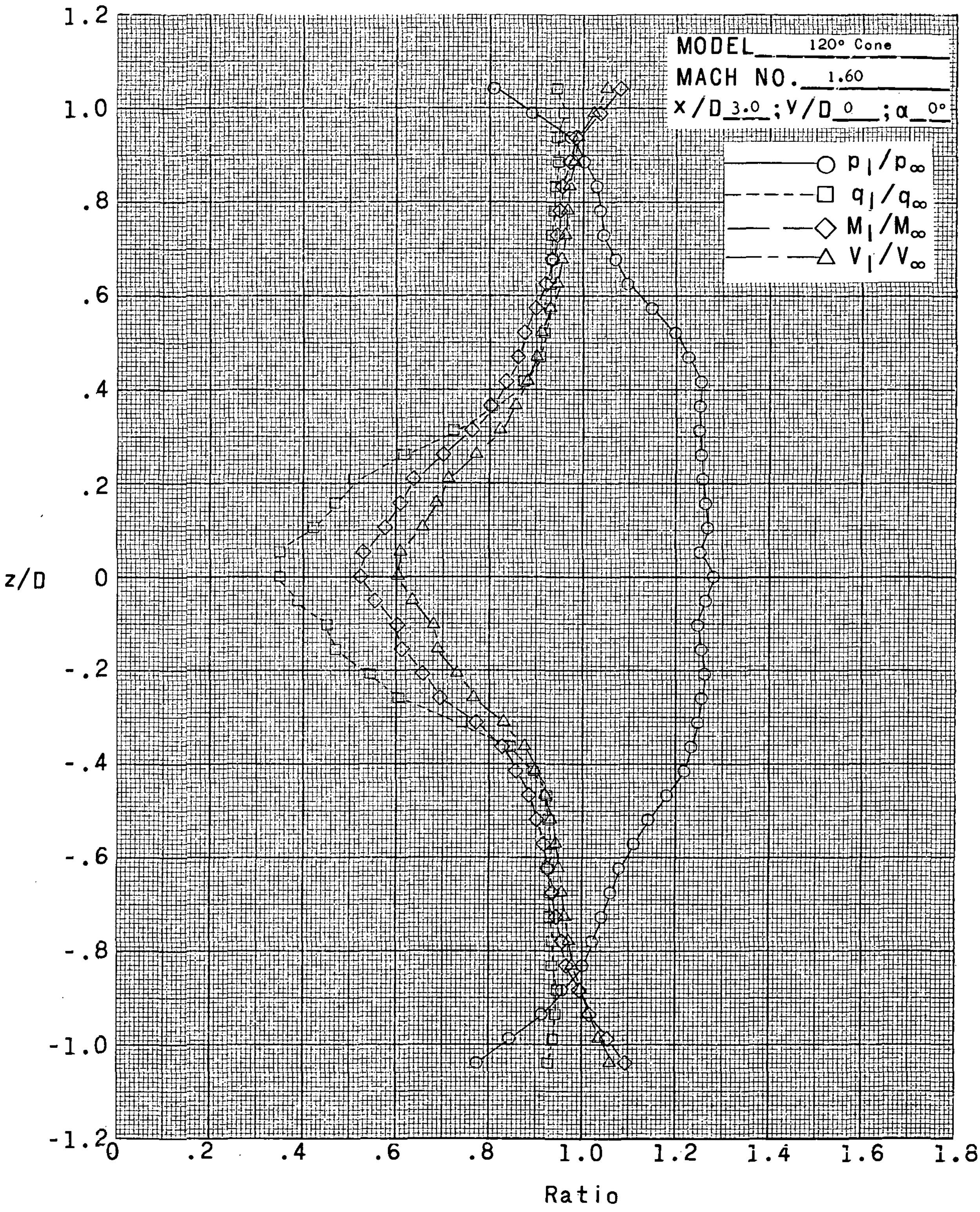
(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 5.- Continued.



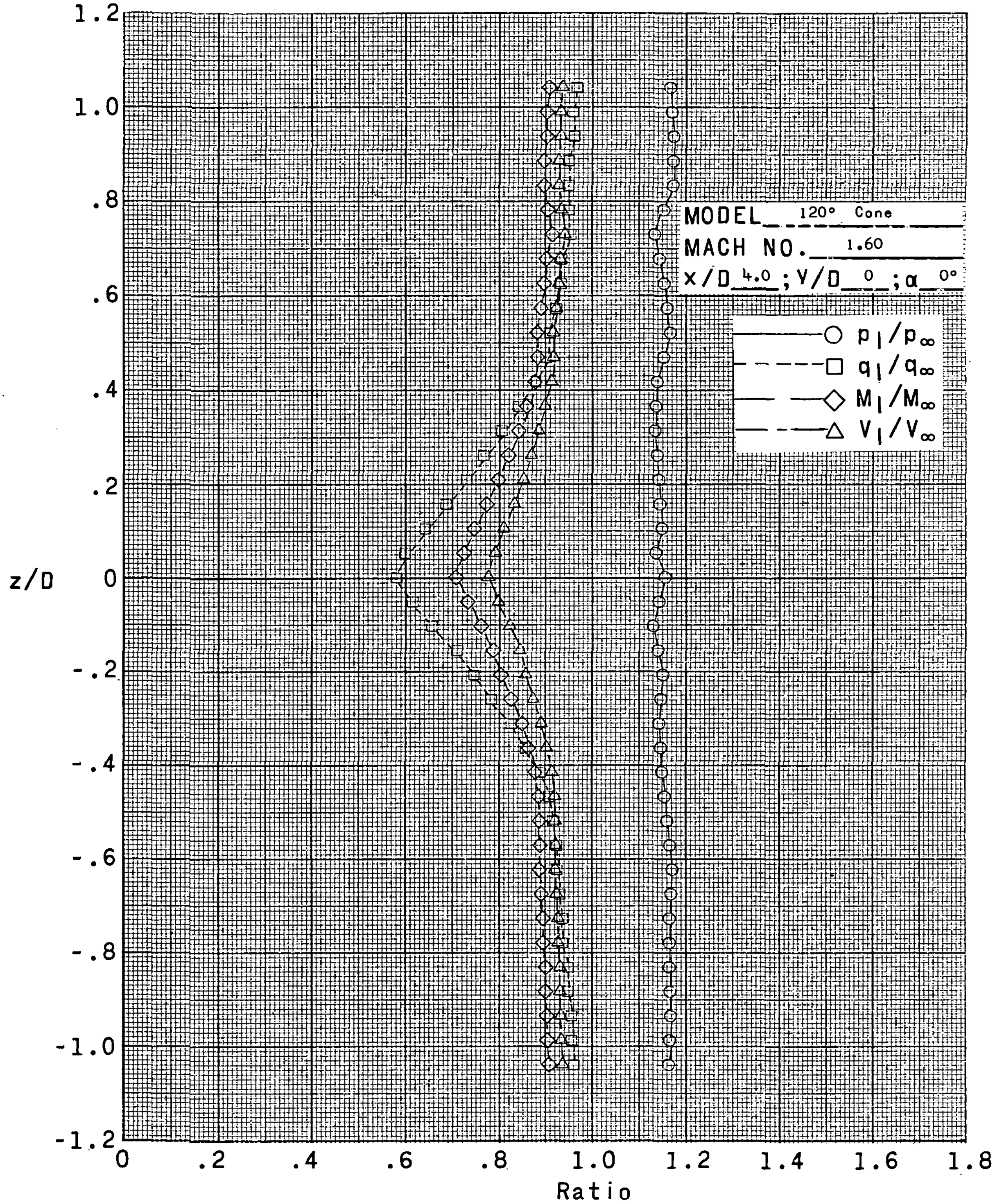
(m) $x/D = 2.5$; $y/D = -0.42$; $\alpha = 0^0$.

Figure 5.- Continued.



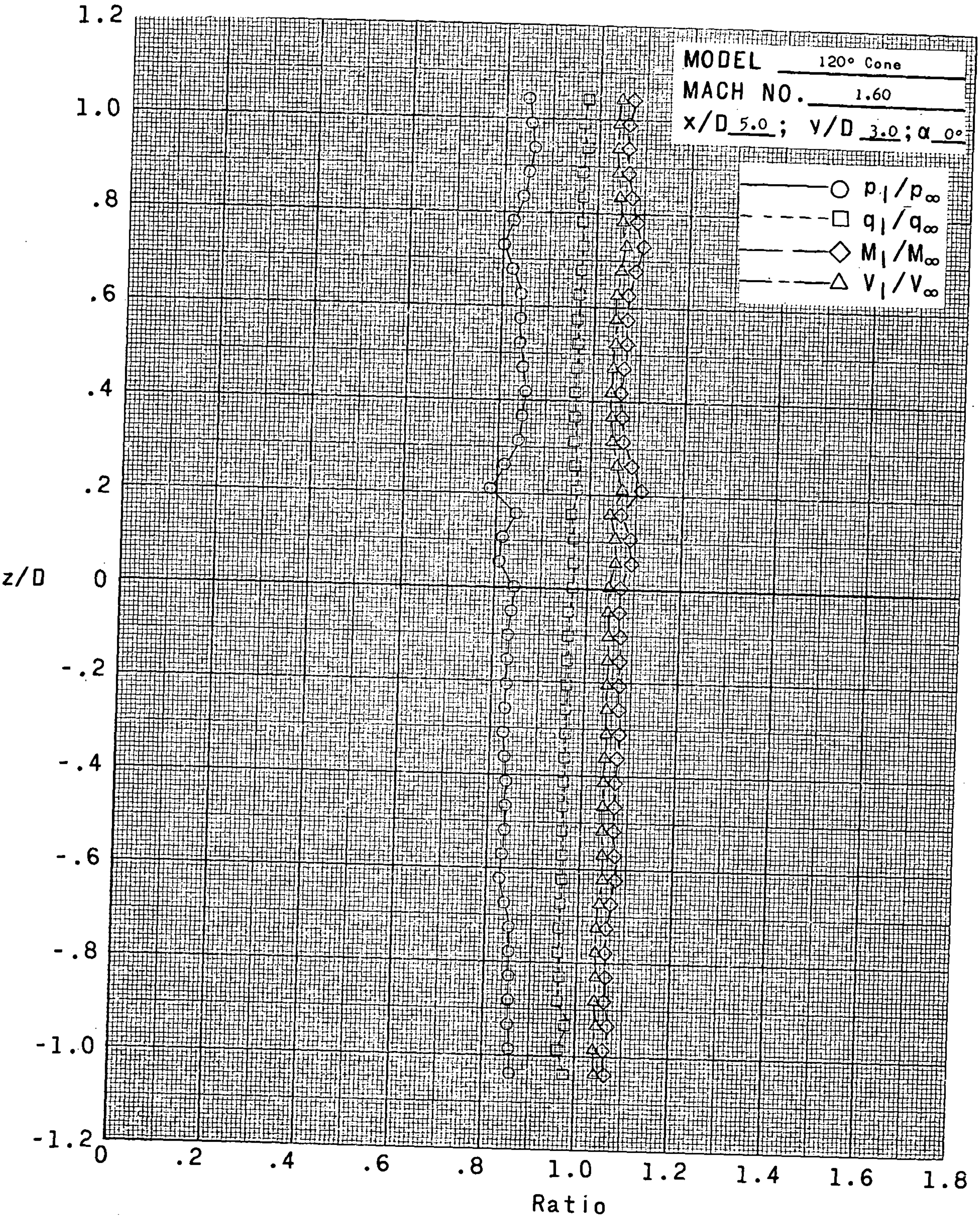
(n) x/D = 3.0; y/D = 0; α = 0°.

Figure 5.- Continued.



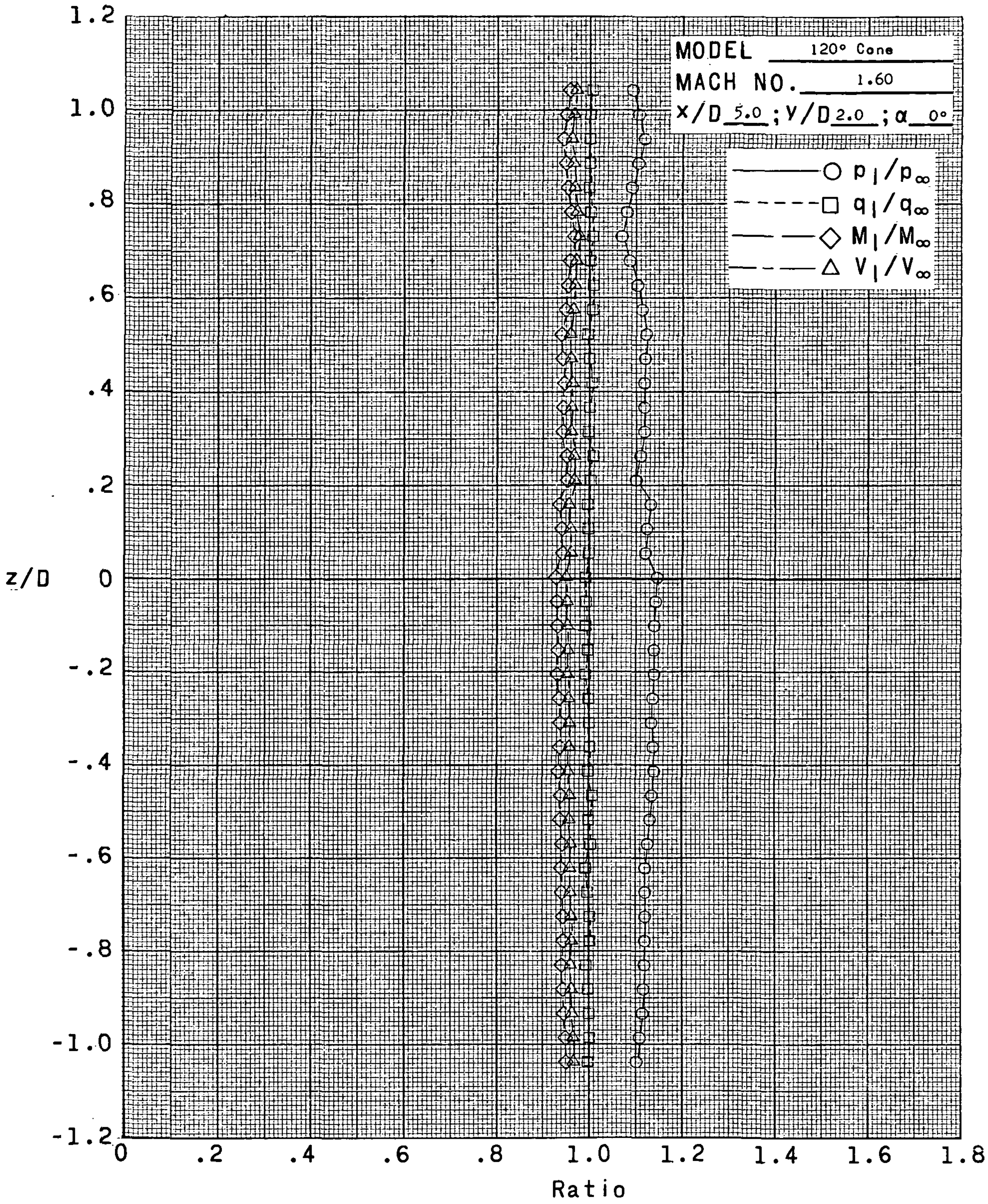
(o) x/D = 4.0; y/D = 0; α = 0°.

Figure 5.- Continued.



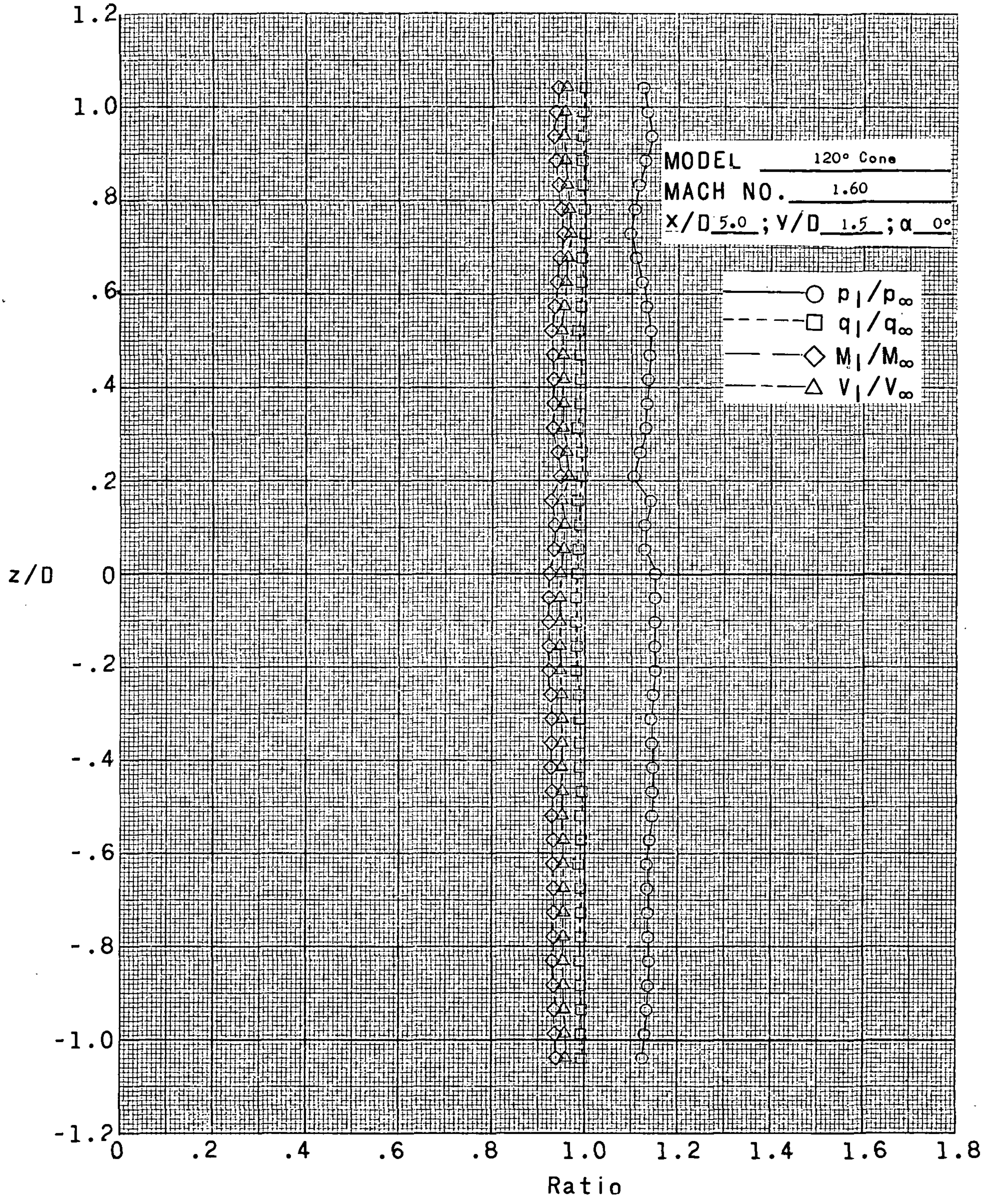
(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^0$.

Figure 5.- Continued.



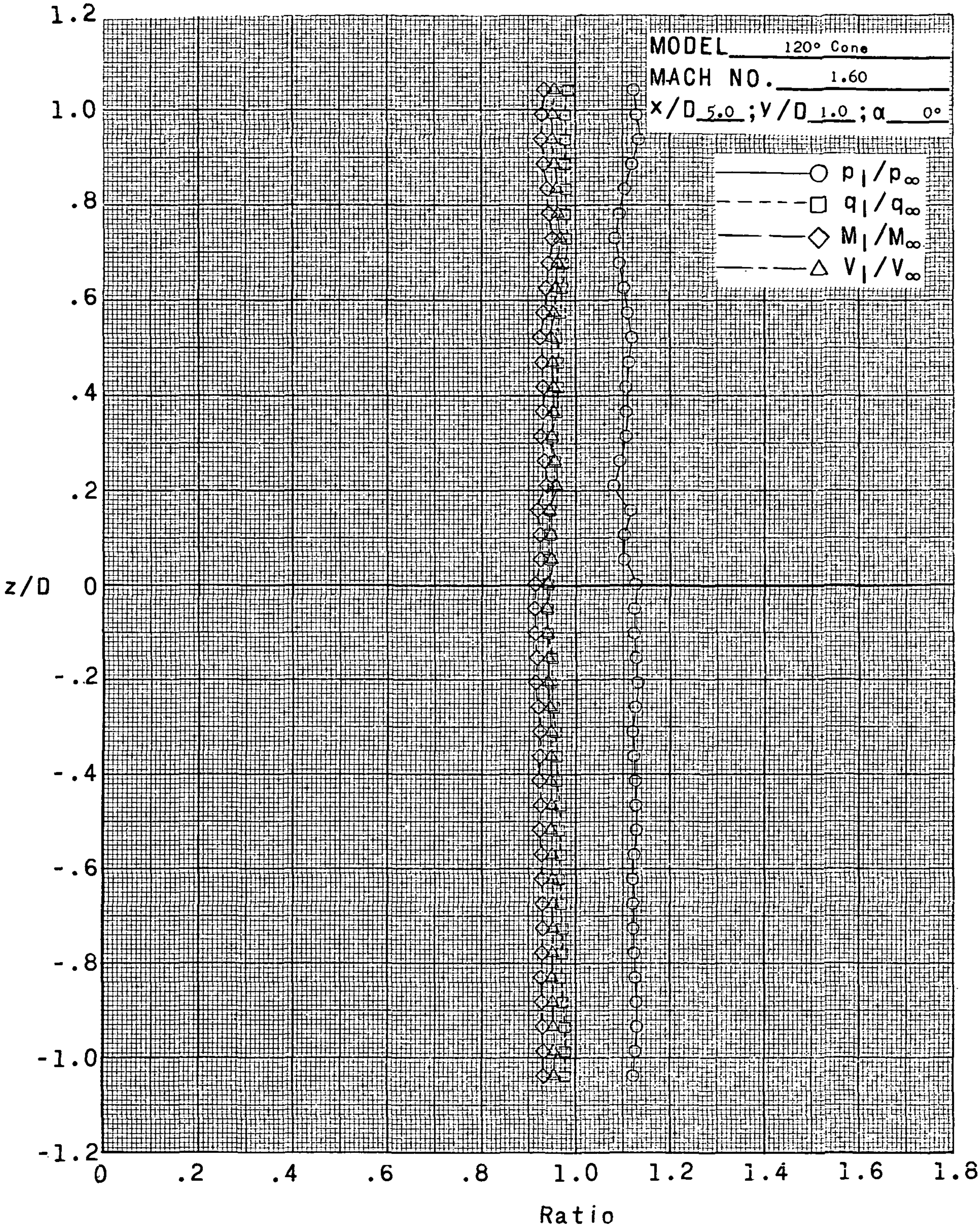
(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^0$.

Figure 5.- Continued.



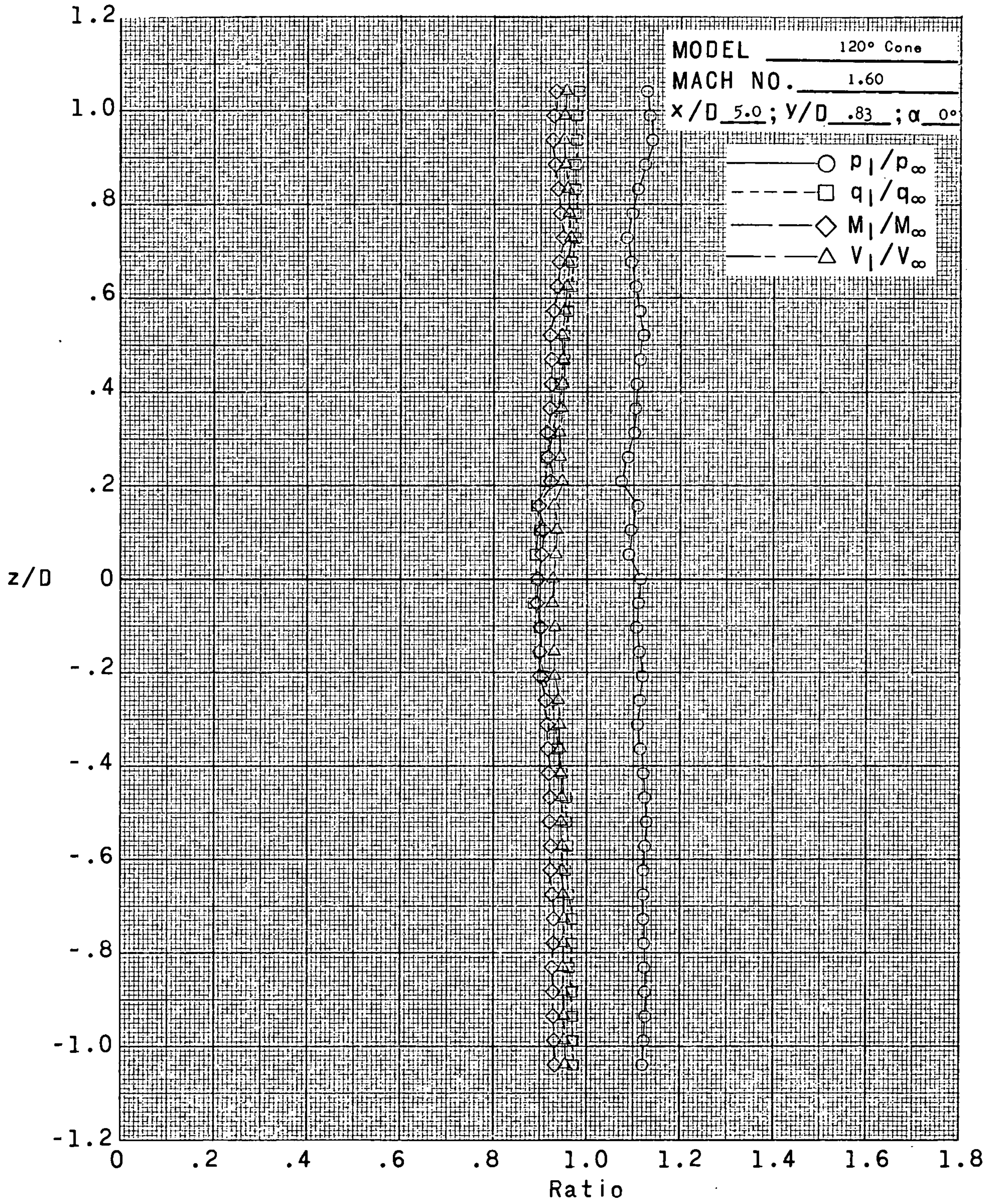
(r) x/D = 5.0; y/D = 1.5; α = 0°.

Figure 5.- Continued.



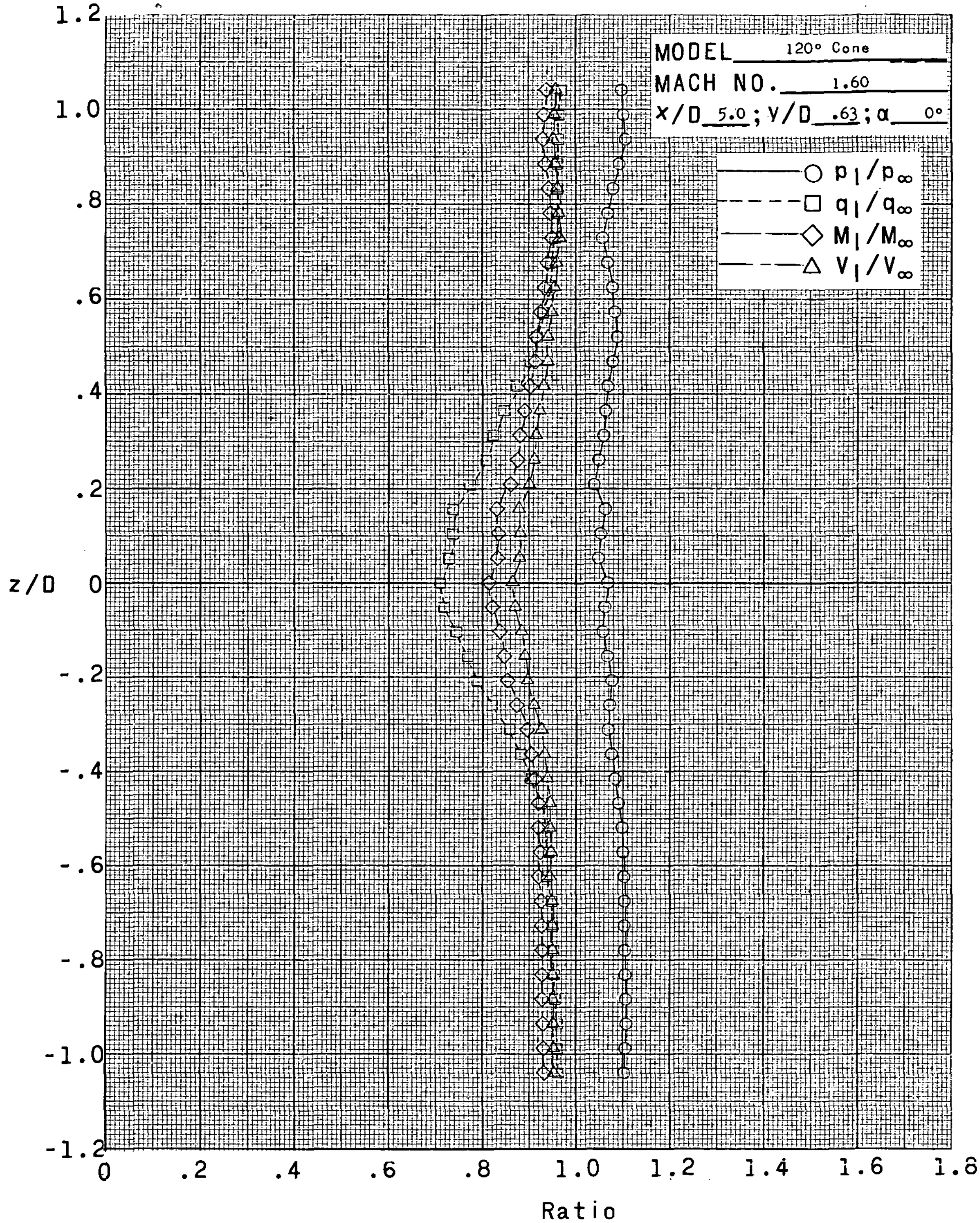
(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^0$.

Figure 5.- Continued.



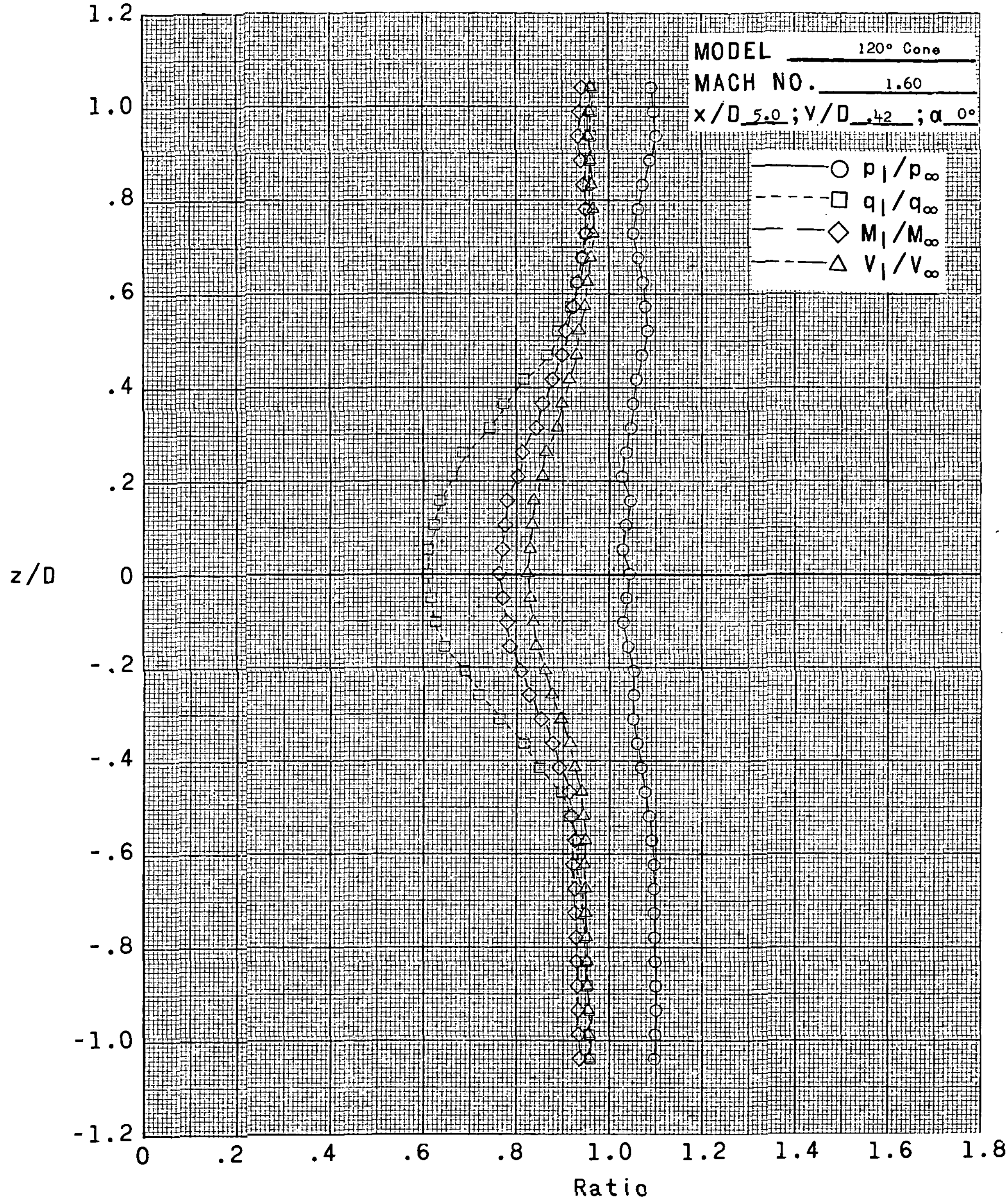
(t) x/D = 5.0; y/D = 0.83; α = 0°.

Figure 5.- Continued.



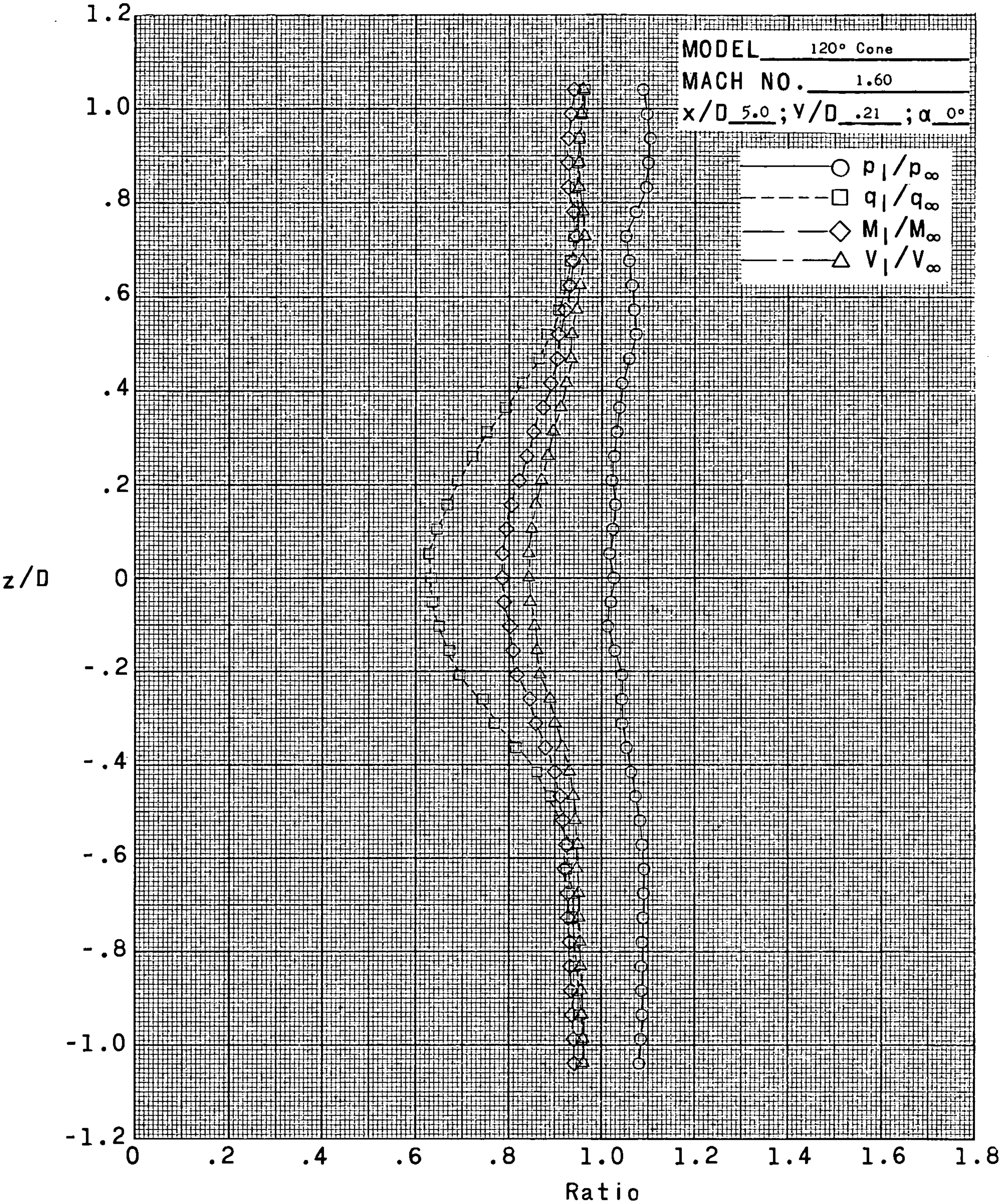
(u) x/D = 5.0; y/D = 0.63; α = 0°.

Figure 5.- Continued.



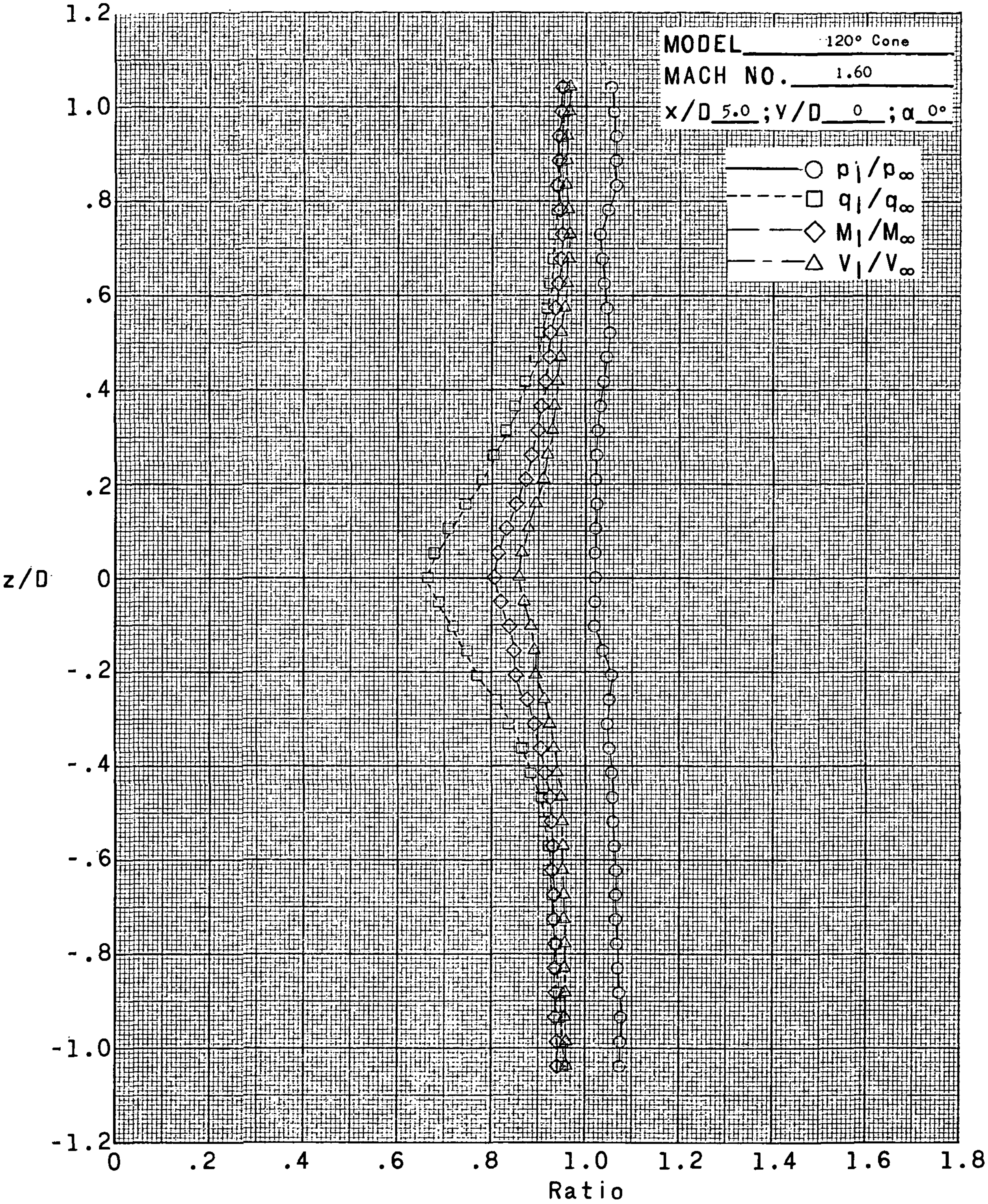
(v) $x/D = 5.0$; $y/D = 0.42$; $\alpha = 0°$.

Figure 5.- Continued.



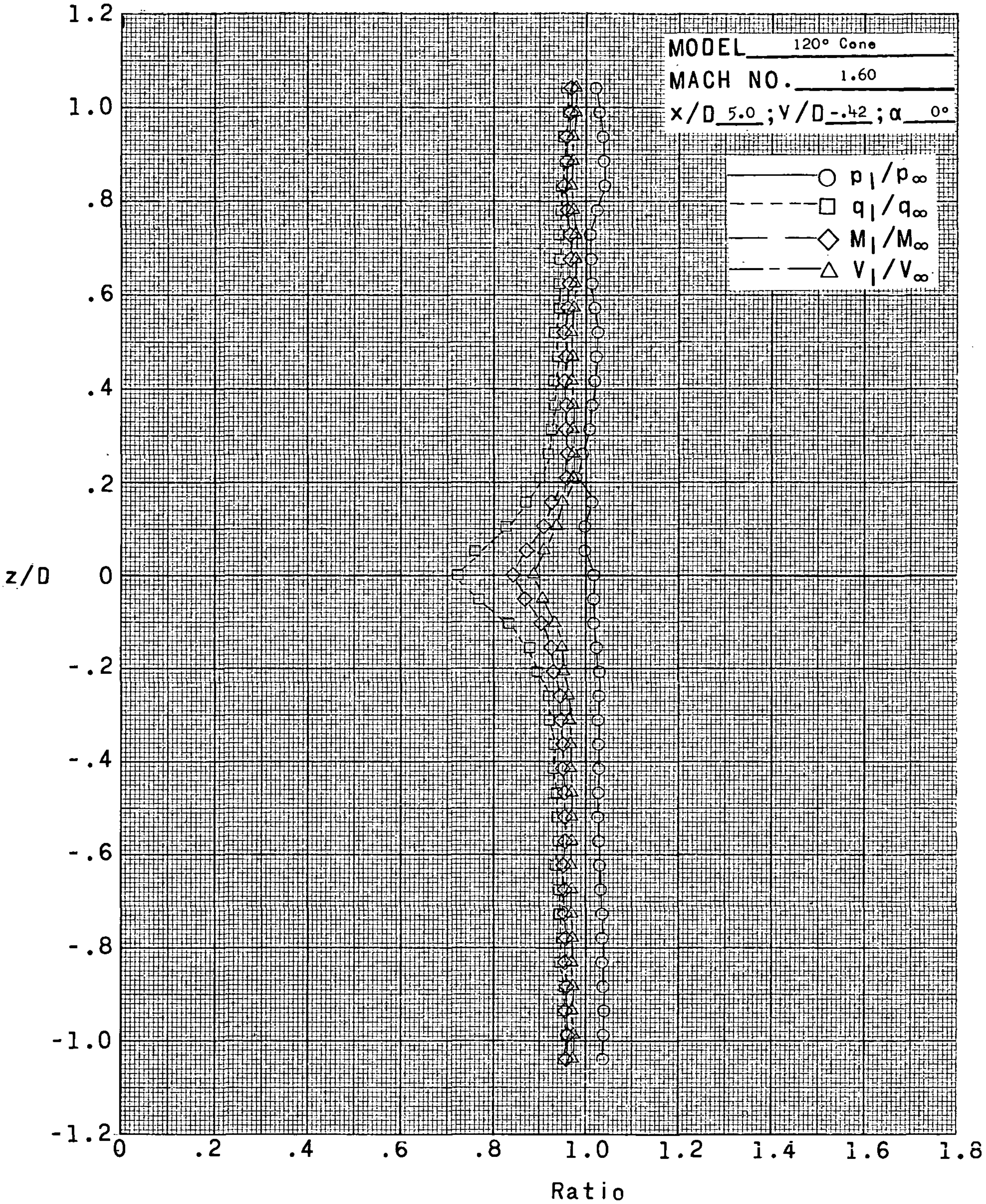
(w) $x/D = 5.0$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 5.- Continued.



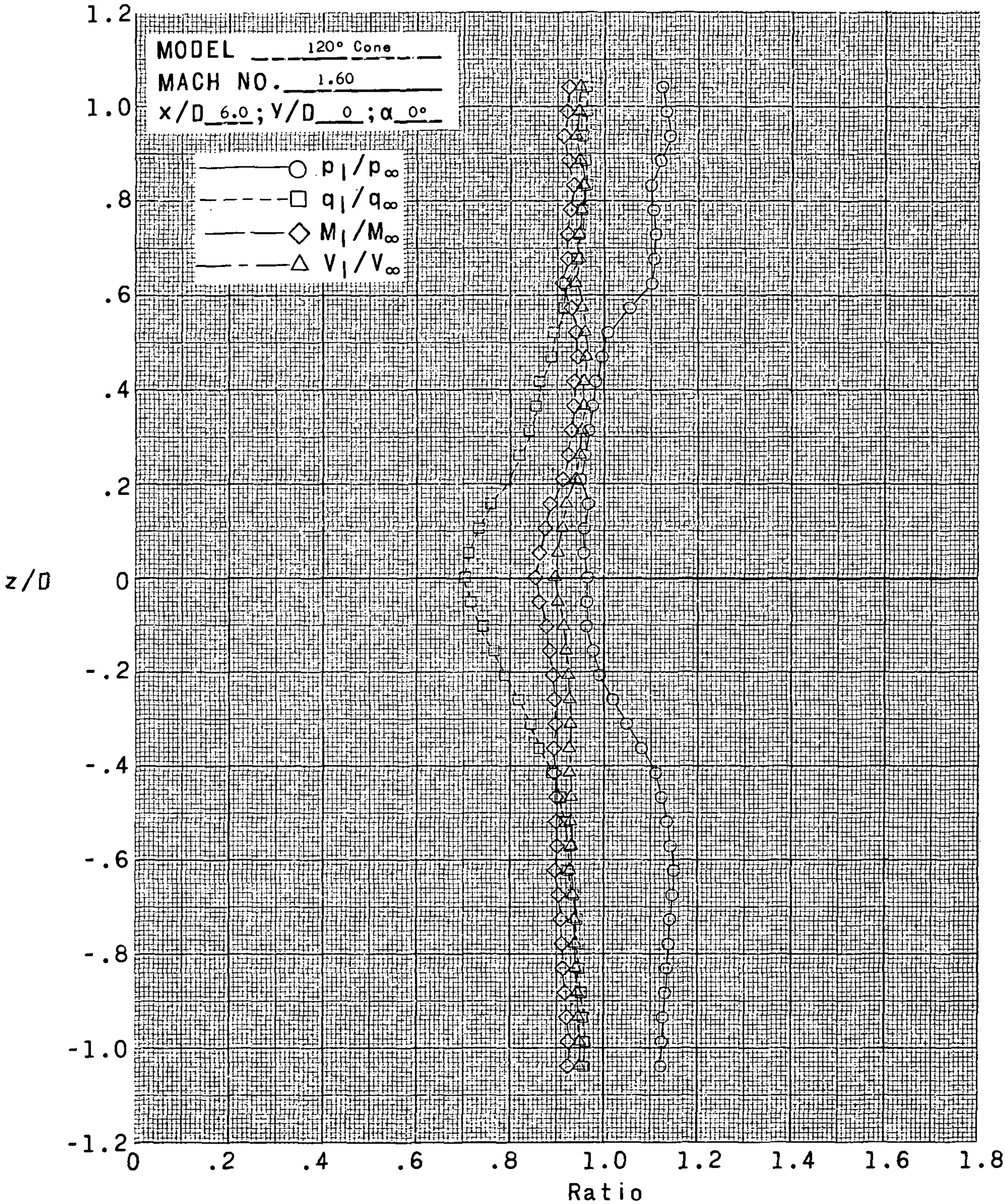
(x) x/D = 5.0; y/D = 0; α = 0°.

Figure 5.- Continued.



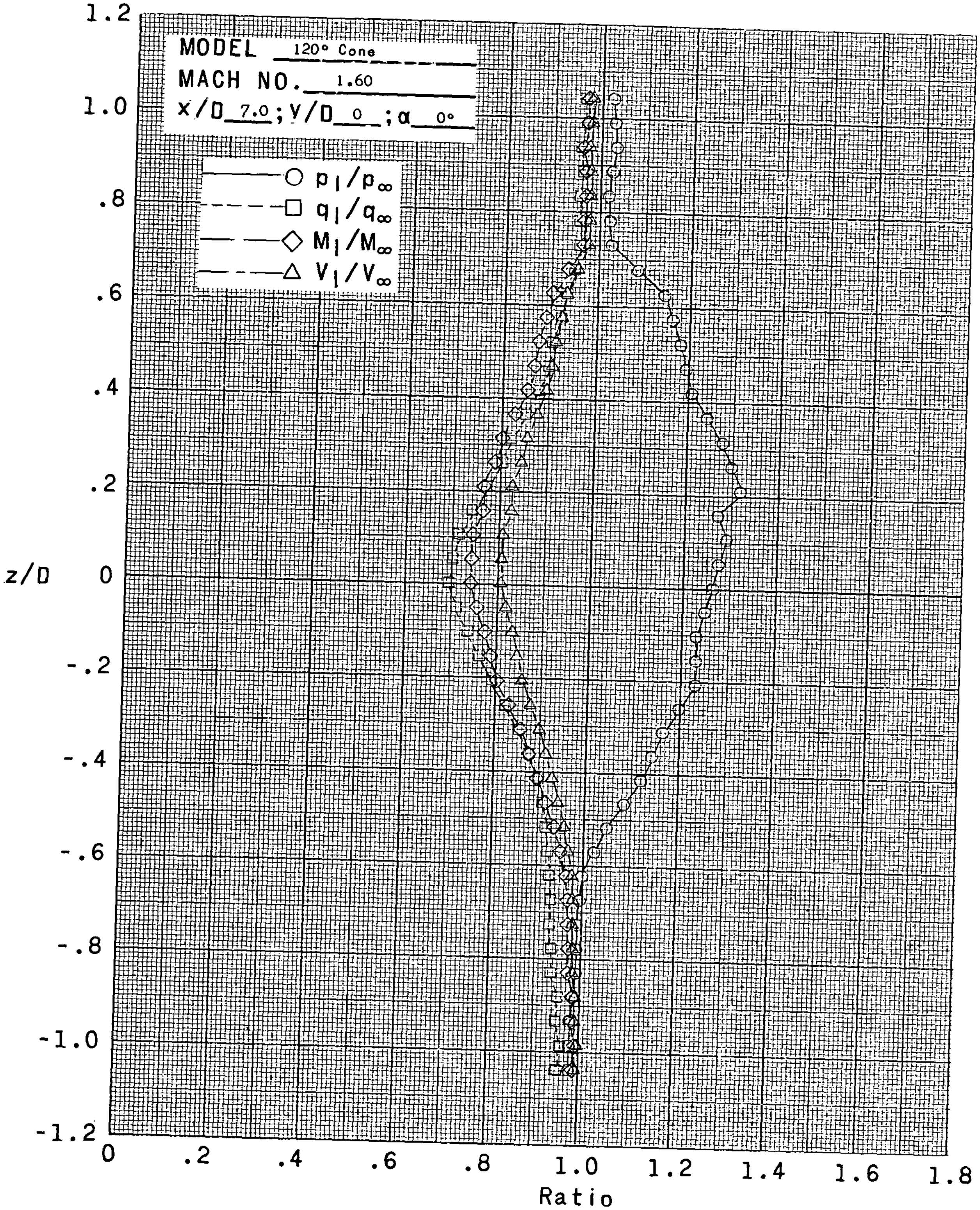
(y) x/D = 5.0; y/D = -0.42; α = 0°.

Figure 5.- Continued.



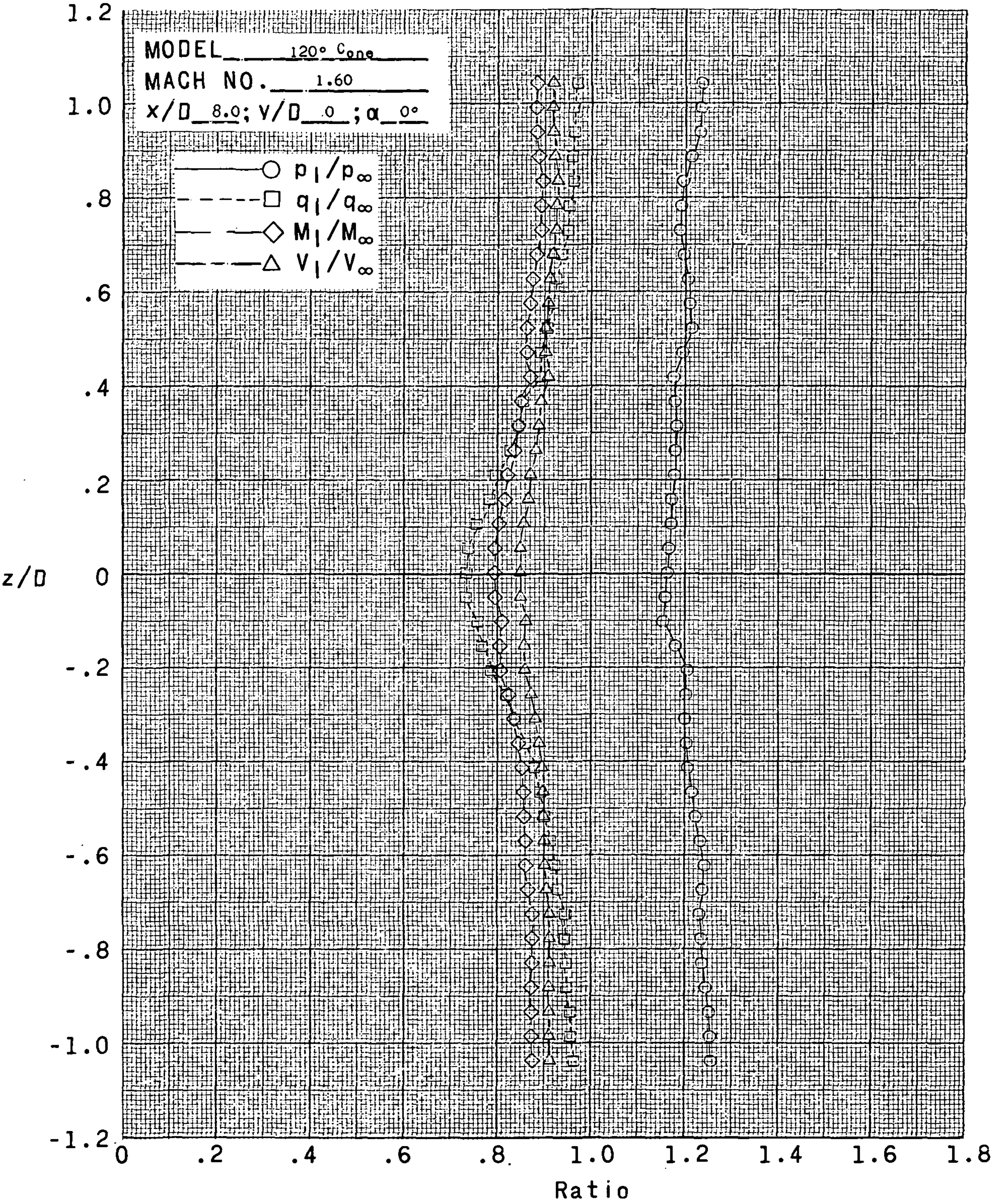
(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 5.- Continued.



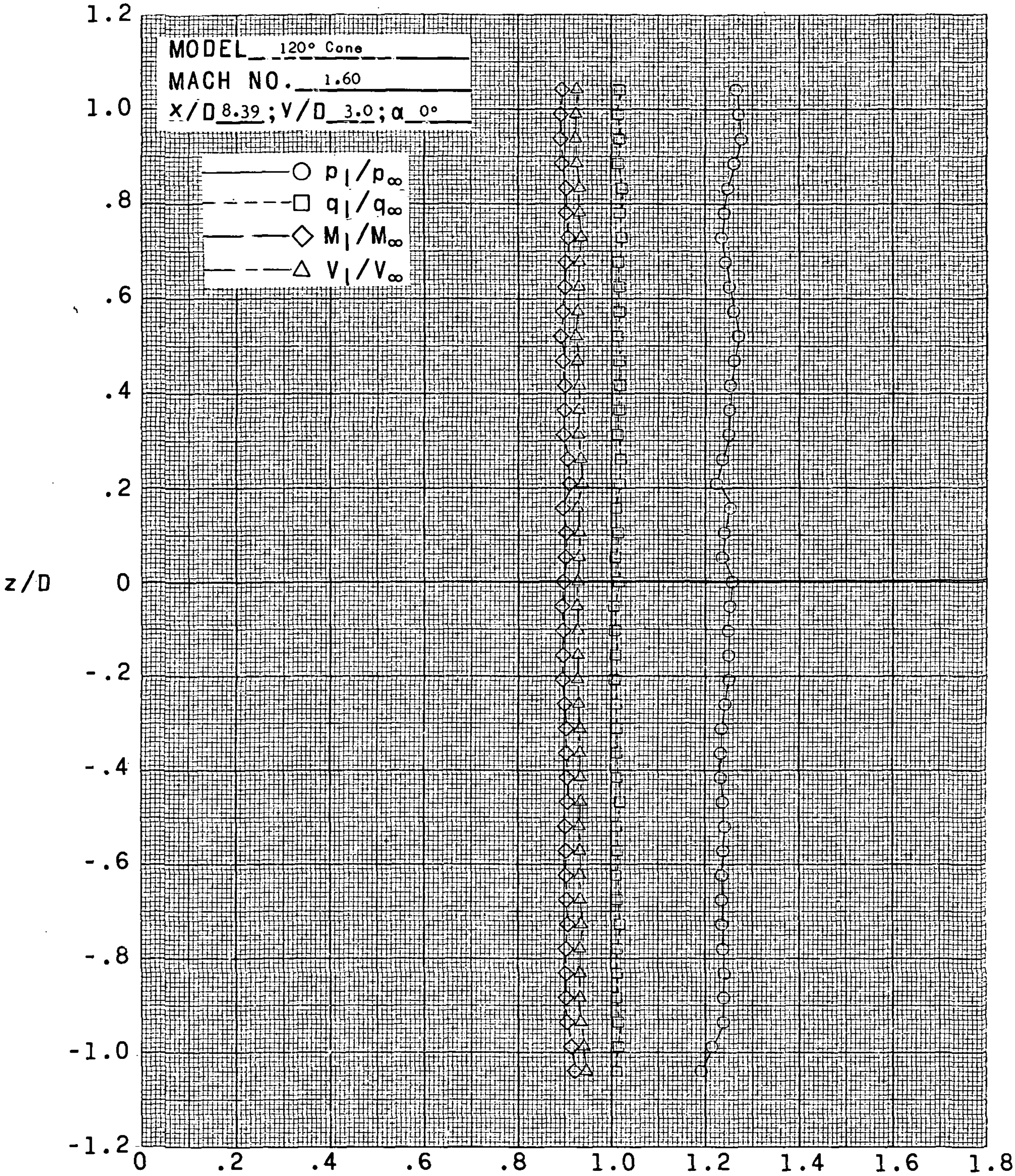
(aa) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 5.- Continued.



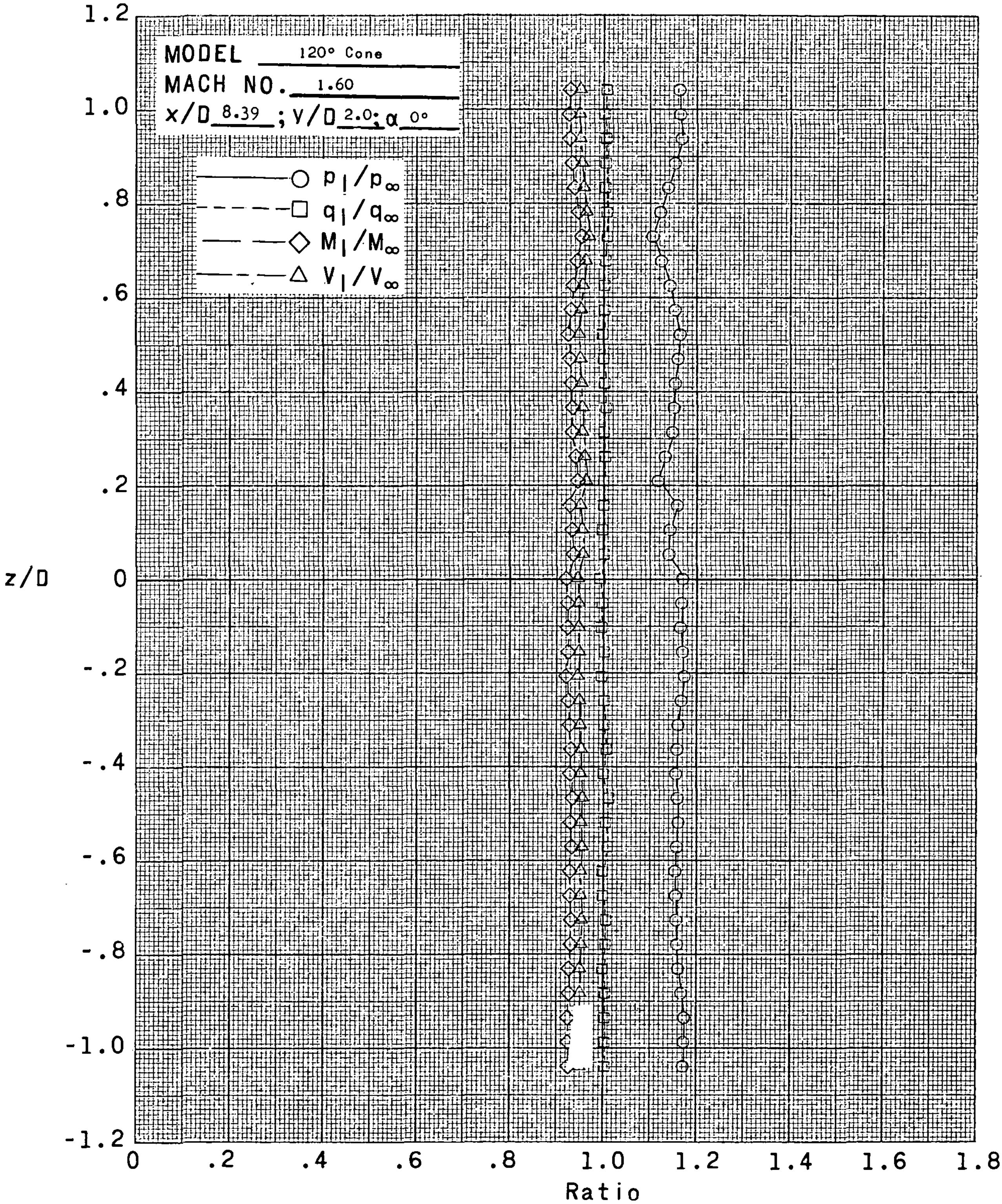
(bb) x/D = 8.0; y/D = 0; α = 0°.

Figure 5.- Continued.



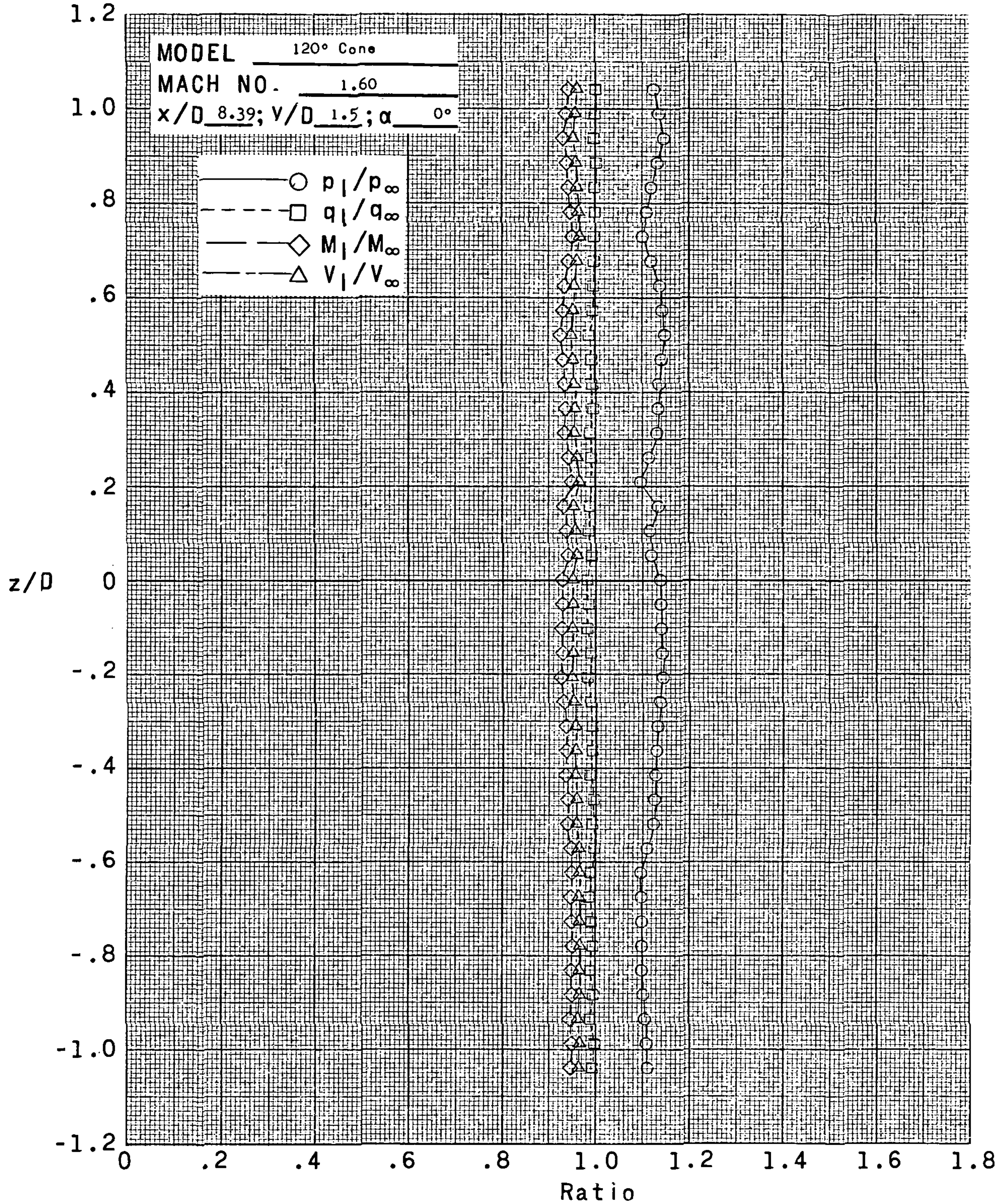
(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^0$.

Figure 5.- Continued.



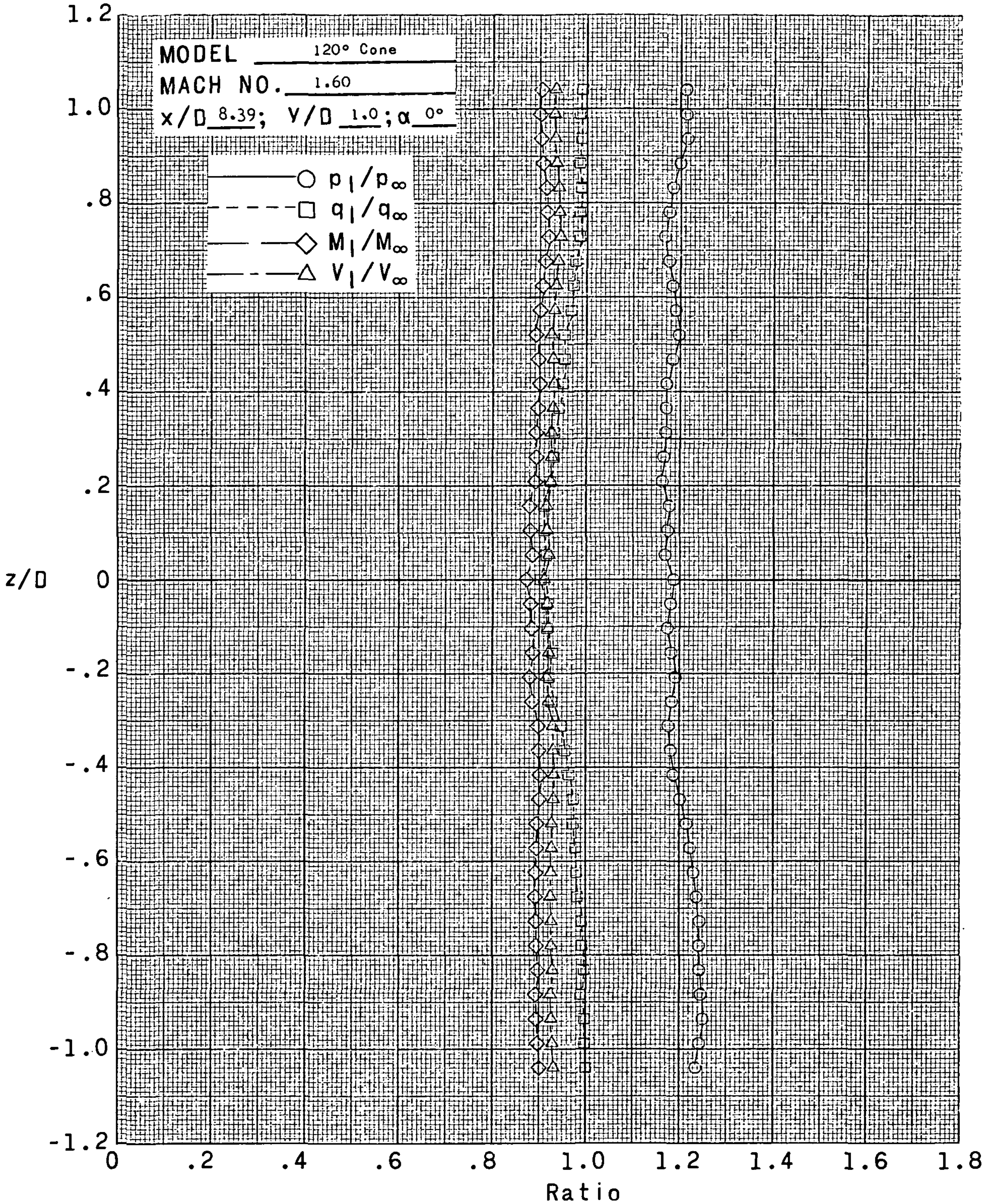
(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^0$.

Figure 5.- Continued.



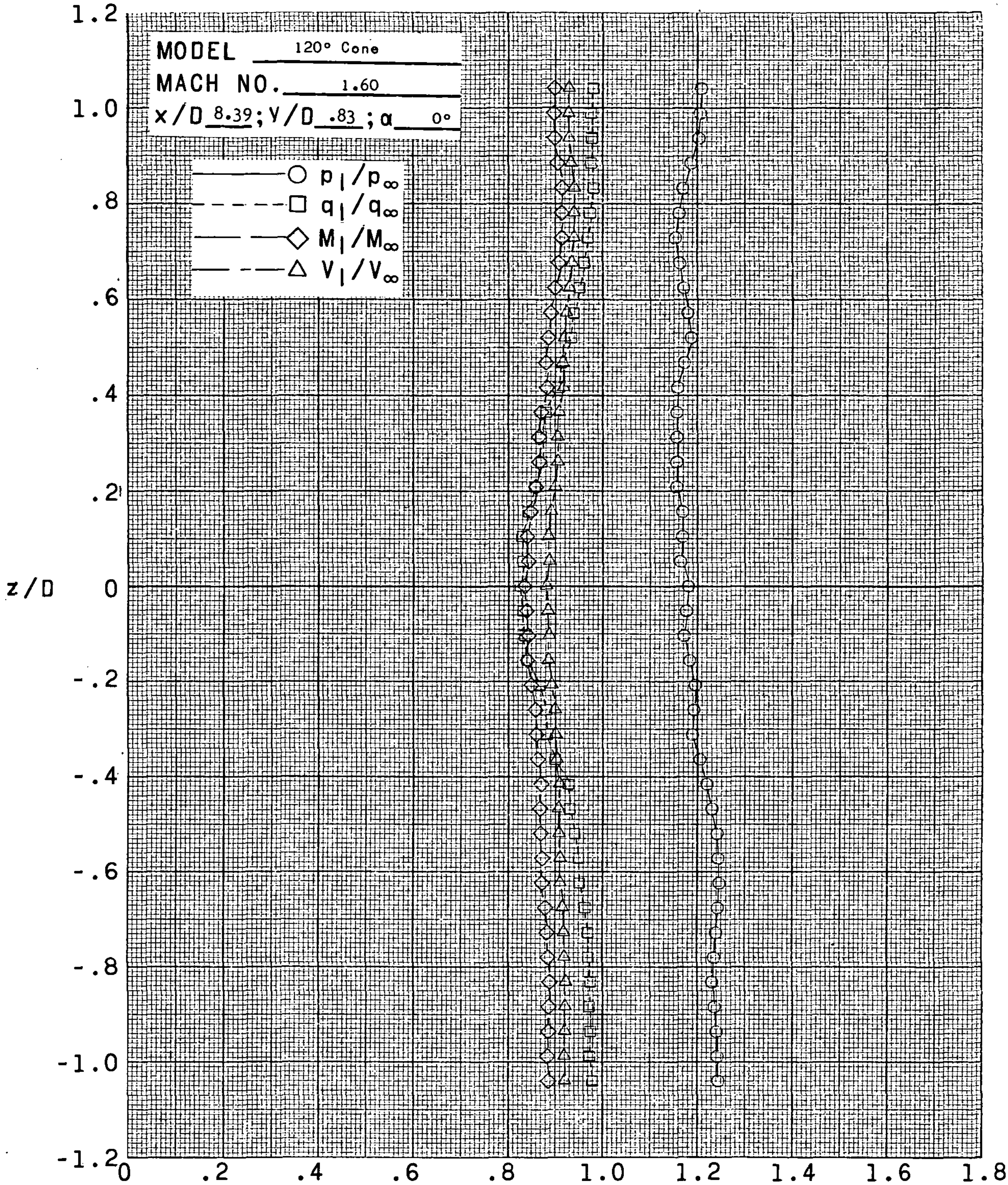
(ee) x/D = 8.39; y/D = 1.5; α = 0°.

Figure 5.- Continued.



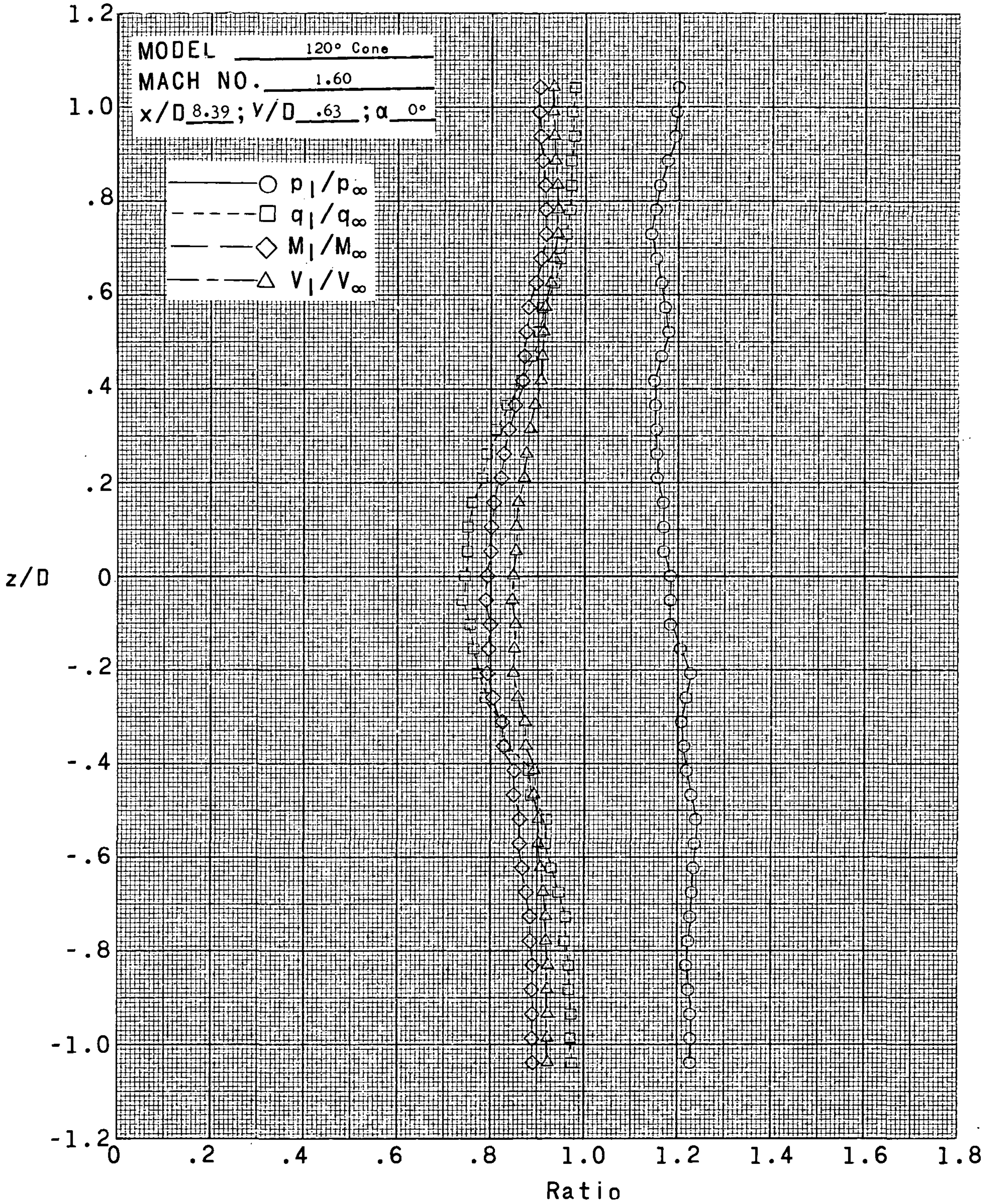
(ff) x/D = 8.39; y/D = 1.0; α = 0°.

Figure 5.- Continued.



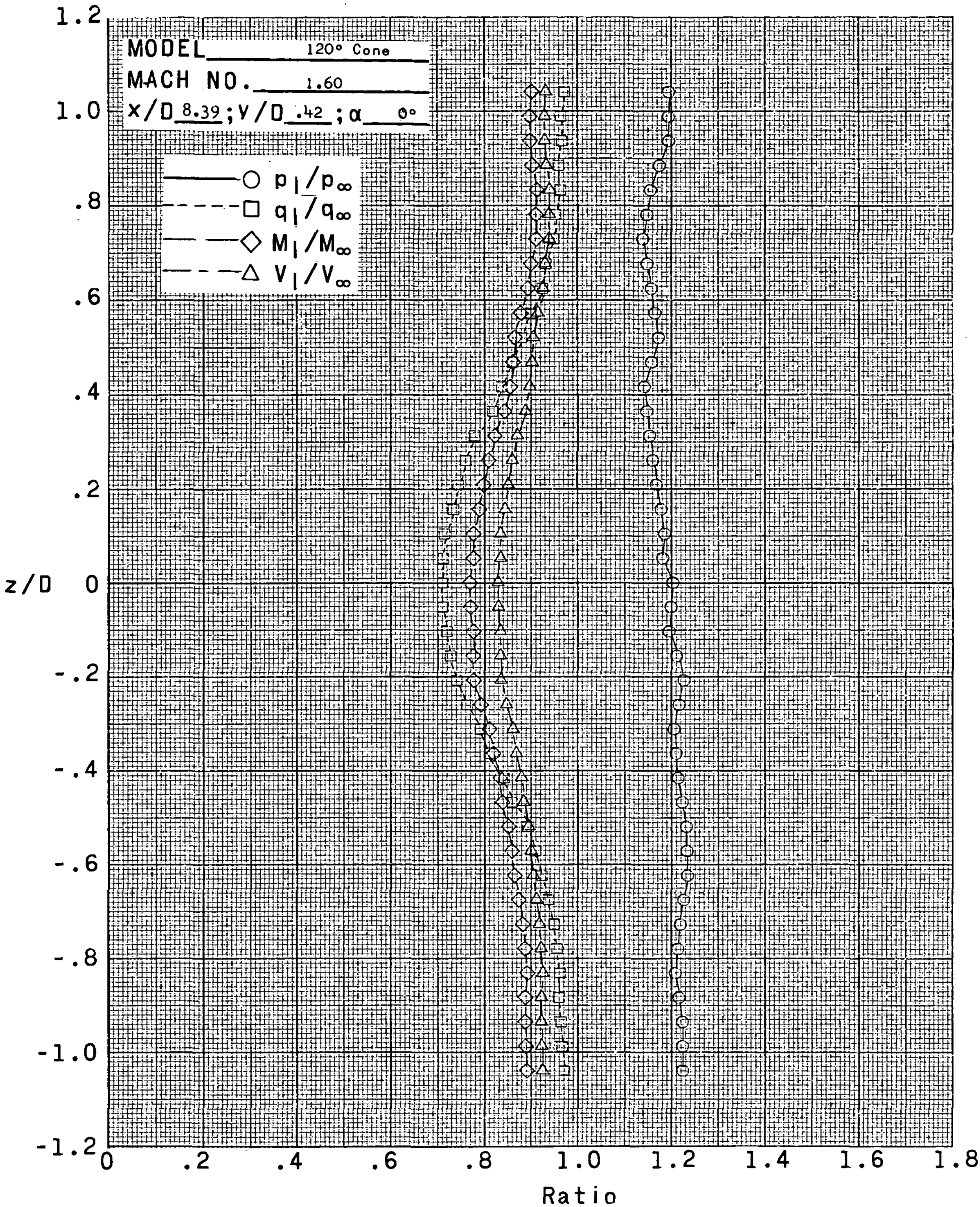
(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^o$.

Figure 5.- Continued.



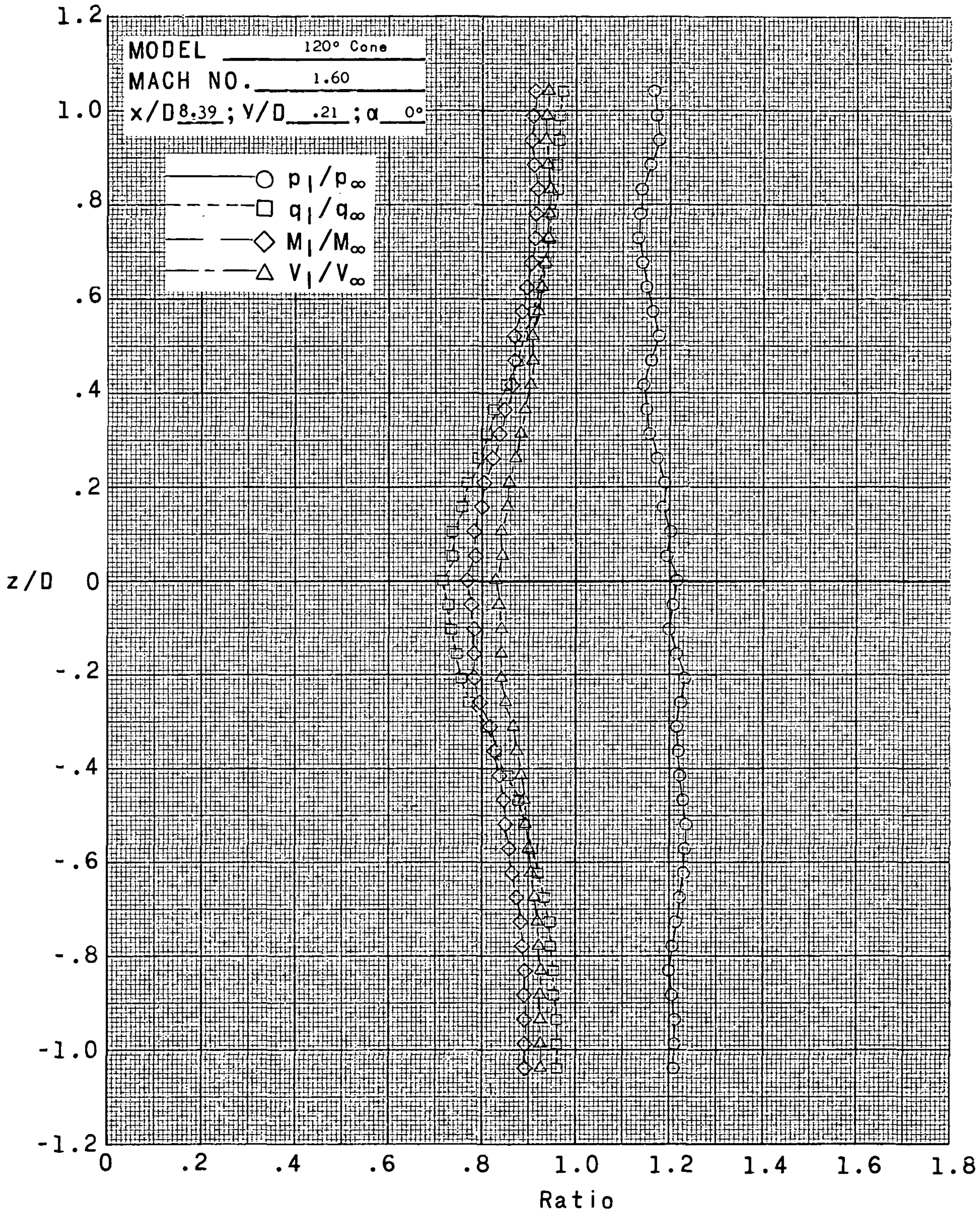
(hh) x/D = 8.39; y/D = 0.63; α = 0°.

Figure 5.- Continued.



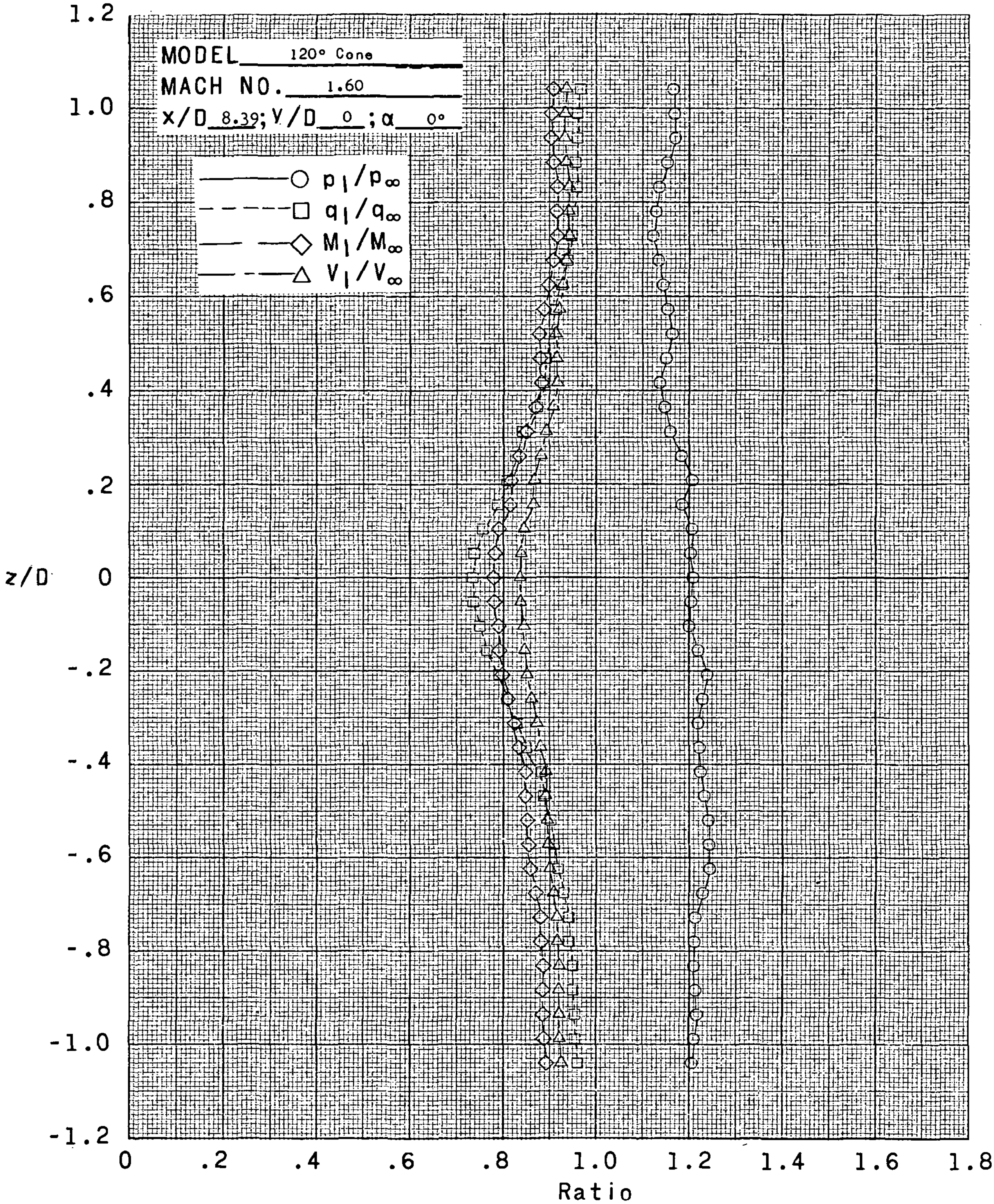
(ii) $x/D = 8.39$; $y/D = 0.42$; $\alpha = 0^0$.

Figure 5.- Continued.



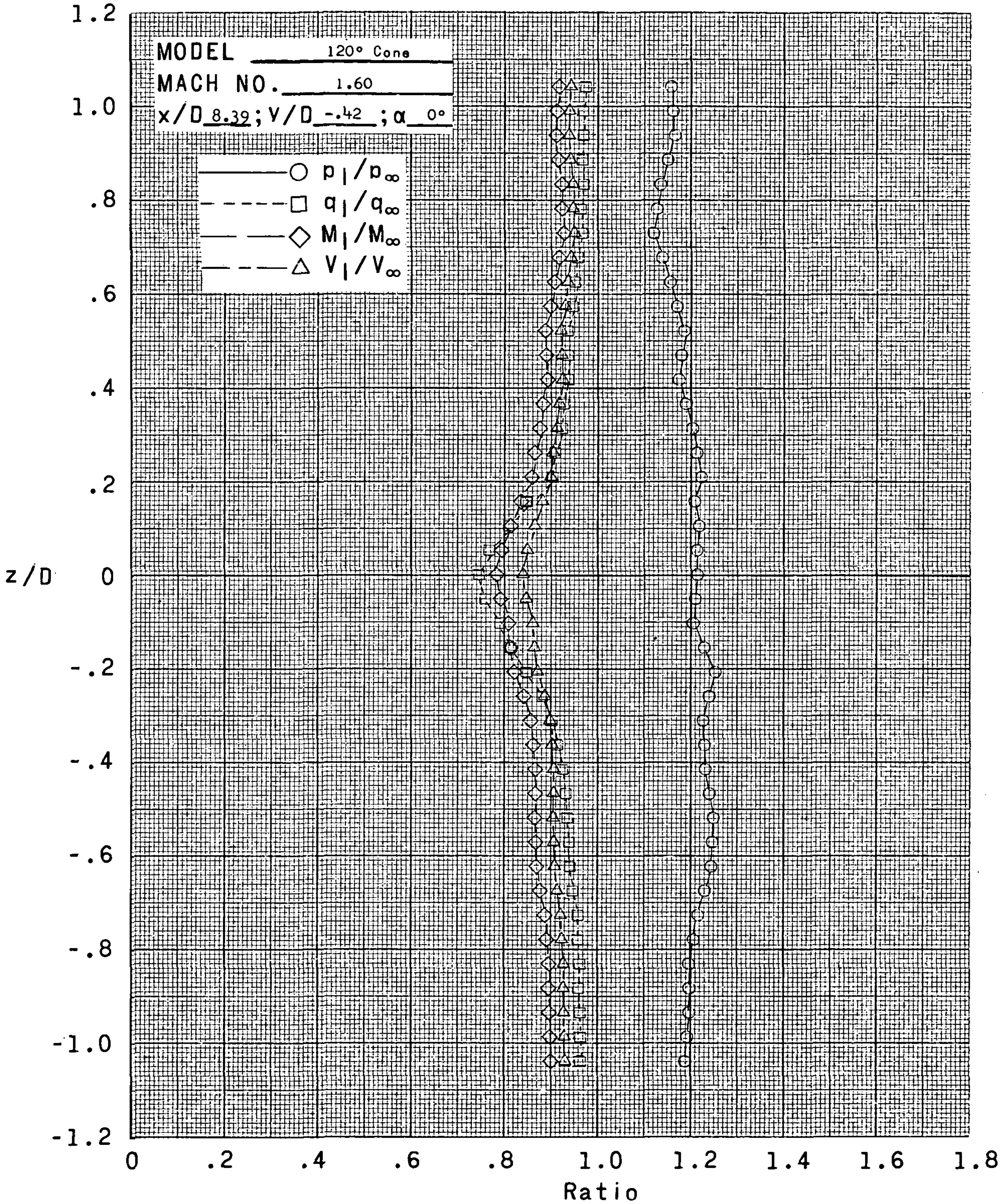
(jj) x/D = 8.39; y/D = 0.21; $\alpha = 0^{0}$.

Figure 5.- Continued.



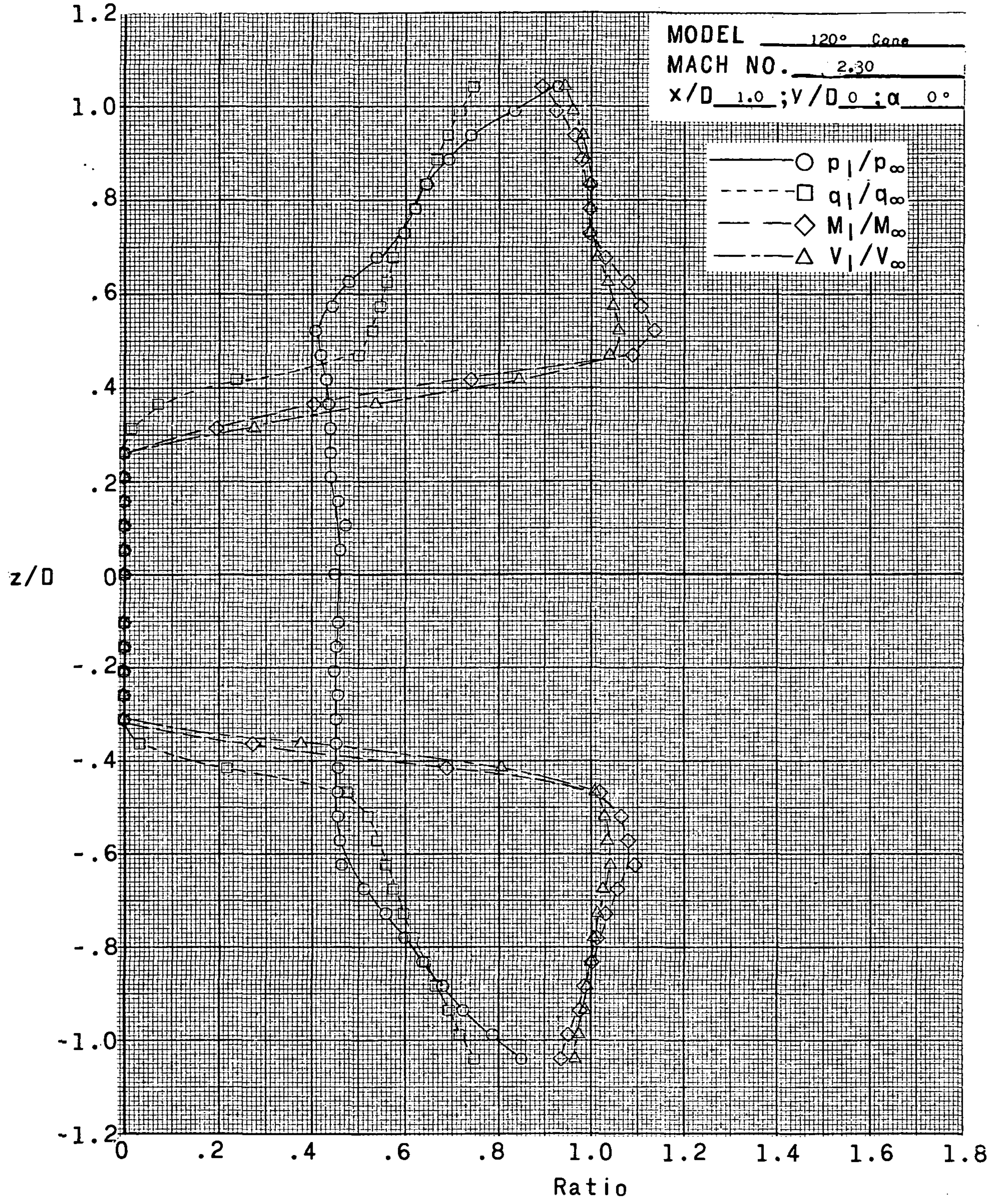
(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^0$.

Figure 5.- Continued.



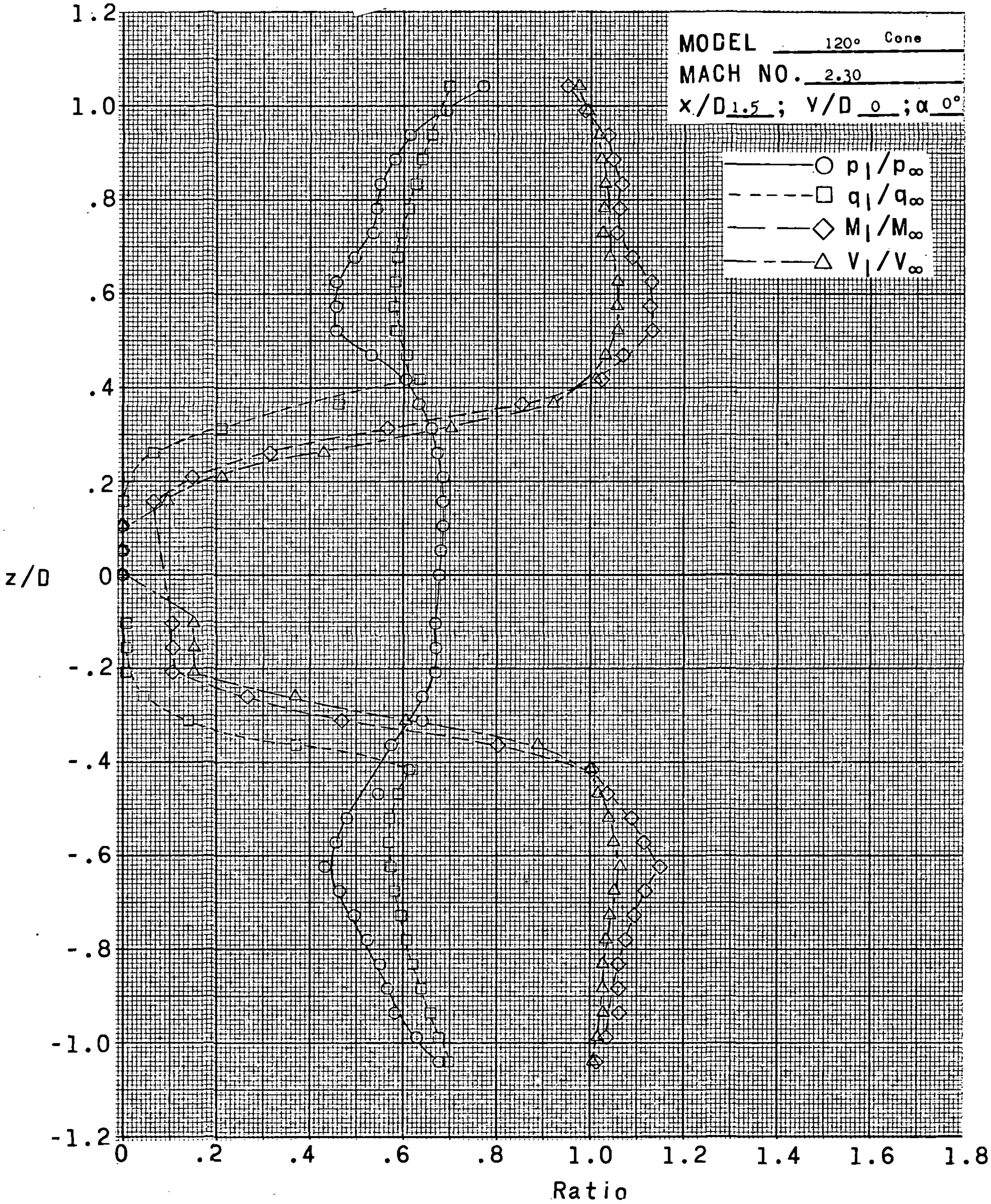
(ll) x/D = 8.39; y/D = -0.42; α = 0°.

Figure 5.- Concluded.



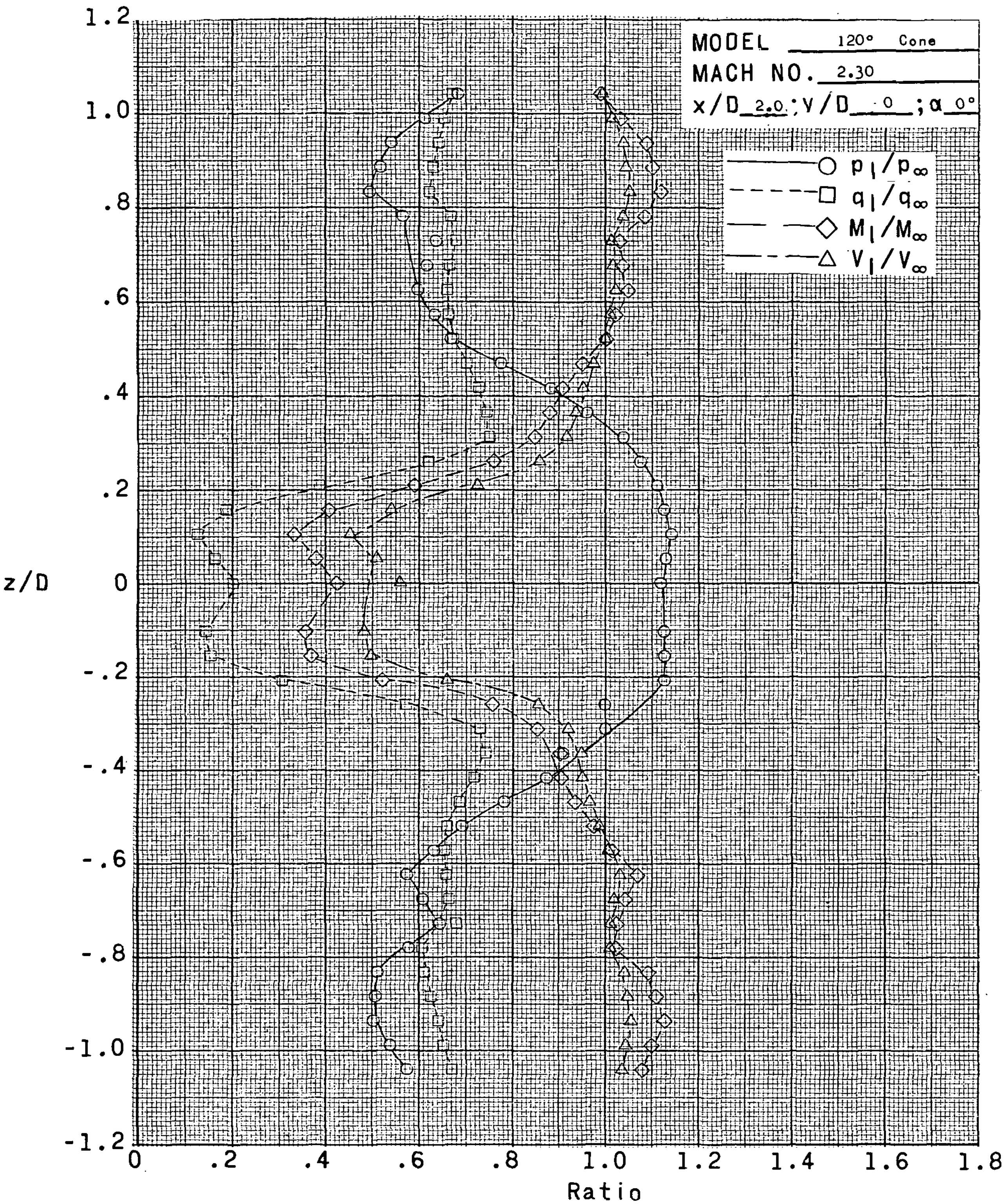
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 6.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in the wake of a 120°-included-angle cone at a Mach number of 2.30 and a Reynolds number of 1.65×10^6 per foot (5.42×10^6 per meter).



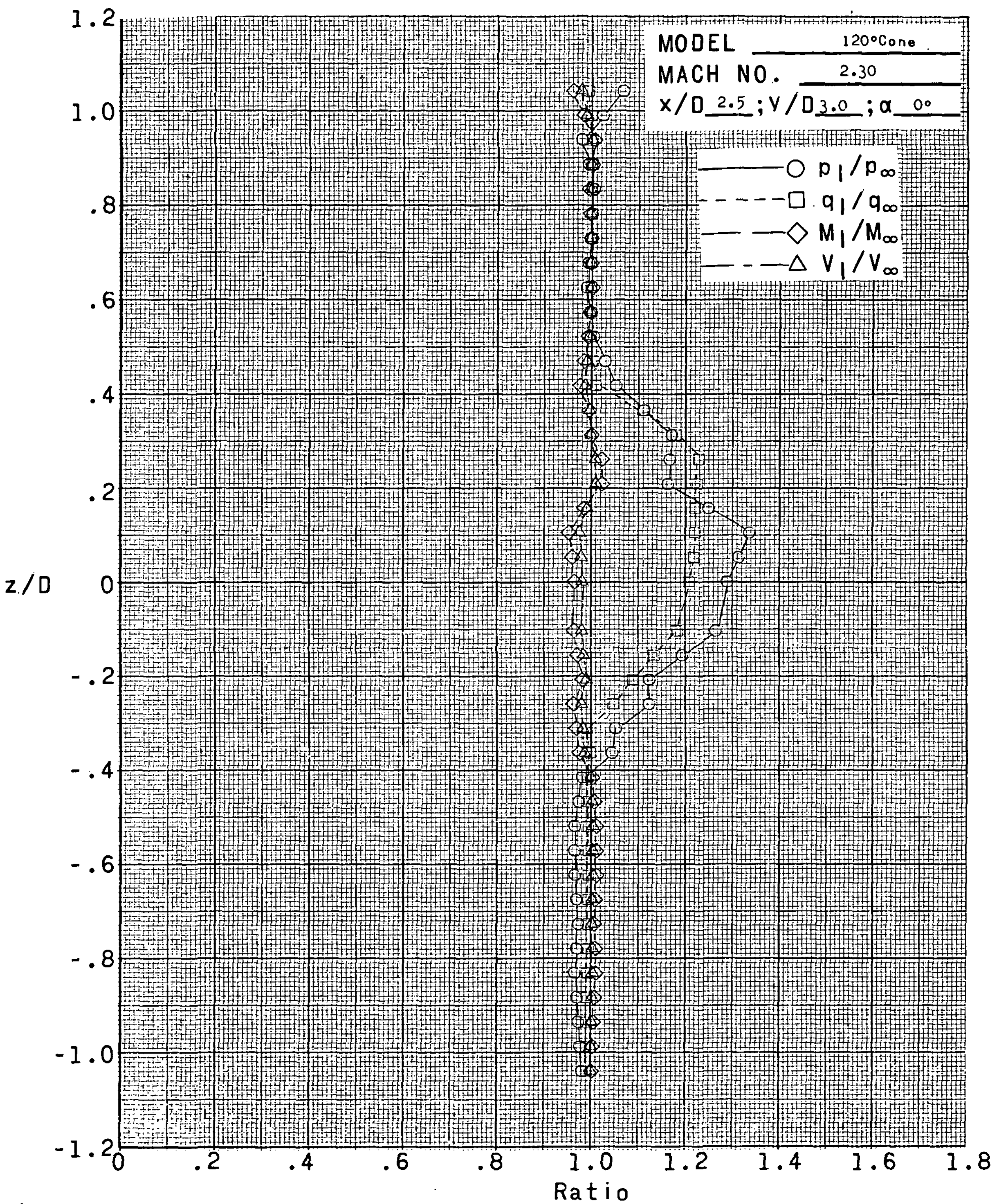
(b) x/D = 1.5; y/D = 0; α = 0°.

Figure 6.- Continued.



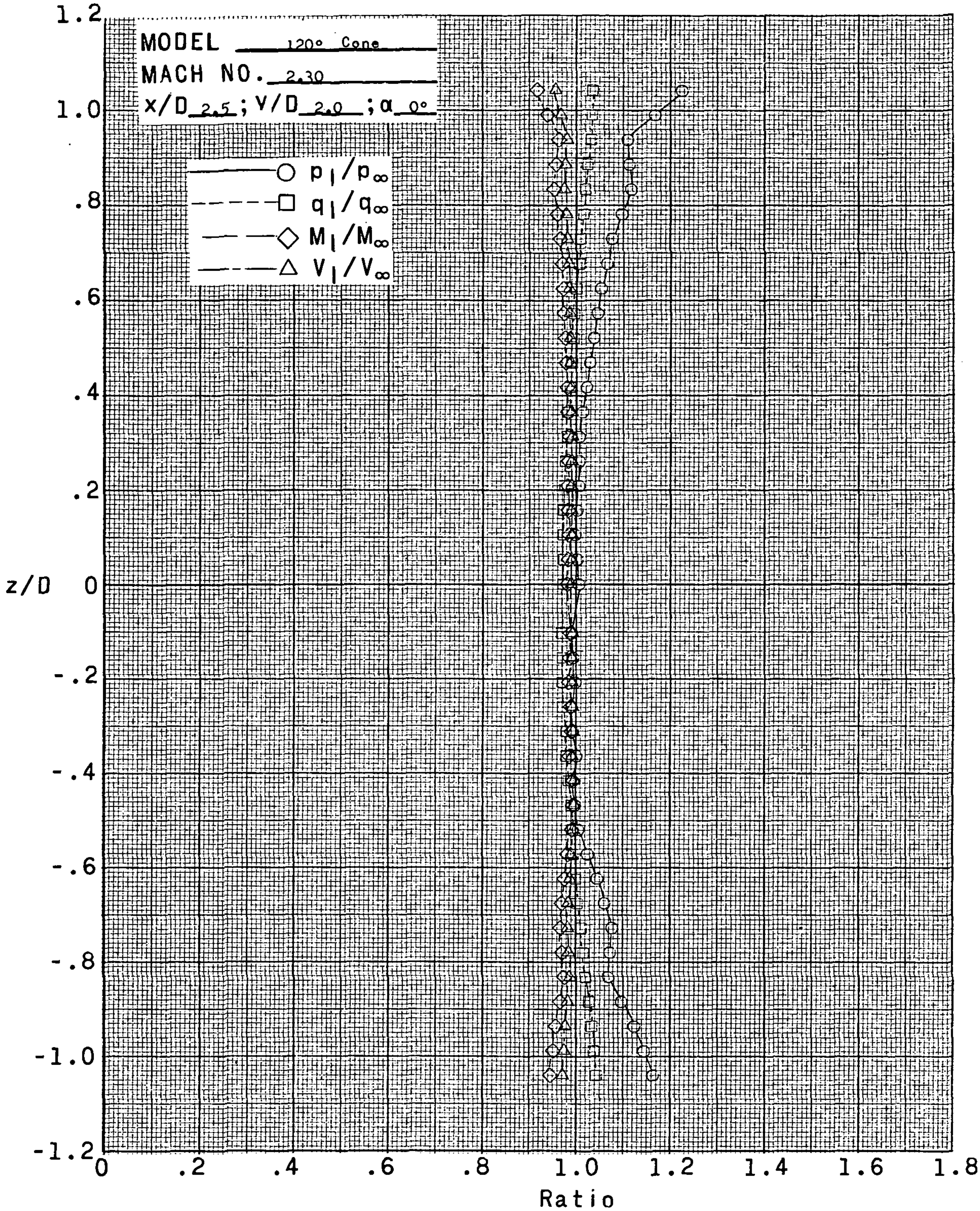
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^{o}$.

Figure 6.- Continued.



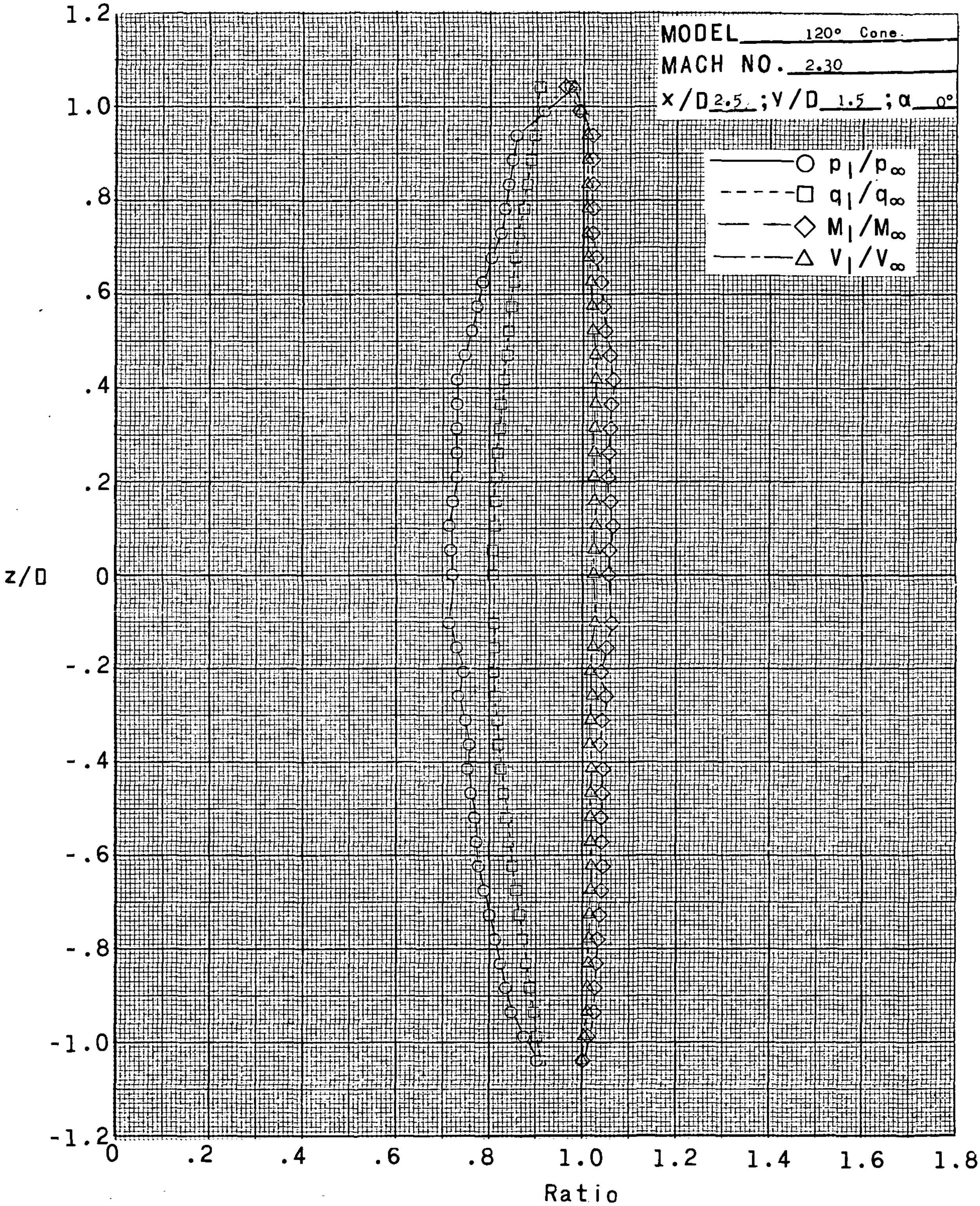
(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^o$.

Figure 6.- Continued.



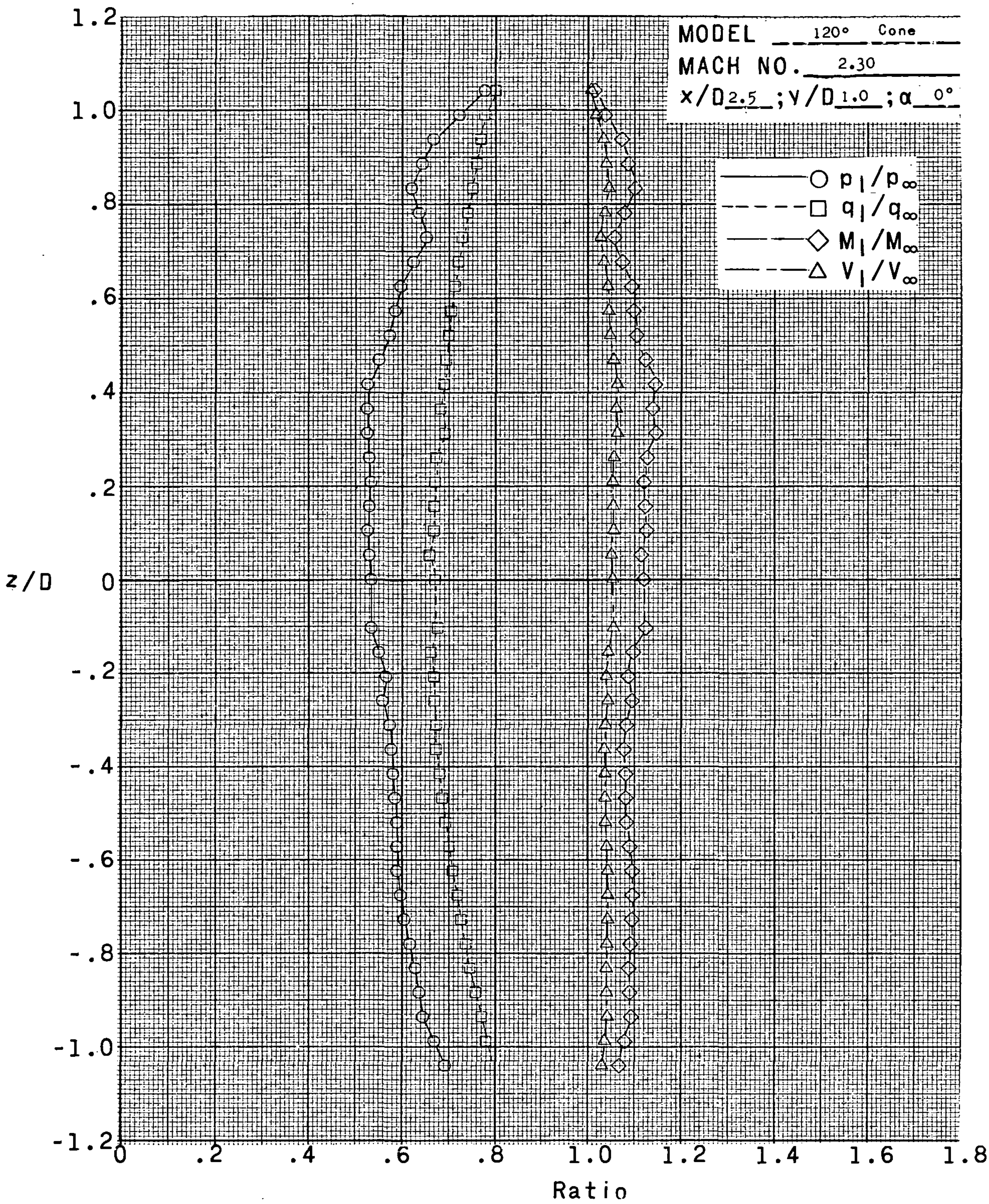
(e) x/D = 2.5; y/D = 2.0; α = 0°.

Figure 6.- Continued.



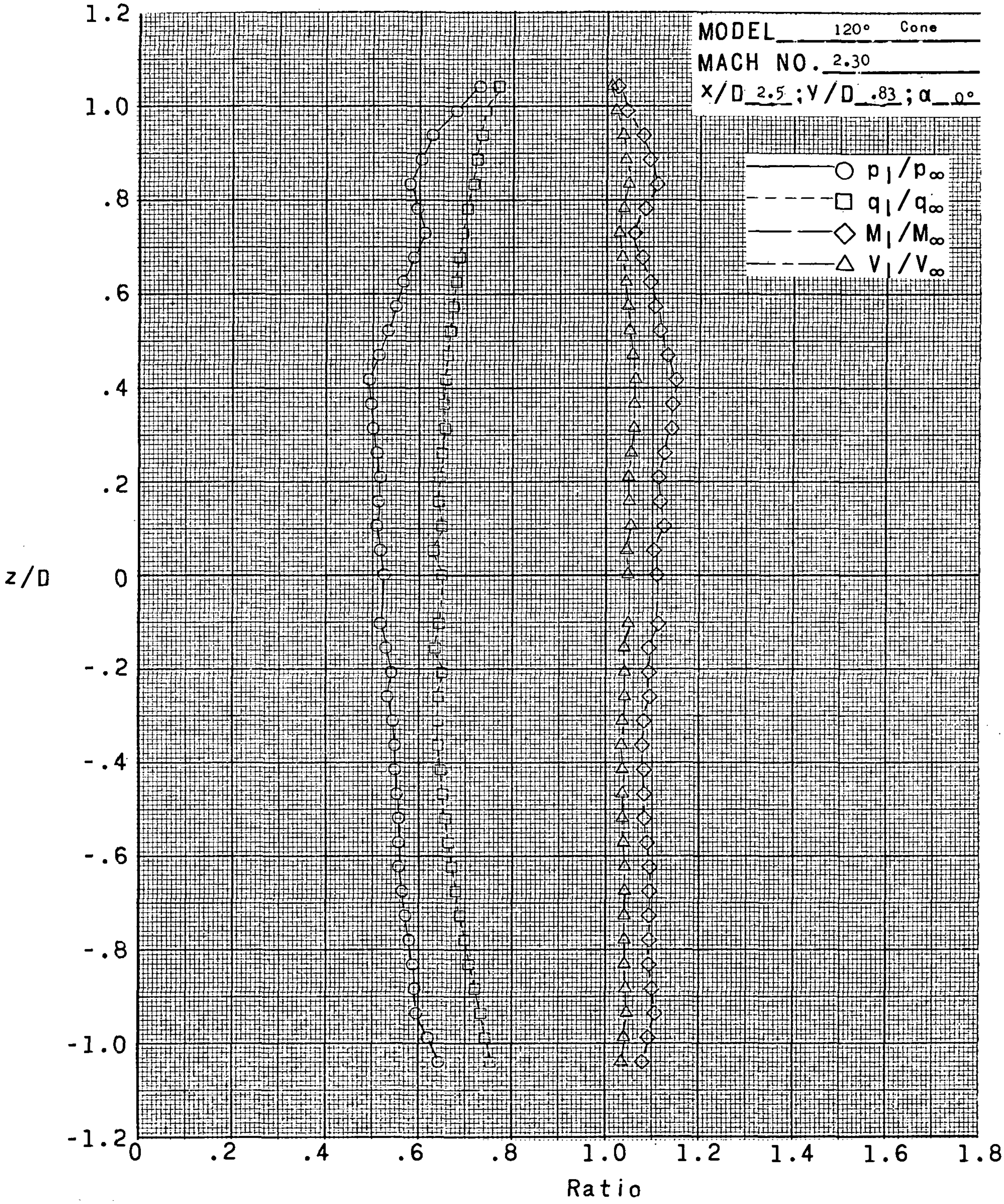
(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^{0}$.

Figure 6.- Continued.



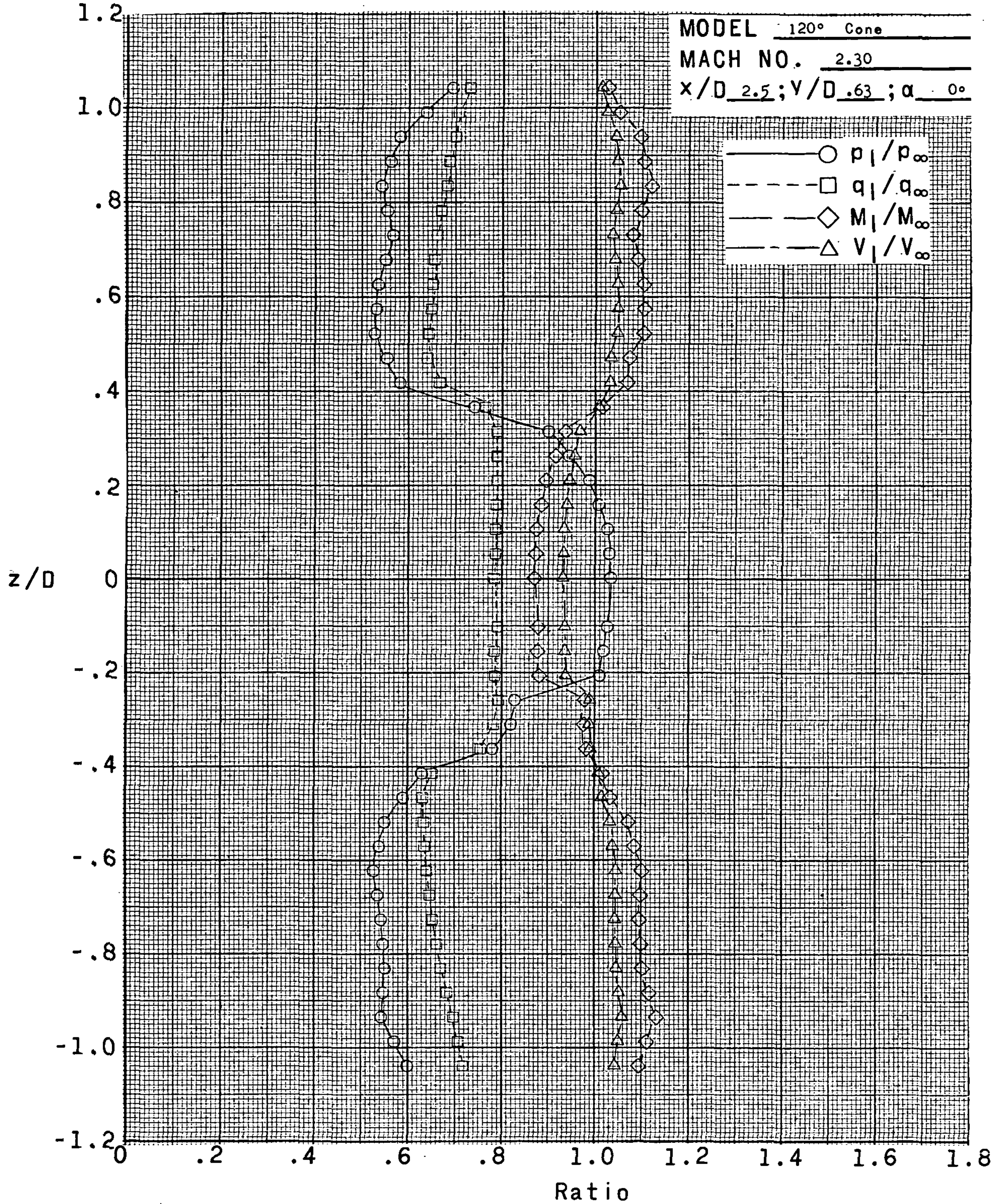
(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0^{0}$.

Figure 6.- Continued.



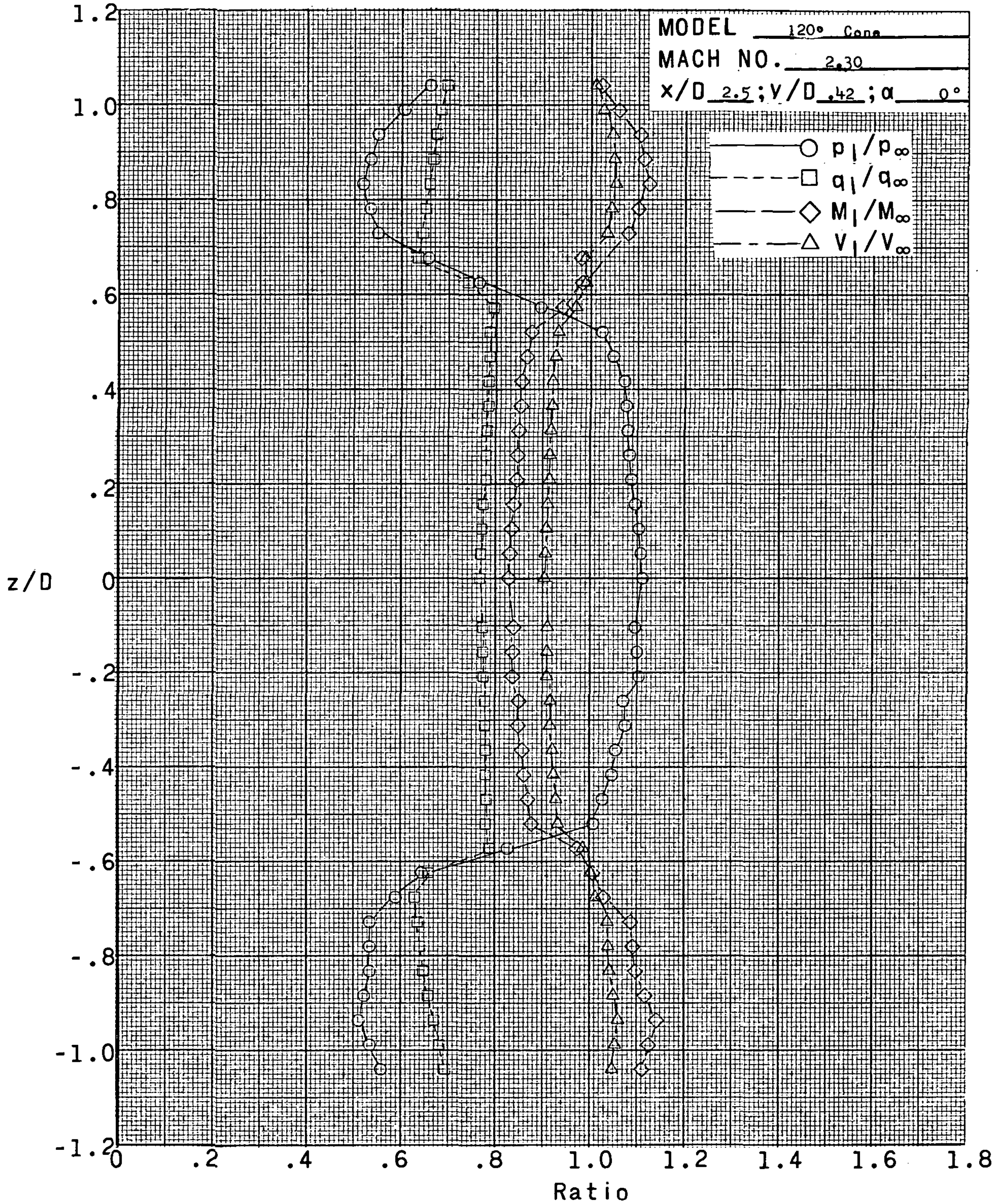
(h) x/D = 2.5; y/D = 0.83; α = 0°.

Figure 6.- Continued.



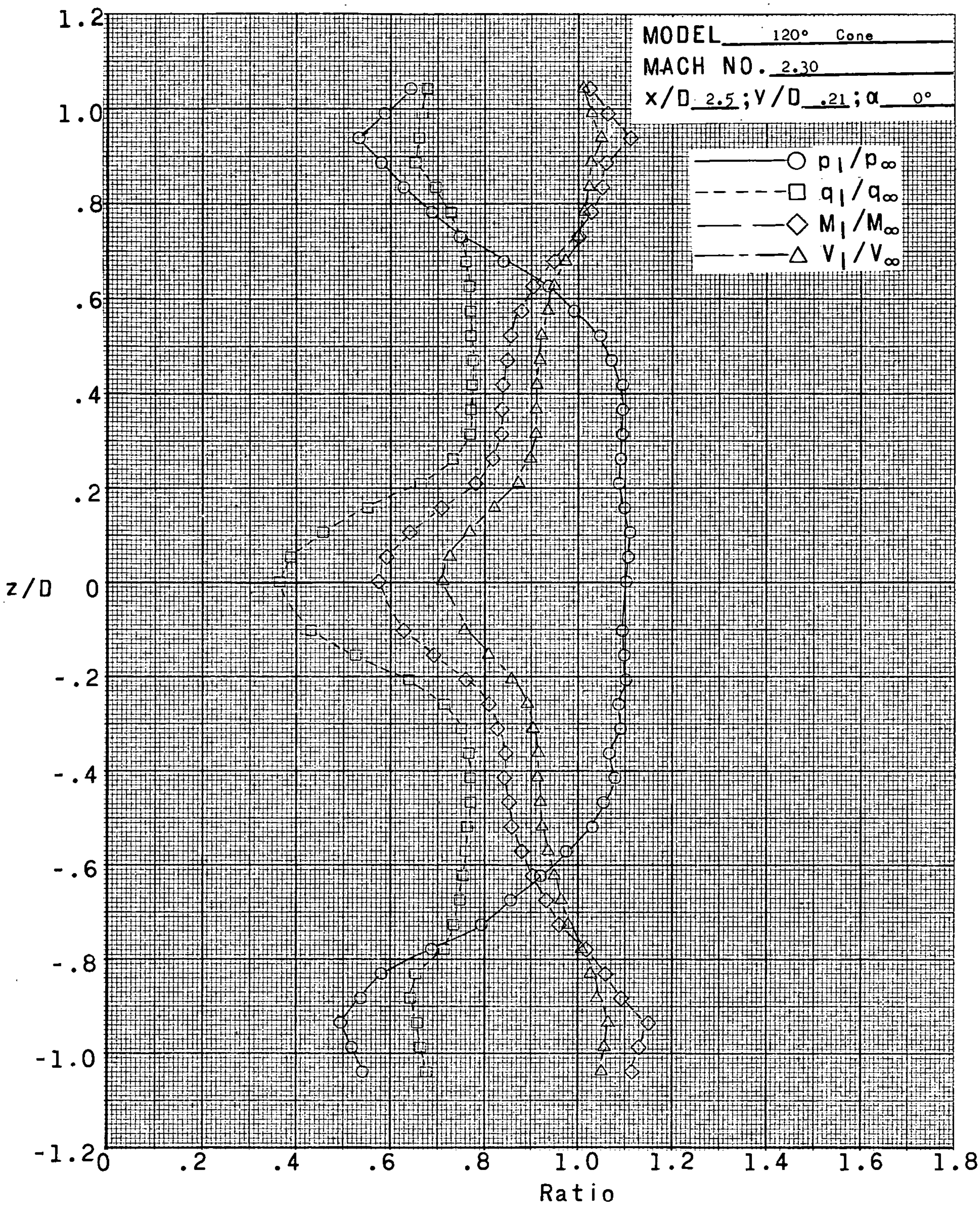
(i) x/D = 2.5; y/D = 0.63; α = 0°.

Figure 6.- Continued.



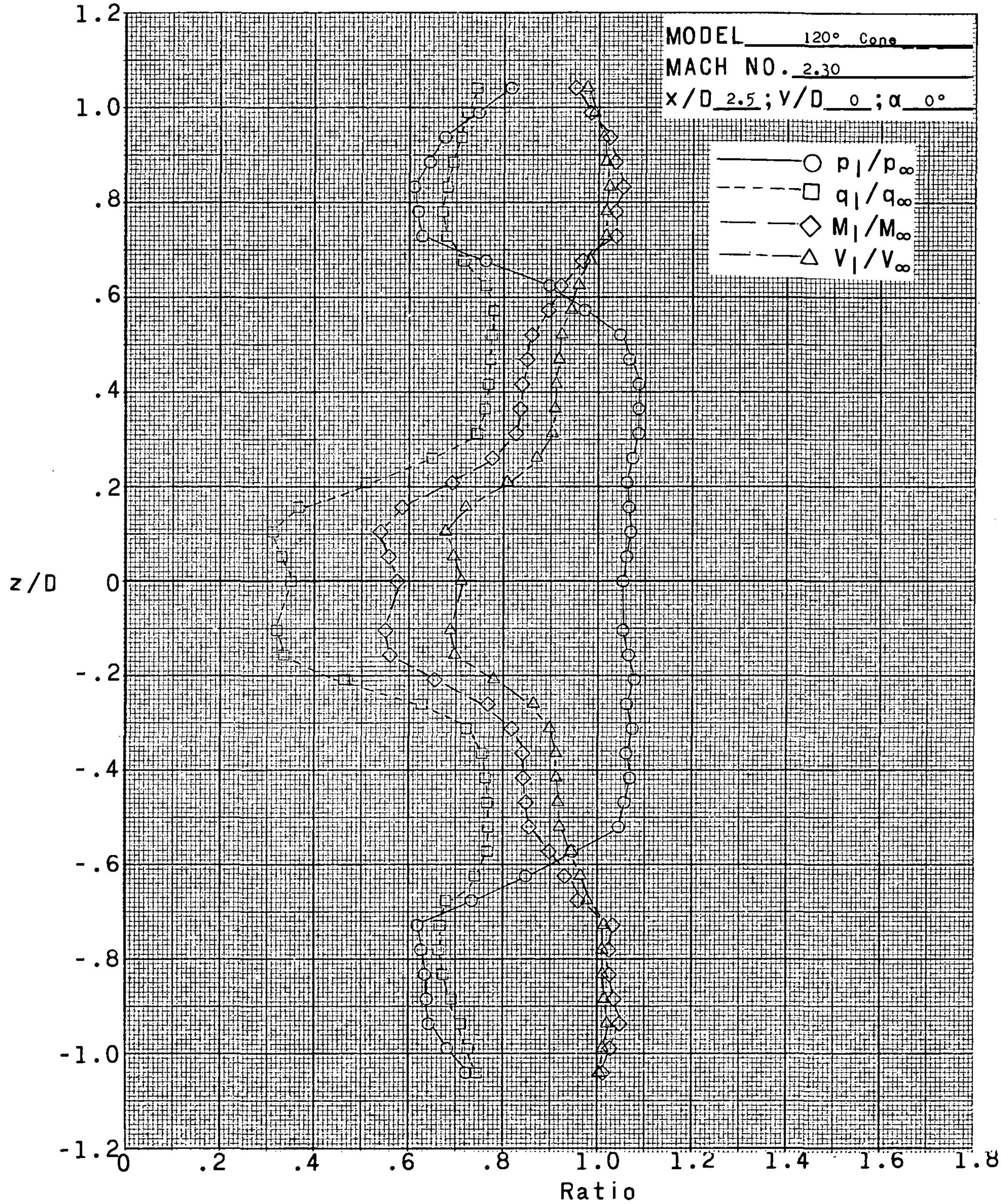
(j) x/D = 2.5; y/D = 0.42; α = 0°.

Figure 6.- Continued.



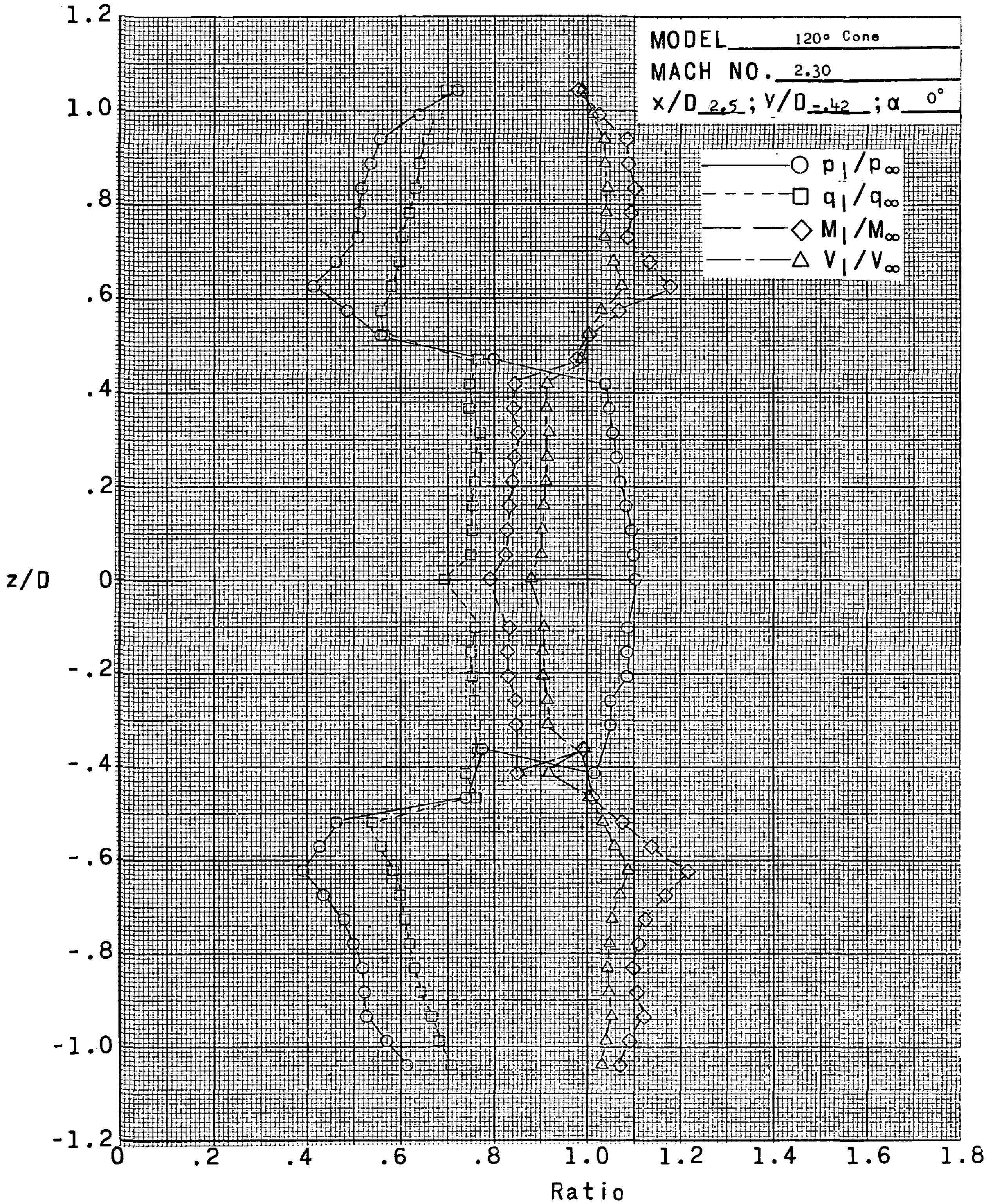
(k) x/D = 2.5; y/D = 0.21; α = 0°.

Figure 6.- Continued.



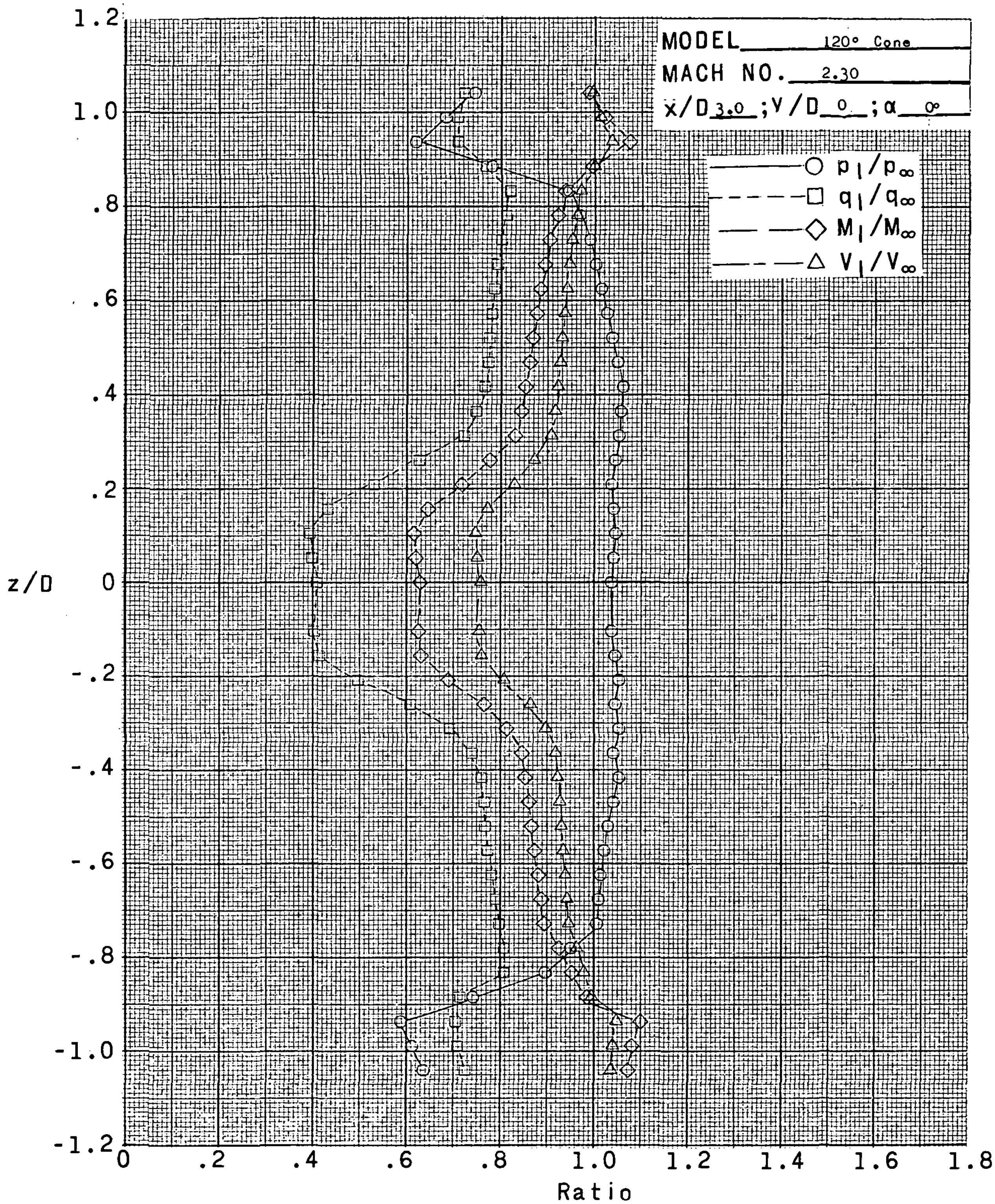
(l) x/D = 2.5; y/D = 0; α = 0°.

Figure 6.- Continued.



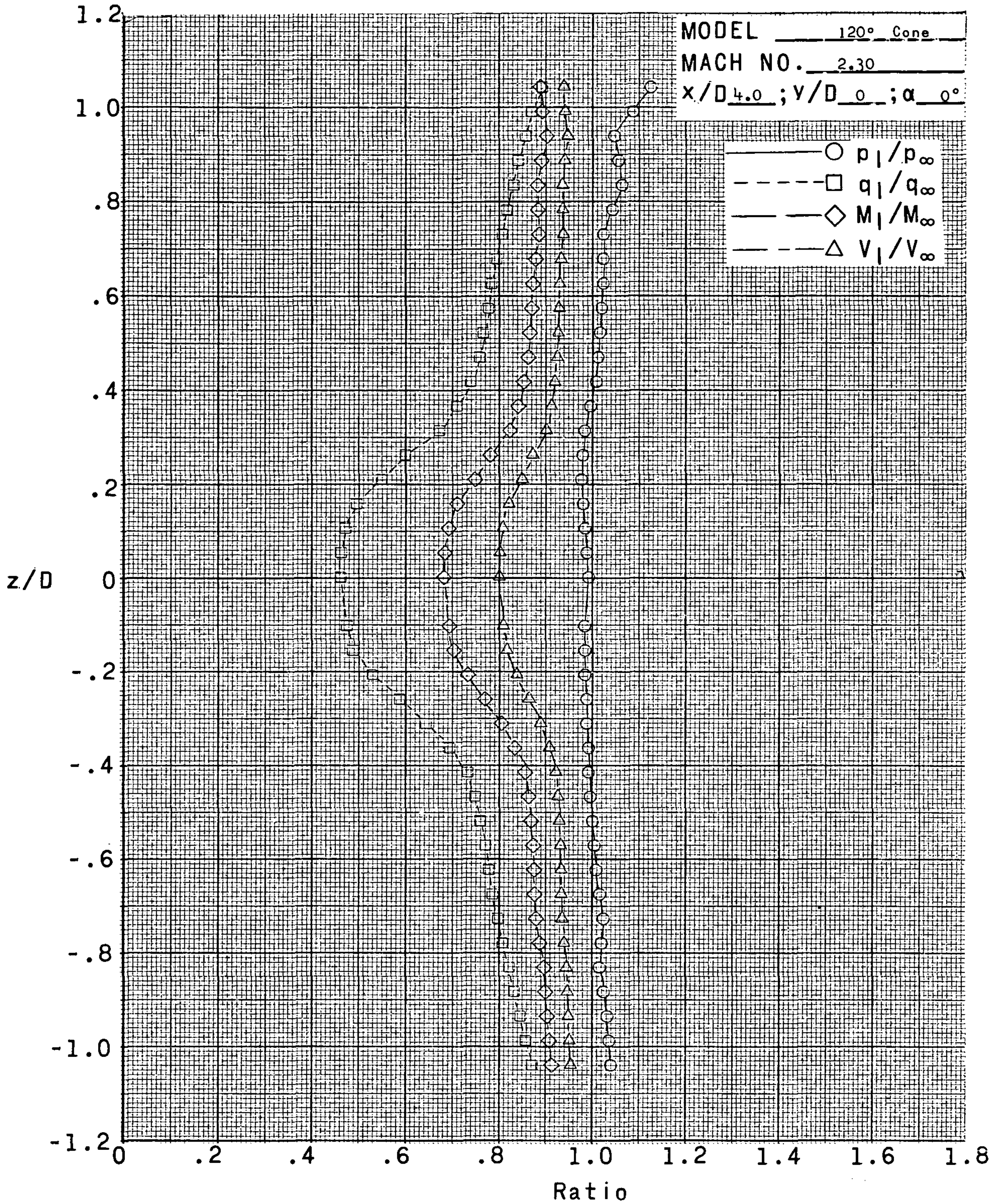
(m) x/D = 2.5; y/D = -0.42; α = 0°.

Figure 6.- Continued.



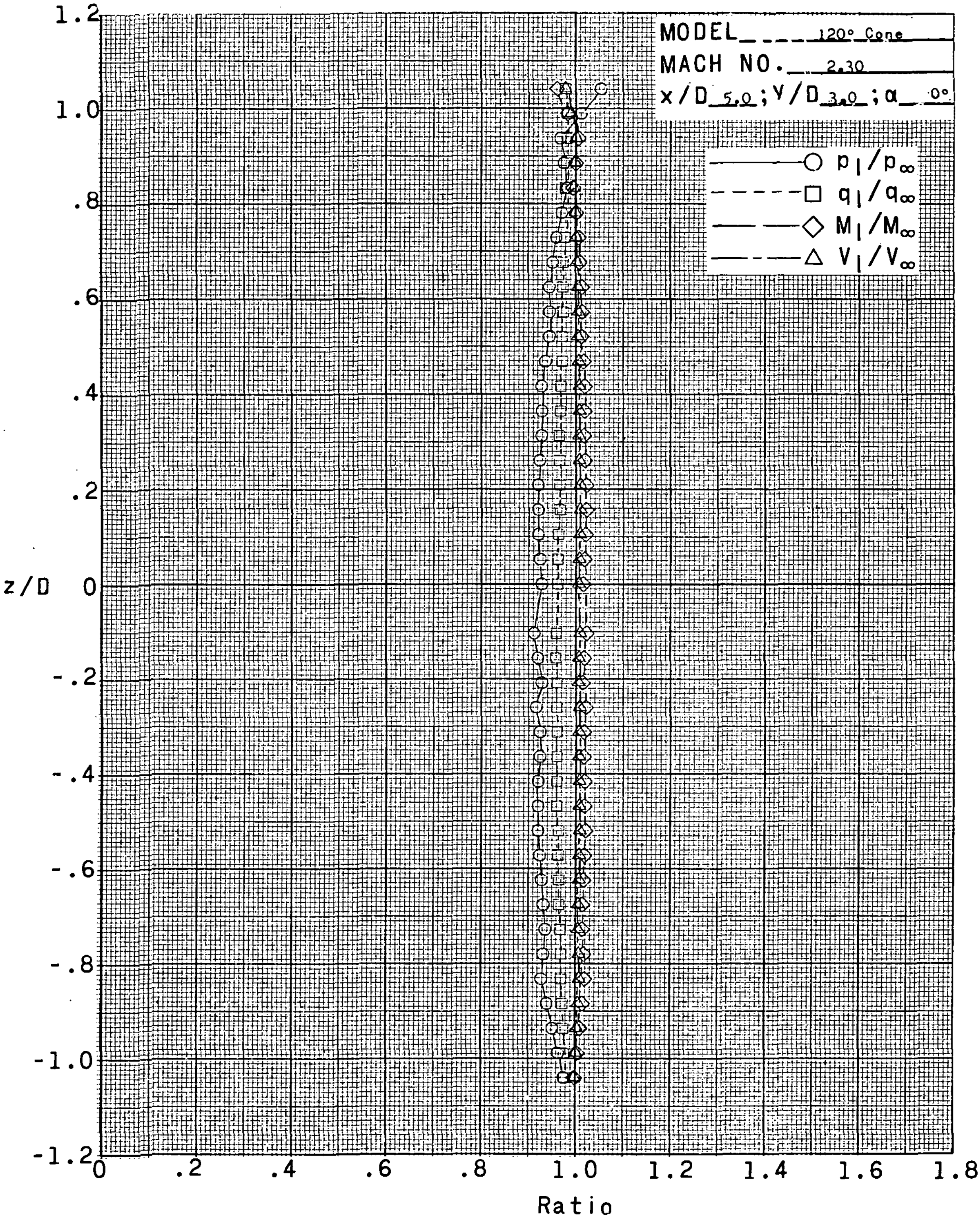
(n) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 6.- Continued.



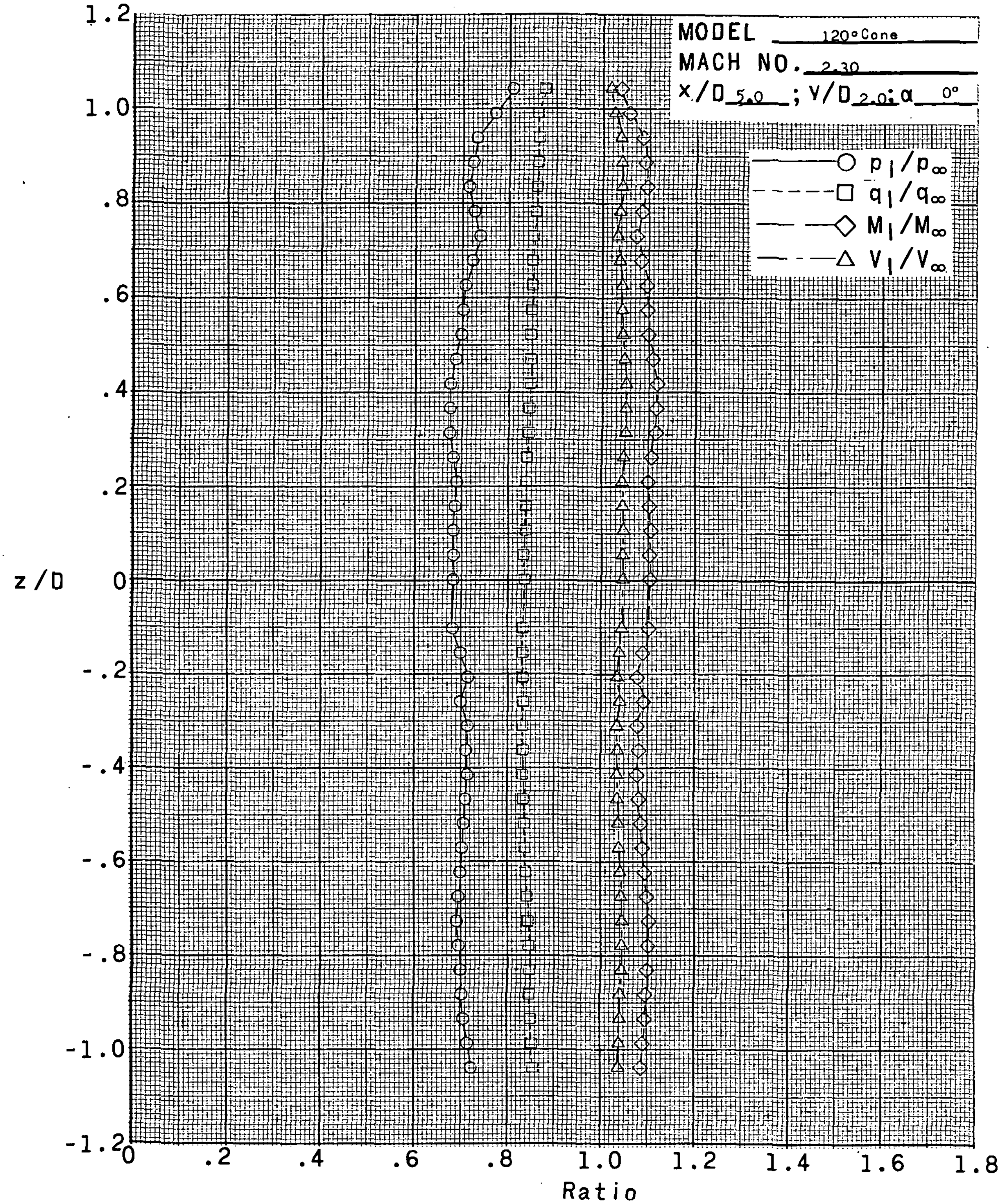
(o) x/D = 4.0; y/D = 0; α = 0°.

Figure 6.- Continued.



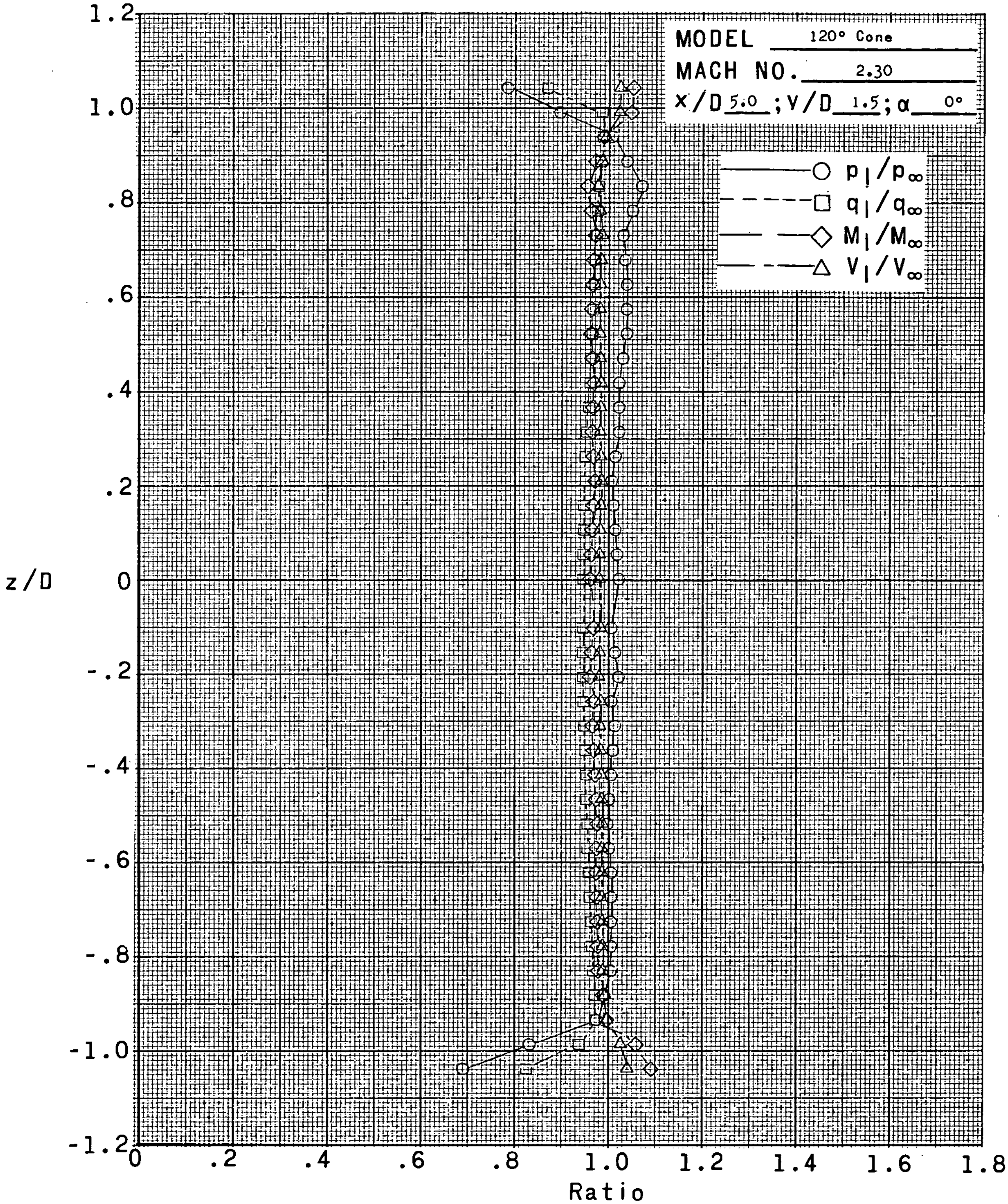
(p) x/D = 5.0; y/D = 3.0; α = 0°.

Figure 6.- Continued.



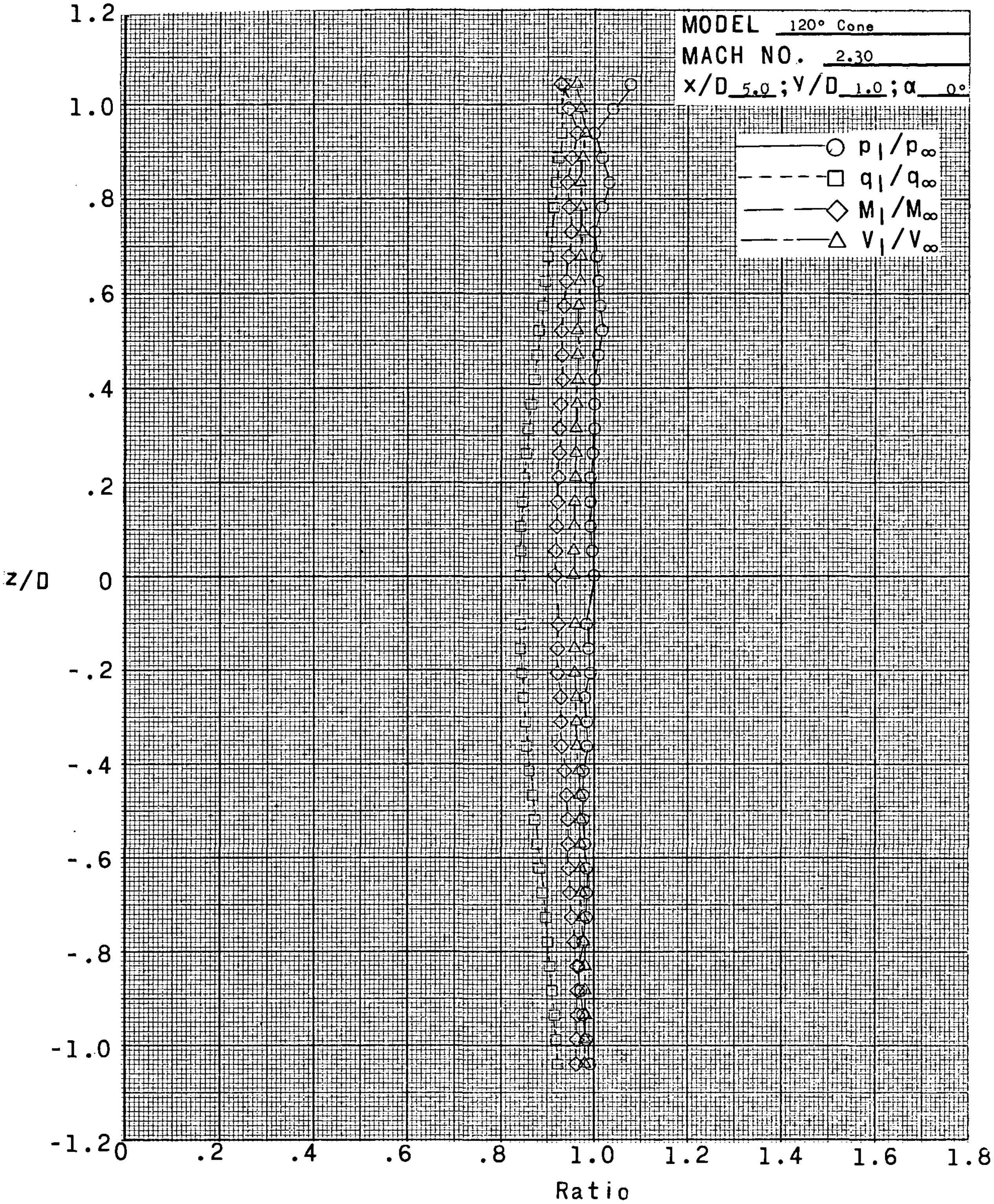
(q) x/D = 5.0; y/D = 2.0; α = 0°.

Figure 6.- Continued.



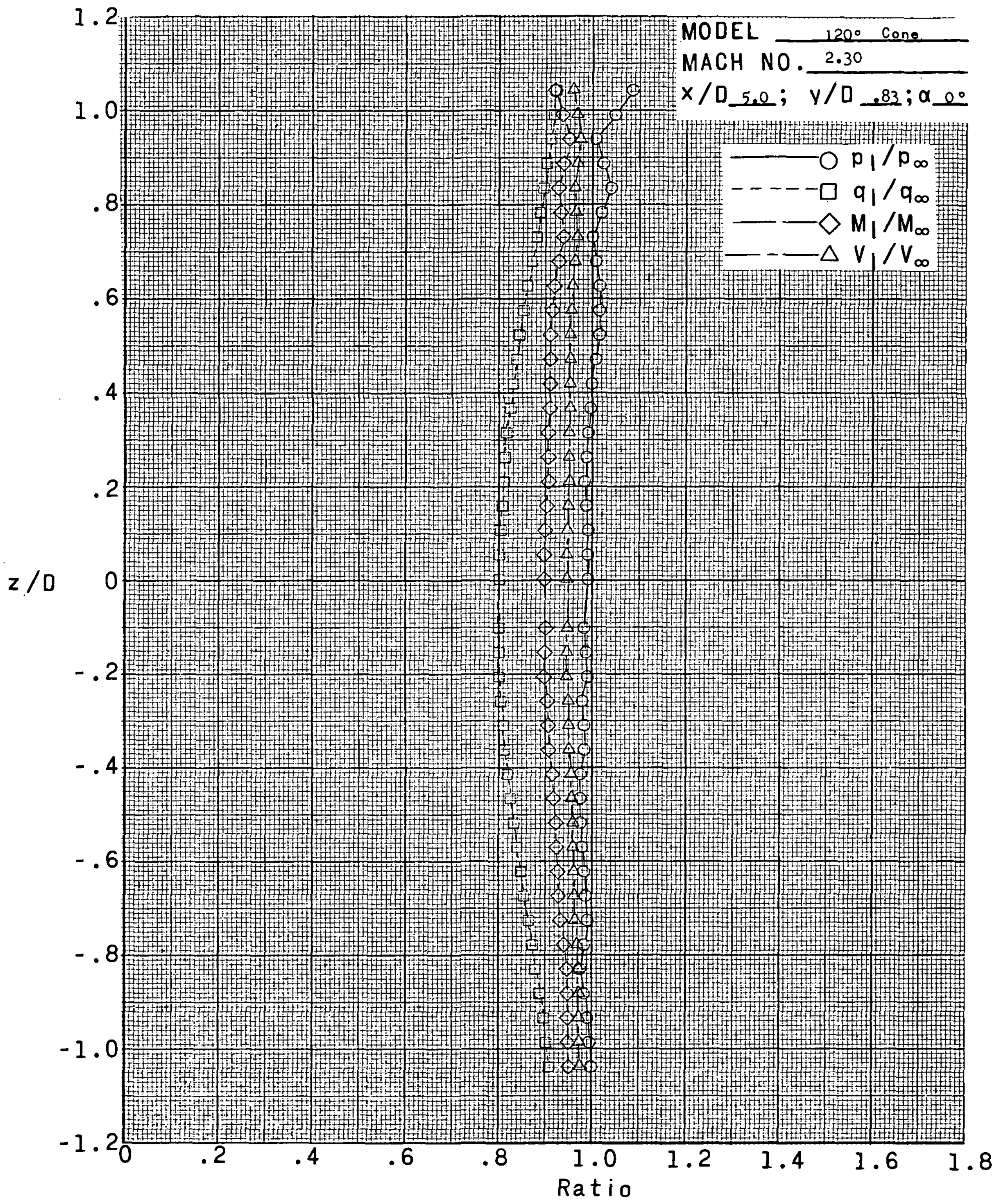
(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0^o$.

Figure 6.- Continued.



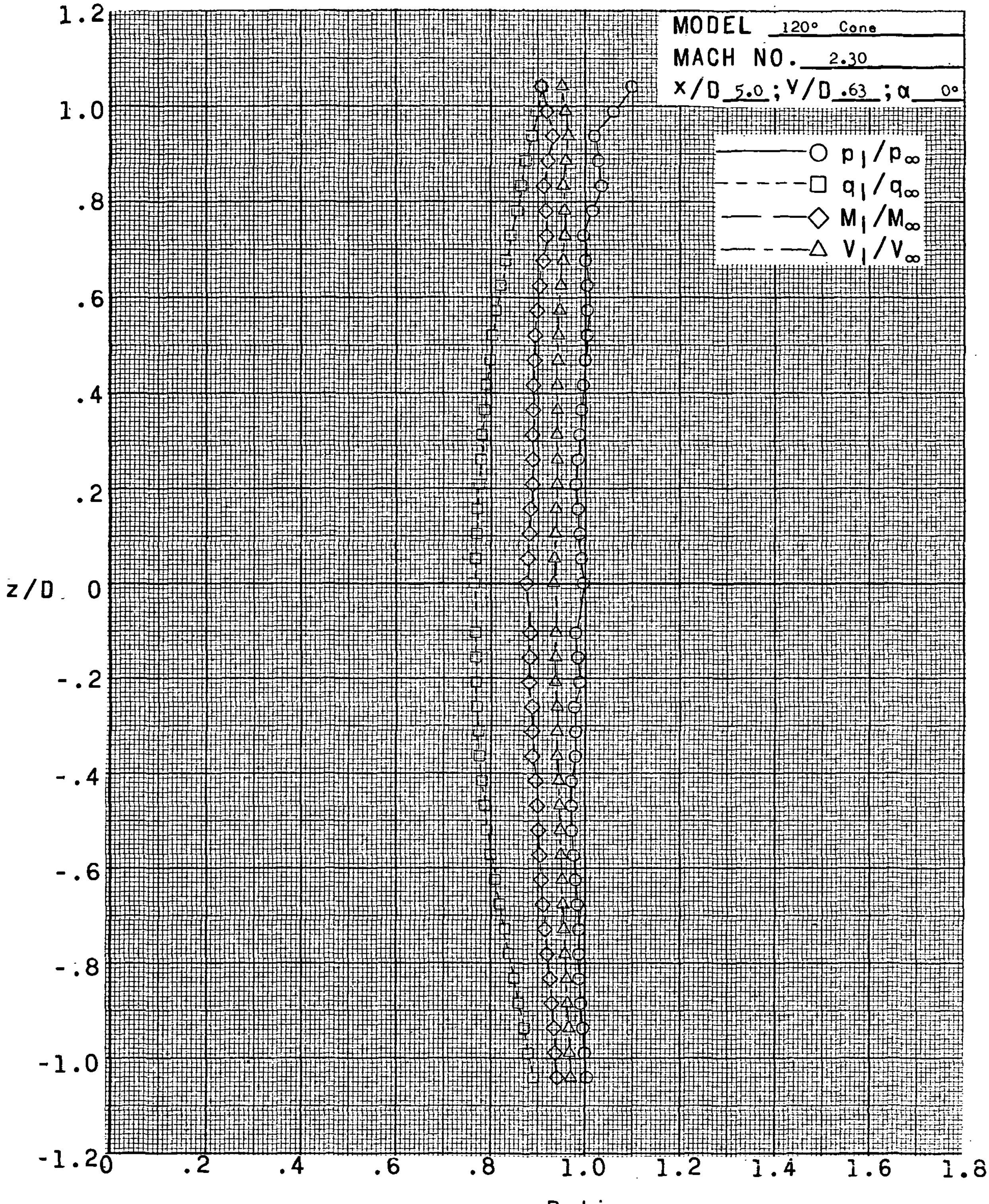
(s) x/D = 5.0; y/D = 1.0; α = 0°.

Figure 6.- Continued.



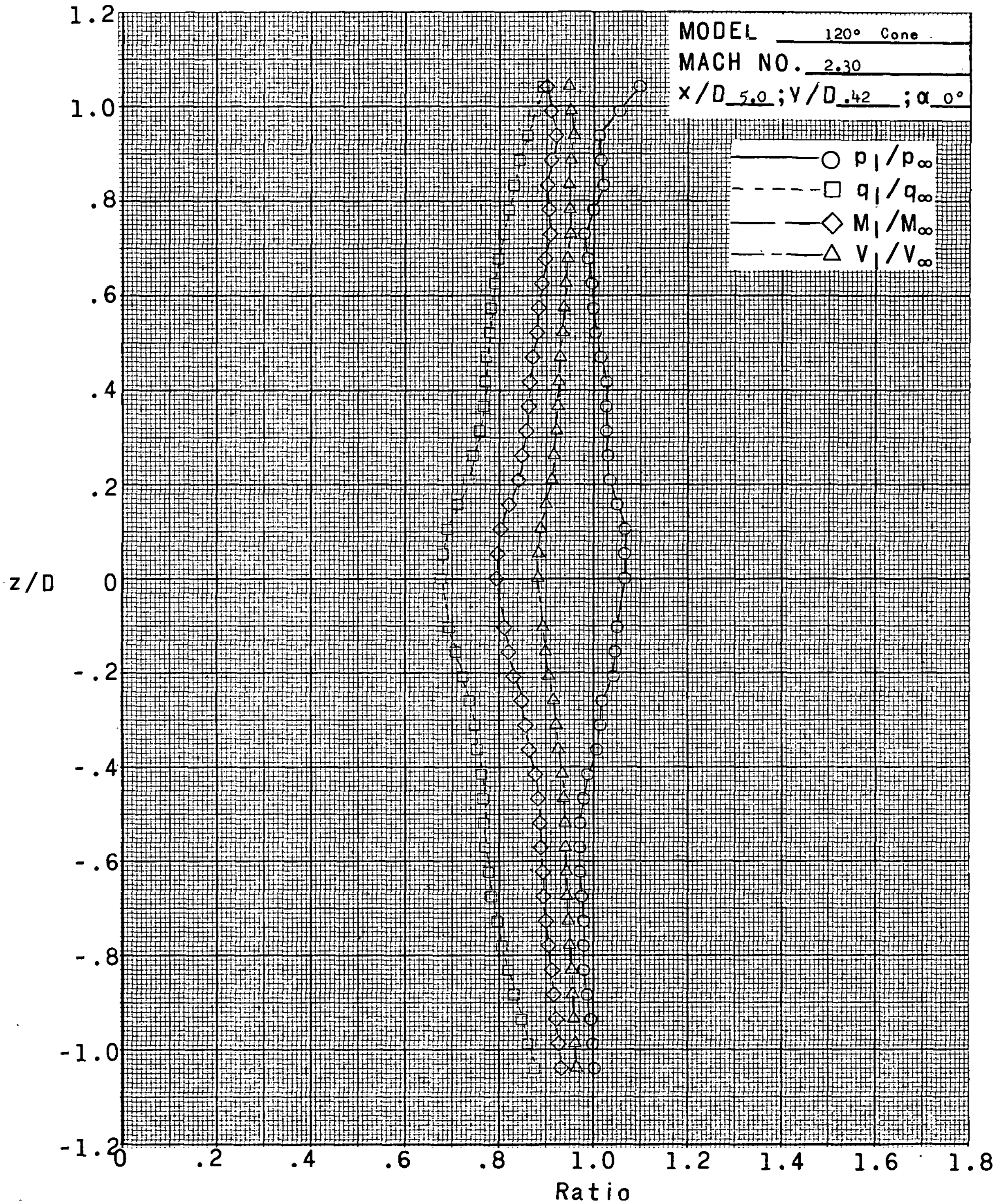
(t) x/D = 5.0; y/D = 0.83; α = 0°.

Figure 6.- Continued.



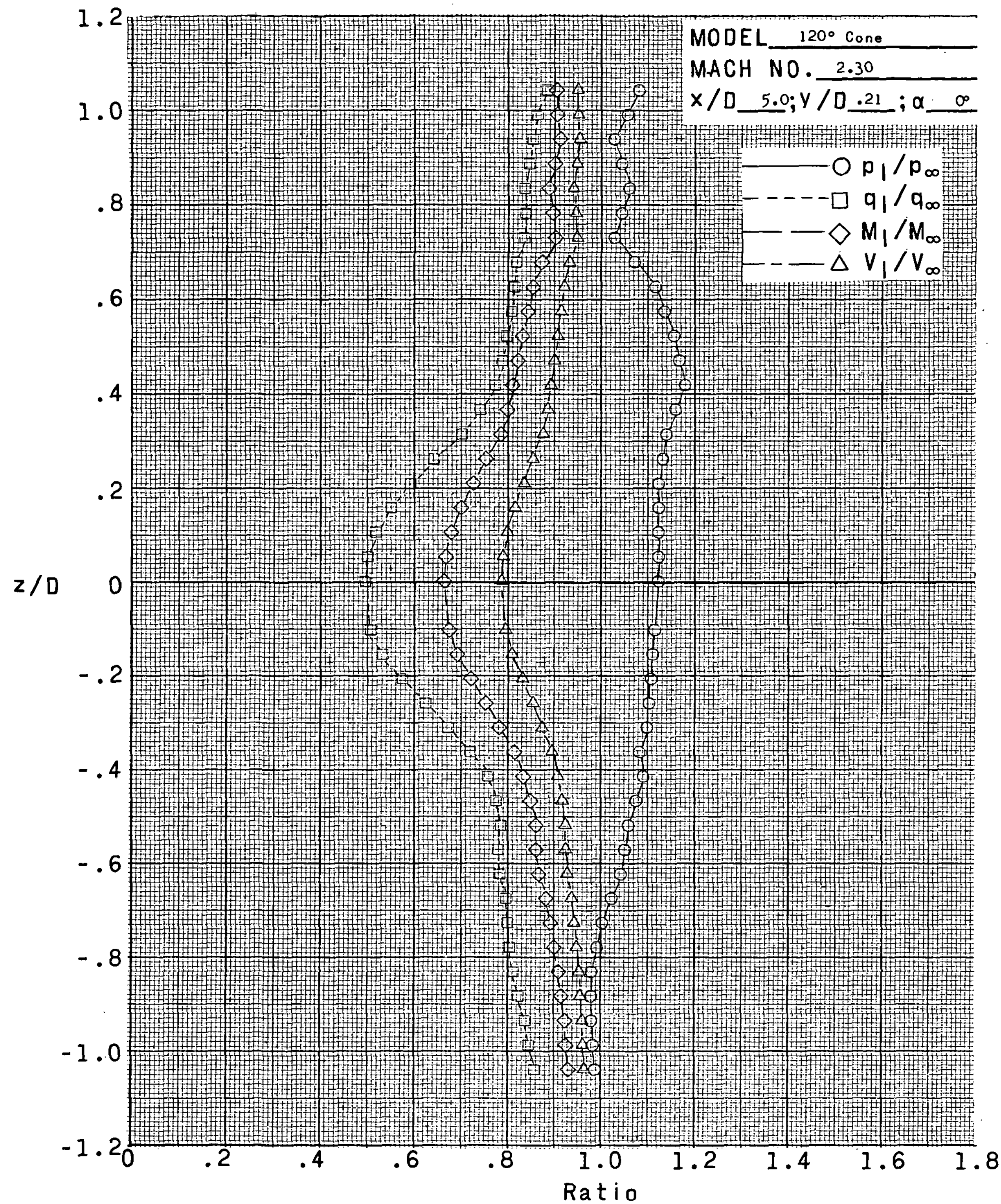
(u) $x/D = 5.0$; $y/D = 0.63$; $\alpha = 0^0$.

Figure 6.- Continued.



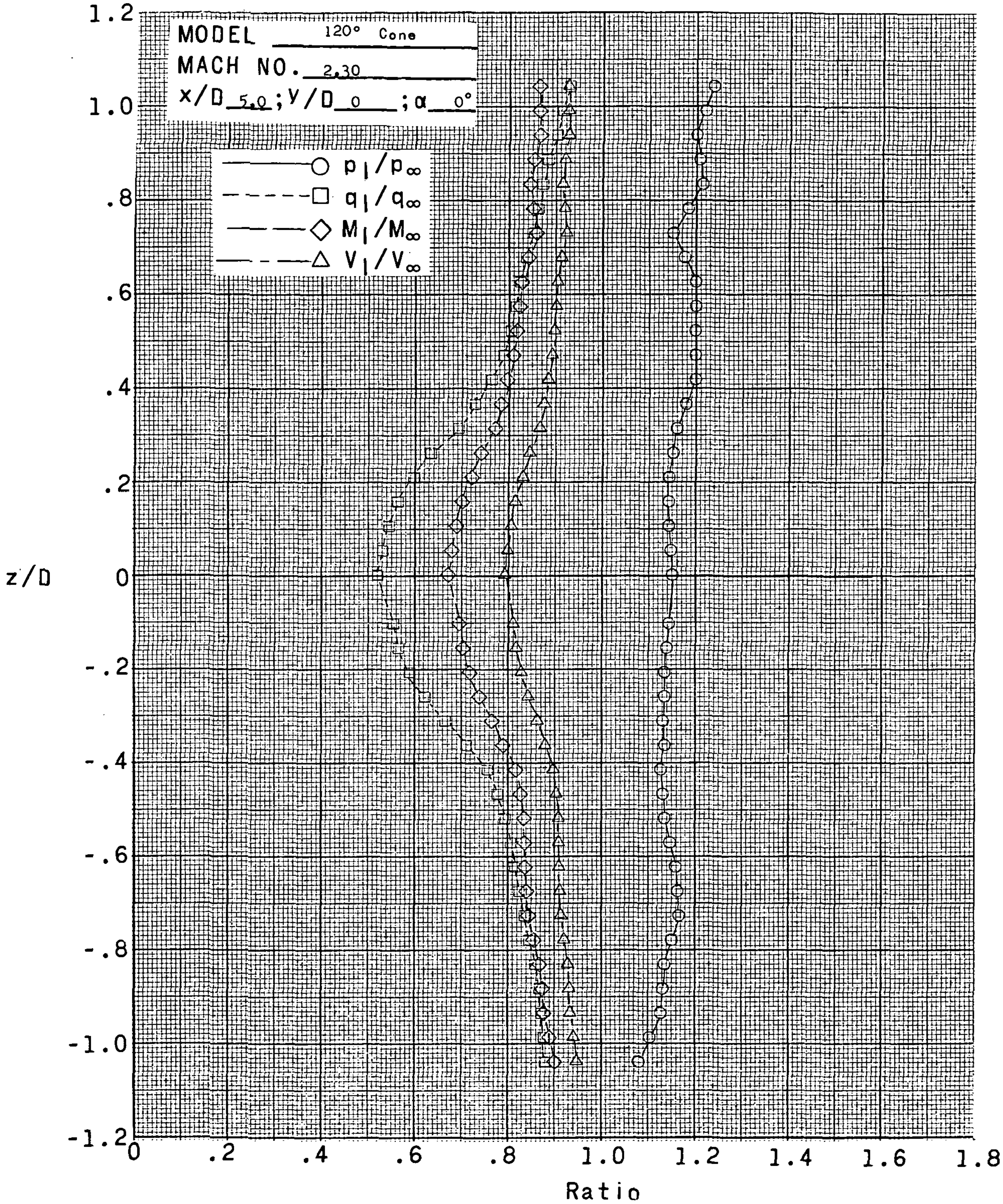
(v) $x/D = 5.0$; $y/D = 0.42$; $\alpha = 0^{0}$.

Figure 6.- Continued.



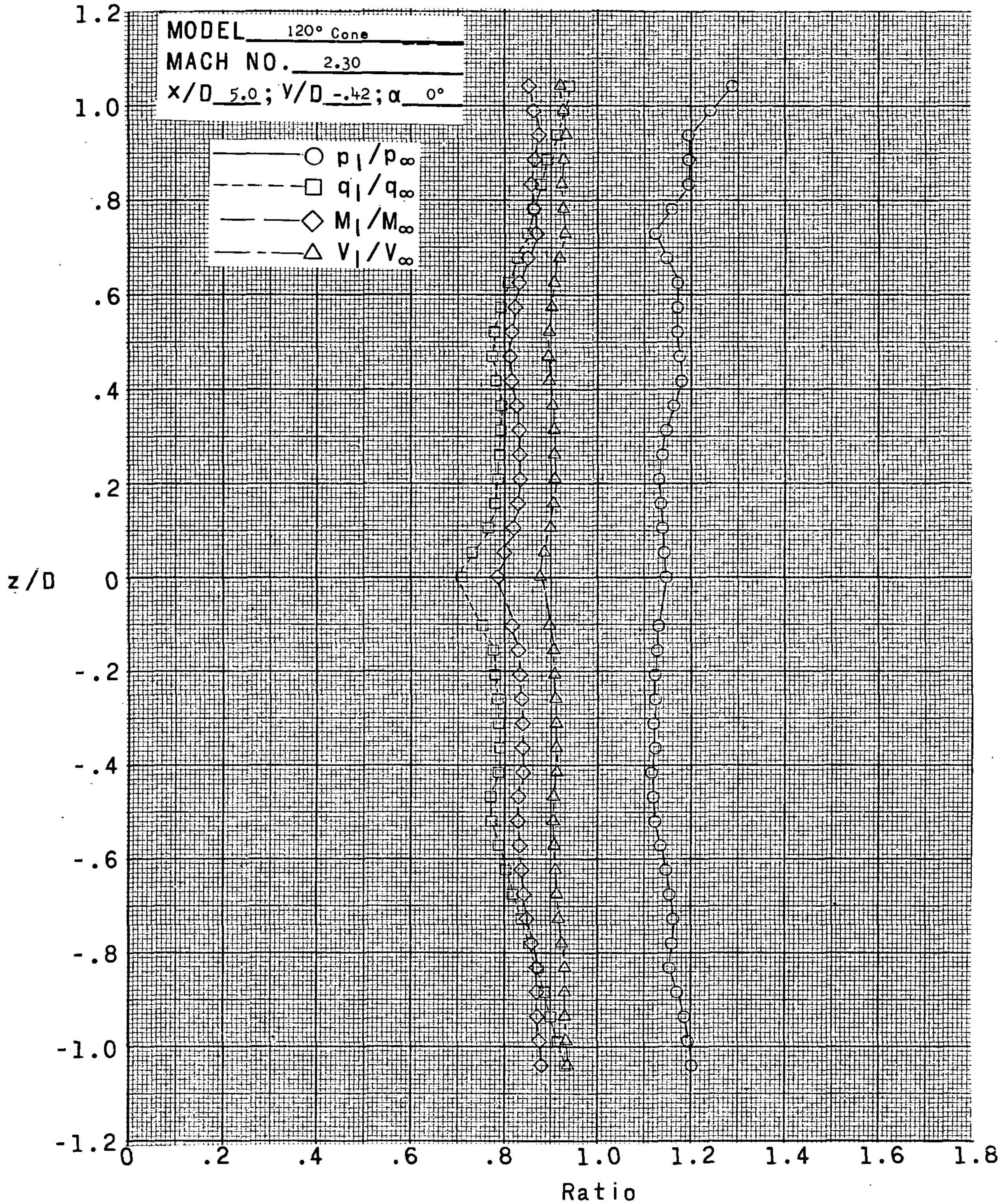
(w) x/D = 5.0; y/D = 0.21; α = 0°.

Figure 6.- Continued.



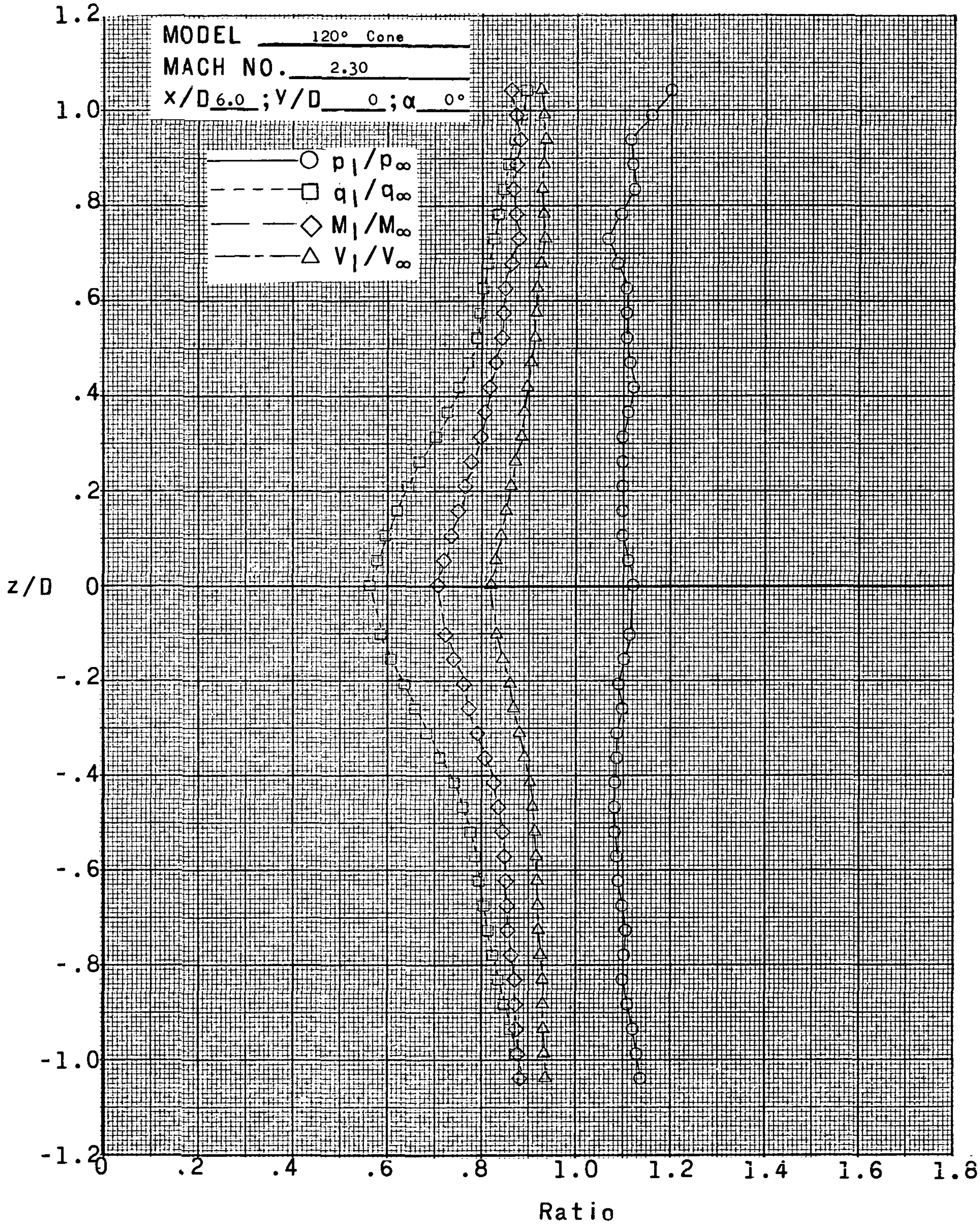
(x) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 6.- Continued.



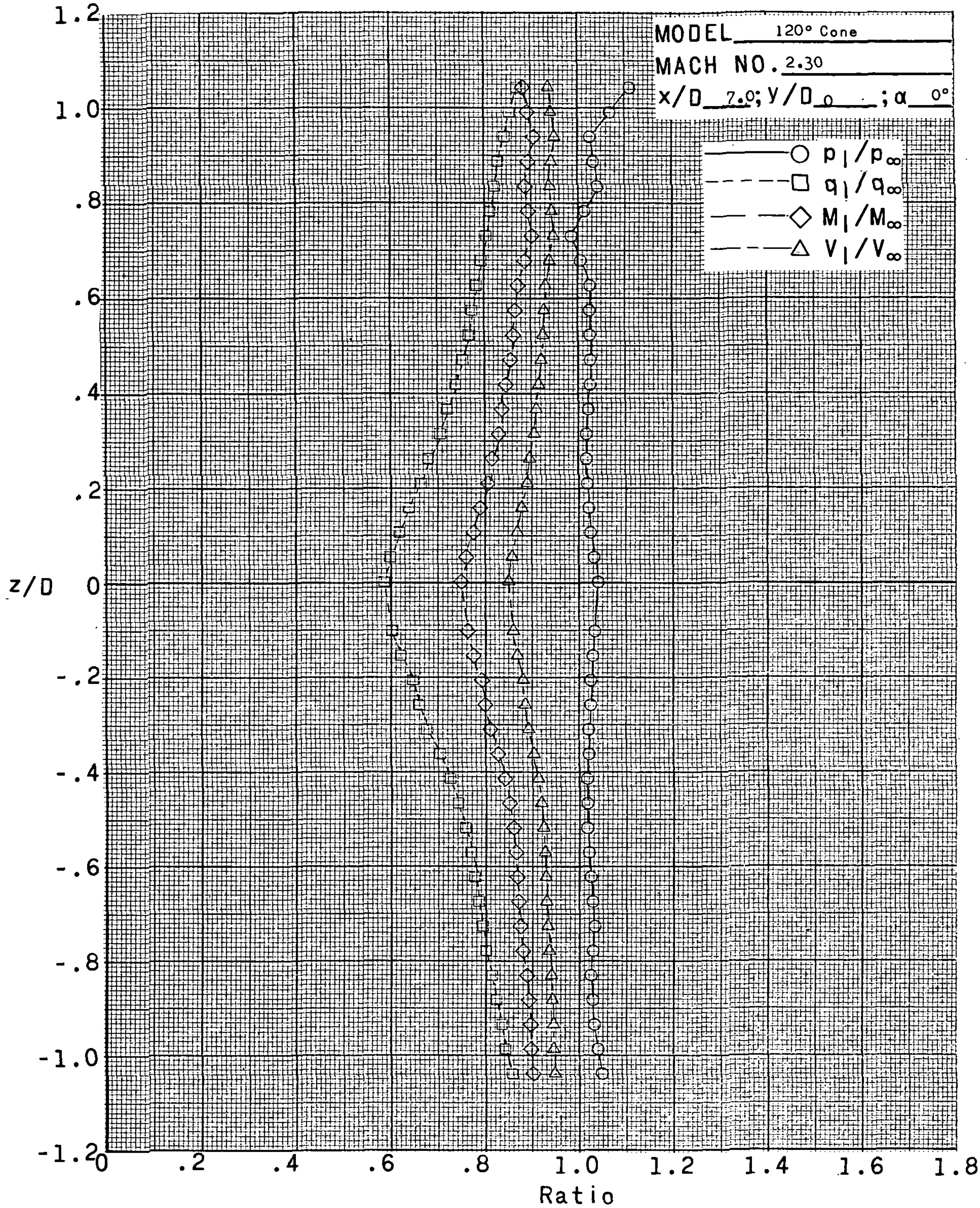
(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^0$.

Figure 6.- Continued.



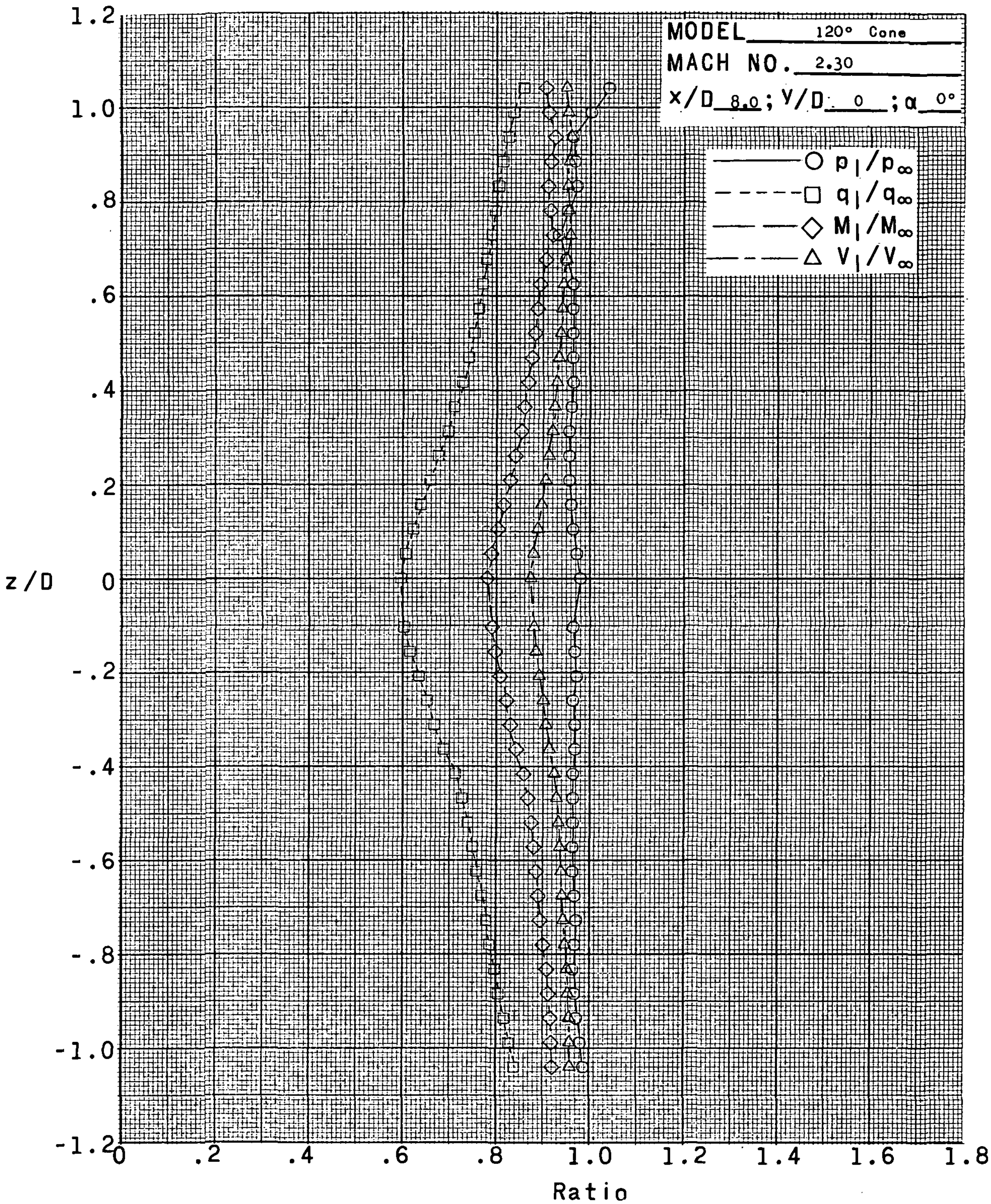
(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^o$.

Figure 6.- Continued.



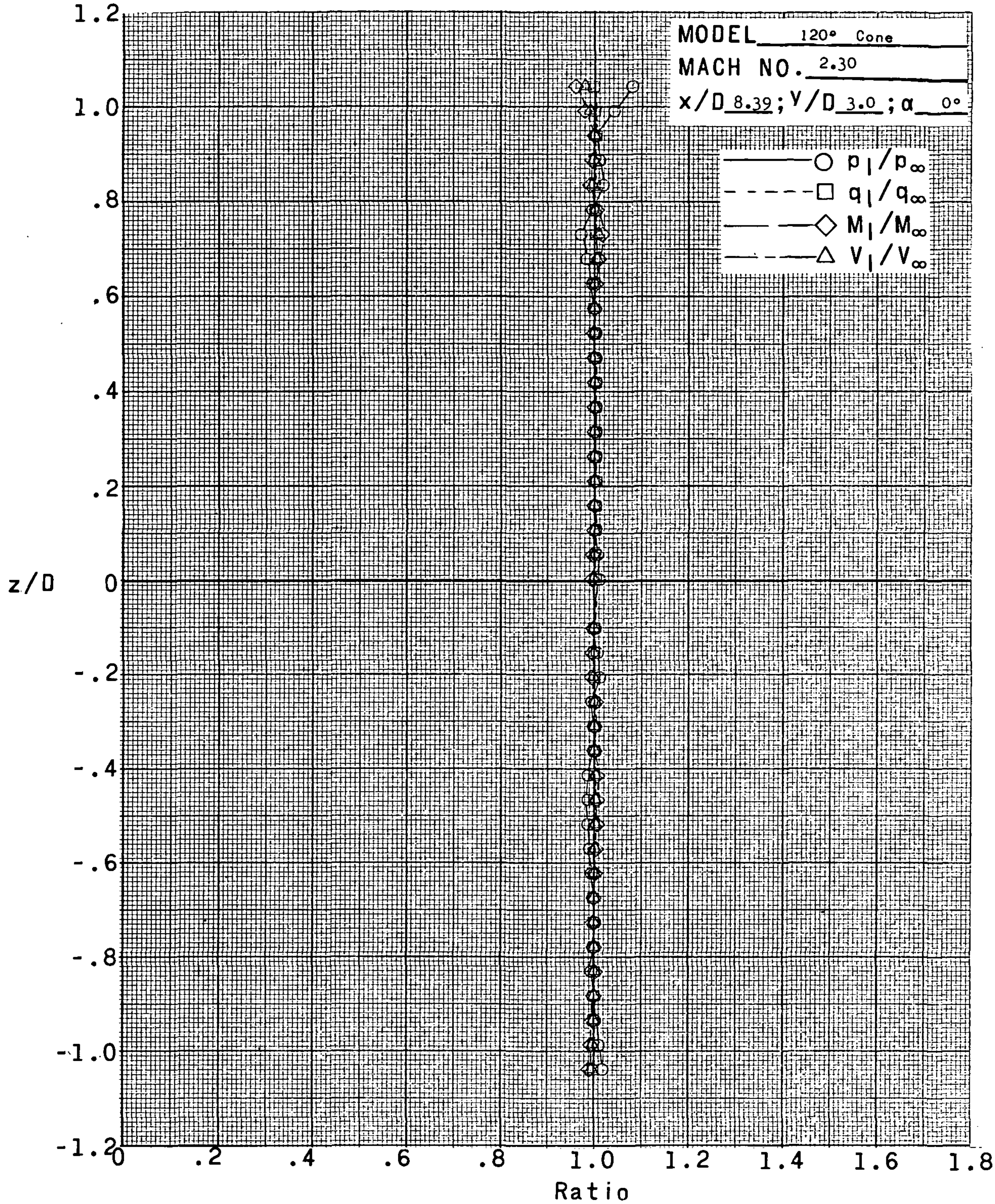
(aa) x/D = 7.0; y/D = 0; α = 0°.

Figure 6.- Continued.



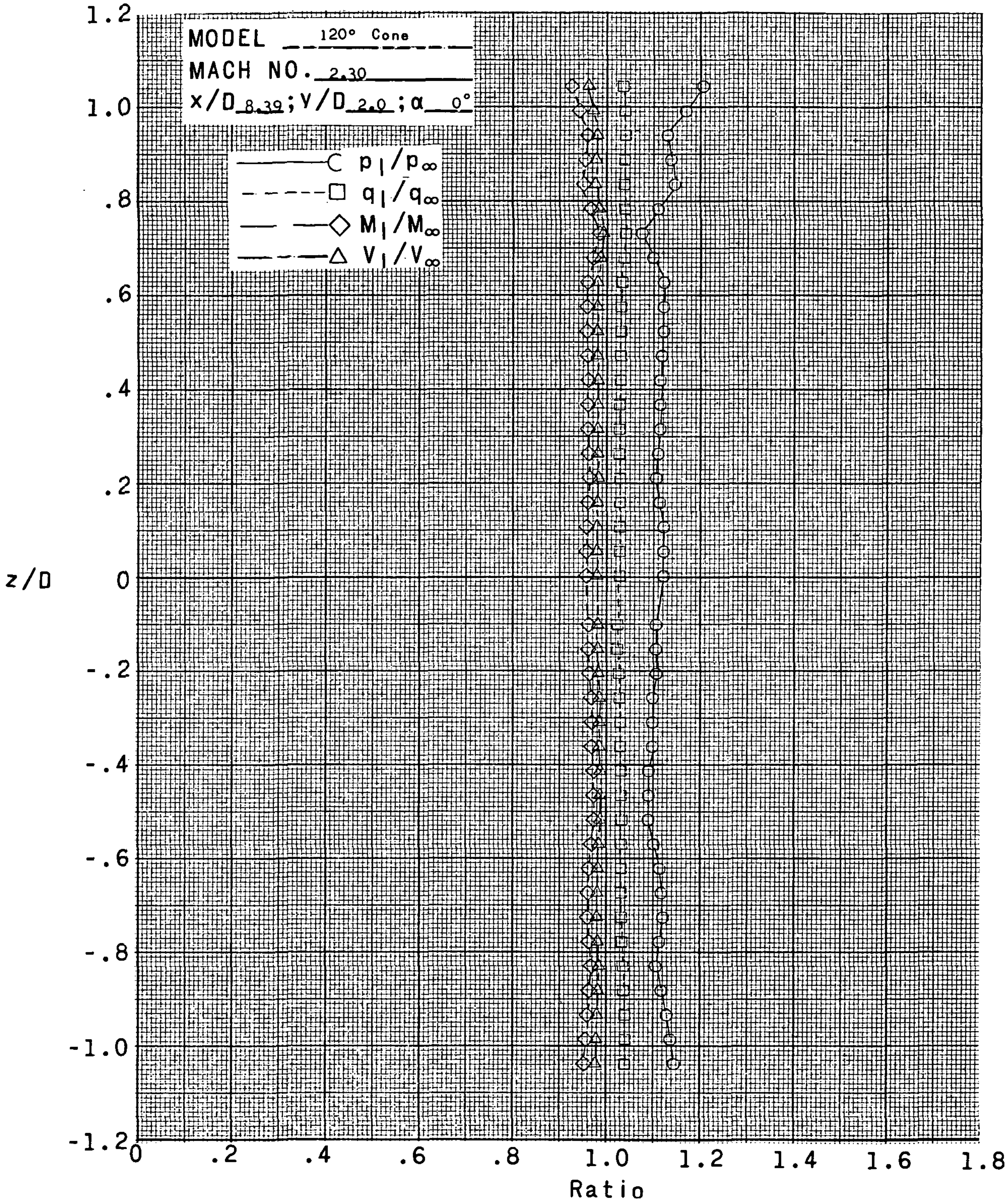
(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^{o}$.

Figure 6.- Continued.



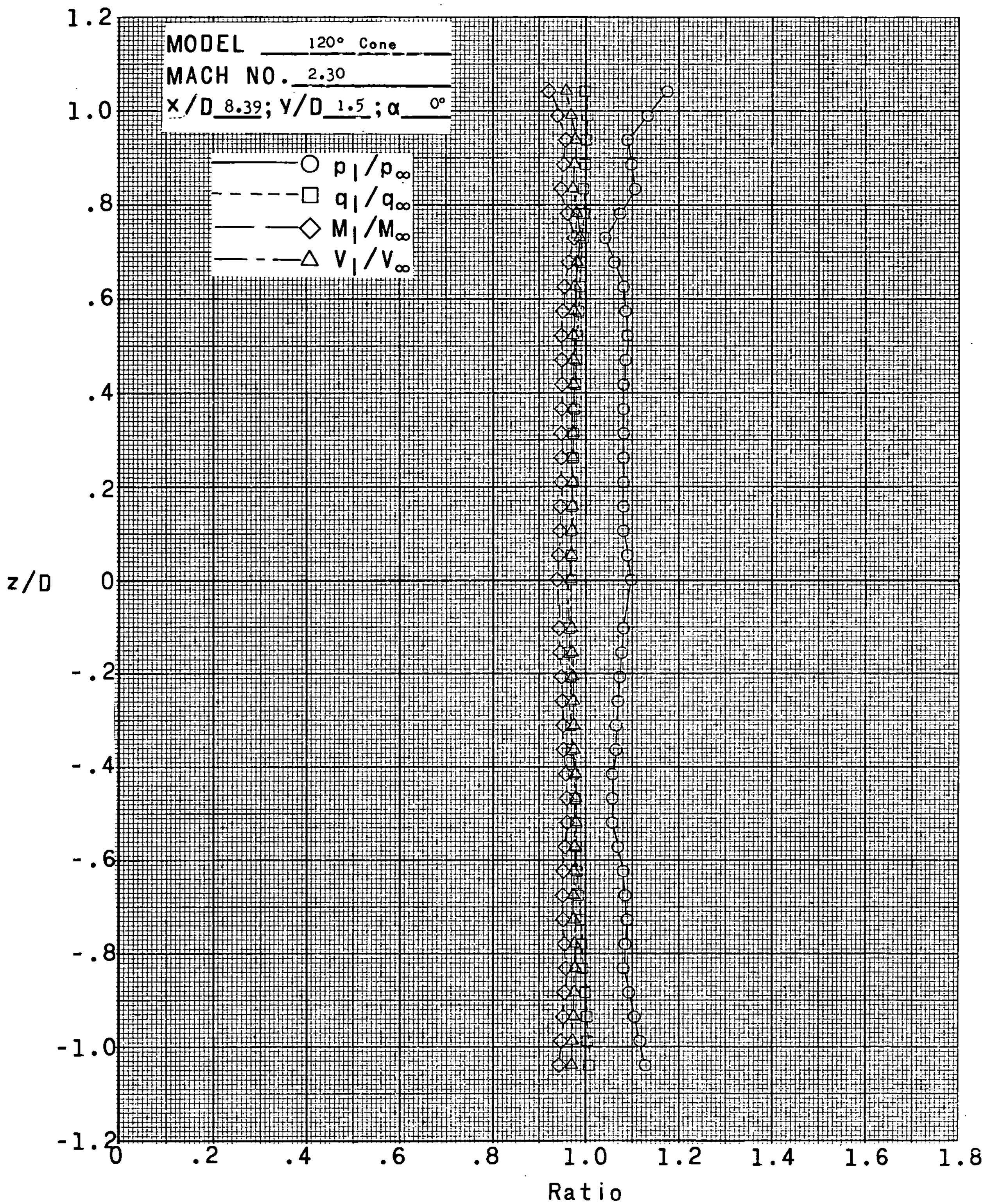
(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^o$.

Figure 6.- Continued.



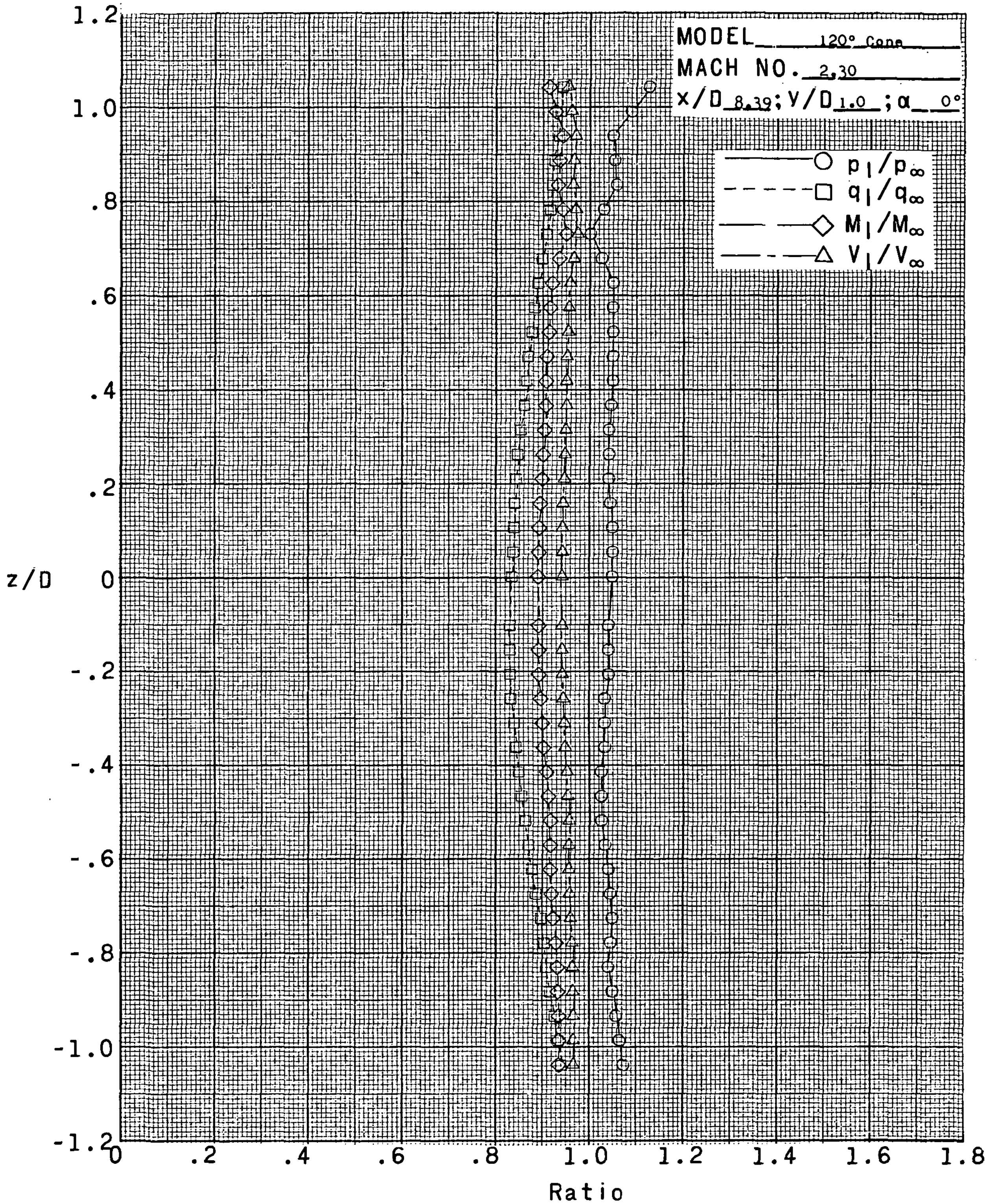
(dd) x/D = 8.39; y/D = 2.0; α = 0°.

Figure 6.- Continued.



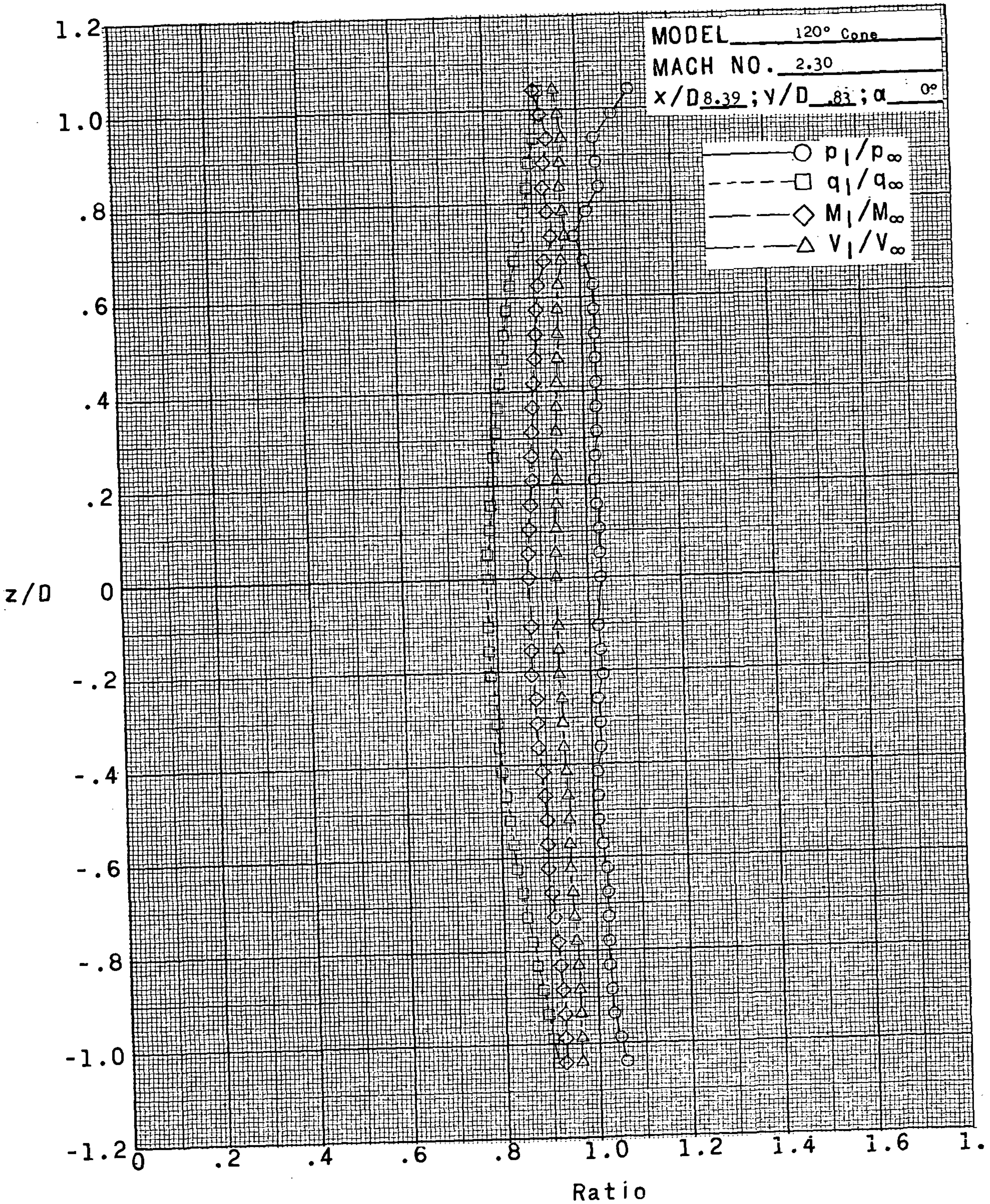
(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^0$.

Figure 6.- Continued.



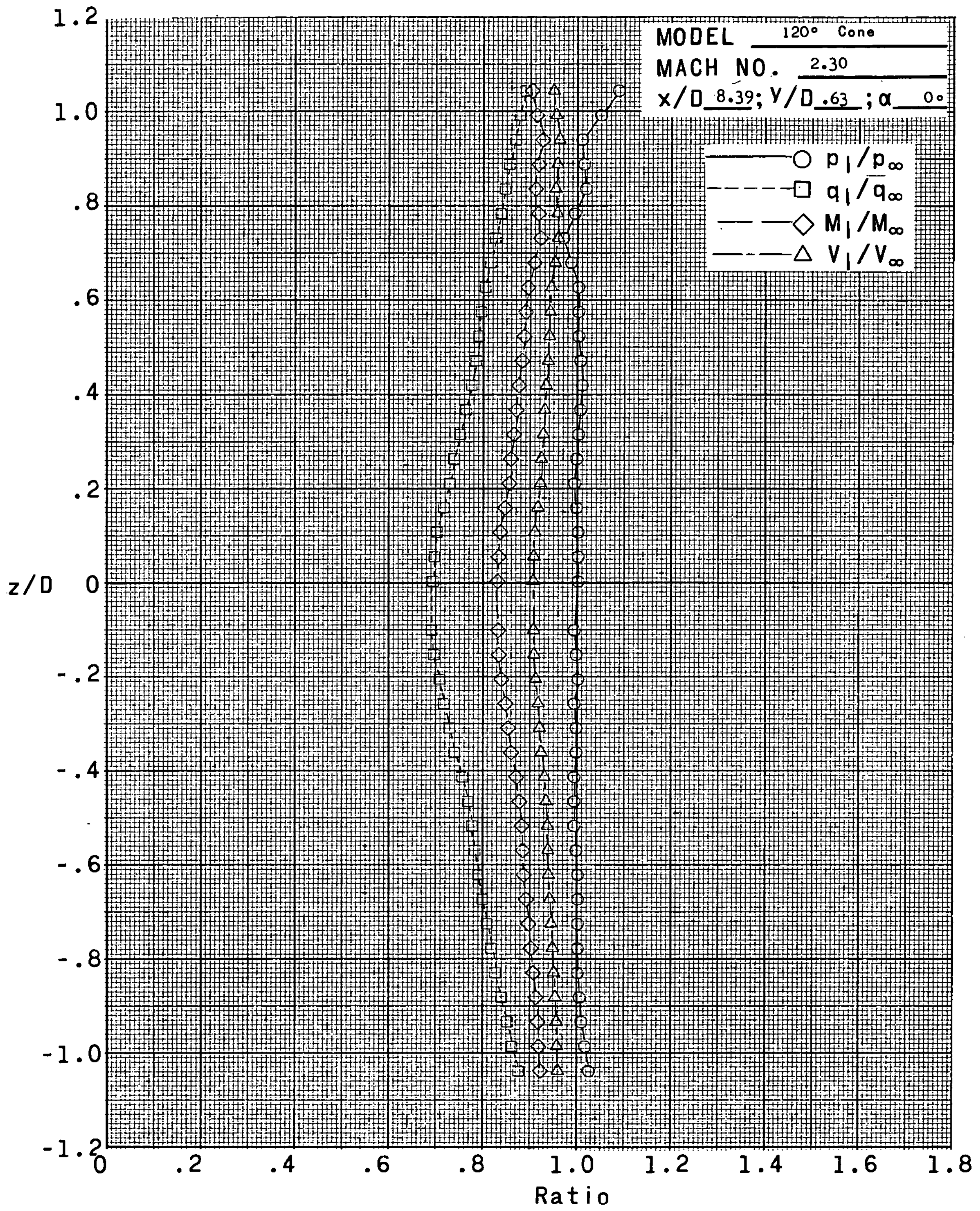
(ff) $x/D = 8.39$; $y/D = 1.0$; $\alpha = 0^{\circ}$.

Figure 6.- Continued.



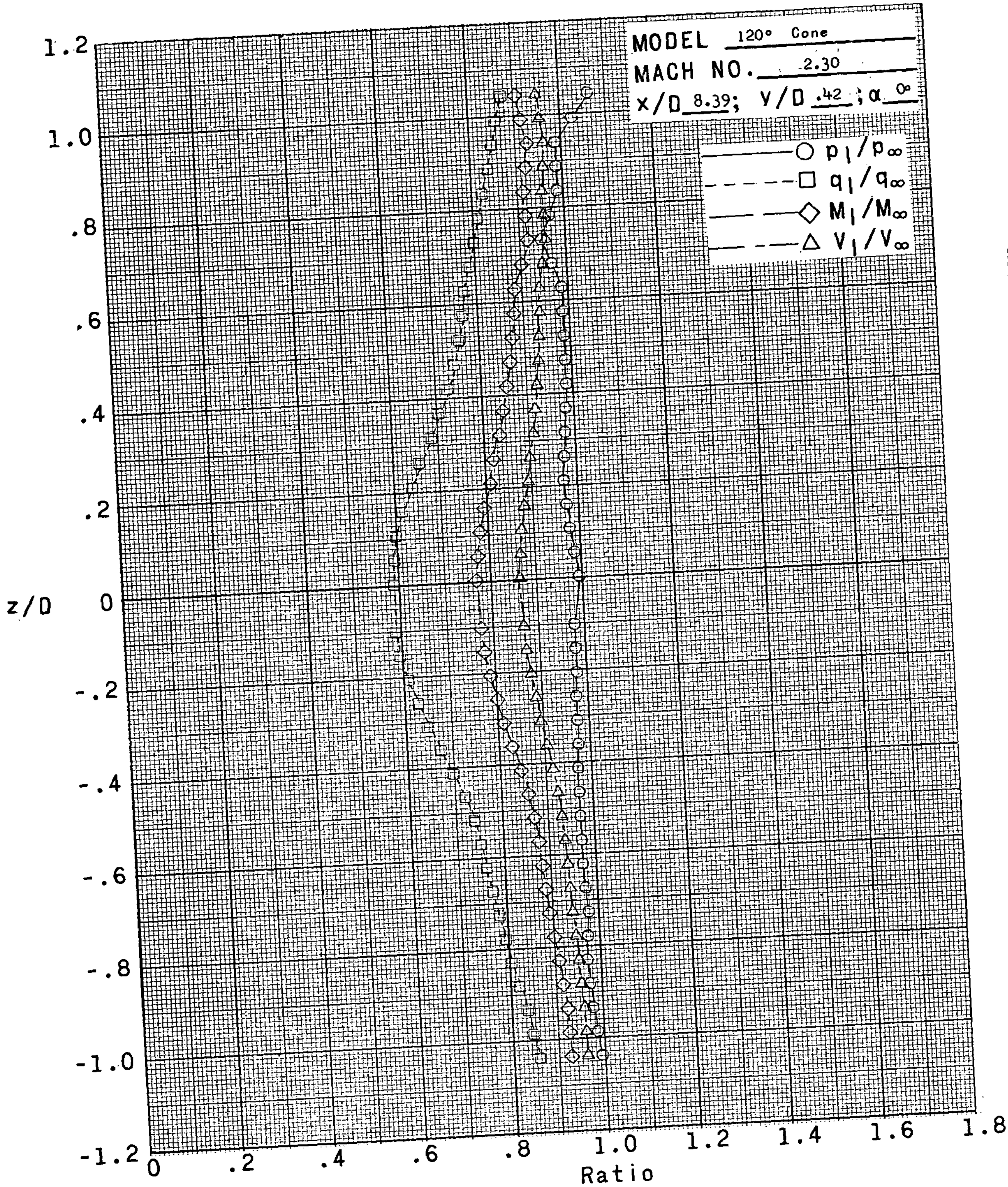
(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 6.- Continued.



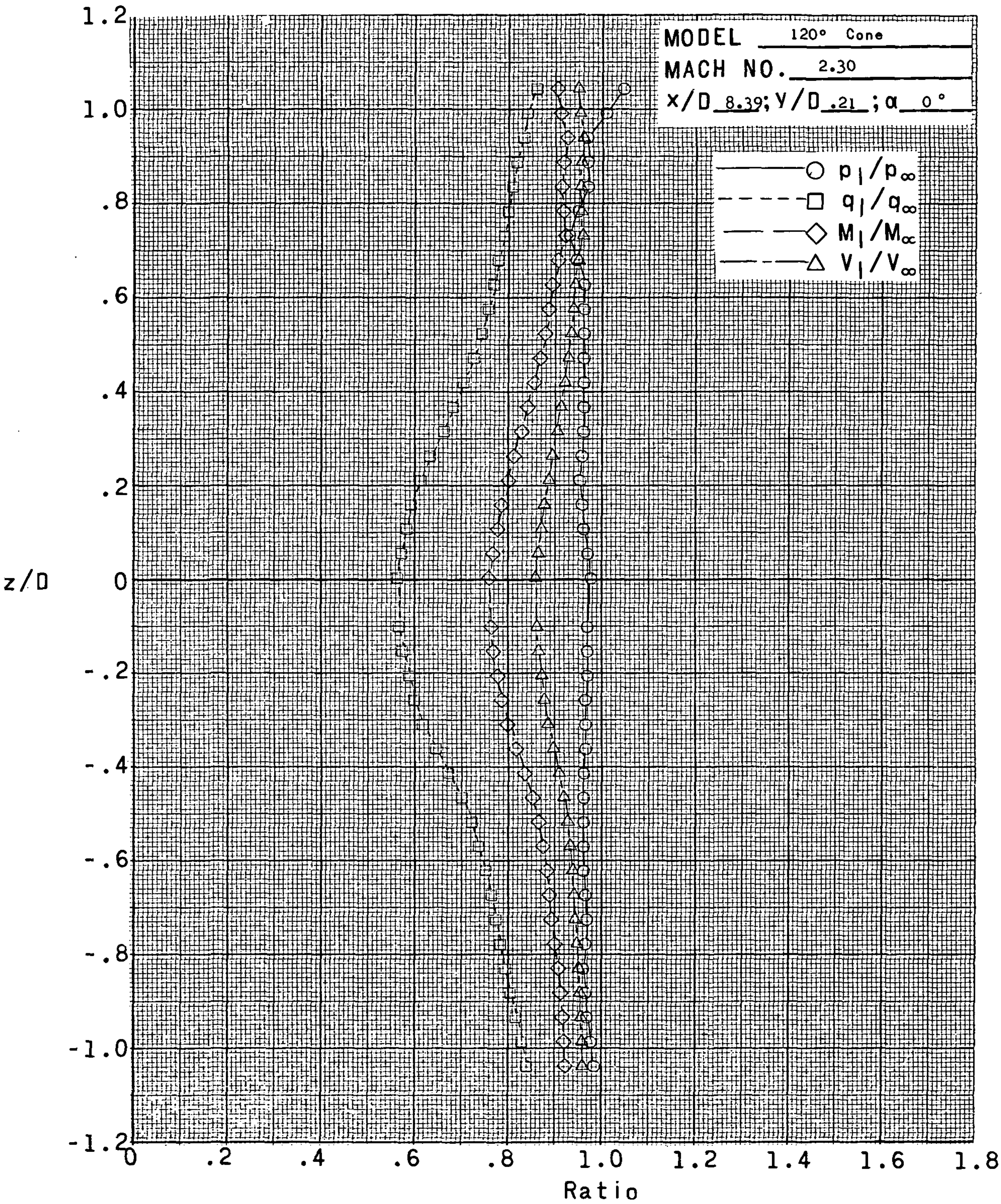
(hh) x/D = 8.39; y/D = 0.63; α = 0°.

Figure 6.- Continued.



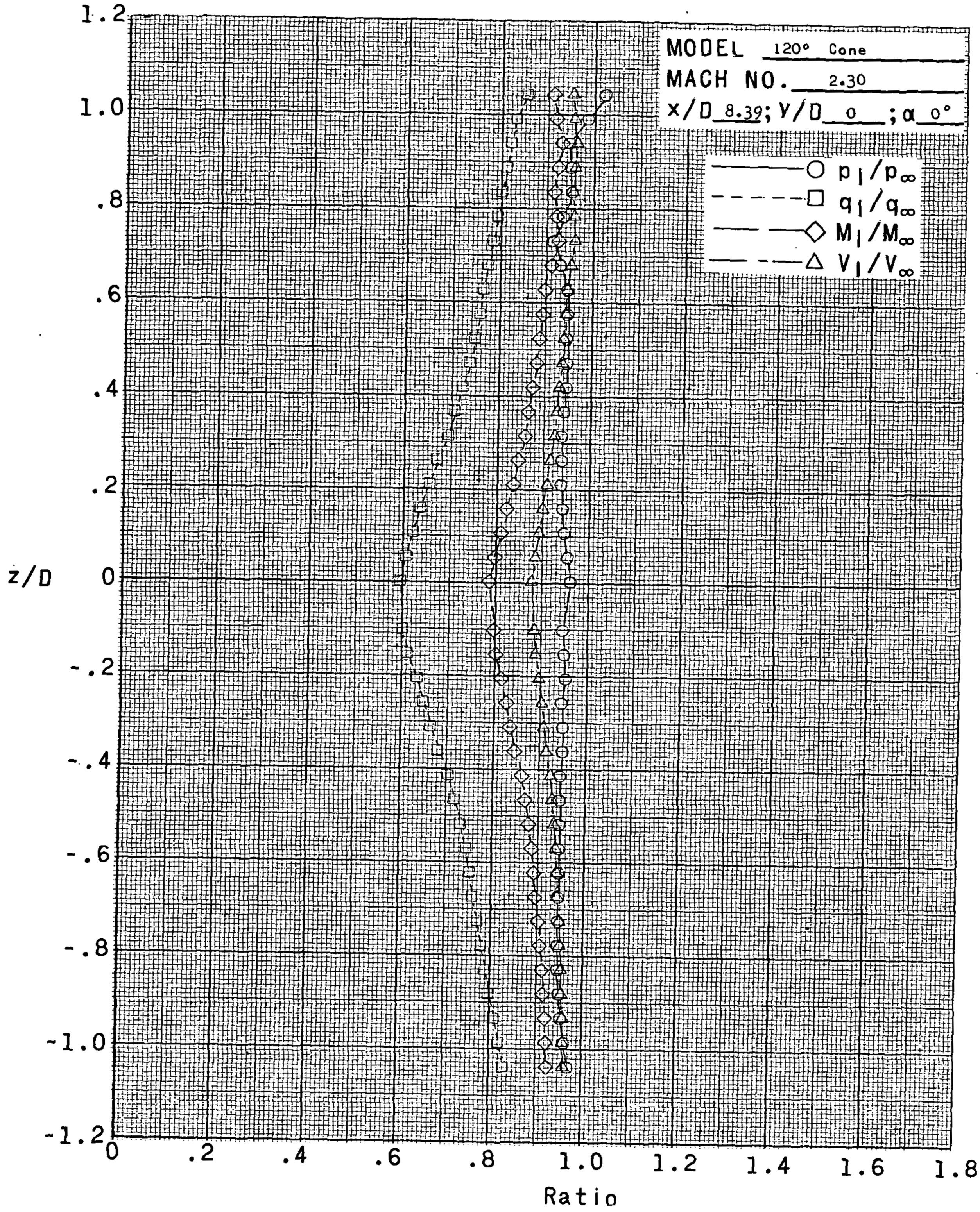
(ii) $x/D = 8.39$; $y/D = 0.42$; $\alpha = 0^{0}$.

Figure 6.- Continued.



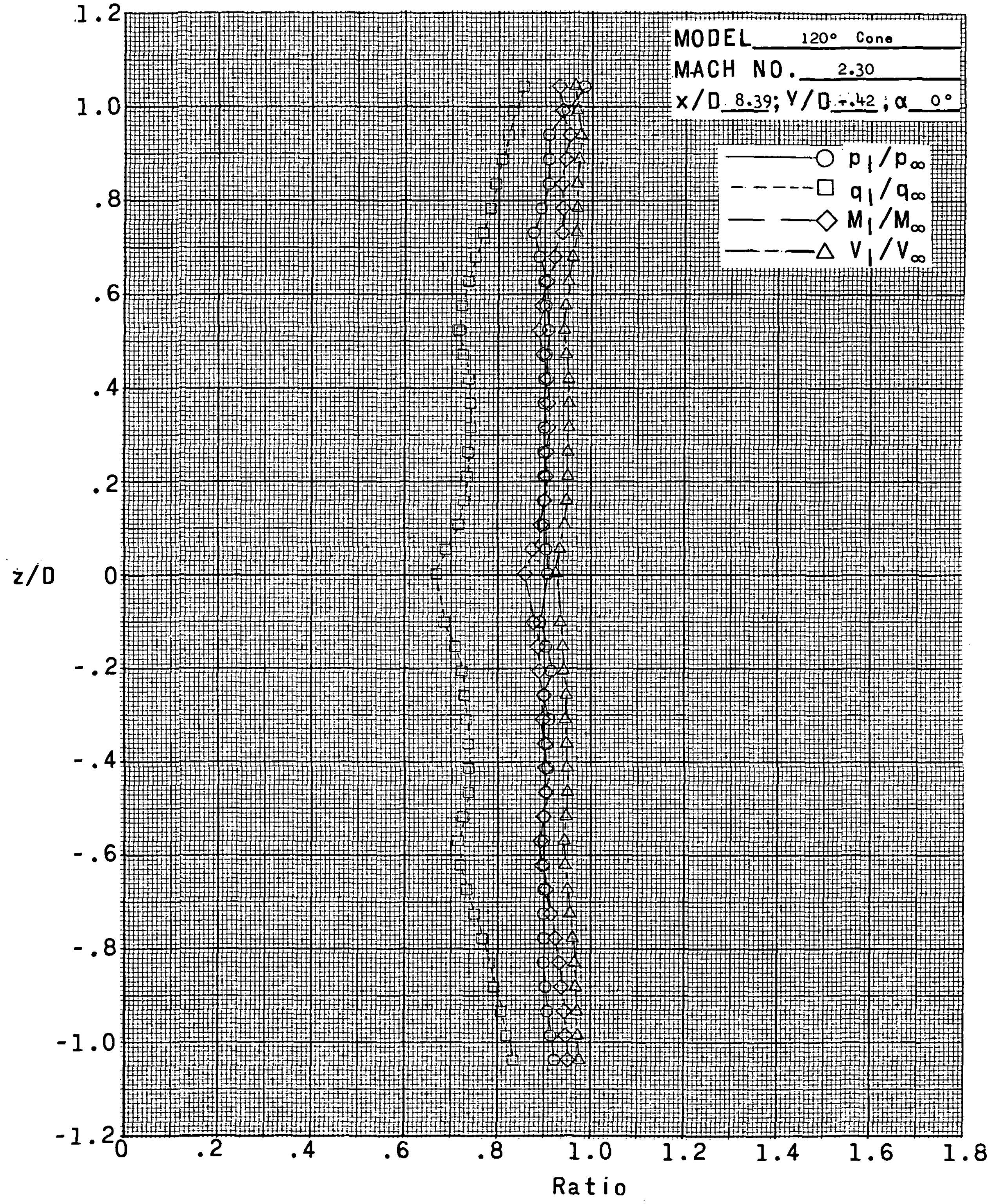
(jj) $x/D = 8.39$; $y/D = 0.21$; $\alpha = 0^{0}$.

Figure 6.- Continued.



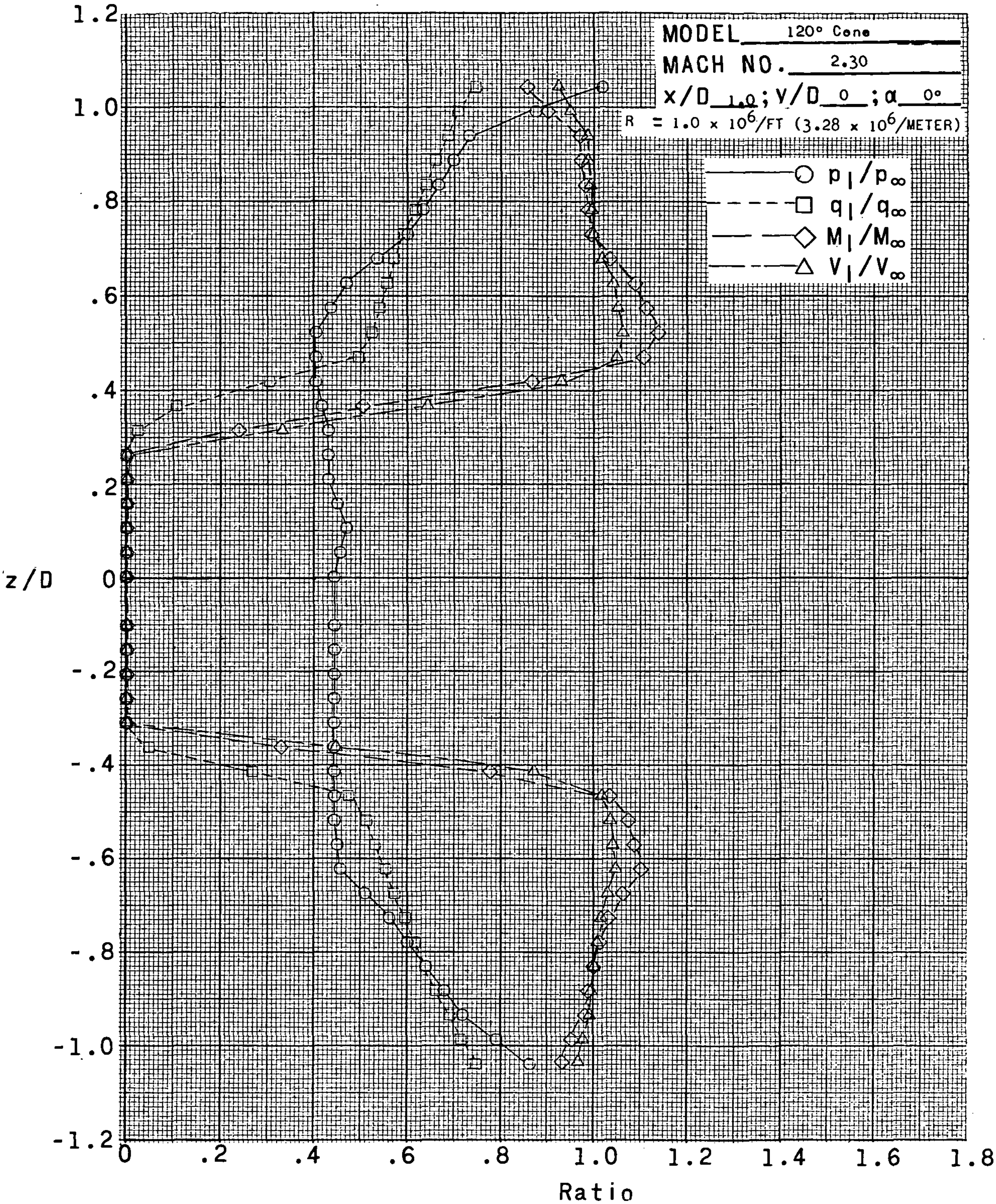
(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^o$.

Figure 6.- Continued.



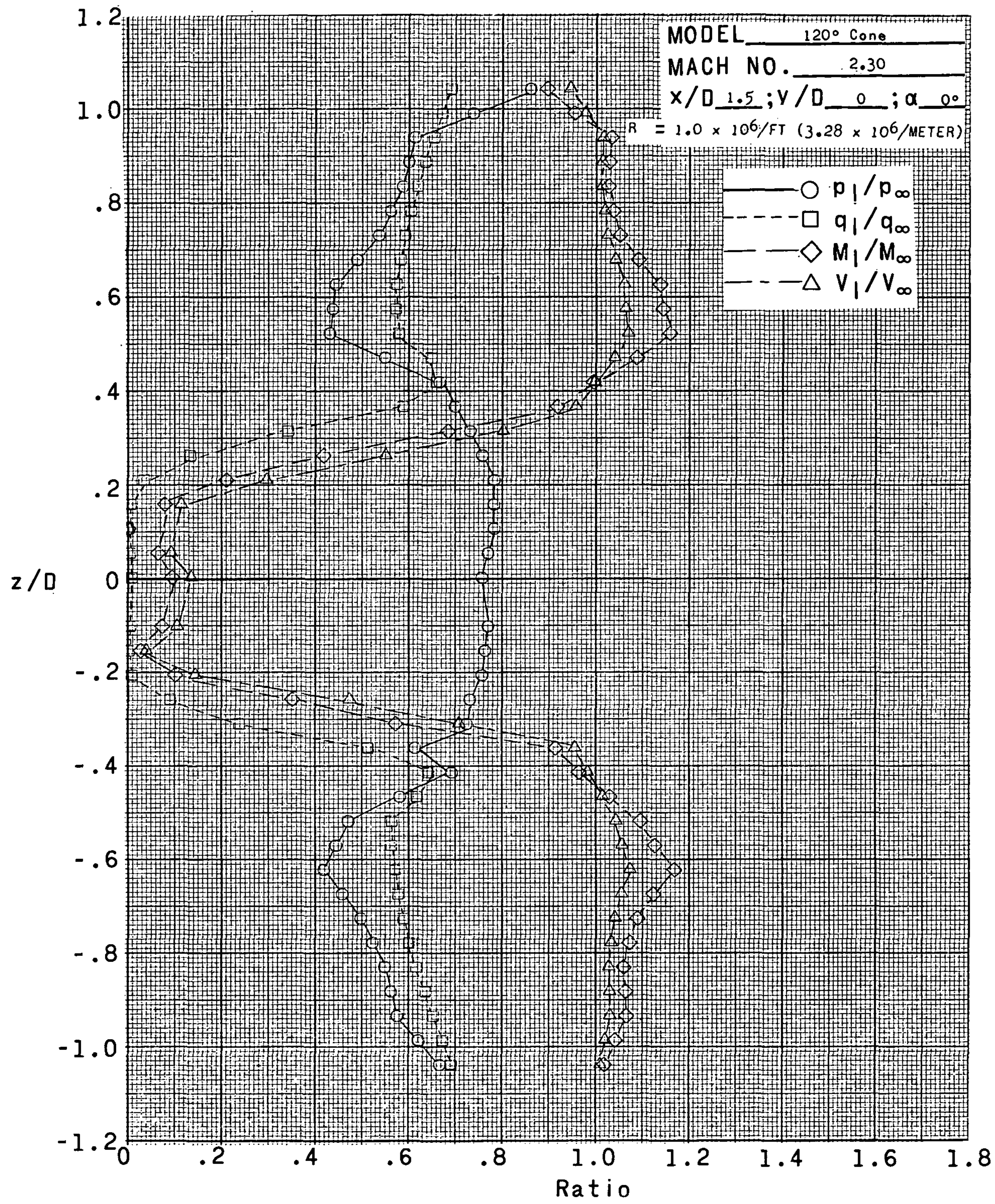
(II) x/D = 8.39; y/D = -0.42; α = 0°.

Figure 6.- Concluded.



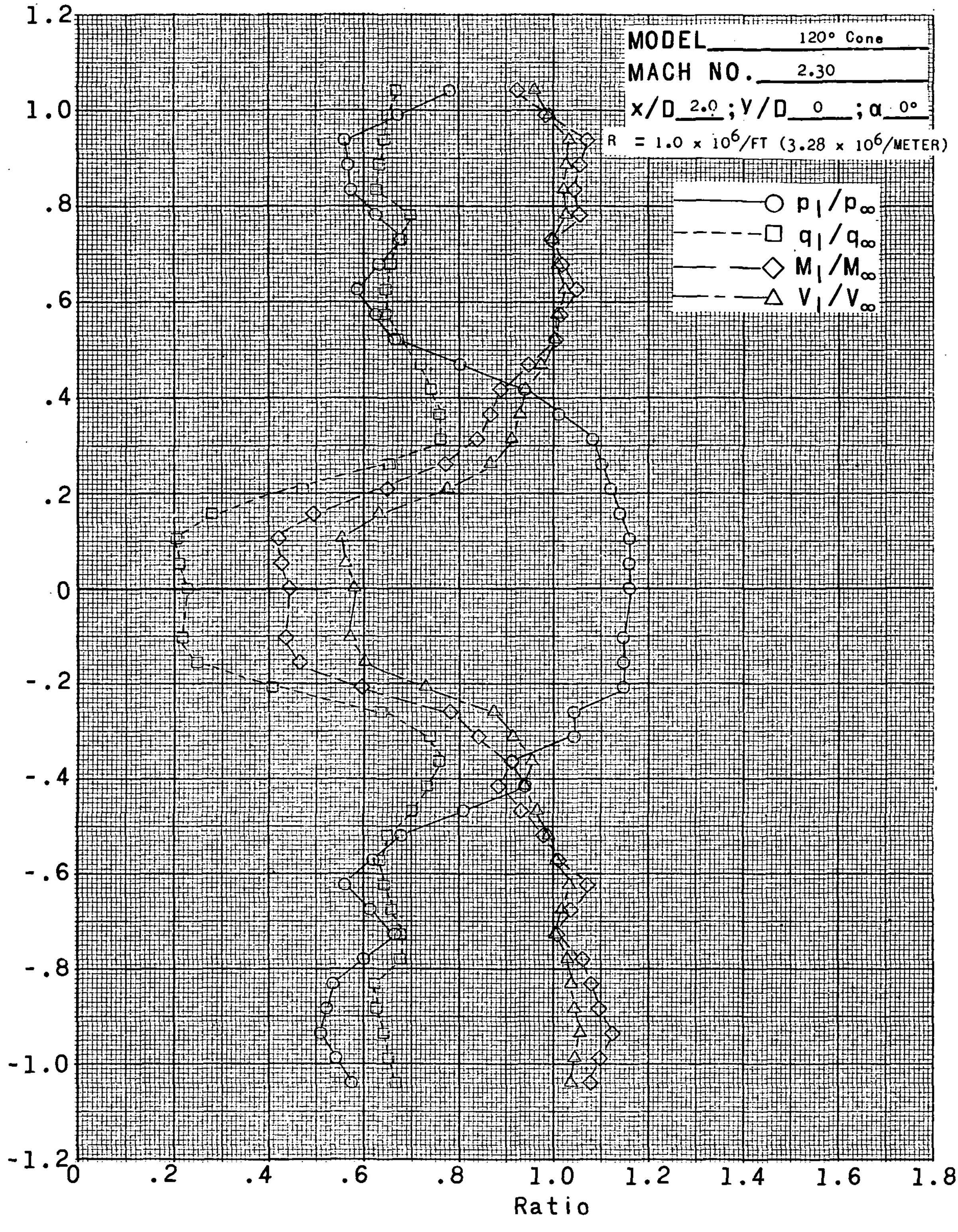
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 7.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in the wake of a 120°-included-angle cone at a Mach number of 2.30 and a Reynolds number of 1.0×10^6 per foot (3.28×10^6 per meter).



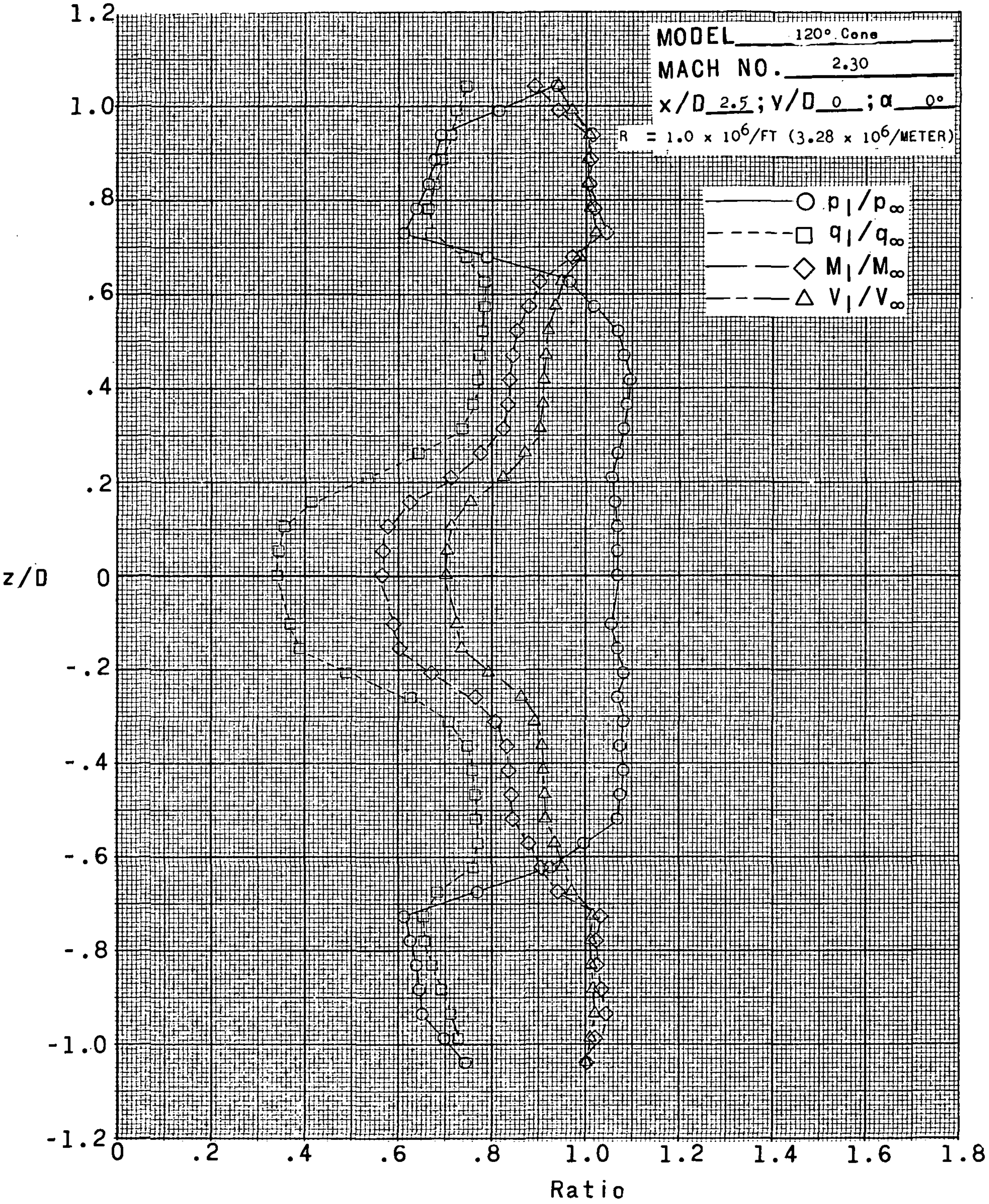
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 7.- Continued.



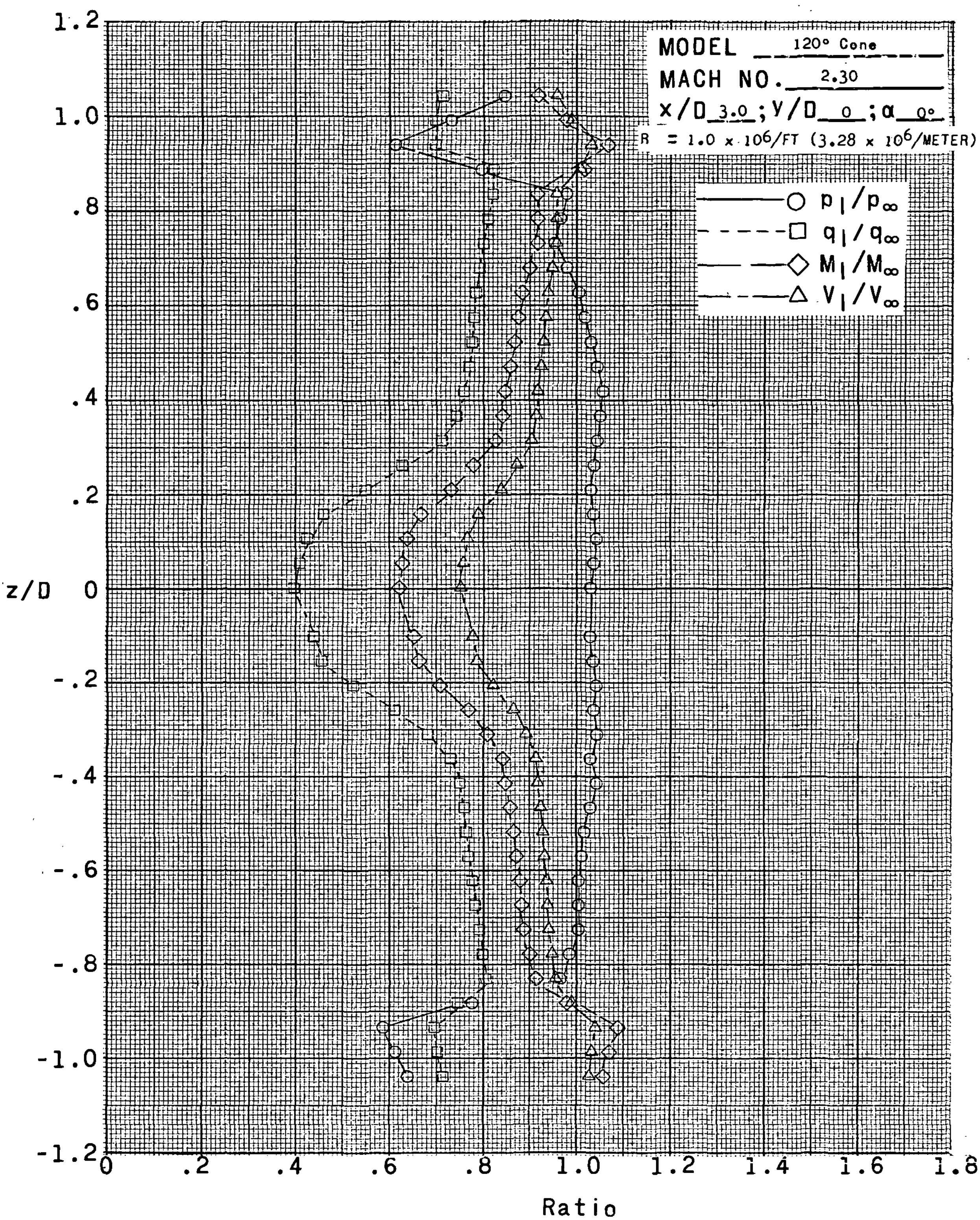
(c) x/D = 2.0; y/D = 0; α = 0°.

Figure 7.- Continued.



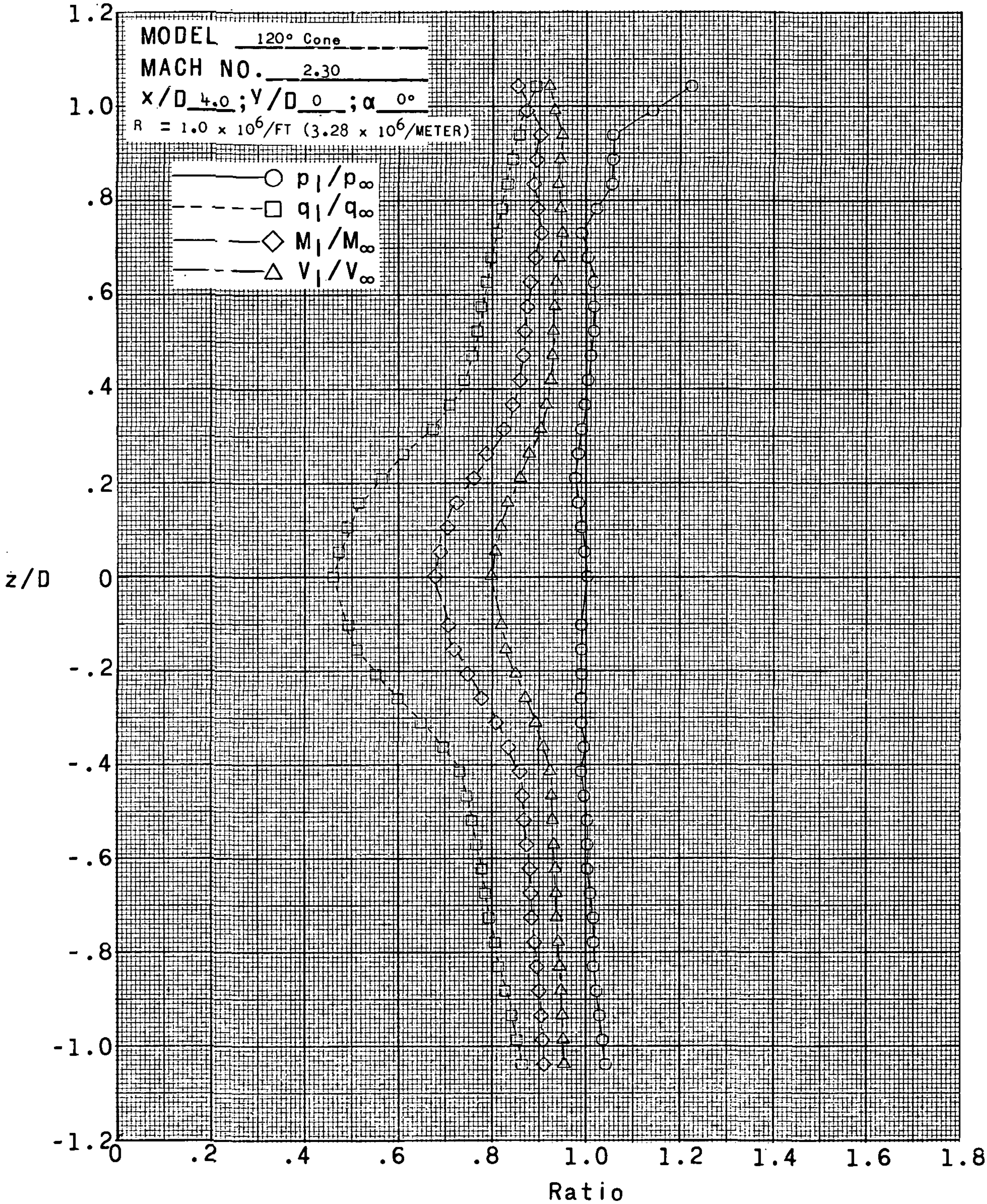
(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^{o}$.

Figure 7.- Continued.



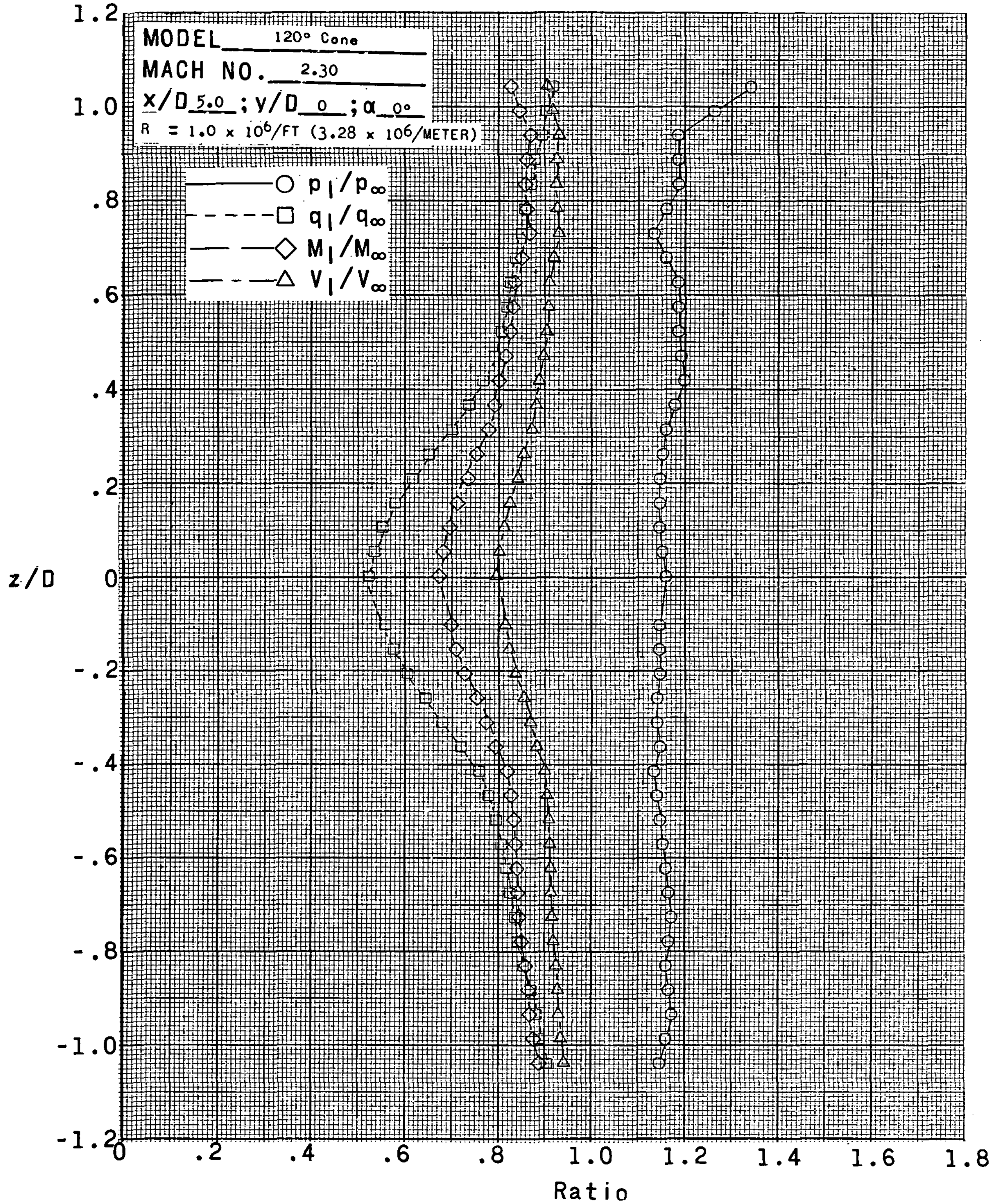
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 7.- Continued.



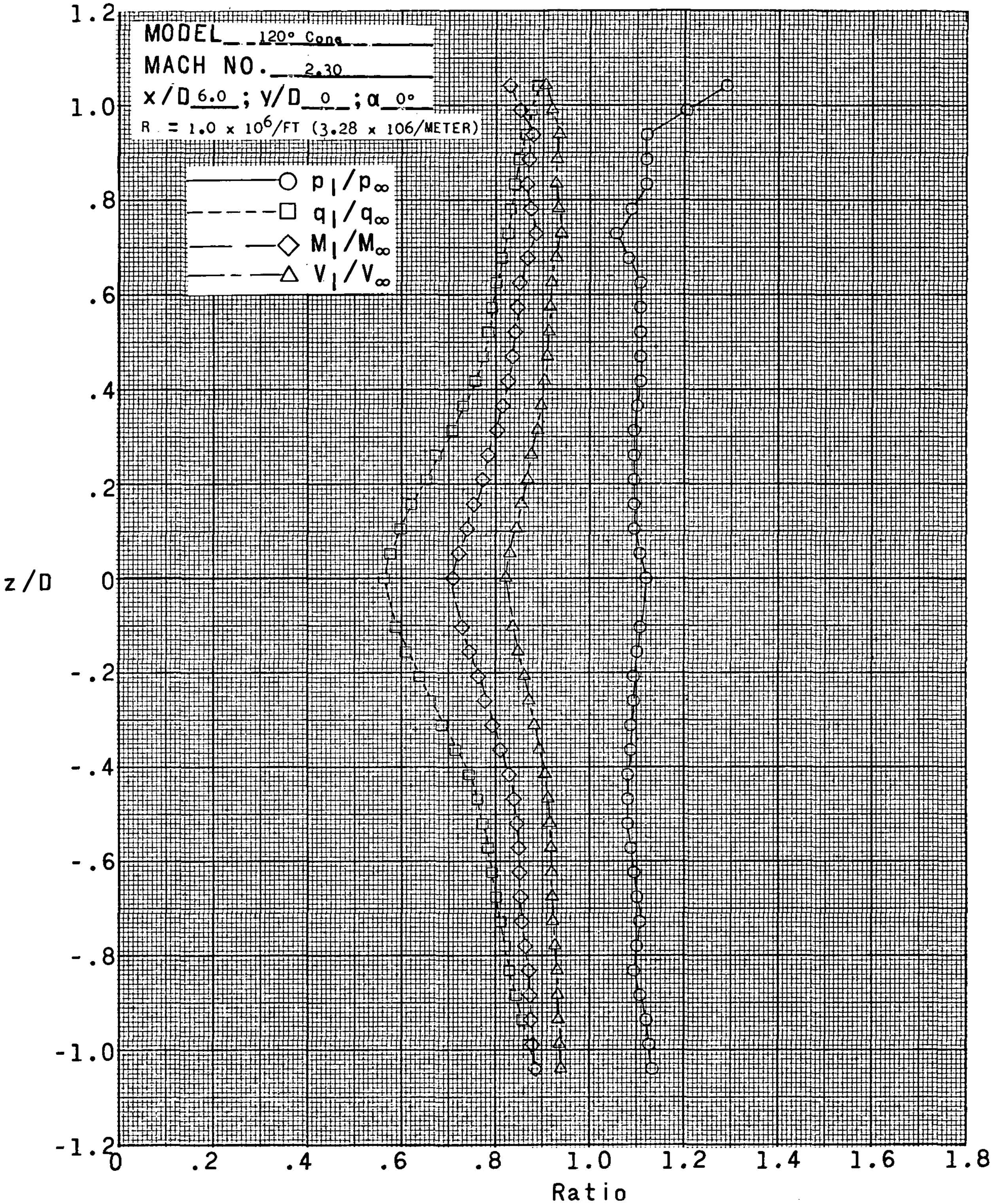
(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 7.- Continued.



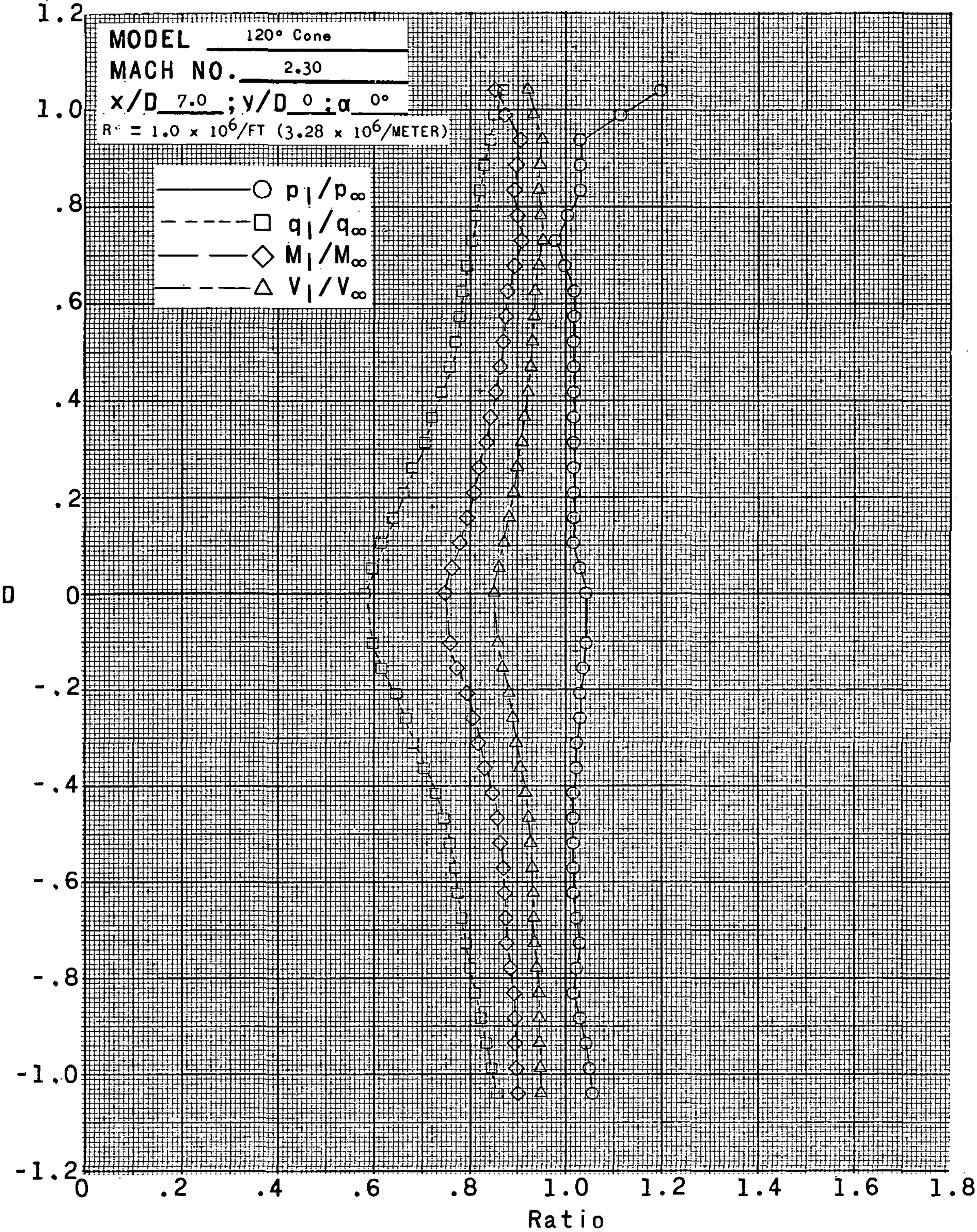
(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 7.- Continued.



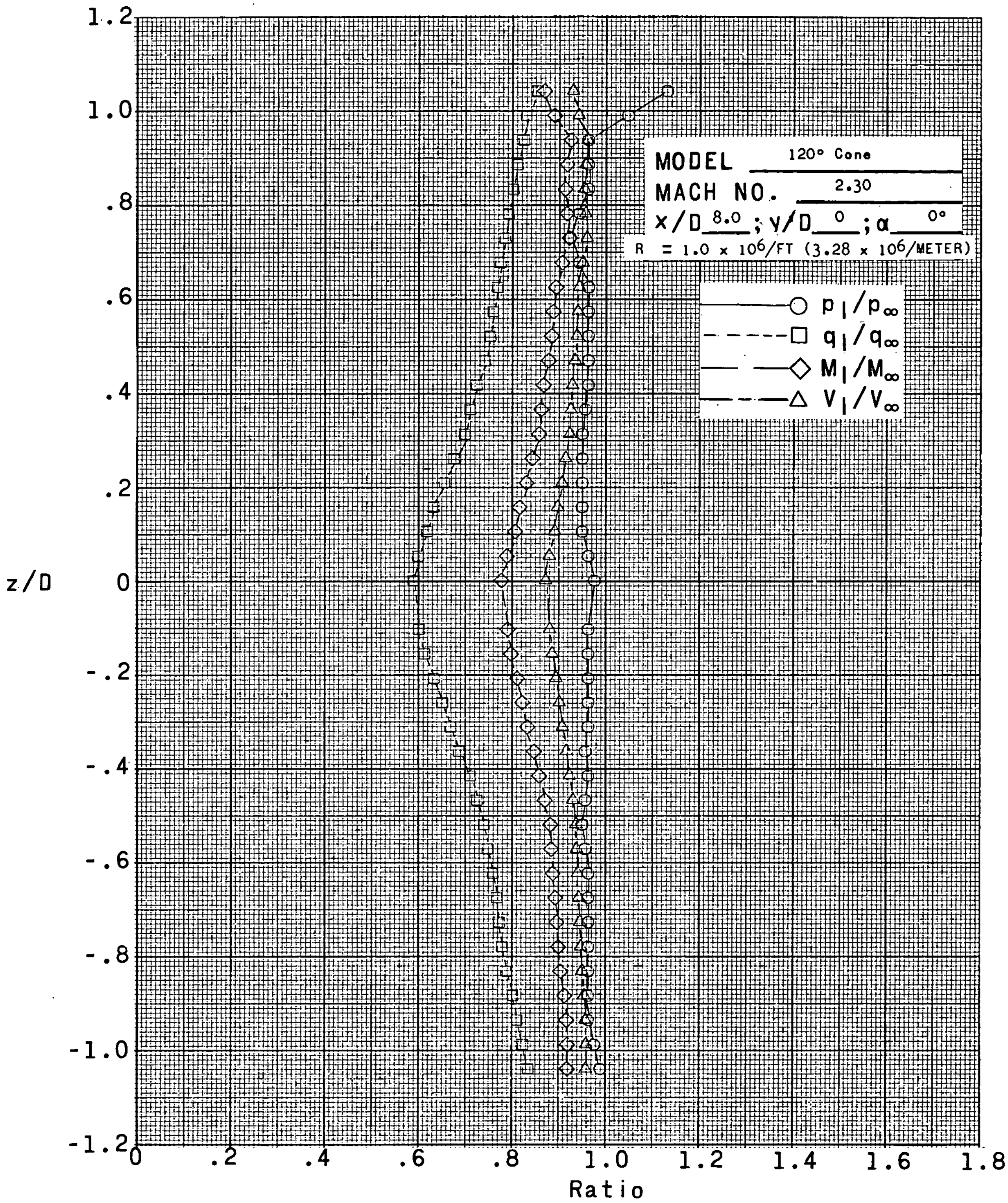
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 7.- Continued.



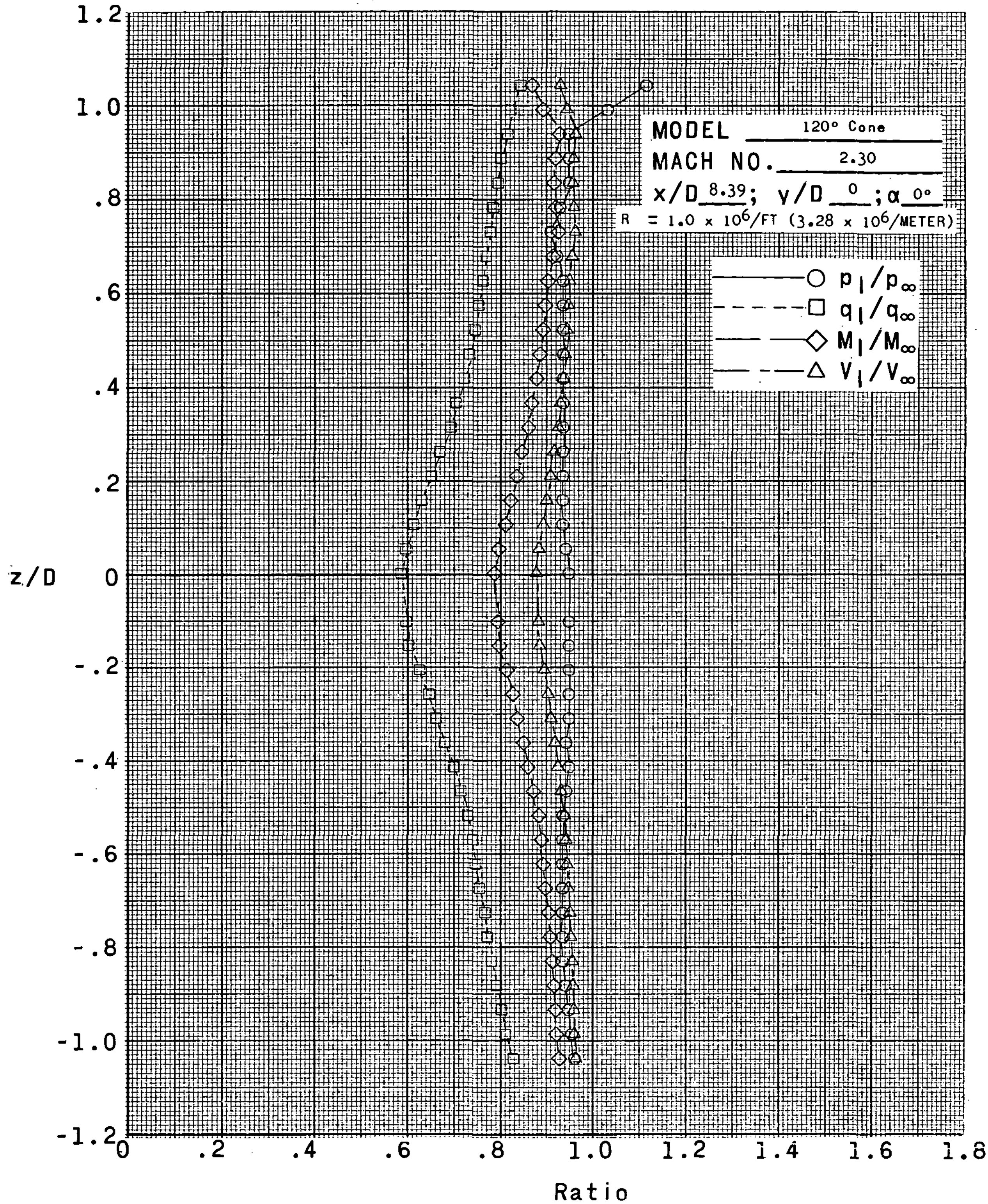
(i) x/D = 7.0; y/D = 0; α = 0°.

Figure 7.- Continued.



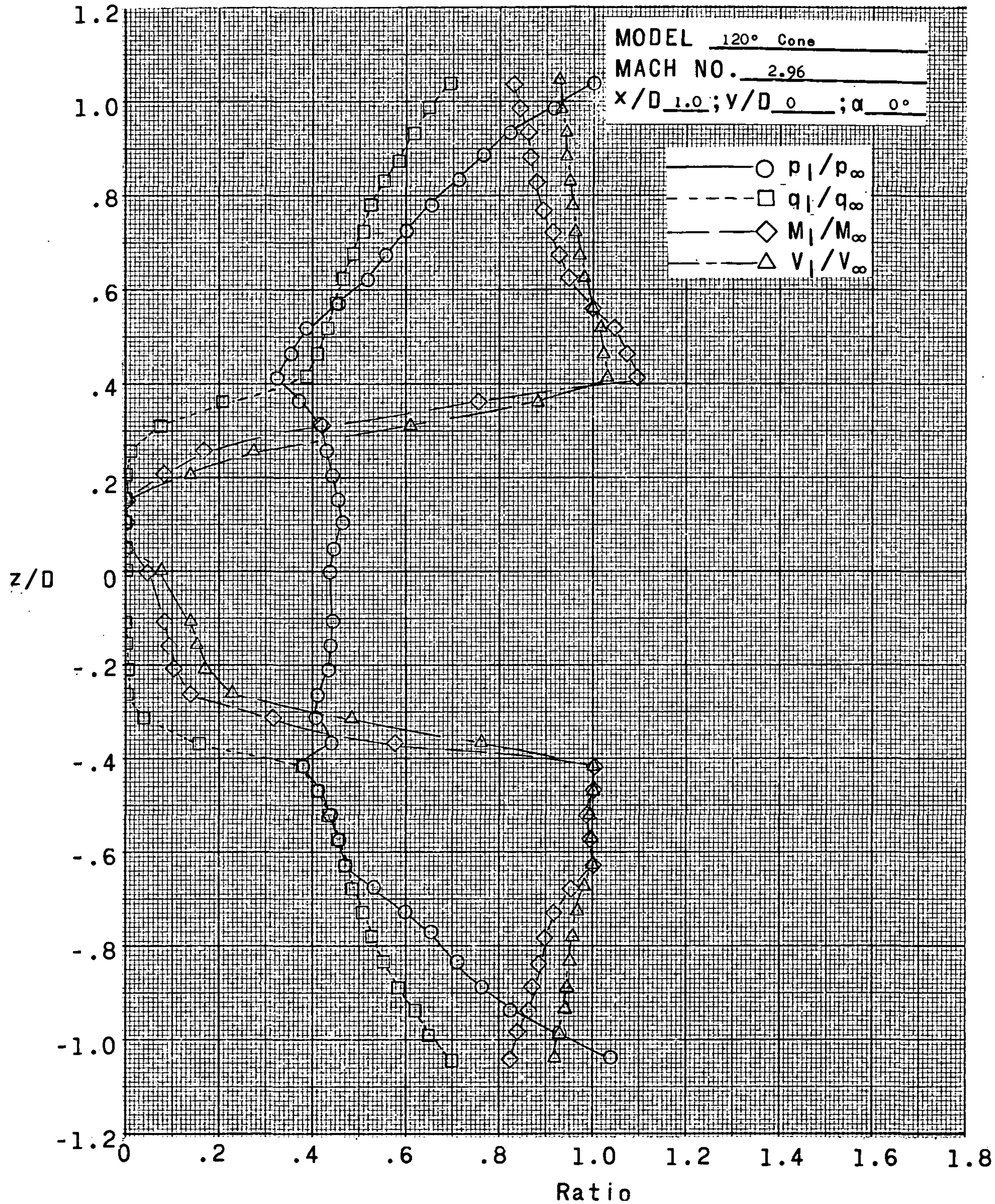
(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 7.- Continued.



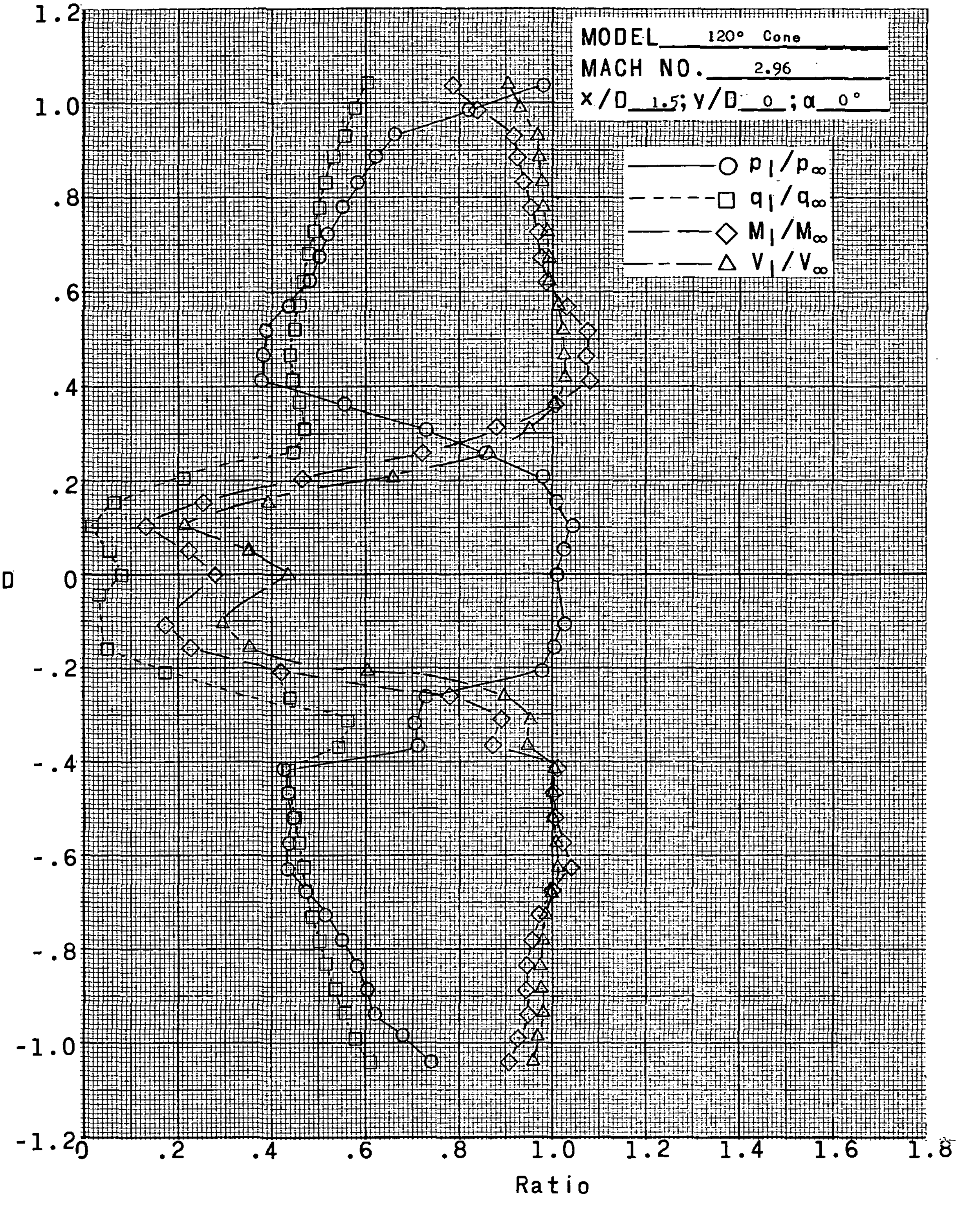
(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^\circ$.

Figure 7.- Concluded.



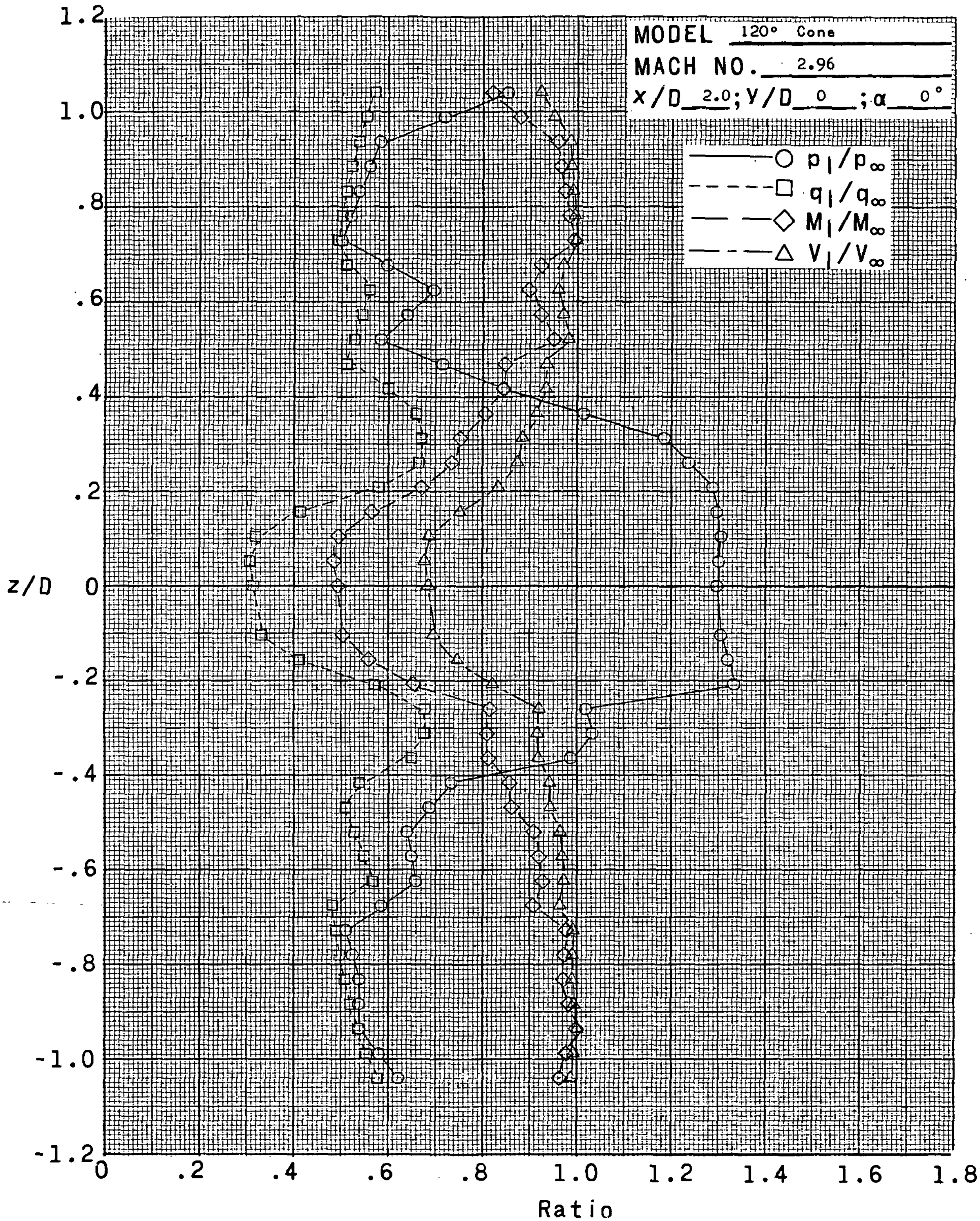
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 8.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in the wake of a 120^{0}-included-angle cone at a Mach number of 2.96 and a Reynolds number of 1.65×10^6 per foot (5.42×10^6 per meter).



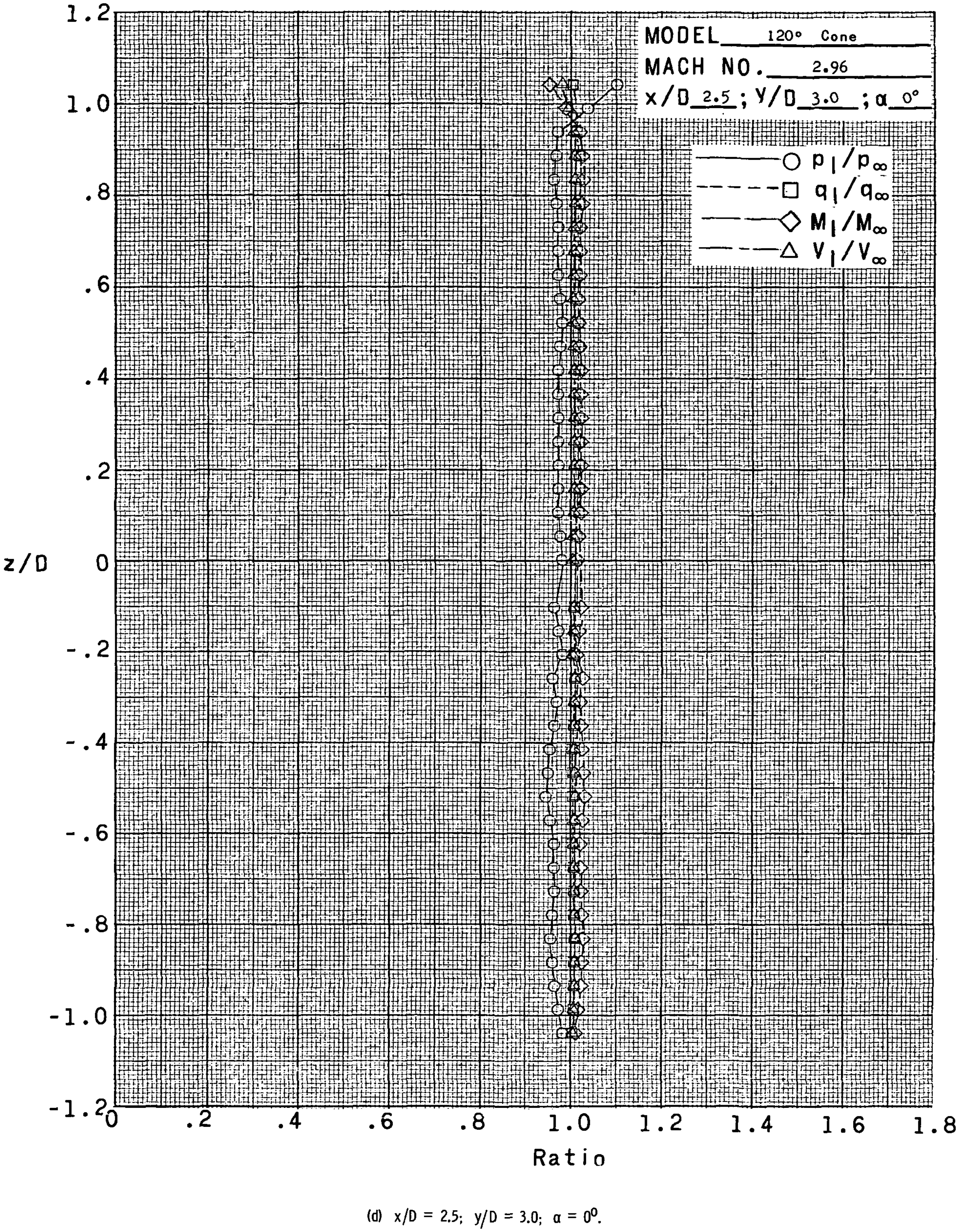
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 8.- Continued.



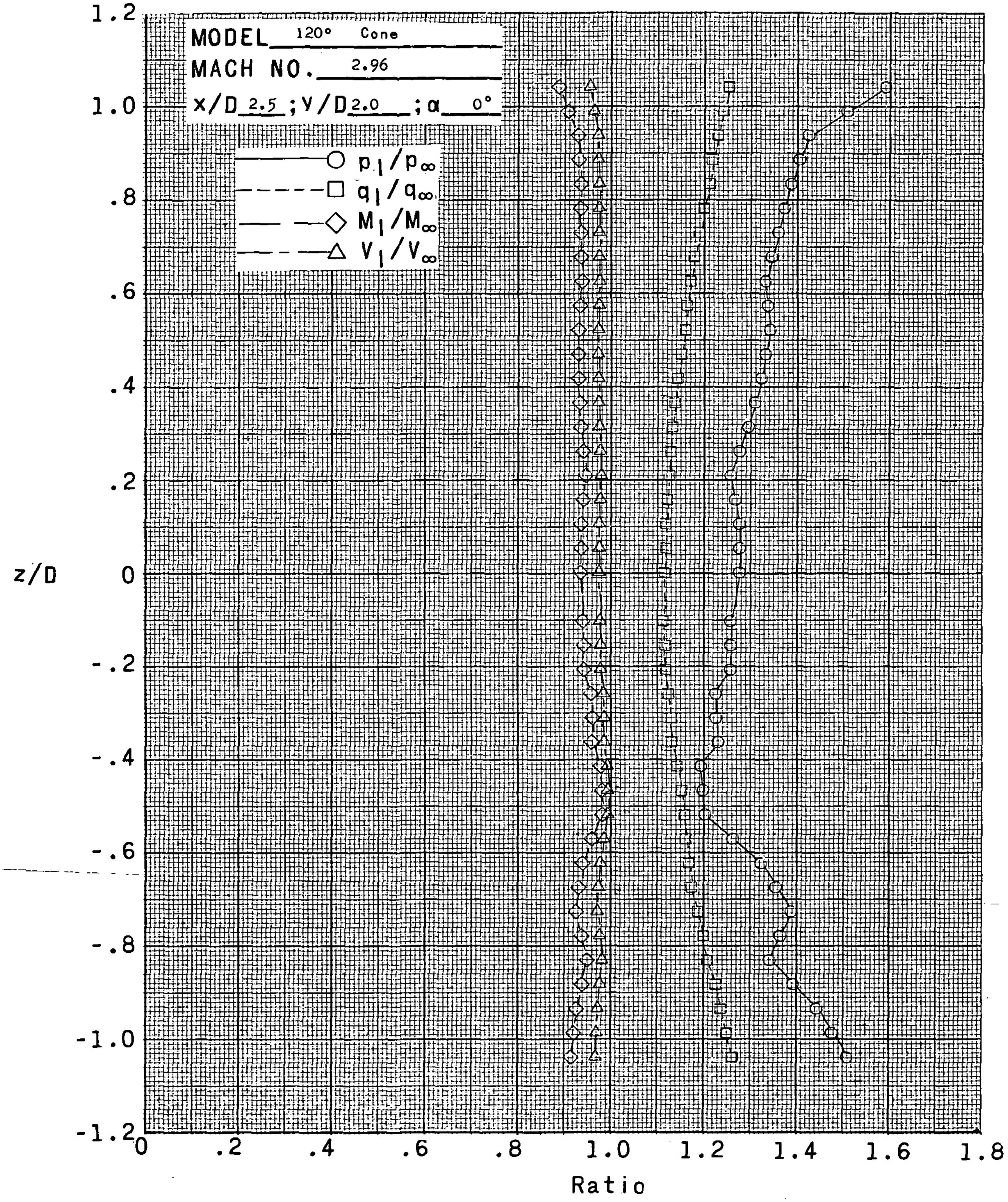
(c) $x/D = 2.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 8.- Continued.



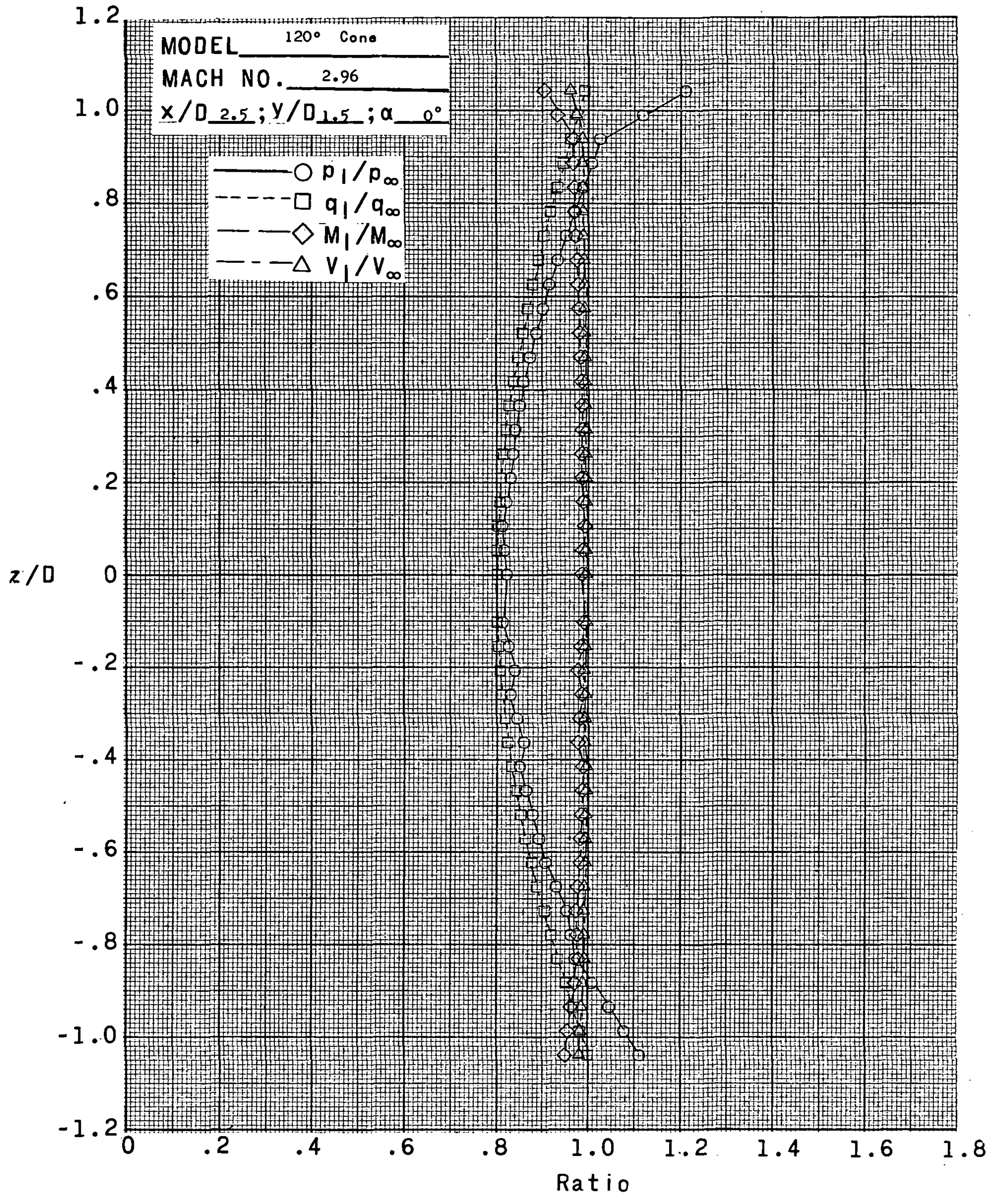
(d) x/D = 2.5; y/D = 3.0; α = 0°.

Figure 8.- Continued.



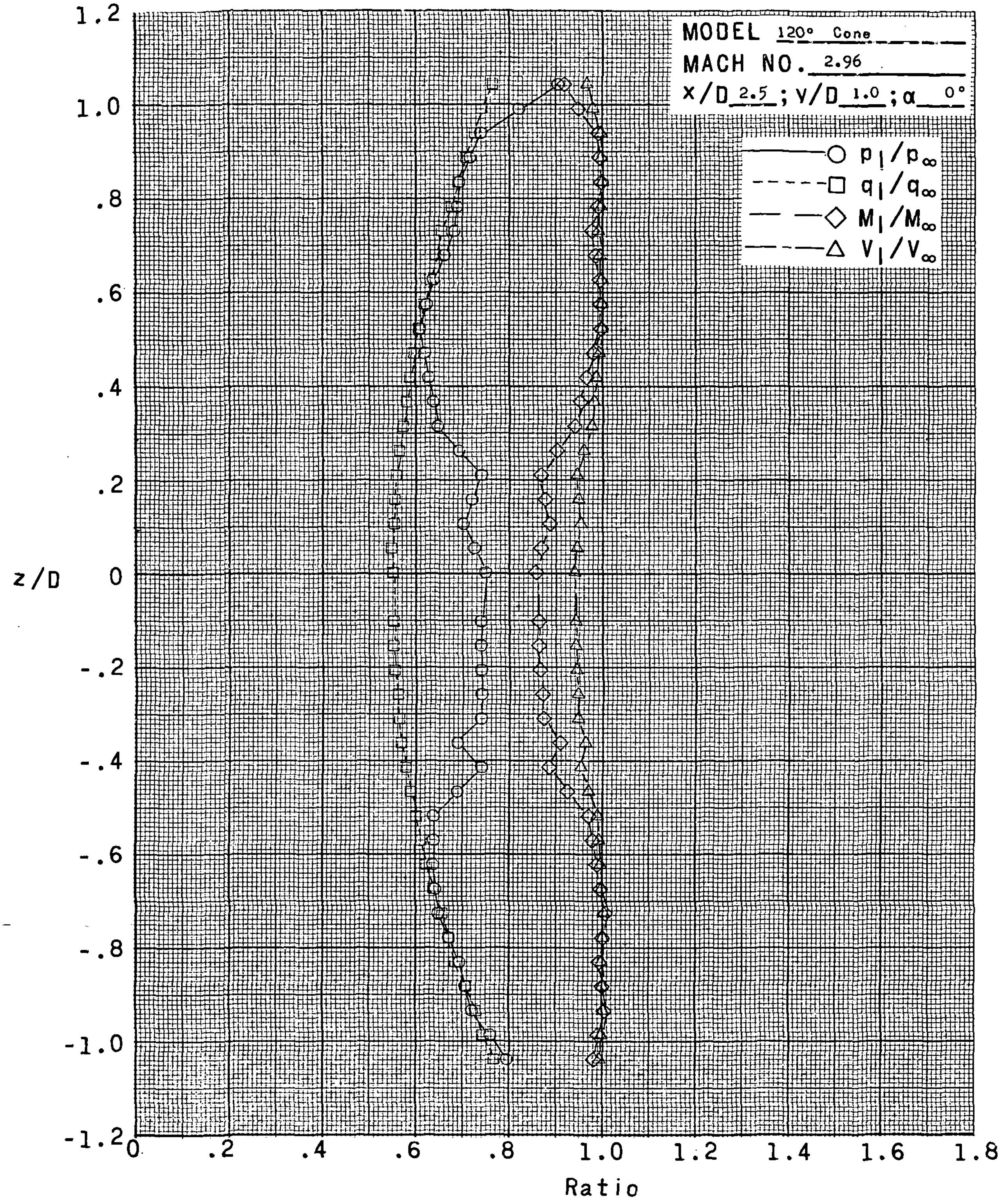
(e) $x/D = 2.5$; $y/D = 2.0$; $\alpha = 0^0$.

Figure 8.- Continued.



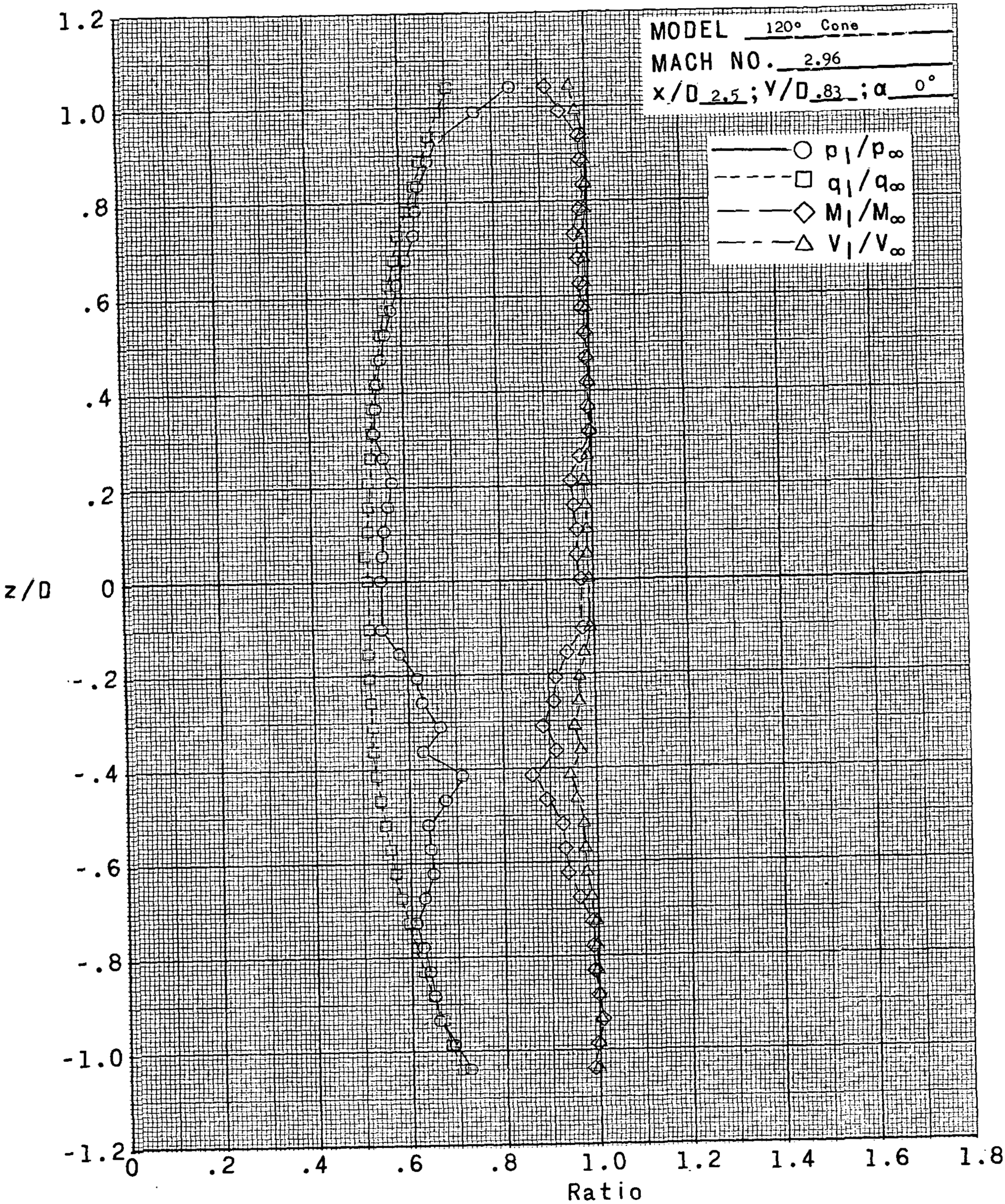
(f) x/D = 2.5; y/D = 1.5; α = 0°.

Figure 8.- Continued.



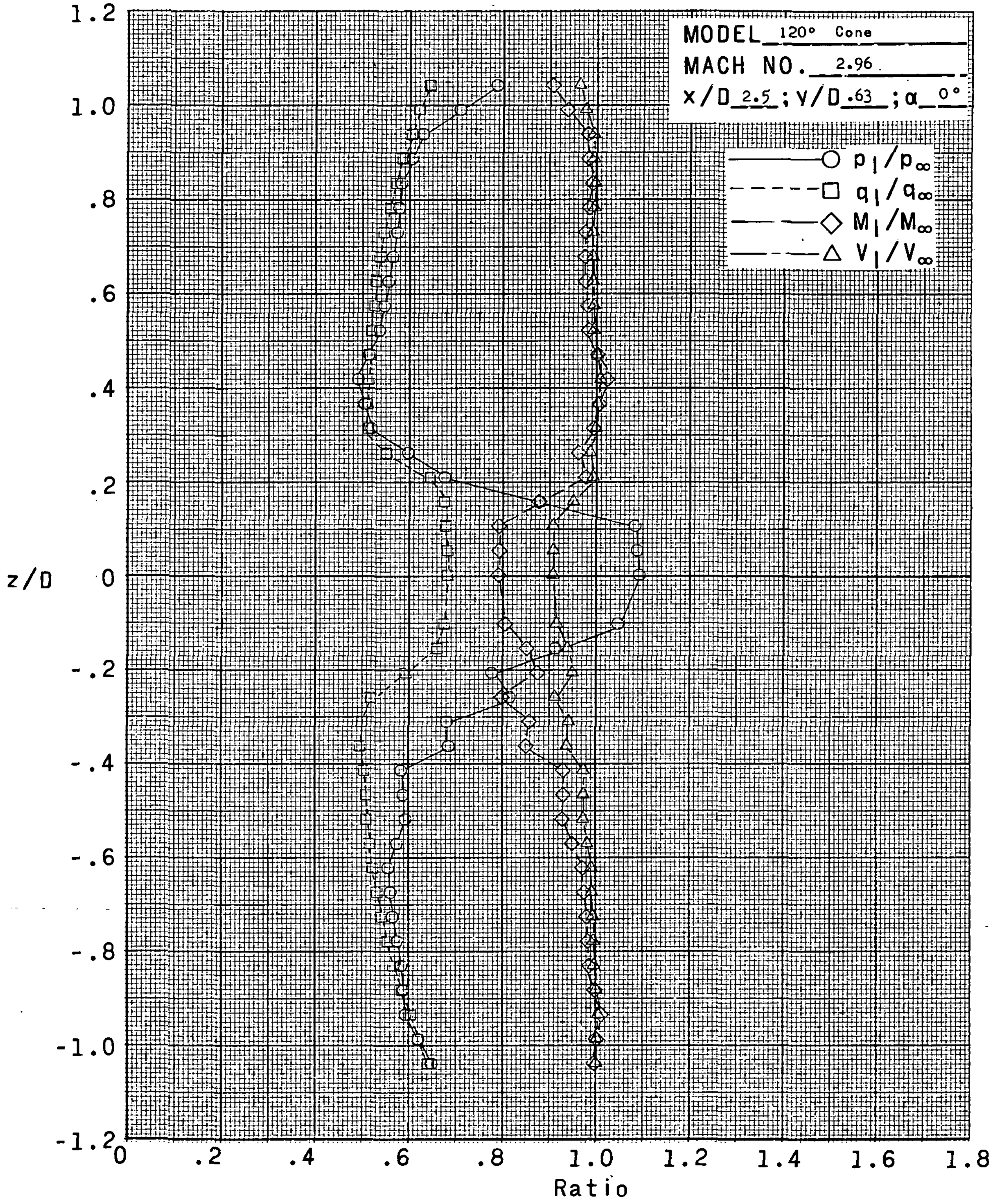
(g) x/D = 2.5; y/D = 1.0; α = 0°.

Figure 8.- Continued.



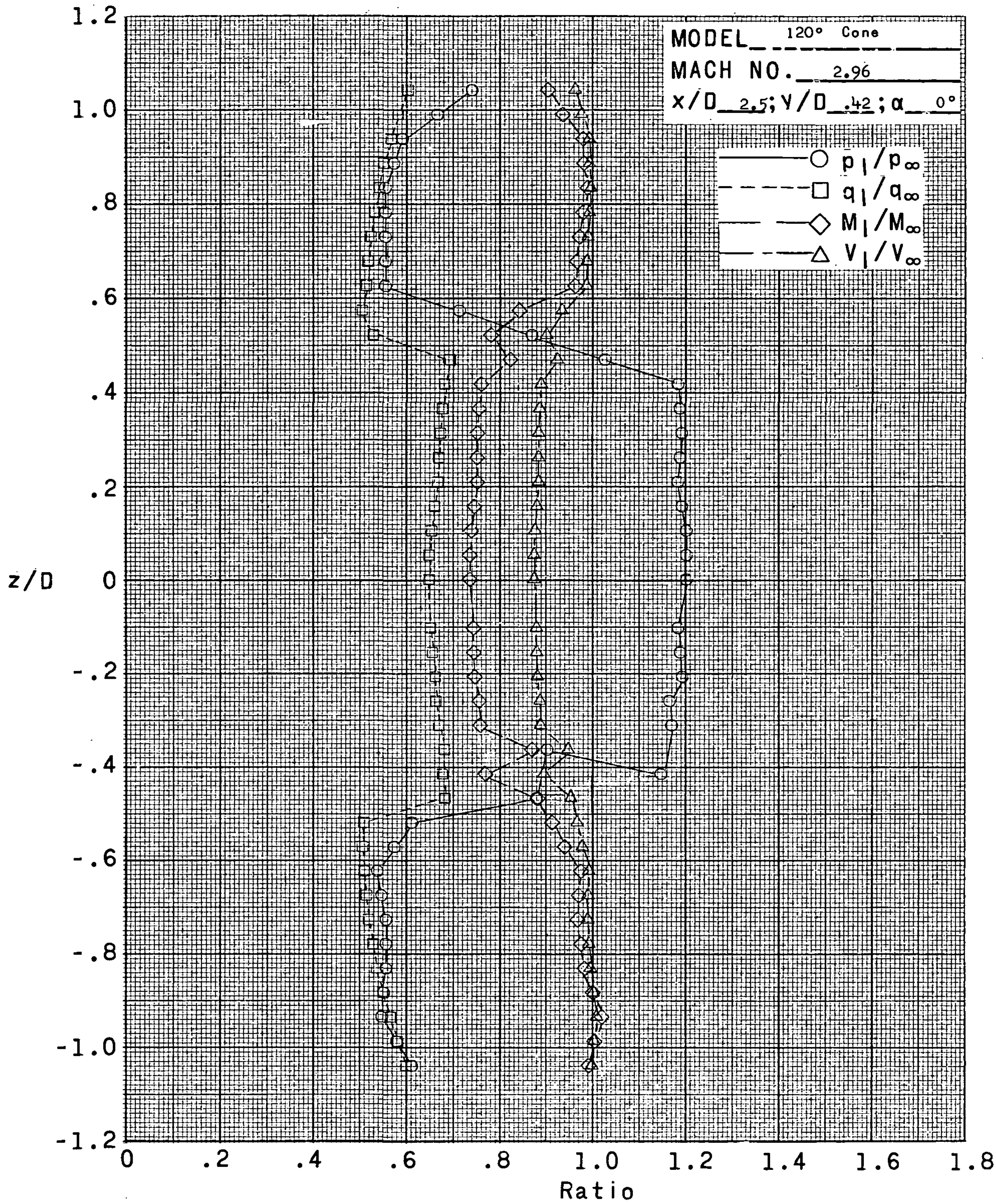
(h) x/D = 2.5; y/D = 0.83; α = 0°.

Figure 8.- Continued.



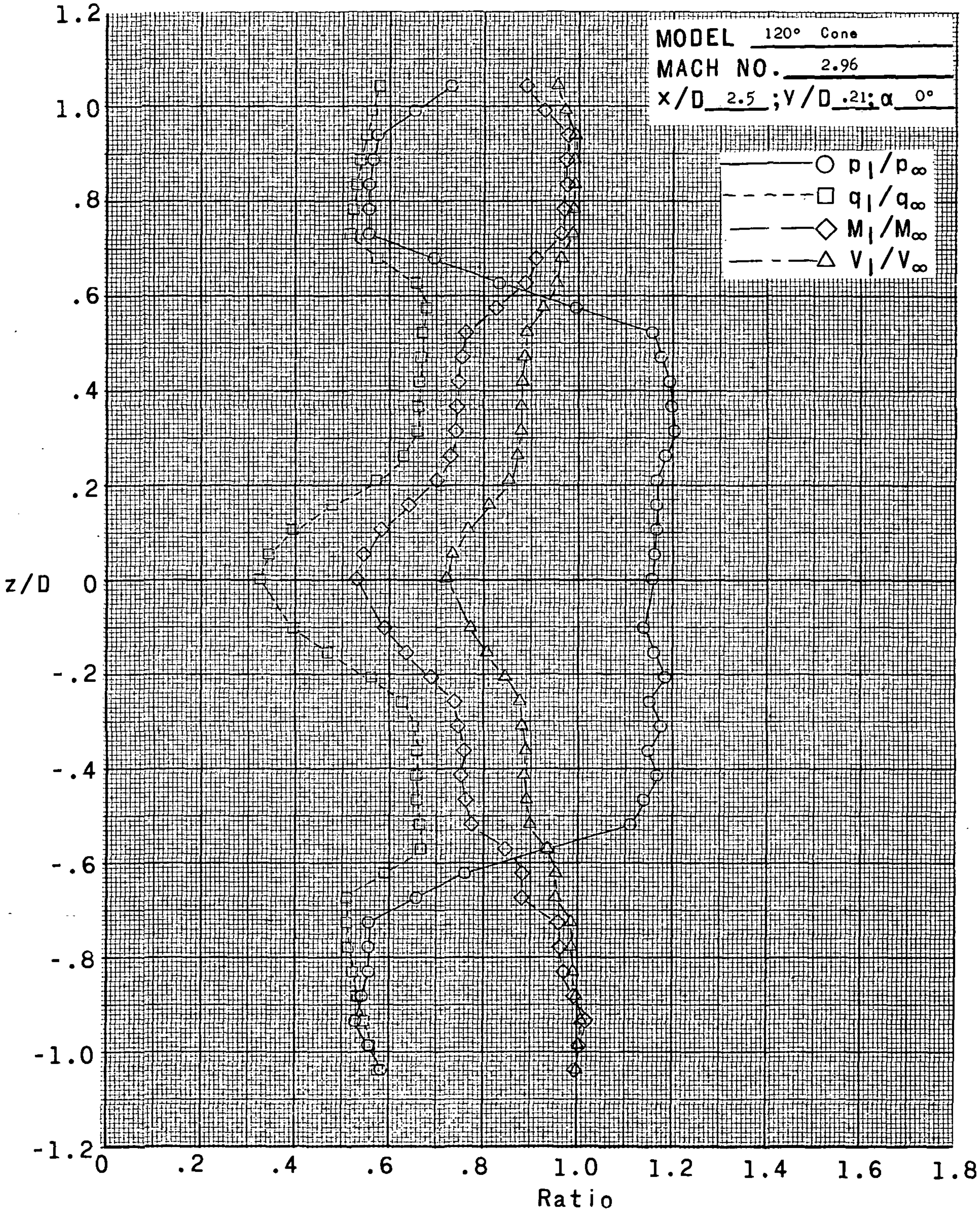
(i) $x/D = 2.5$; $y/D = 0.63$; $\alpha = 0^0$.

Figure 8.- Continued.



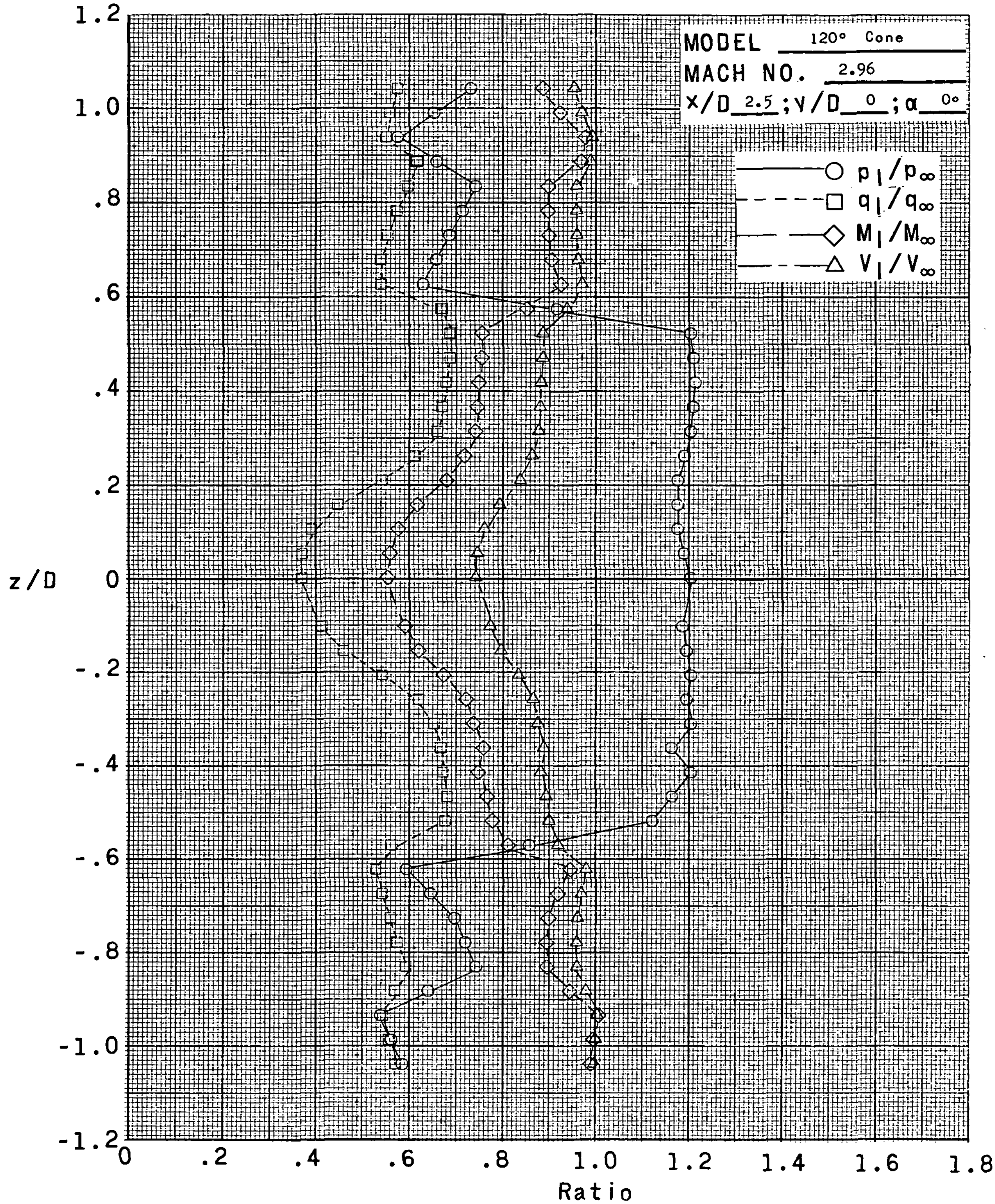
(j) x/D = 2.5; y/D = 0.42; α = 0°.

Figure 8.- Continued.



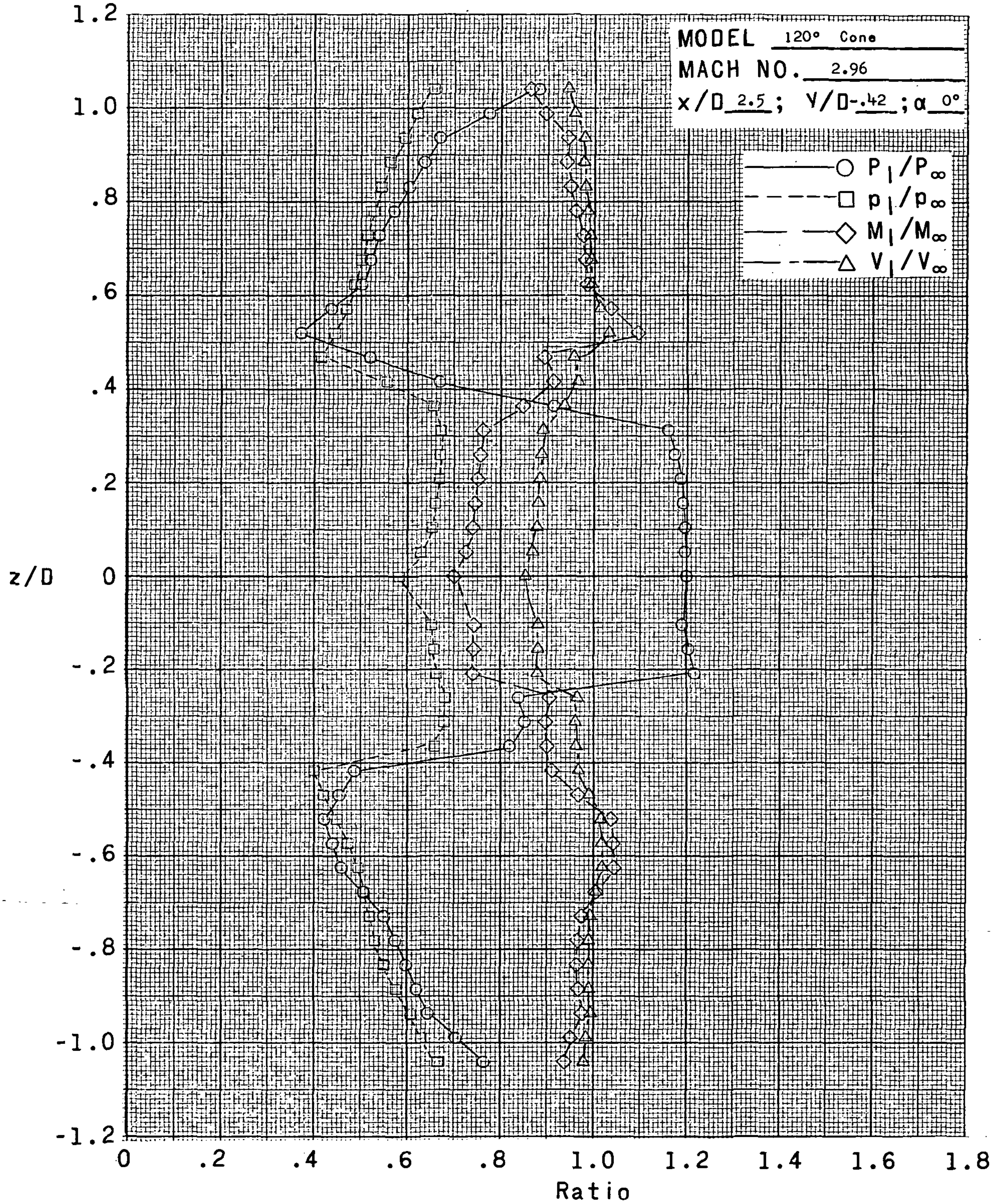
(k) x/D = 2.5; y/D = 0.21; α = 0°.

Figure 8.- Continued.



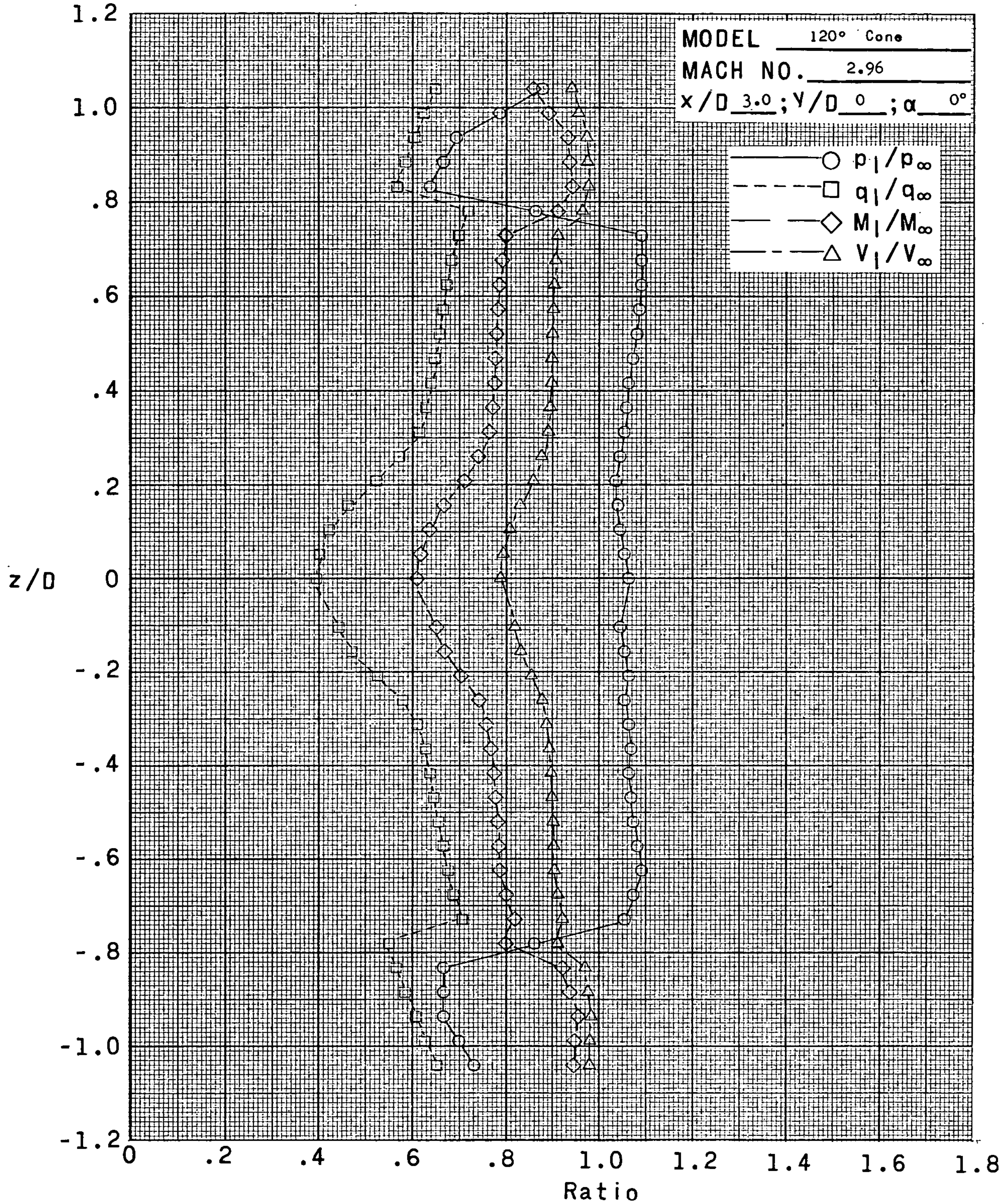
(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^0$.

Figure 8.- Continued.



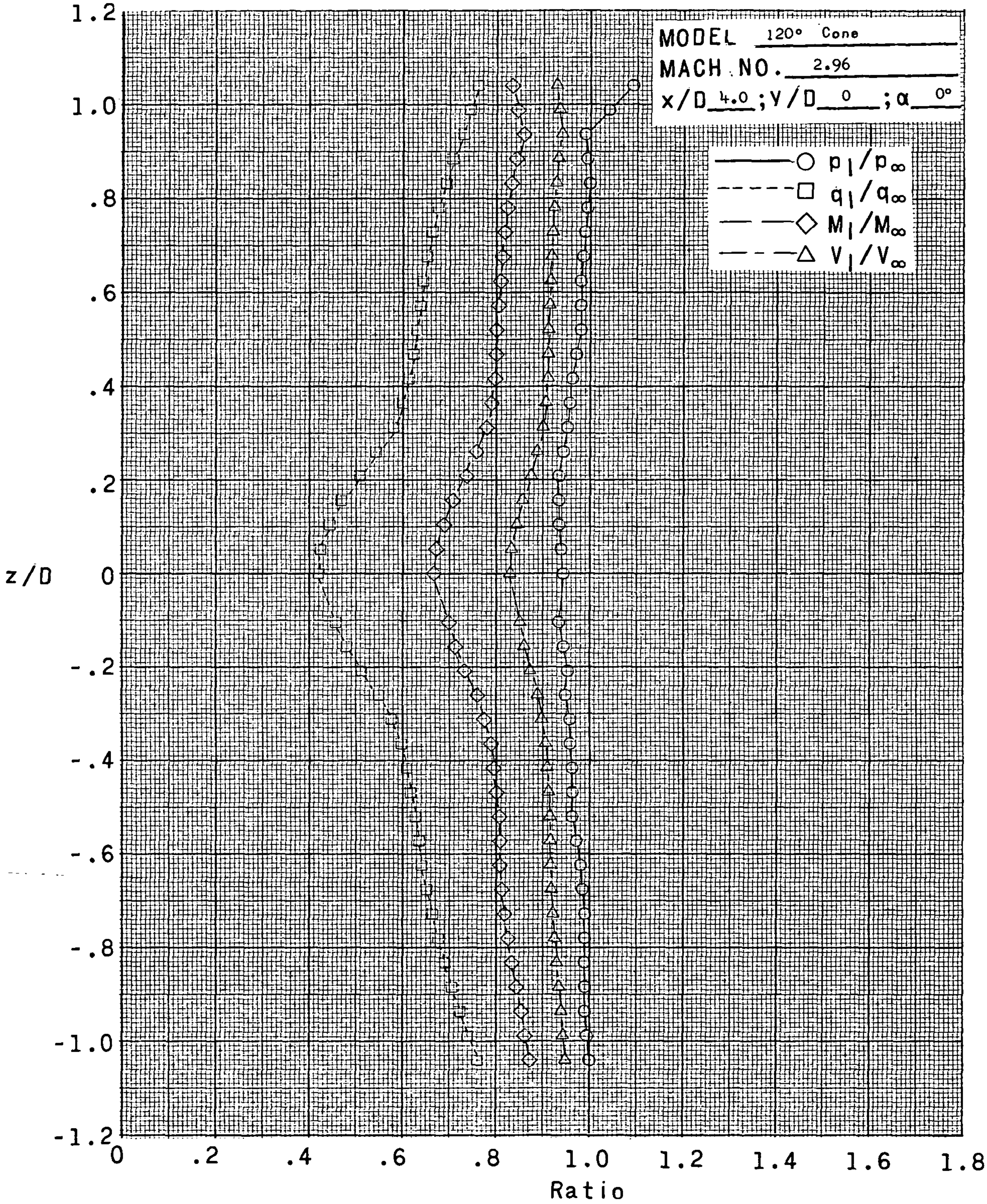
(m) $x/D = 2.5$; $y/D = -0.42$; $\alpha = 0^o$.

Figure 8.- Continued.



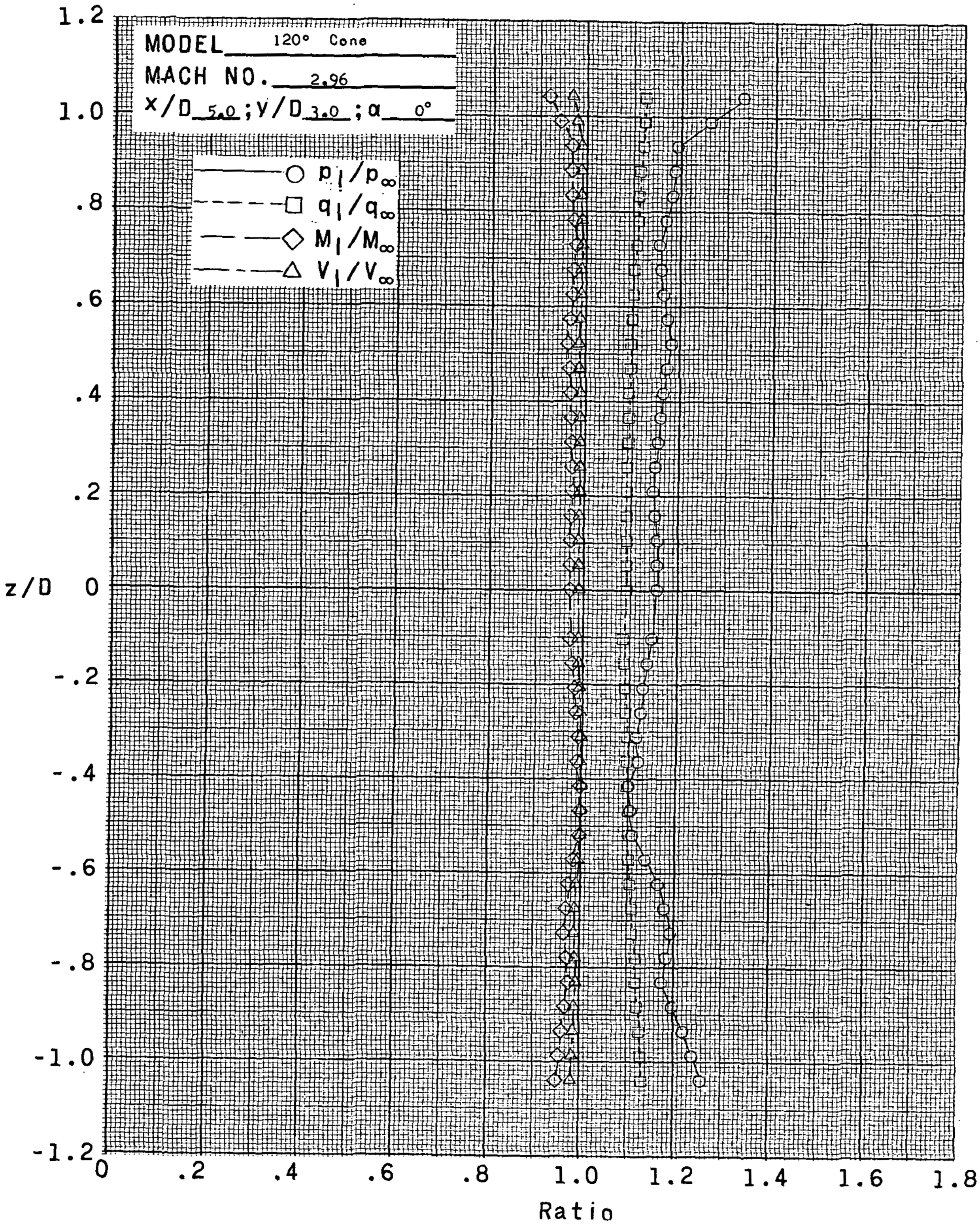
(n) $x/D = 3.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 8.- Continued.



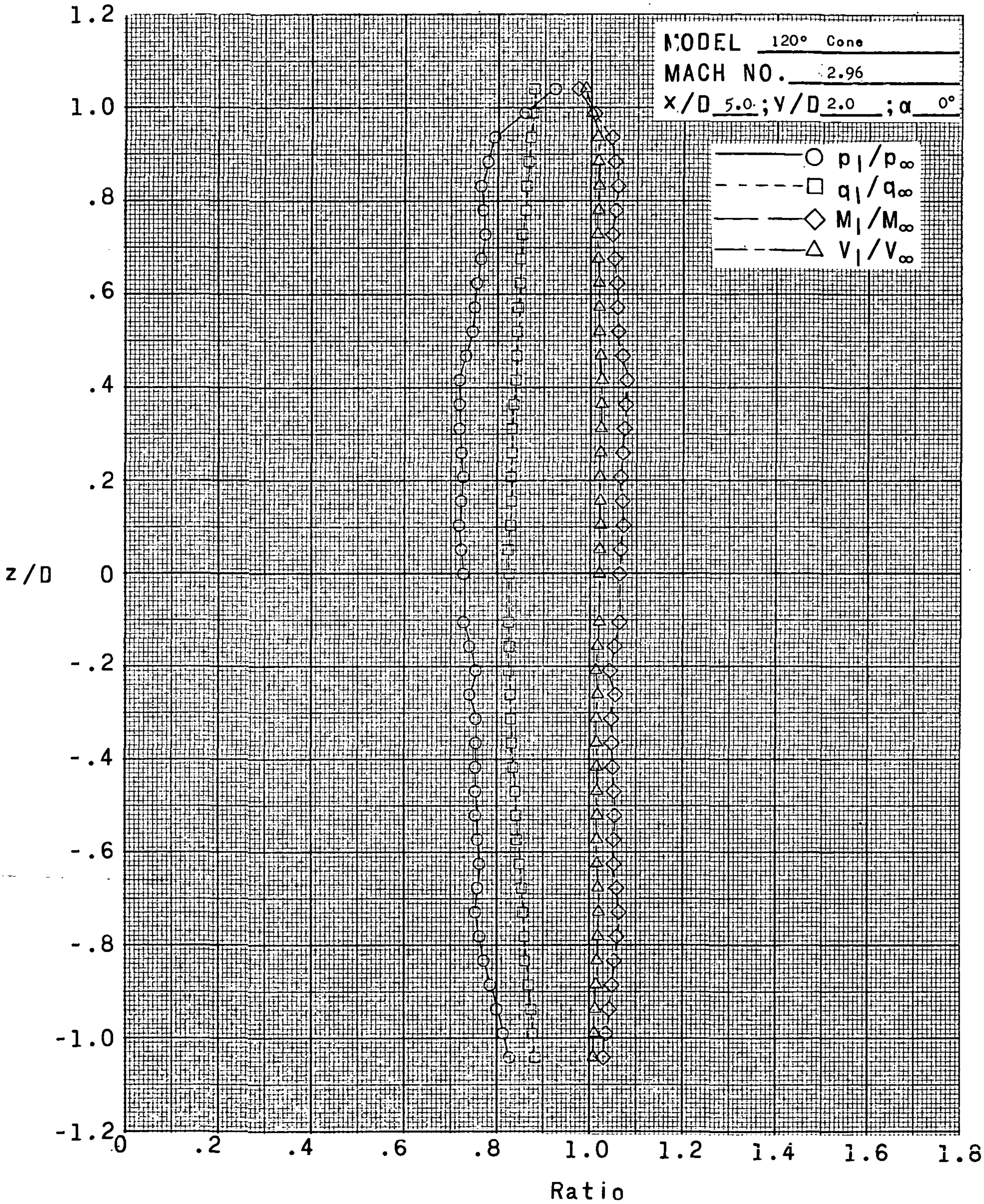
(o) x/D = 4.0; y/D = 0; α = 0°.

Figure 8.- Continued.



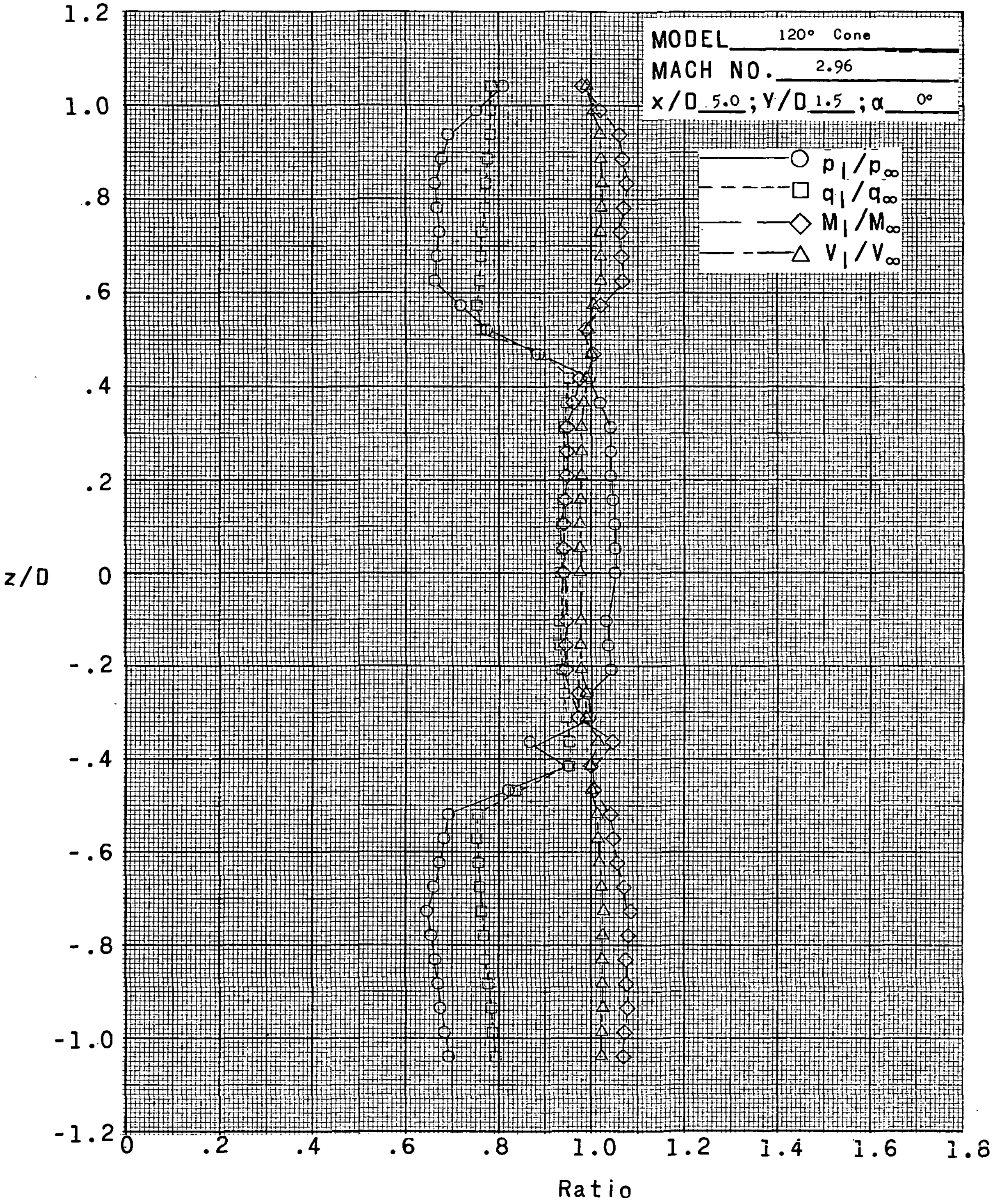
(p) $x/D = 5.0$; $y/D = 3.0$; $\alpha = 0^0$.

Figure 8.- Continued.



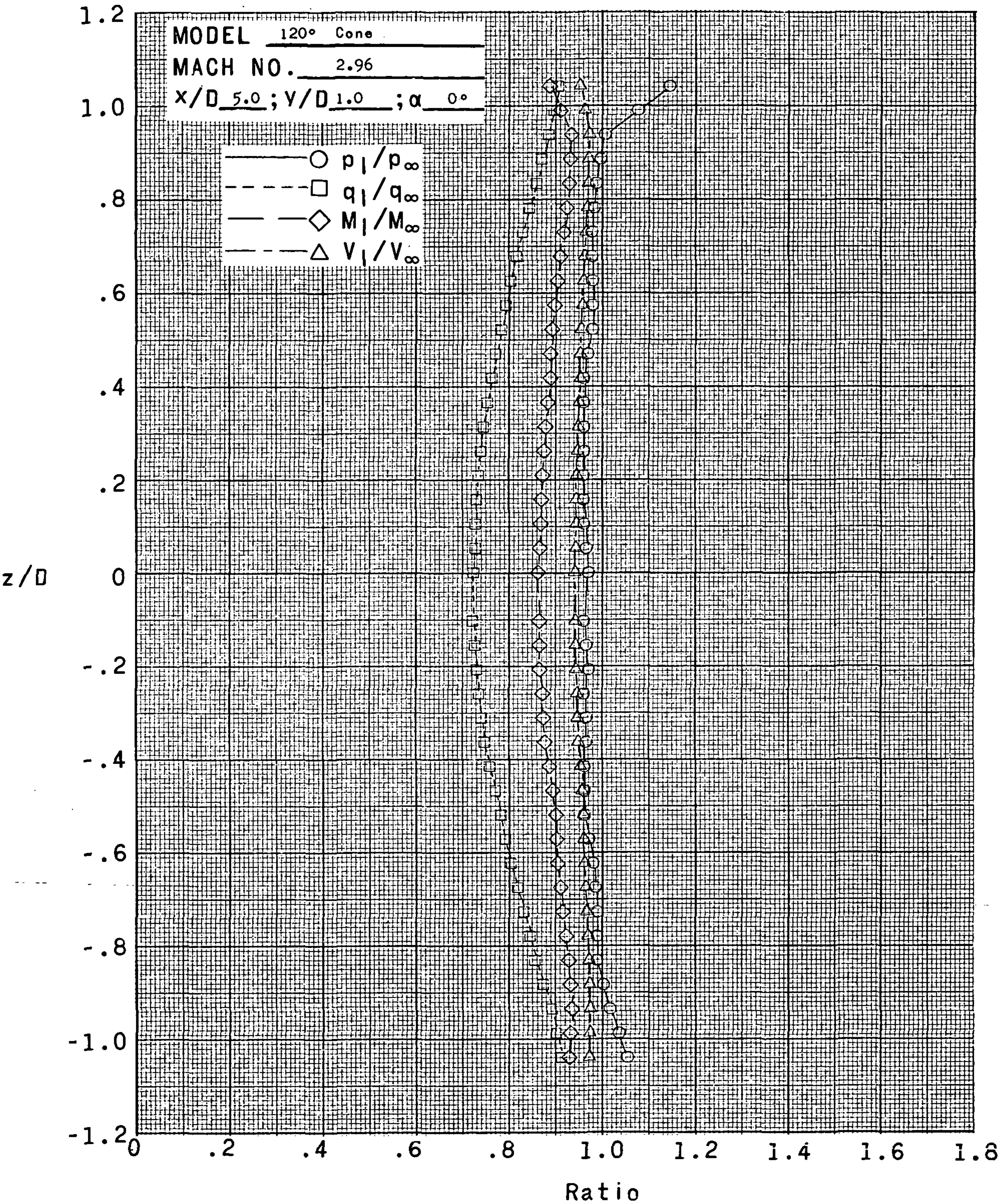
(q) x/D = 5.0; y/D = 2.0; α = 0°.

Figure 8.- Continued.



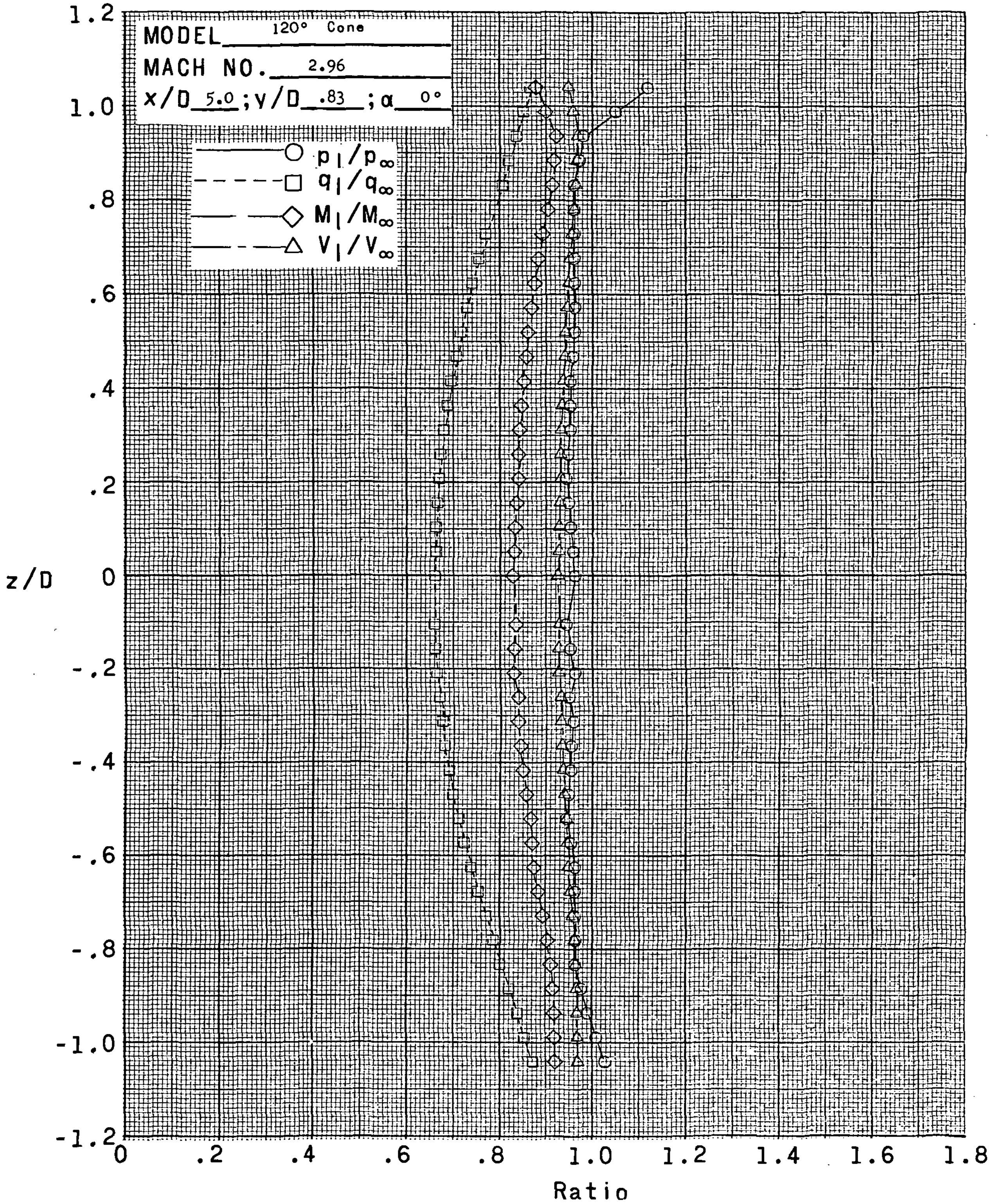
(r) x/D = 5.0; y/D = 1.5; α = 0°.

Figure 8.- Continued.



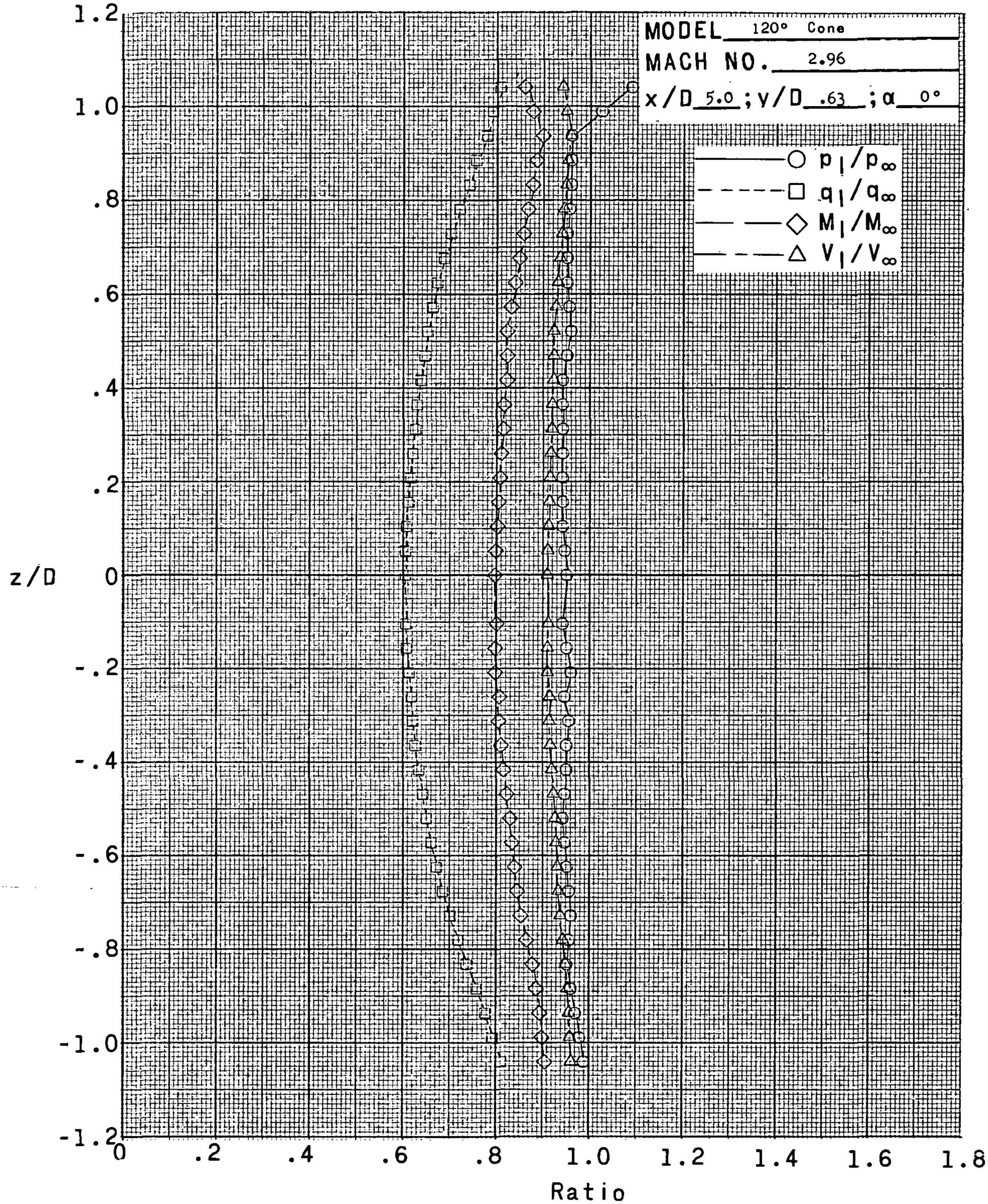
(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^0$.

Figure 8.- Continued.



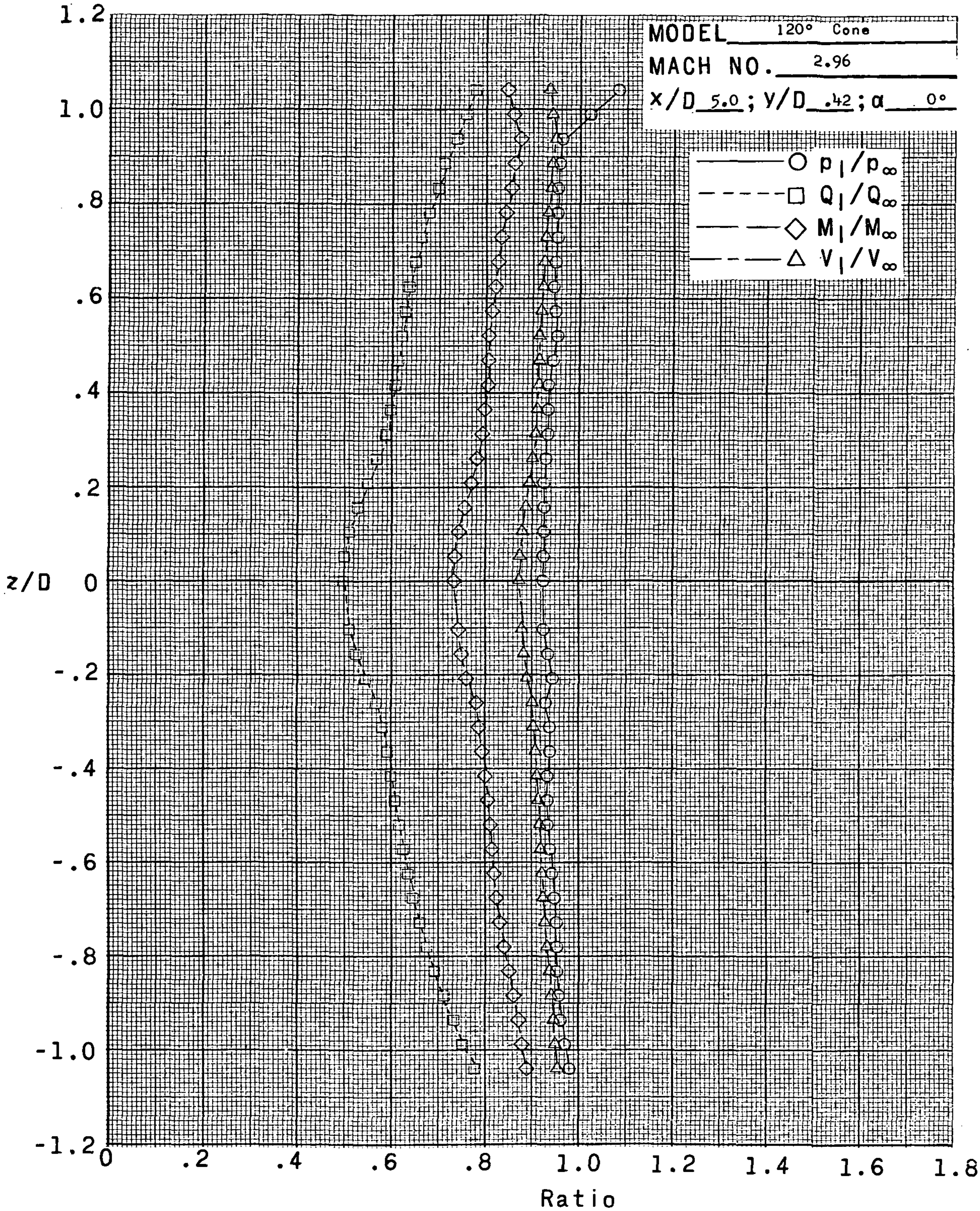
(t) $x/D = 5.0$; $y/D = 0.83$; $\alpha = 0^{\circ}$.

Figure 8.- Continued.



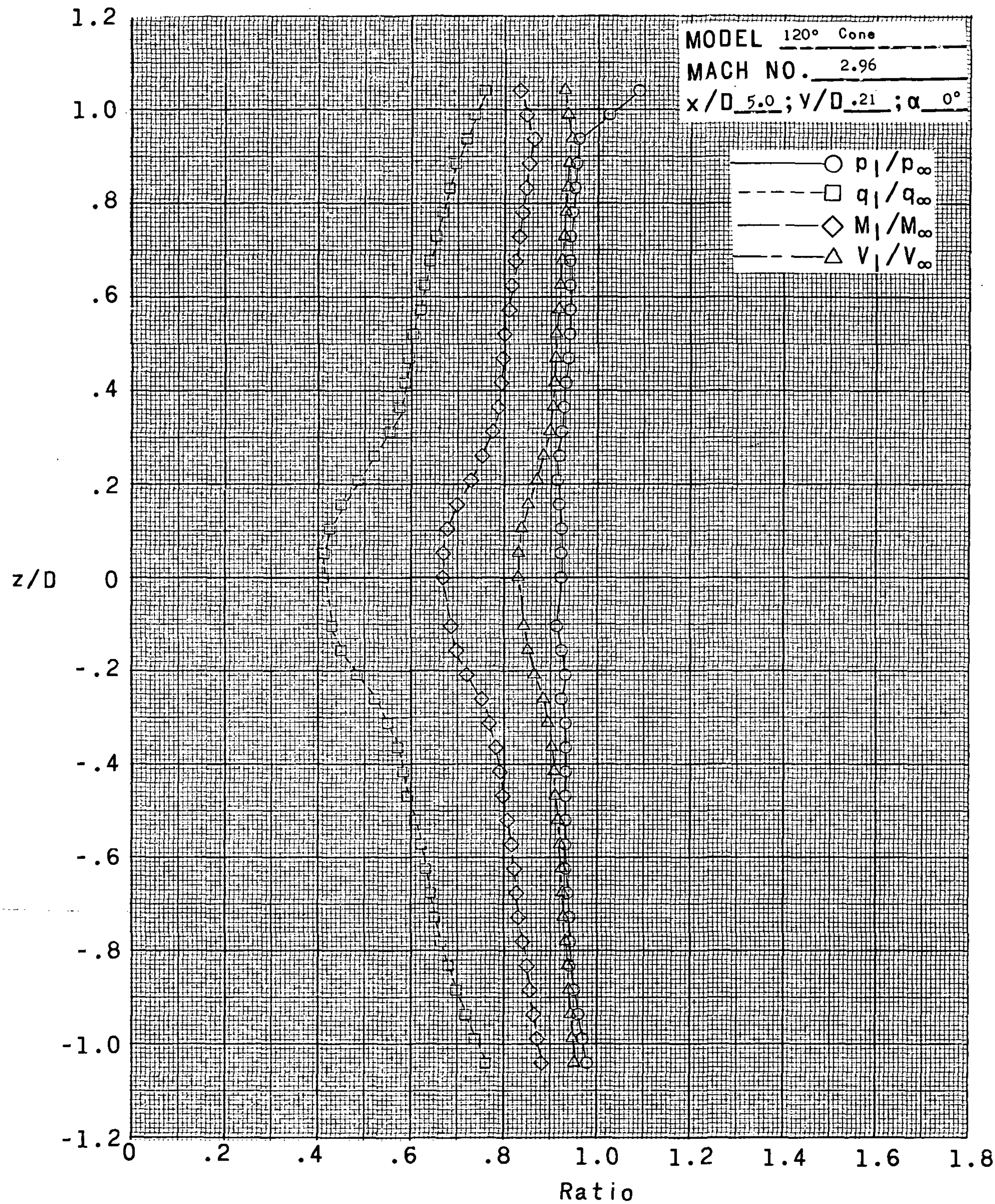
(u) $x/D = 5.0$; $y/D = 0.63$; $\alpha = 0^{0}$.

Figure 8.- Continued.



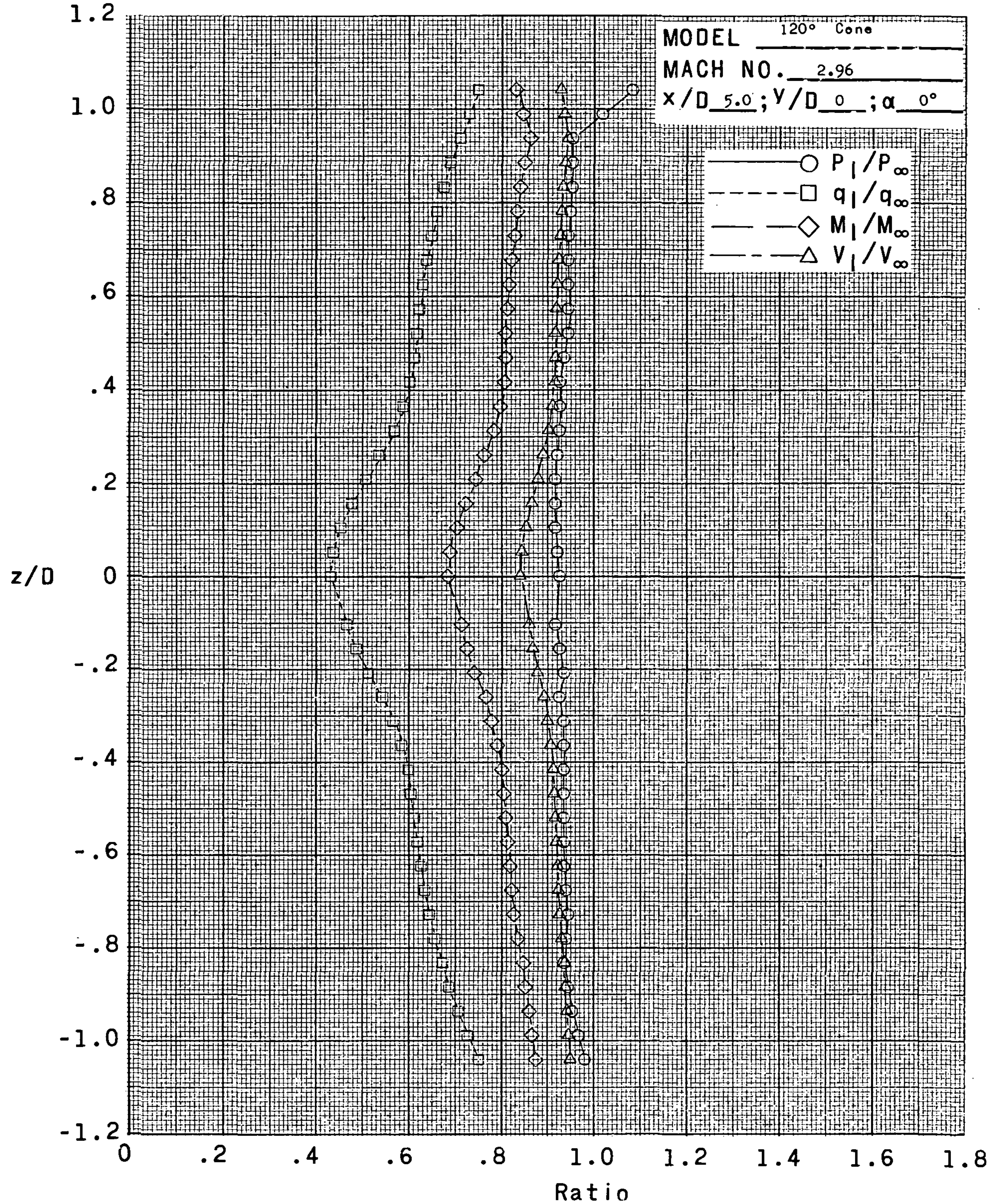
(v) $x/D = 5.0$; $y/D = 0.42$; $\alpha = 0^\circ$.

Figure 8.- Continued.



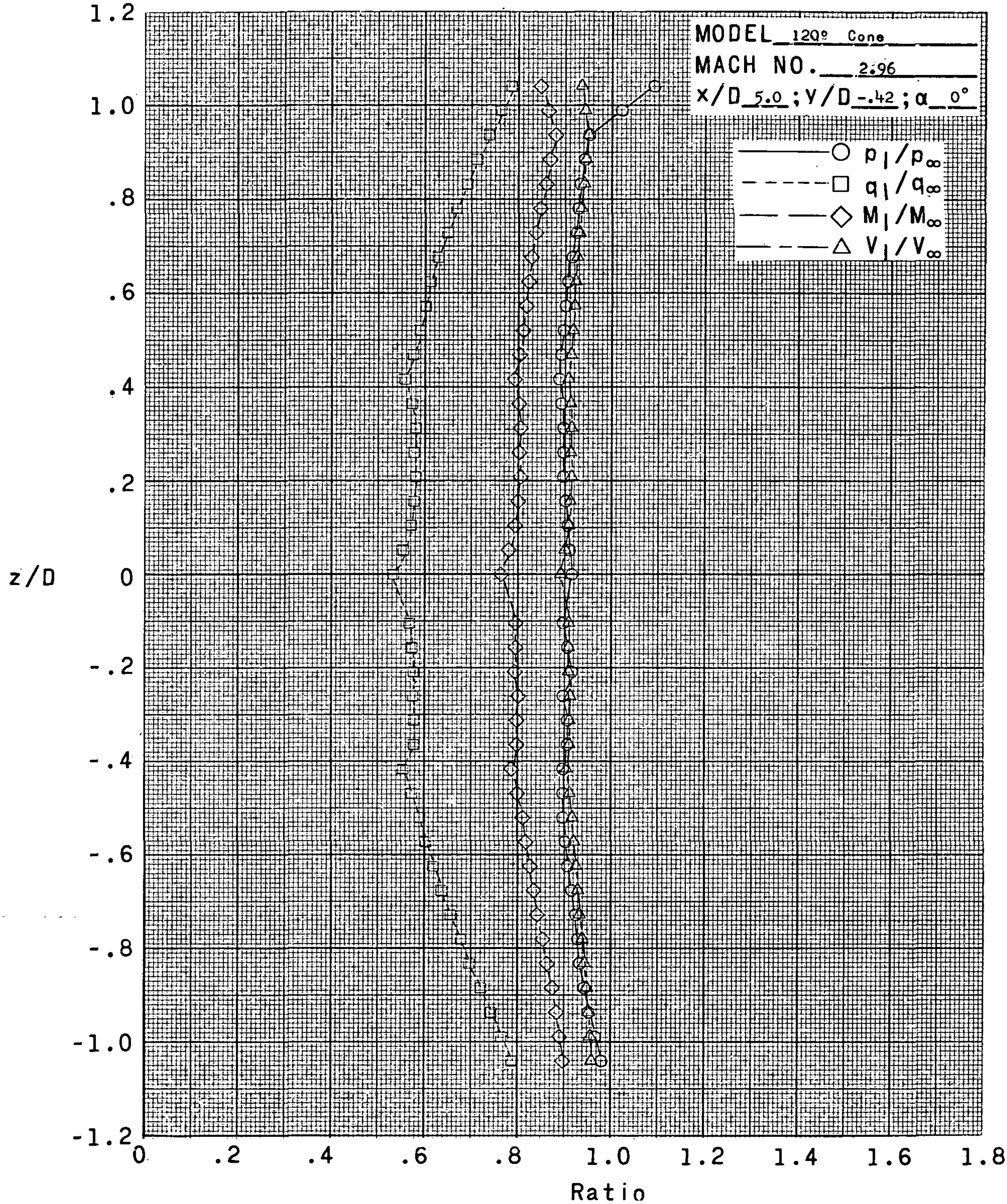
(w) x/D = 5.0; y/D = 0.21; α = 0°.

Figure 8.- Continued.



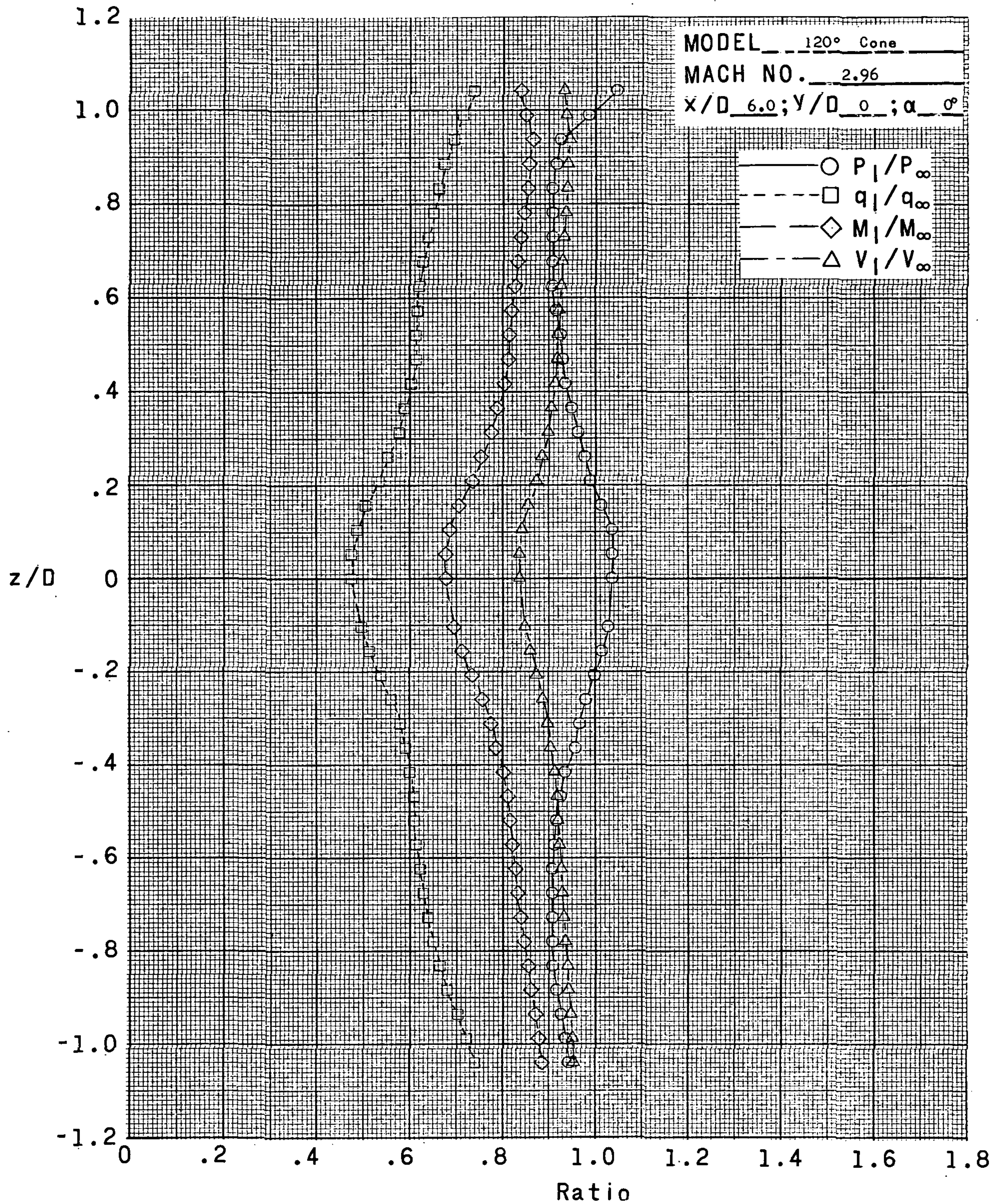
(x) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 8.- Continued.



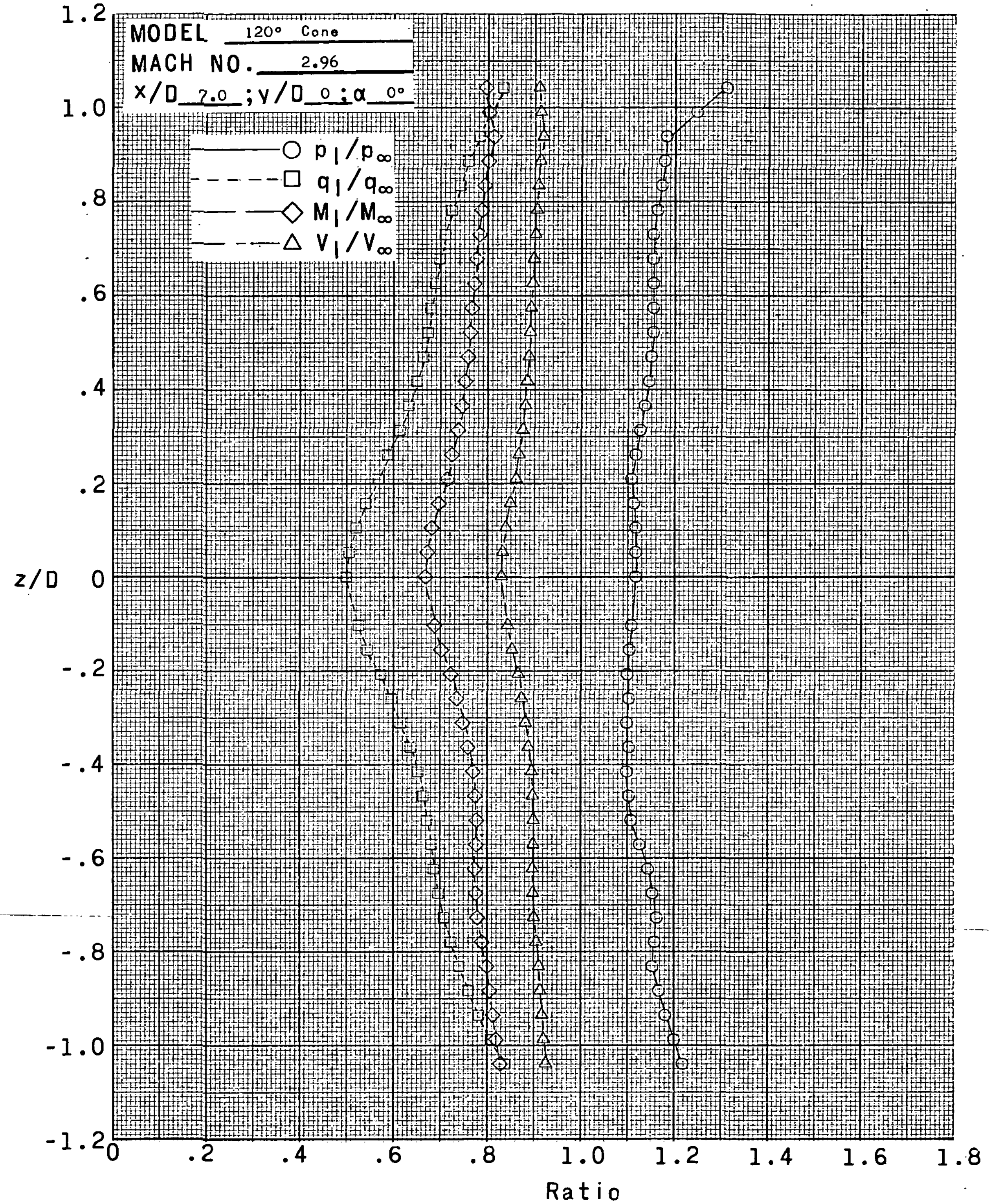
(y) x/D = 5.0; y/D = -0.42; α = 0°.

Figure 8.- Continued.



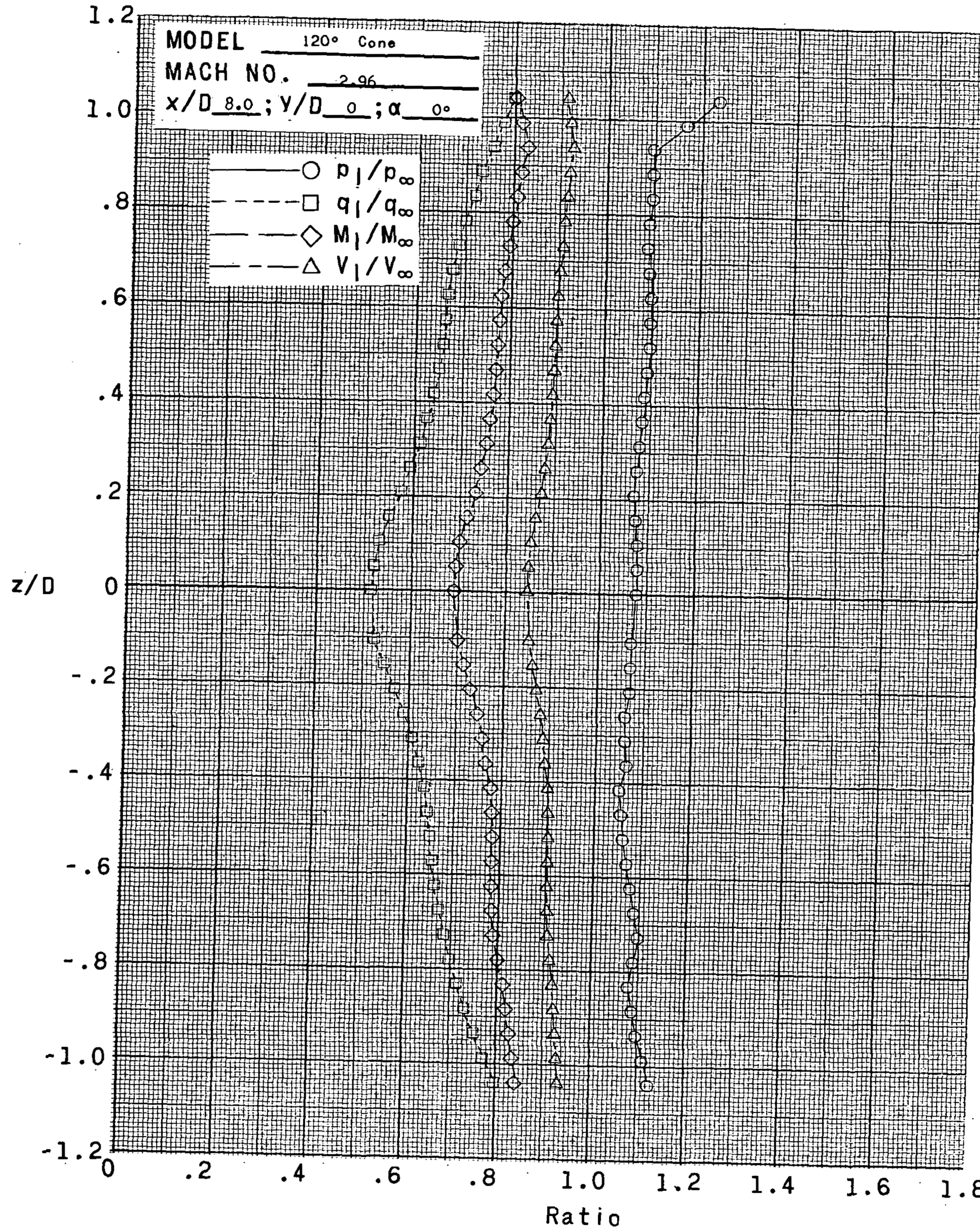
(z) x/D = 6.0; y/D = 0; α = 0°.

Figure 8.- Continued.



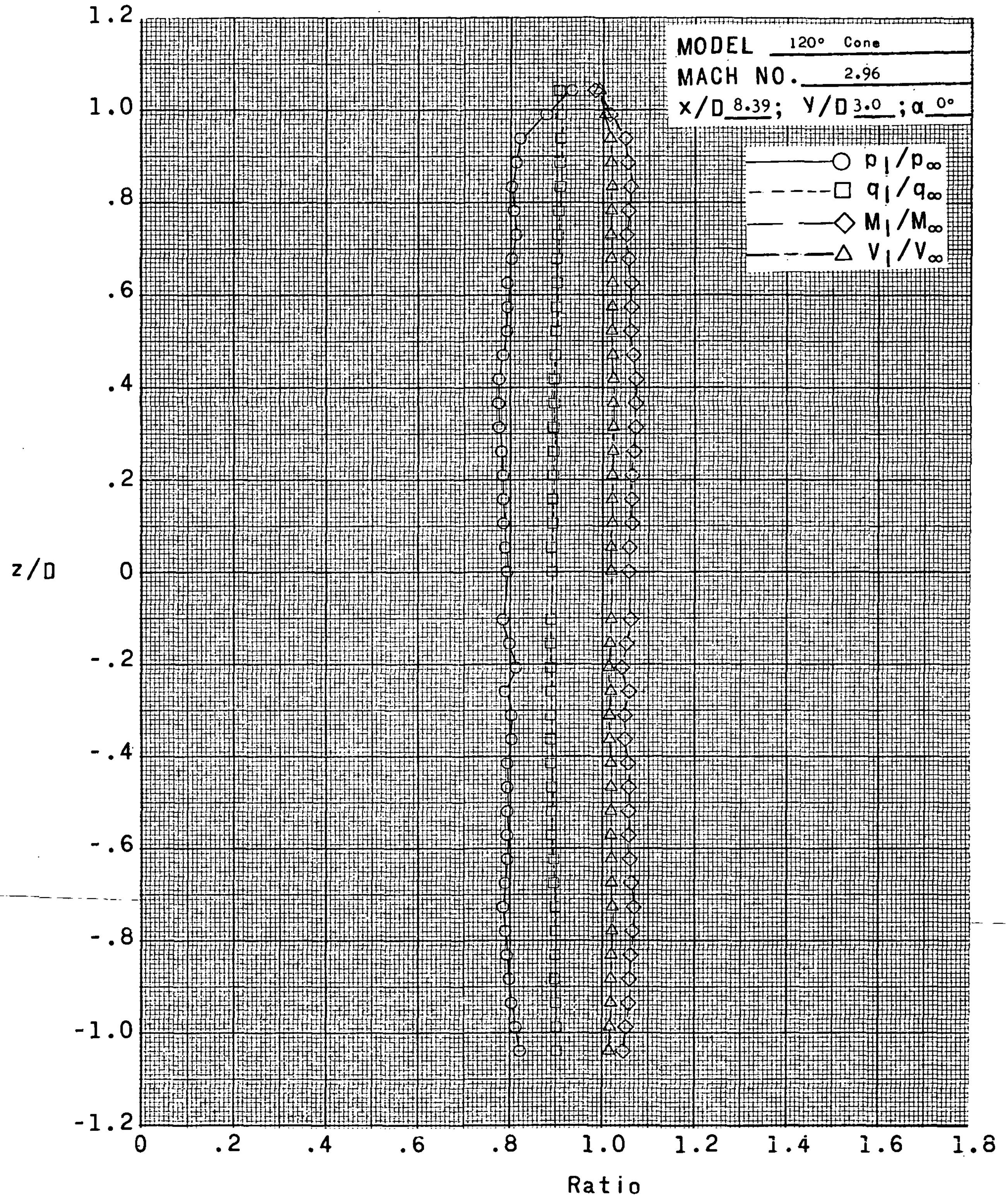
(aa) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^o$.

Figure 8.- Continued.



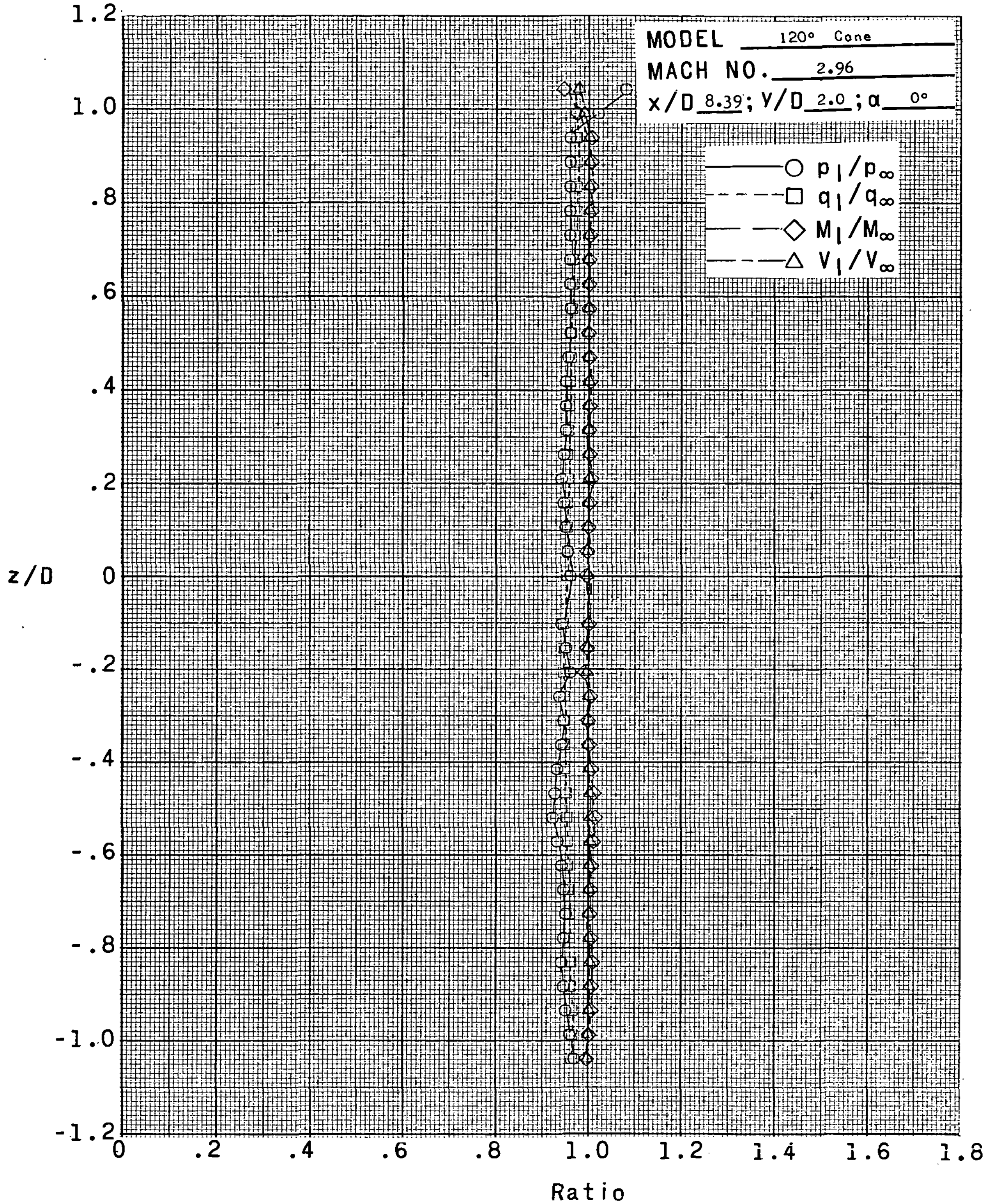
(bb) x/D = 8.0; y/D = 0; α = 0°.

Figure 8.- Continued.



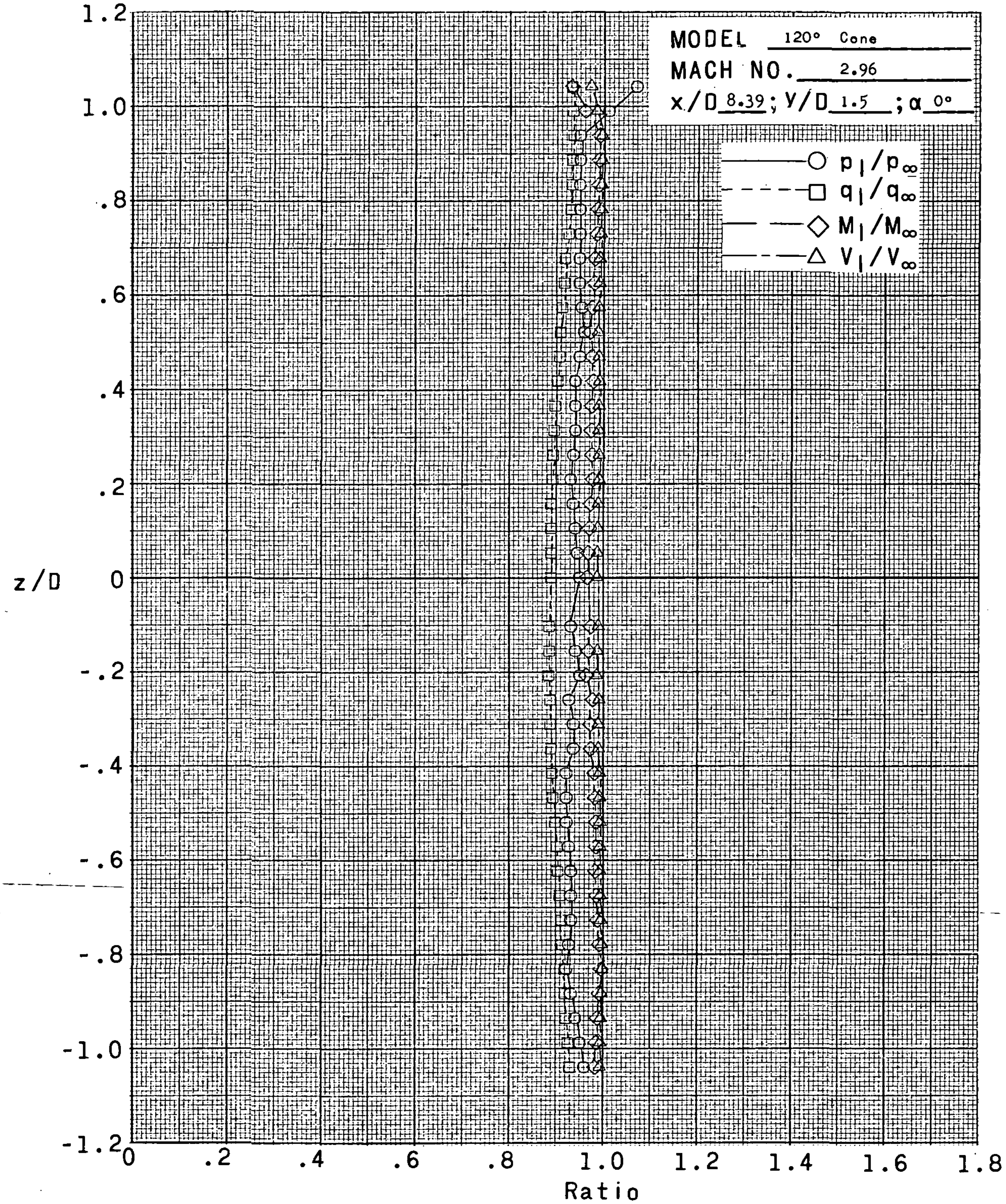
(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^0$.

Figure 8.- Continued.



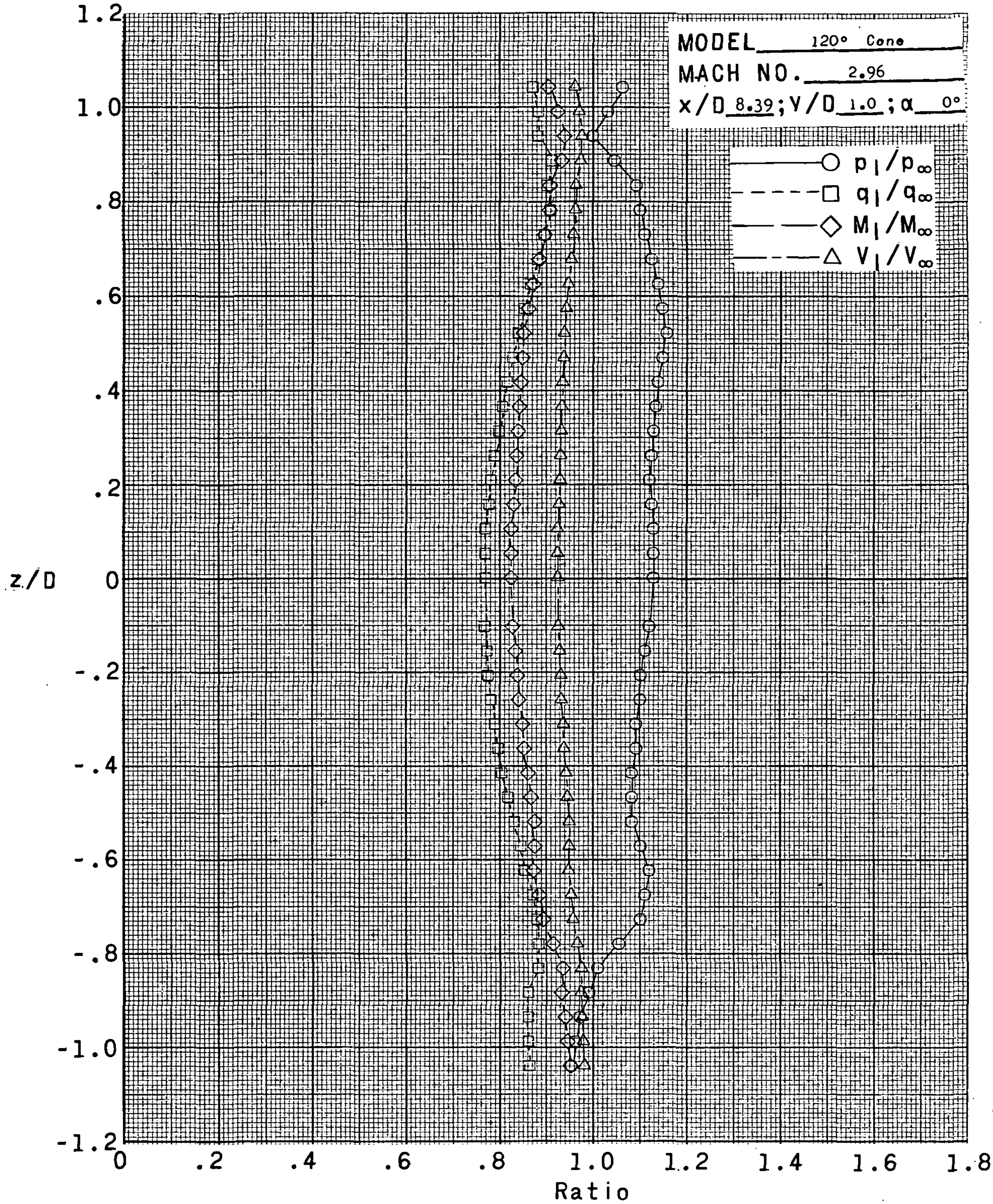
(dd) $x/D = 8.39$; $y/D = 2.0$; $\alpha = 0^{0}$.

Figure 8.- Continued.



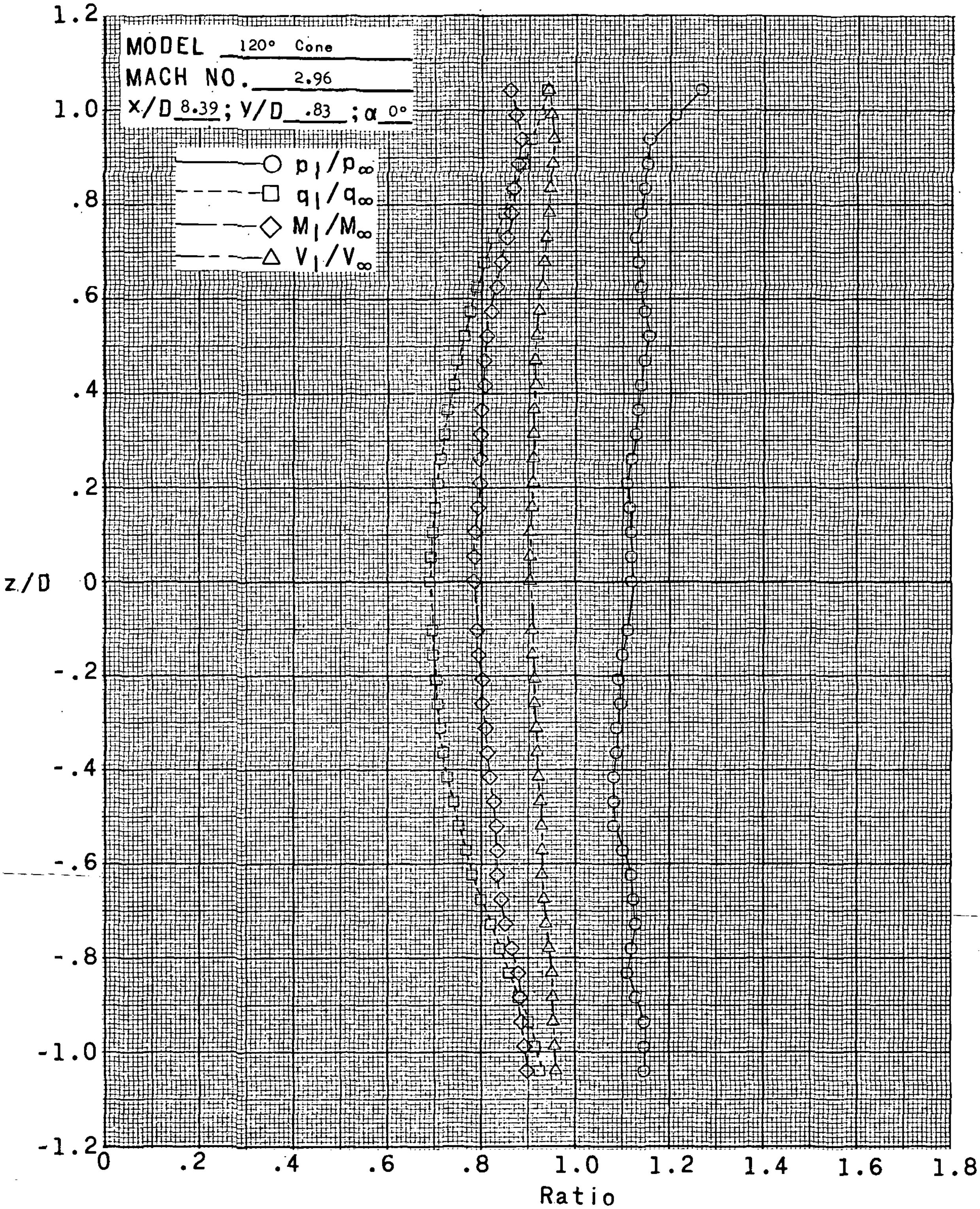
(ee) x/D = 8.39; y/D = 1.5; α = 0°.

Figure 8.- Continued.



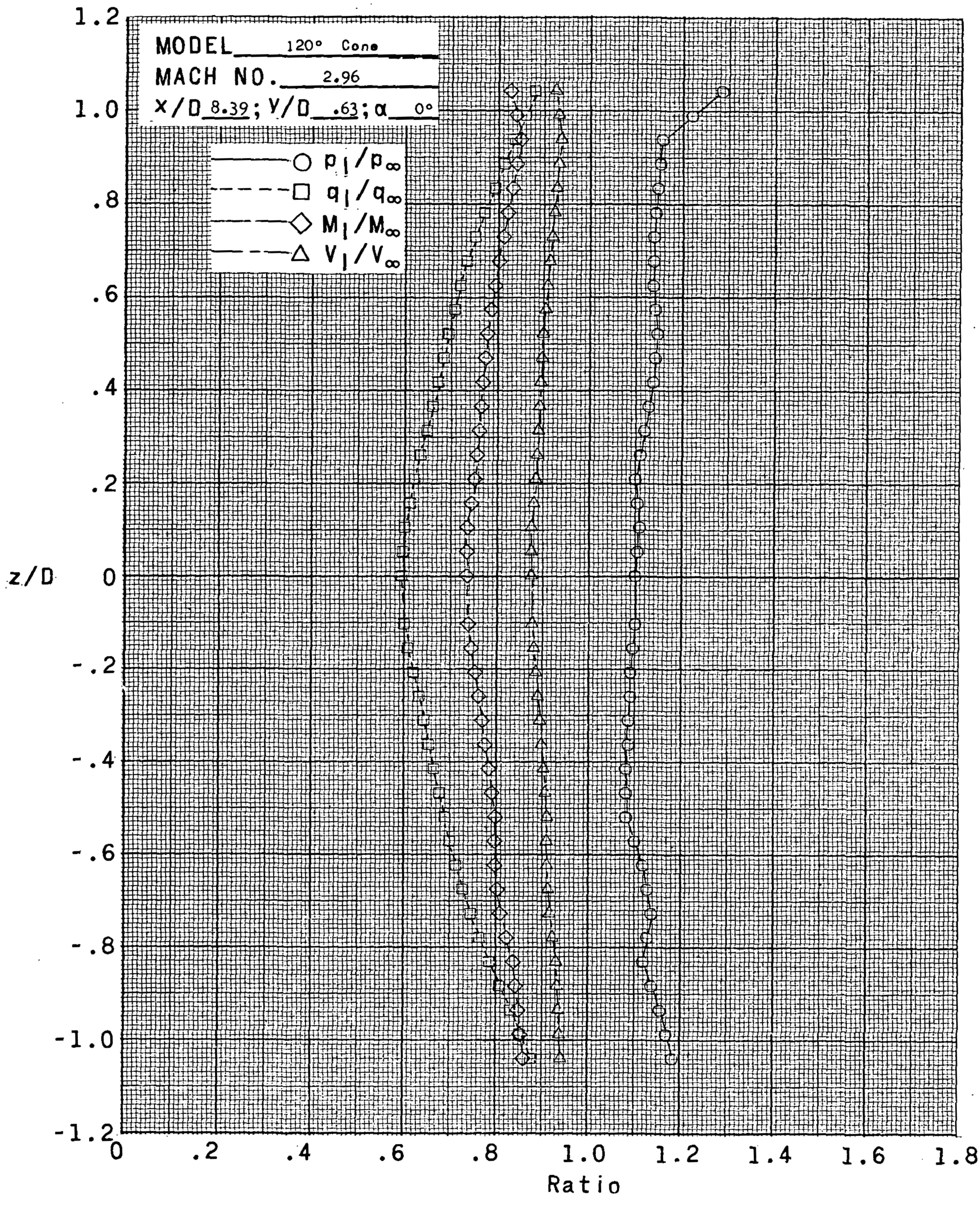
(ff) x/D = 8.39; y/D = 1.0; α = 0°.

Figure 8.- Continued.



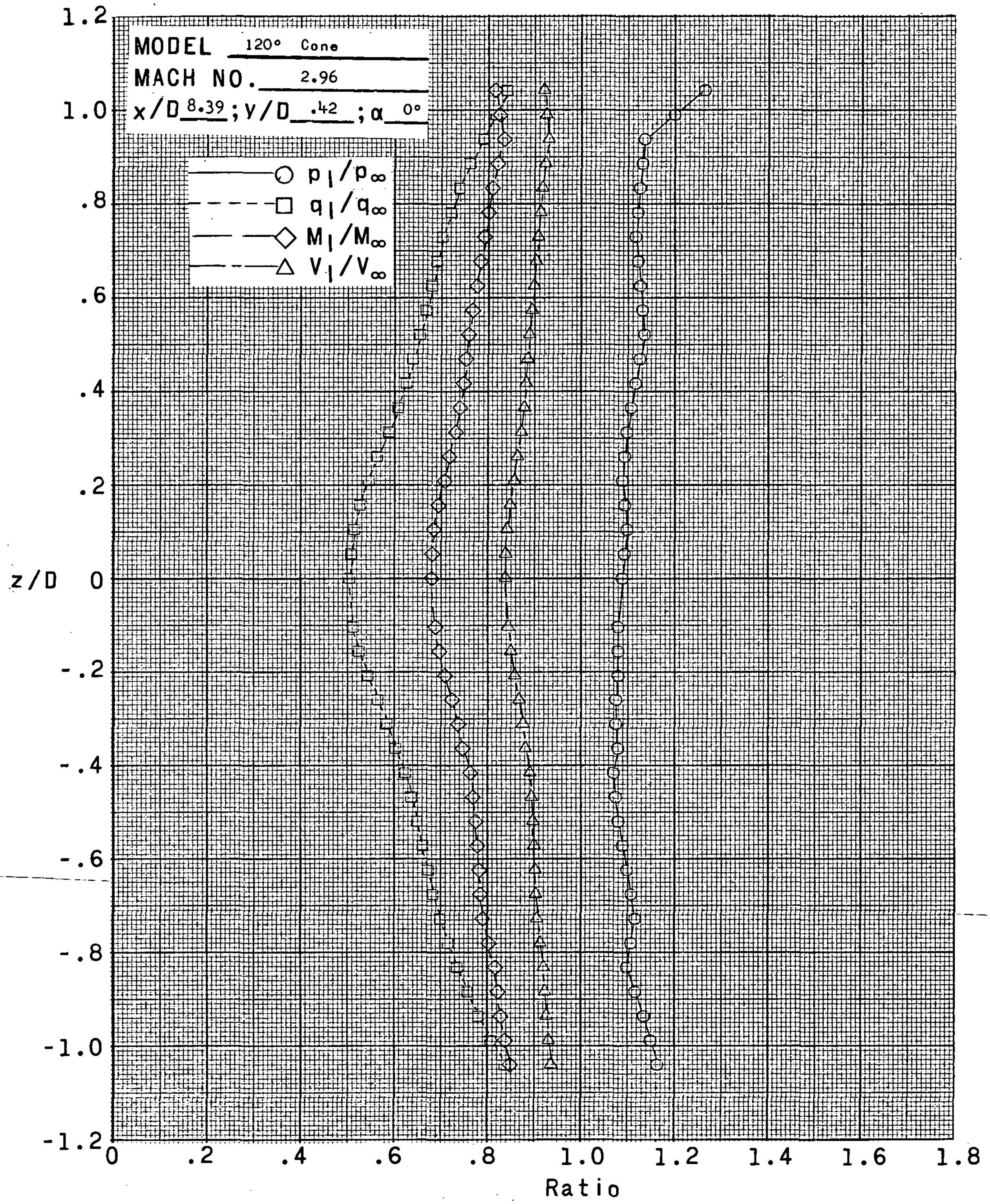
(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 8.- Continued.



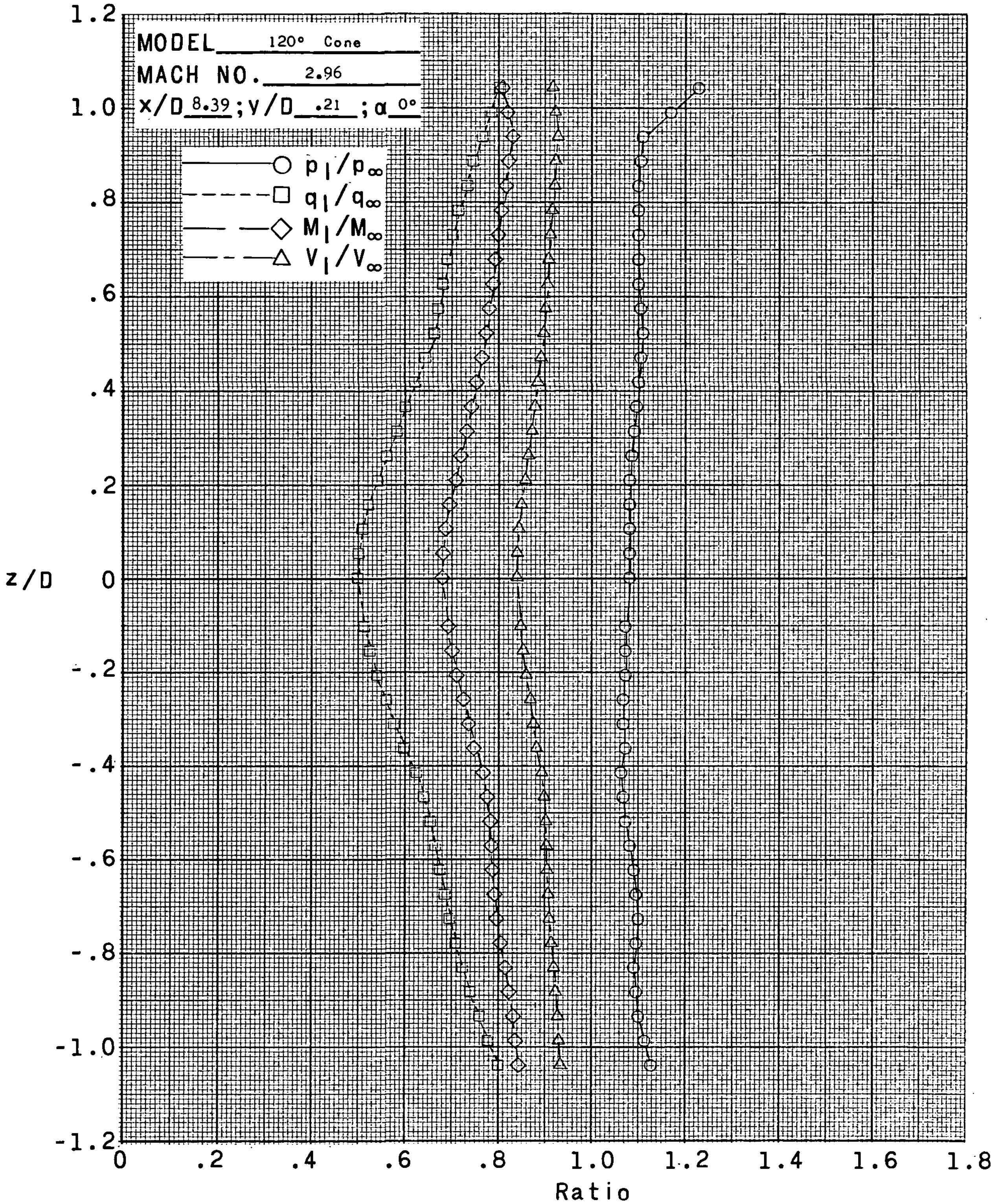
(hh) $x/D = 8.39$; $y/D = 0.63$; $\alpha = 0^o$.

Figure 8.- Continued.



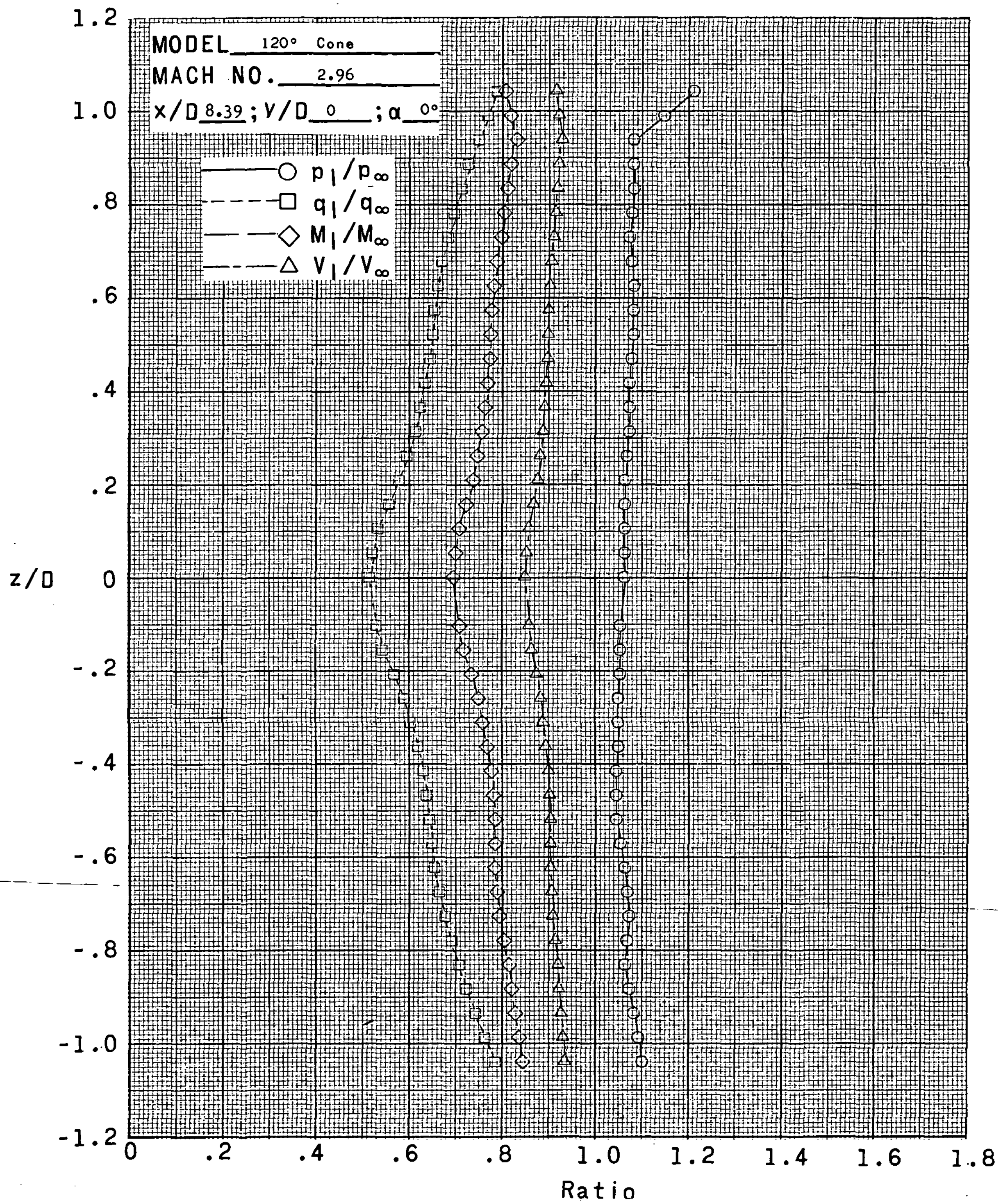
(ii) x/D = 8.39; y/D = 0.42; α = 0°.

Figure 8.- Continued.



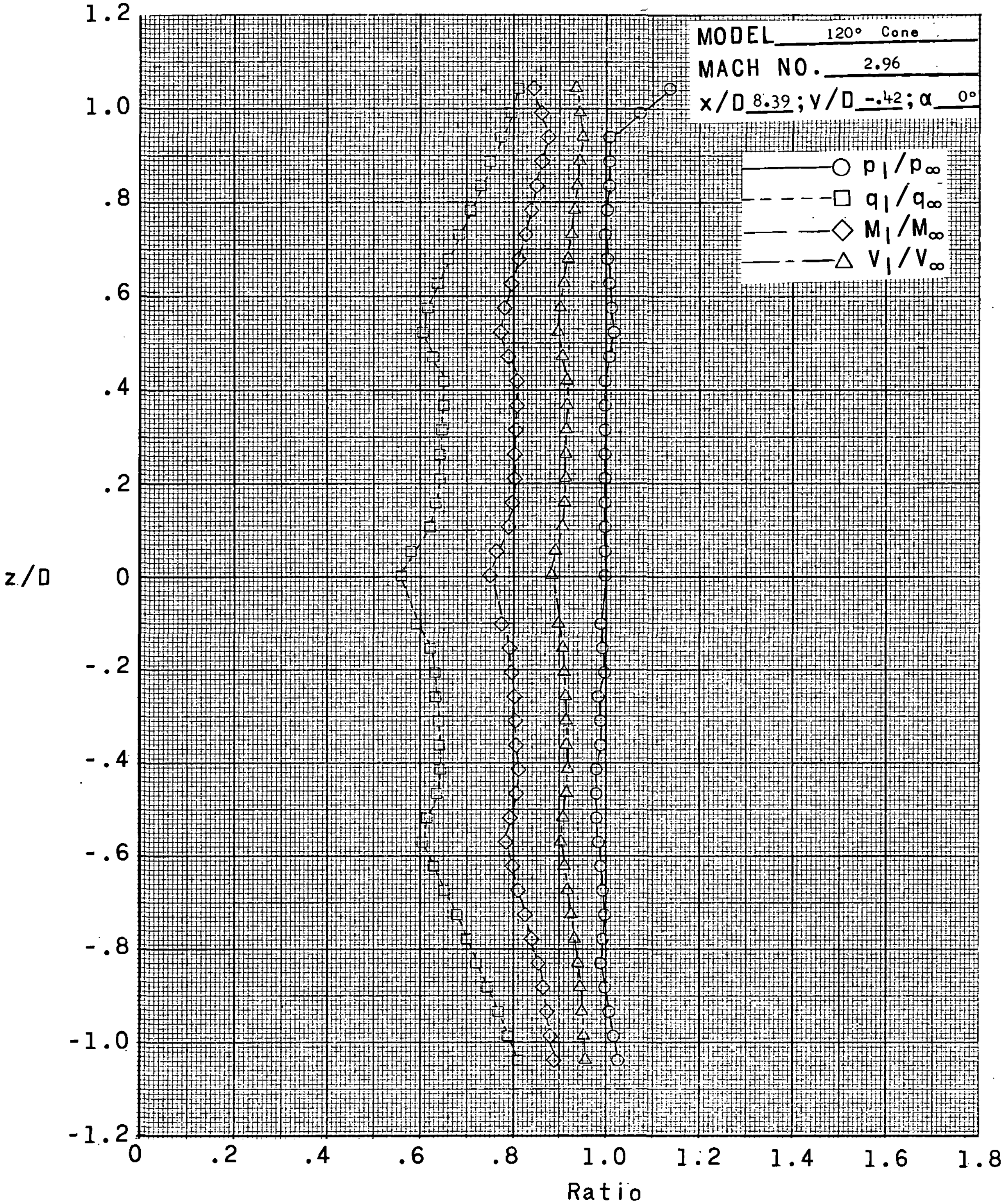
(jj) x/D = 8.39; y/D = 0.21; α = 0°.

Figure 8.- Continued.



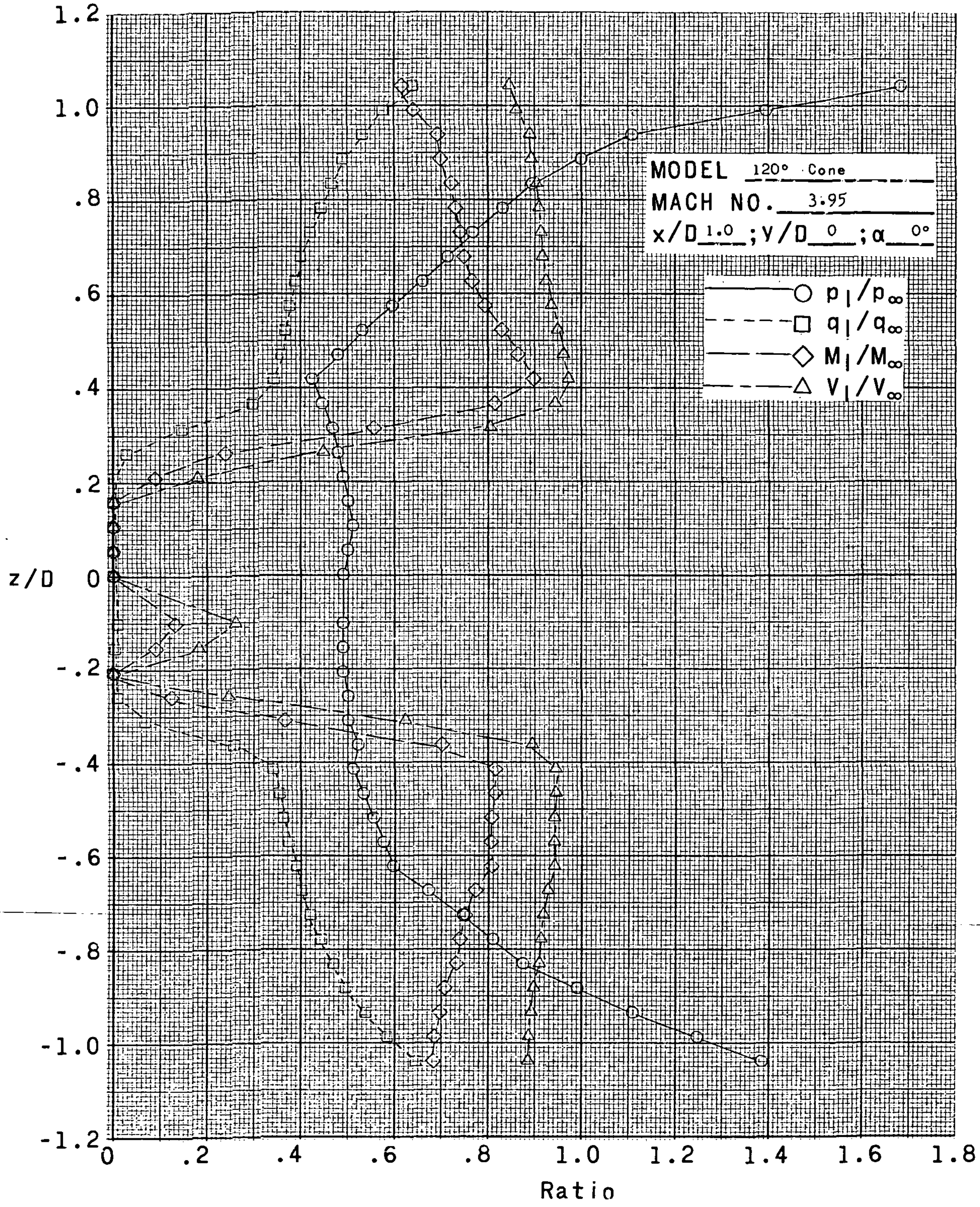
(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^0$.

Figure 8.- Continued.



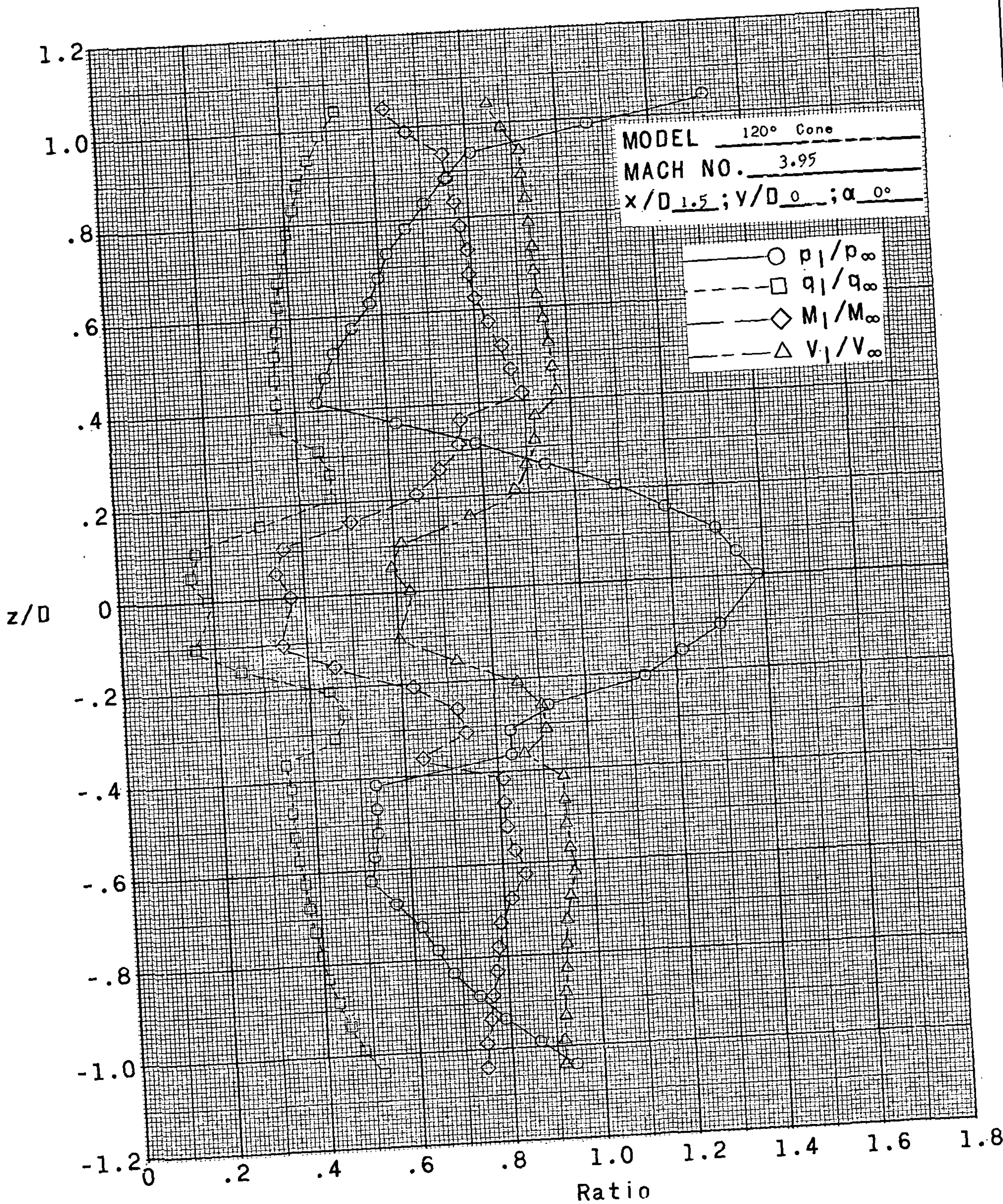
(ll) $x/D = 8.39$; $y/D = -0.42$; $\alpha = 0^{0}$.

Figure 8.- Concluded.



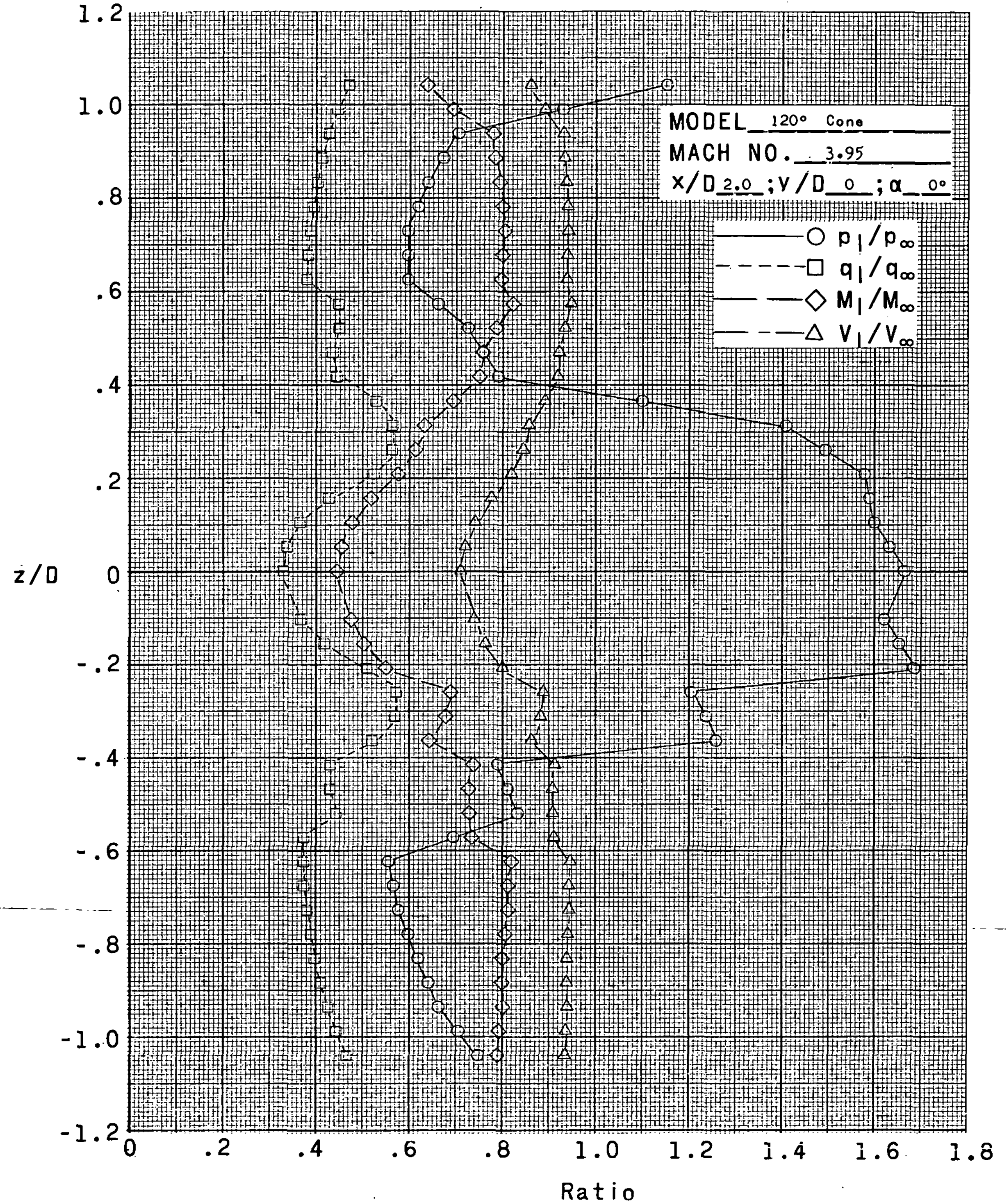
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 9.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D in the wake of a 120°-included-angle cone at a Mach number of 3.95 and a Reynolds number of 1.65×10^6 per foot (5.42×10^6 per meter).



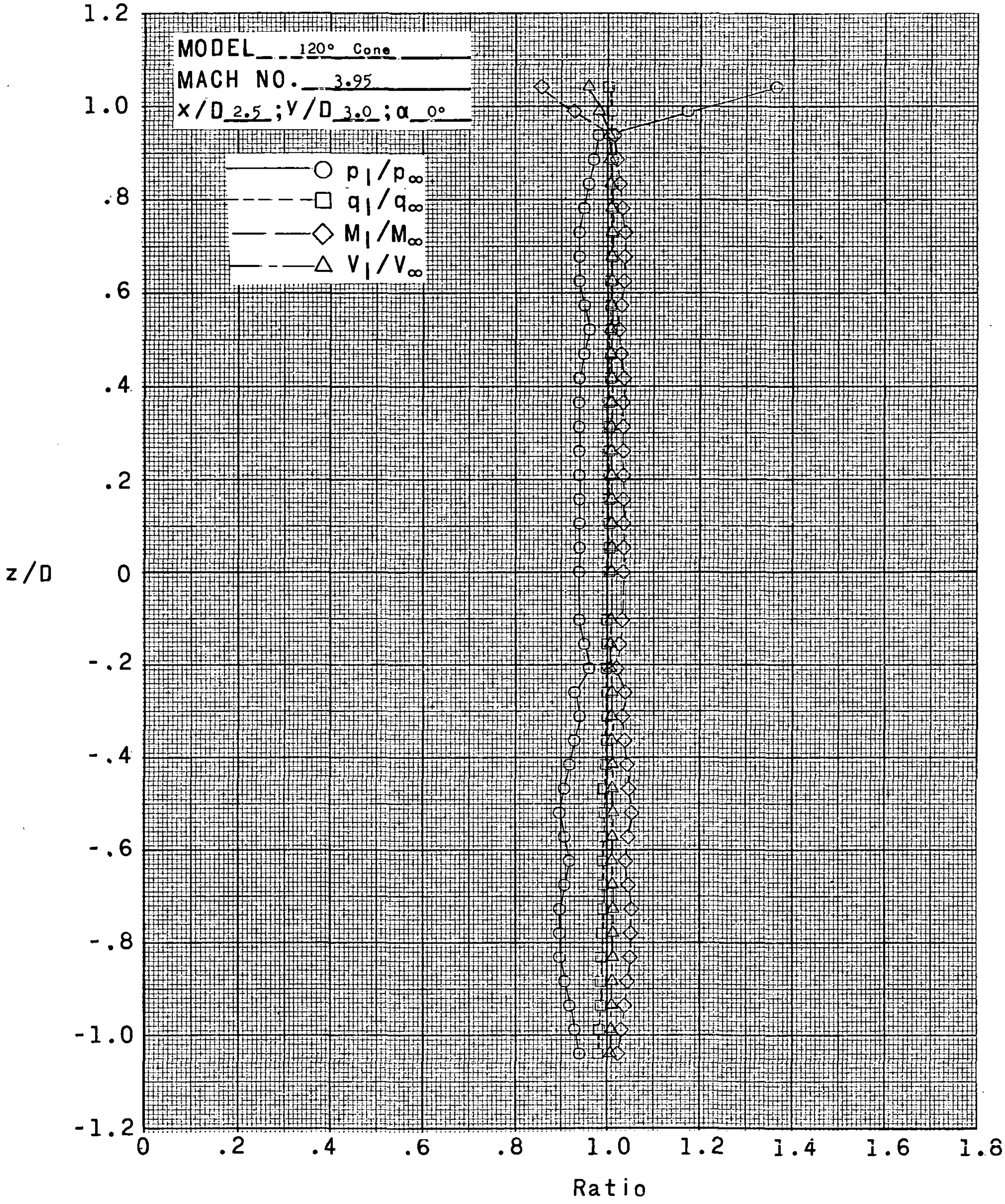
(b) $x/D = 1.50$; $y/D = 0$; $\alpha = 0^{0}$.

Figure 9.- Continued.



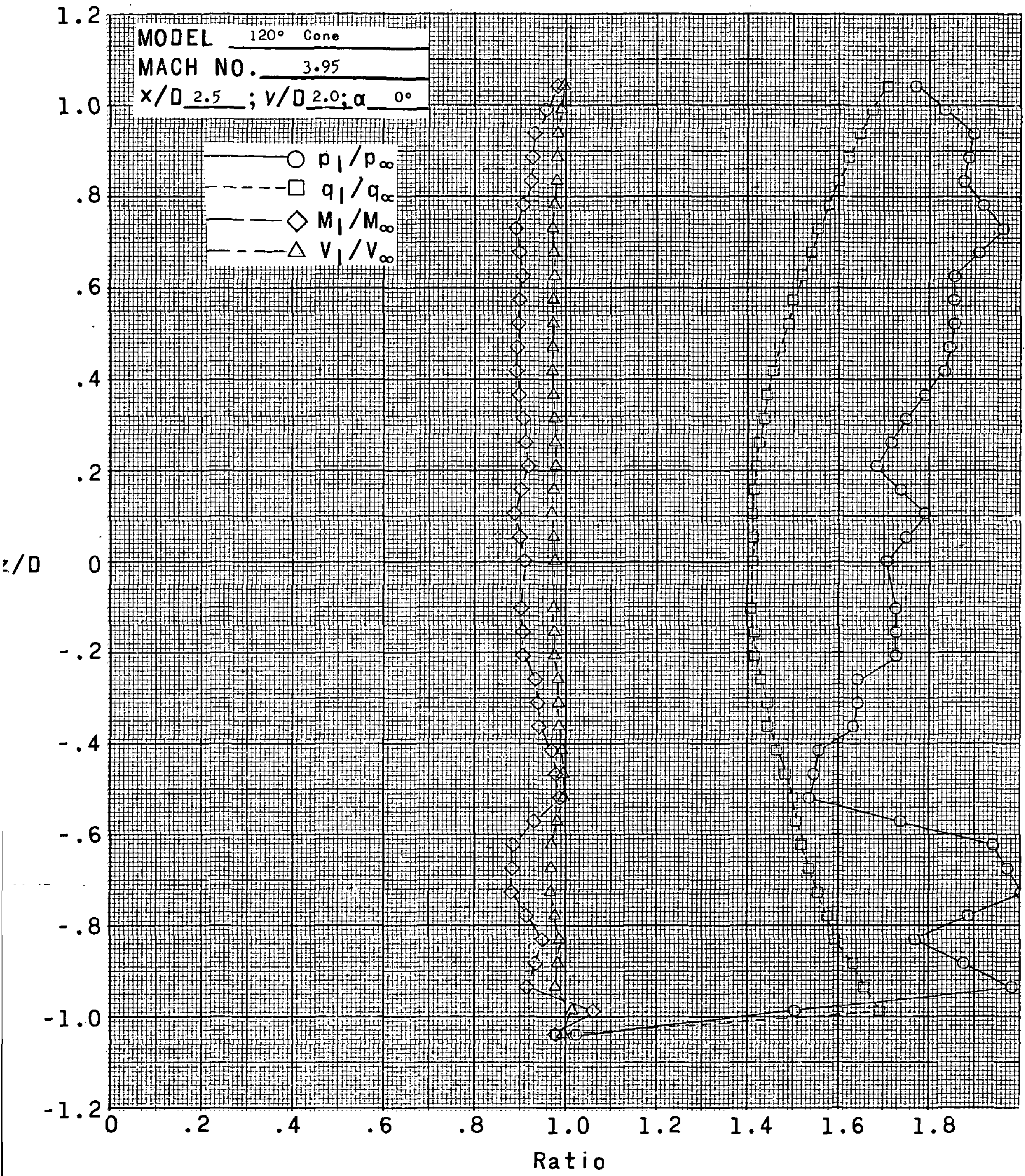
(c) x/D = 2.0; y/D = 0; α = 0°.

Figure 9.- Continued.



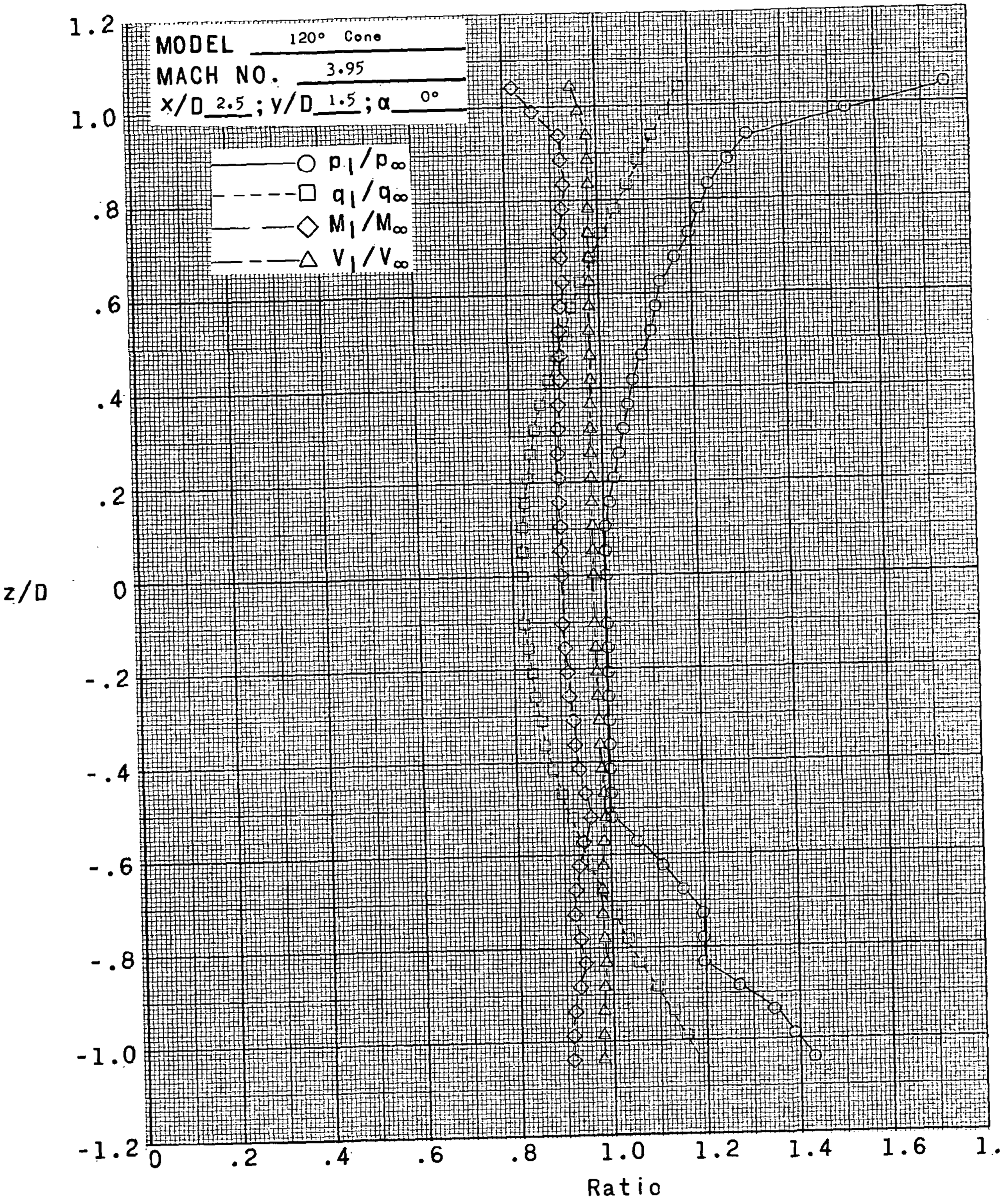
(d) $x/D = 2.5$; $y/D = 3.0$; $\alpha = 0^0$.

Figure 9.- Continued.



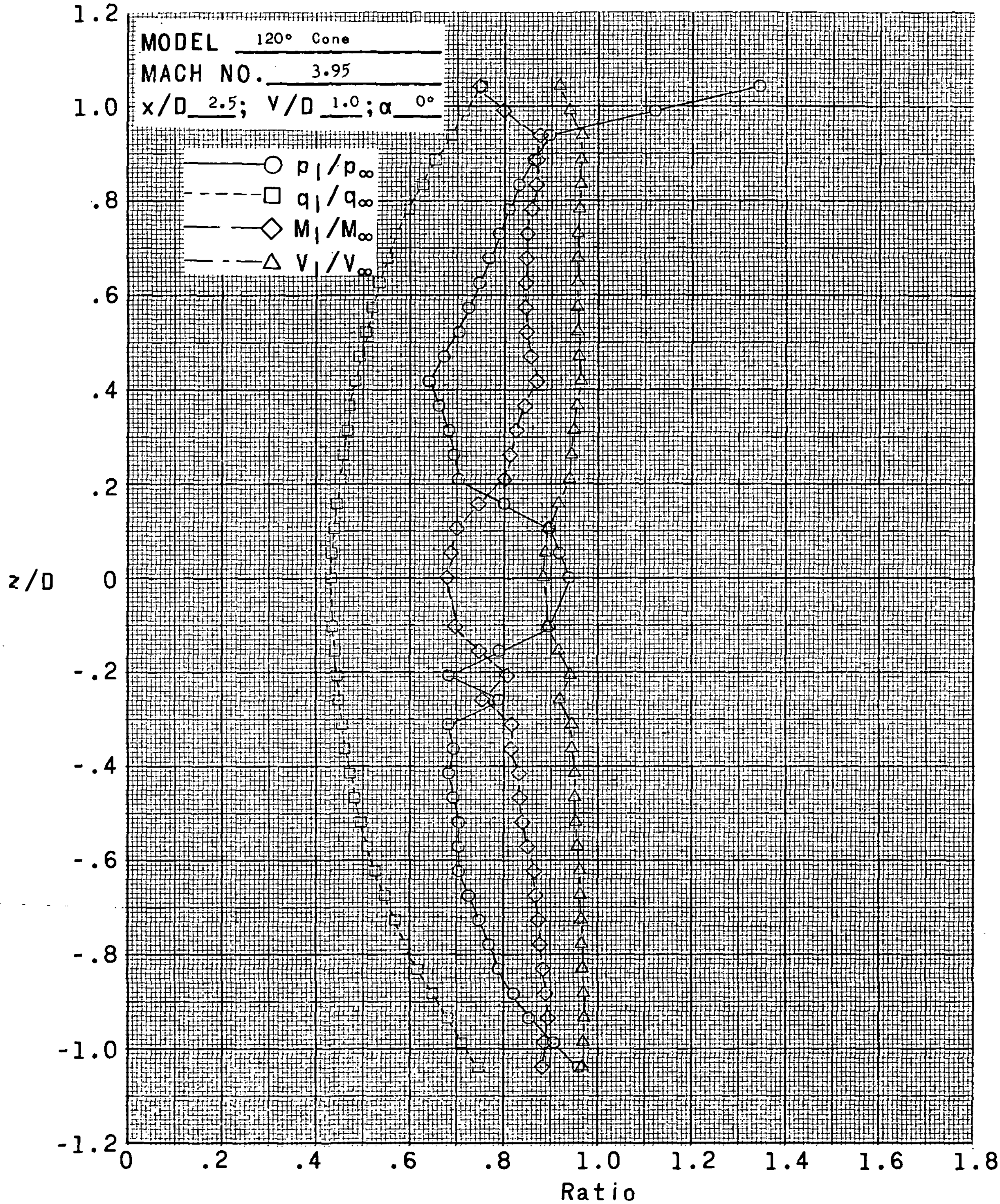
(e) x/D = 2.5, y/D = 2.0; α = 0°.

Figure 9.- Continued.



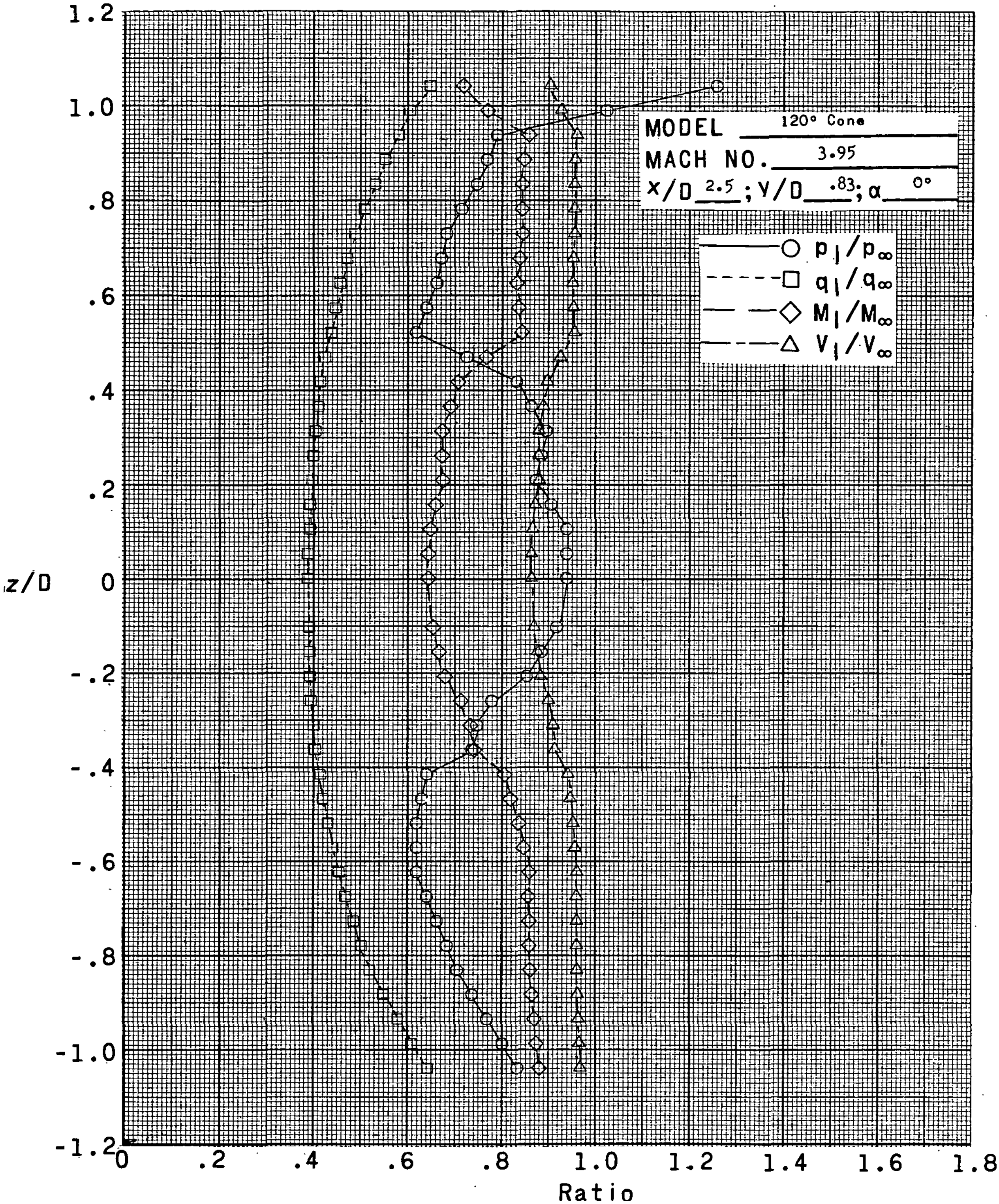
(f) $x/D = 2.5$; $y/D = 1.5$; $\alpha = 0^{\circ}$.

Figure 9.- Continued.



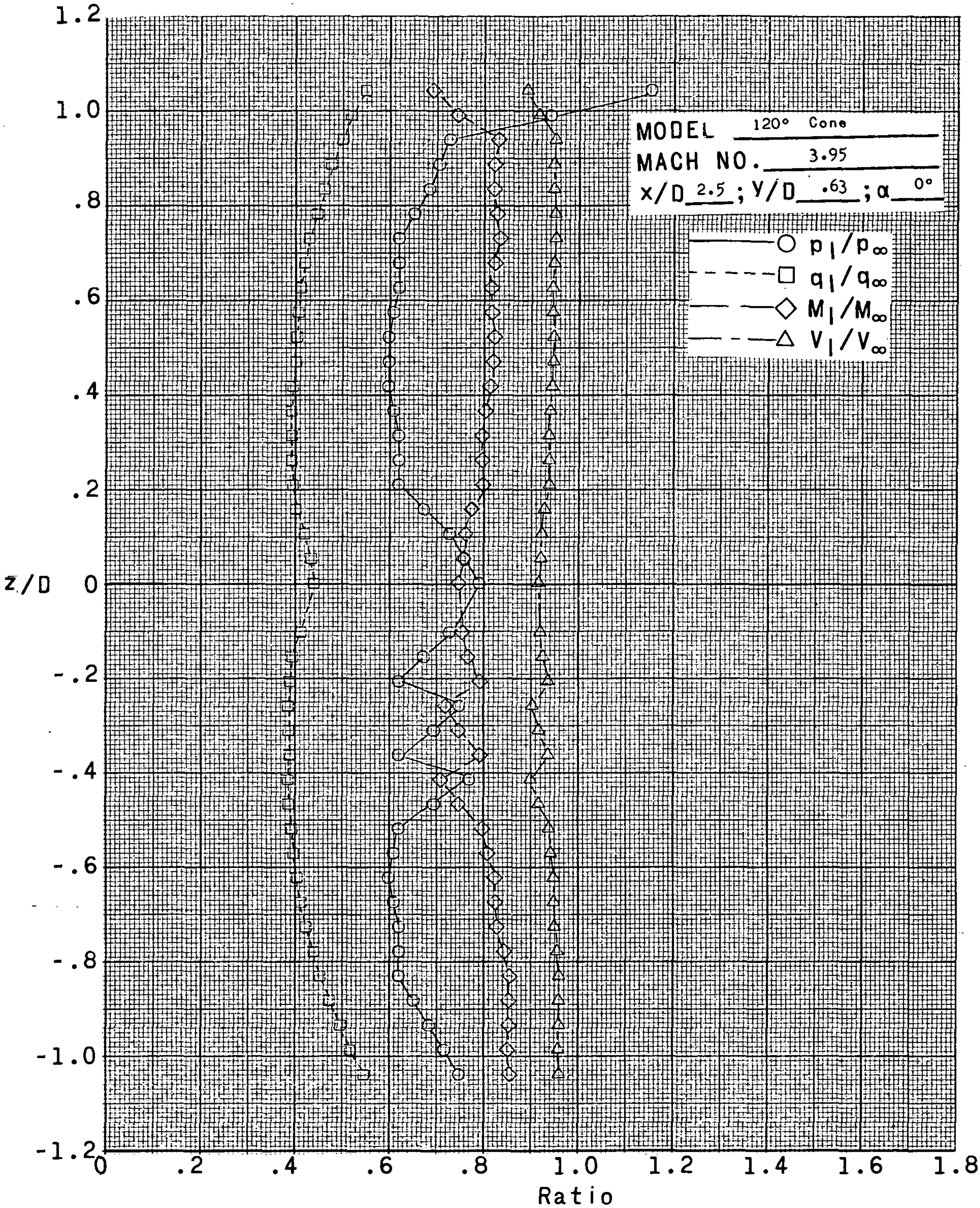
(g) $x/D = 2.5$; $y/D = 1.0$; $\alpha = 0°$.

Figure 9.- Continued.



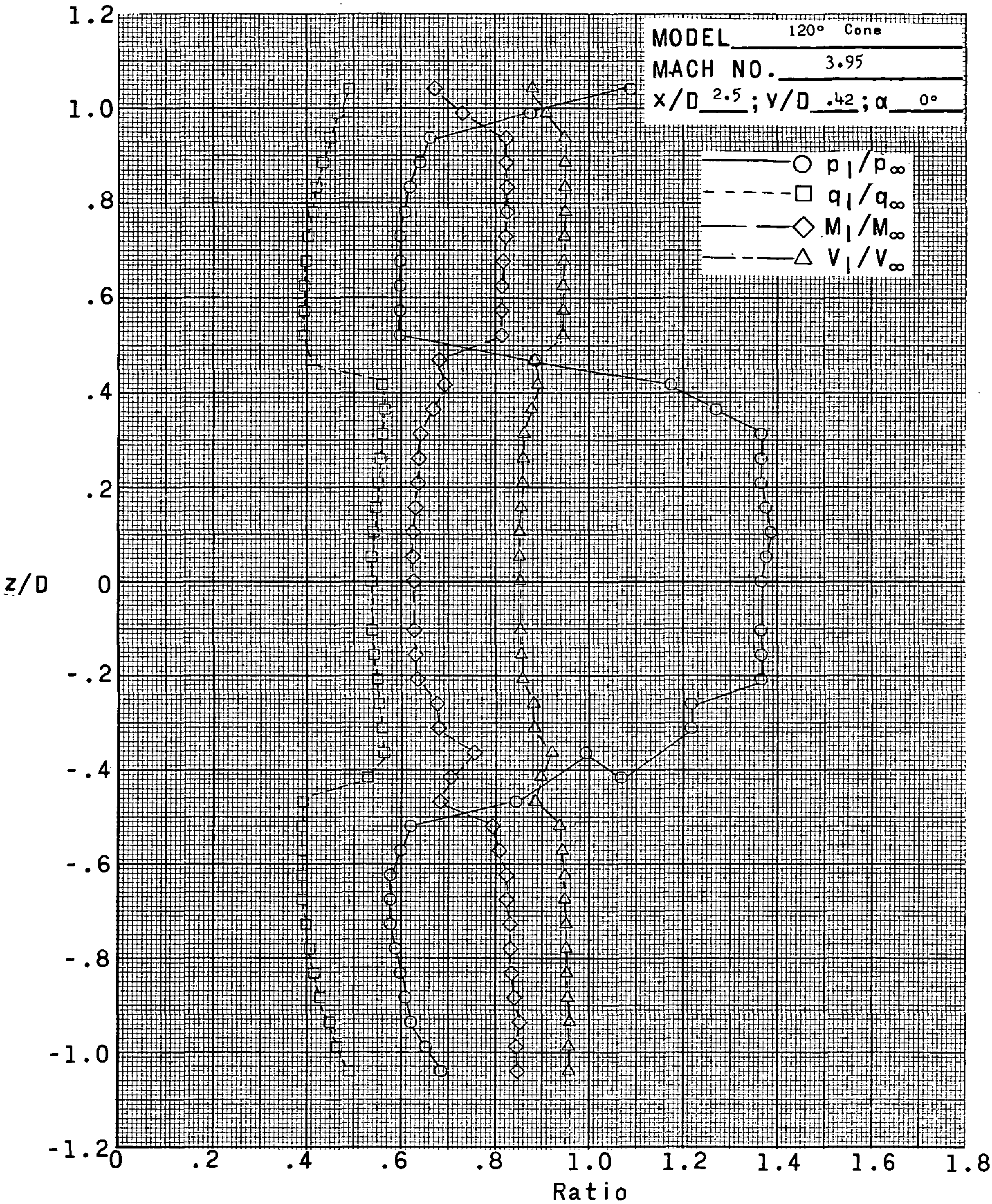
(h) x/D = 2.5; y/D = 0.83; α = 0°.

Figure 9.- Continued.



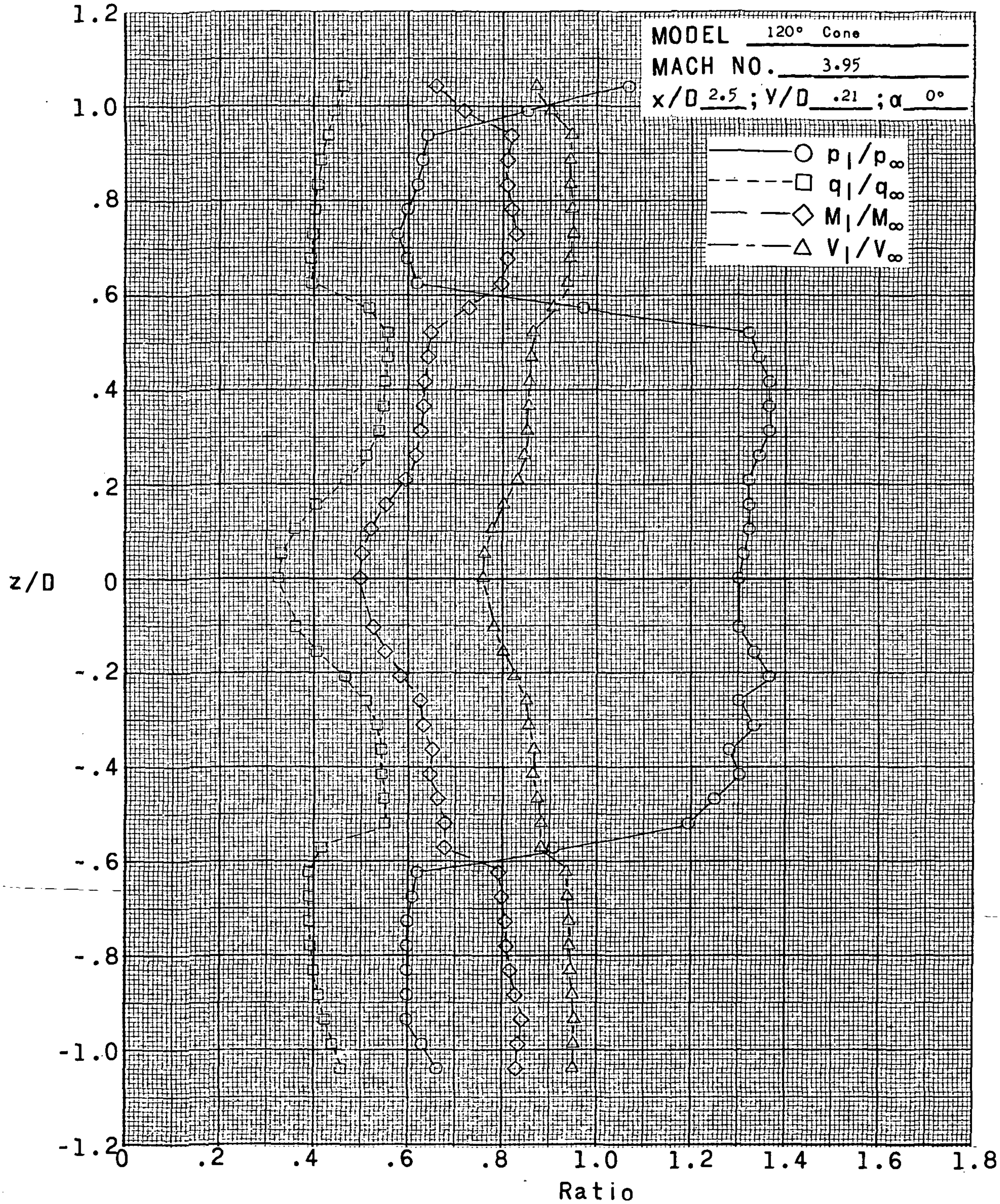
(i) $x/D = 2.5$; $y/D = 0.63$; $\alpha = 0^{0}$.

Figure 9.- Continued.



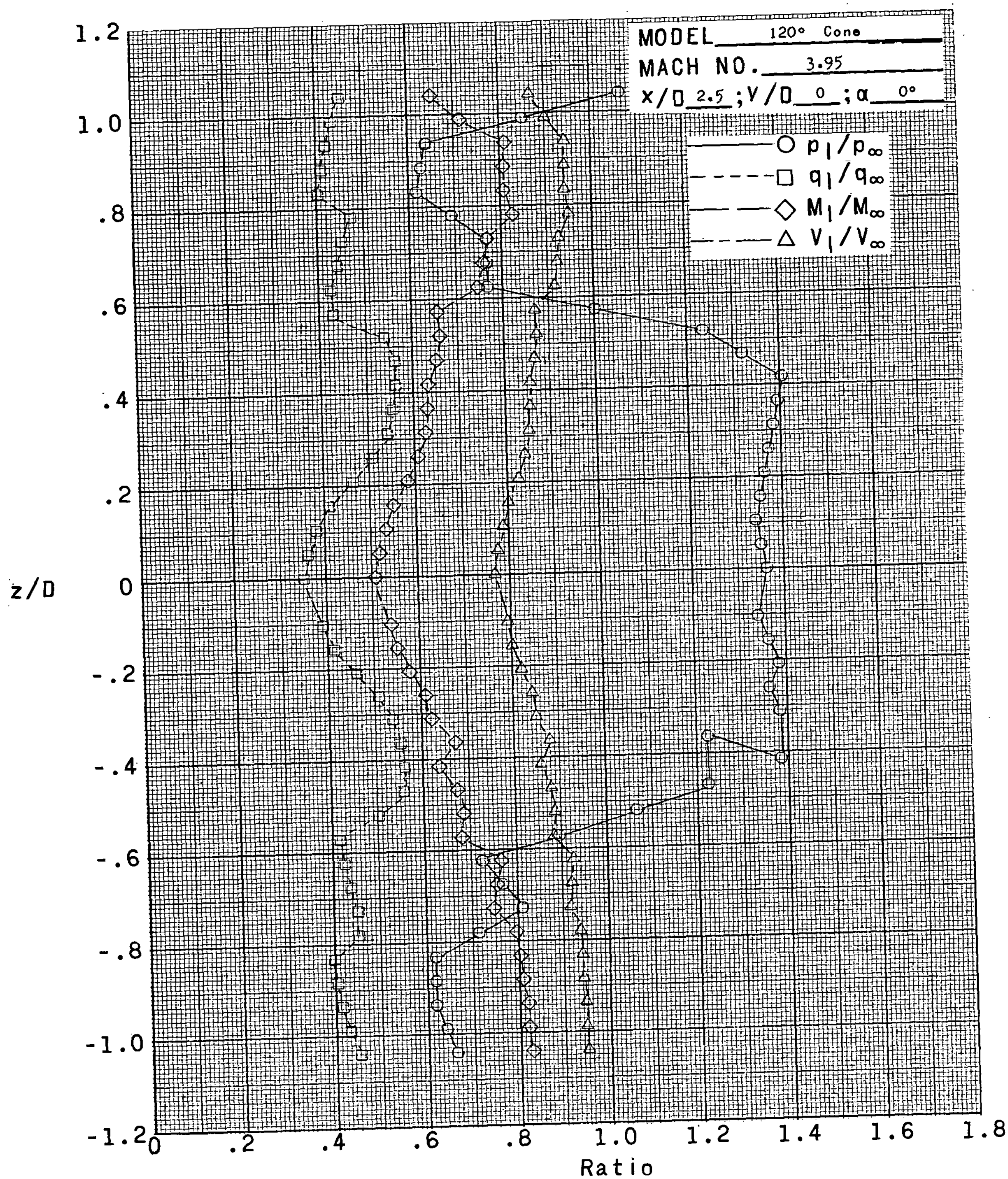
(j) x/D = 2.5; y/D = 0.42; α = 0°.

Figure 9.- Continued.



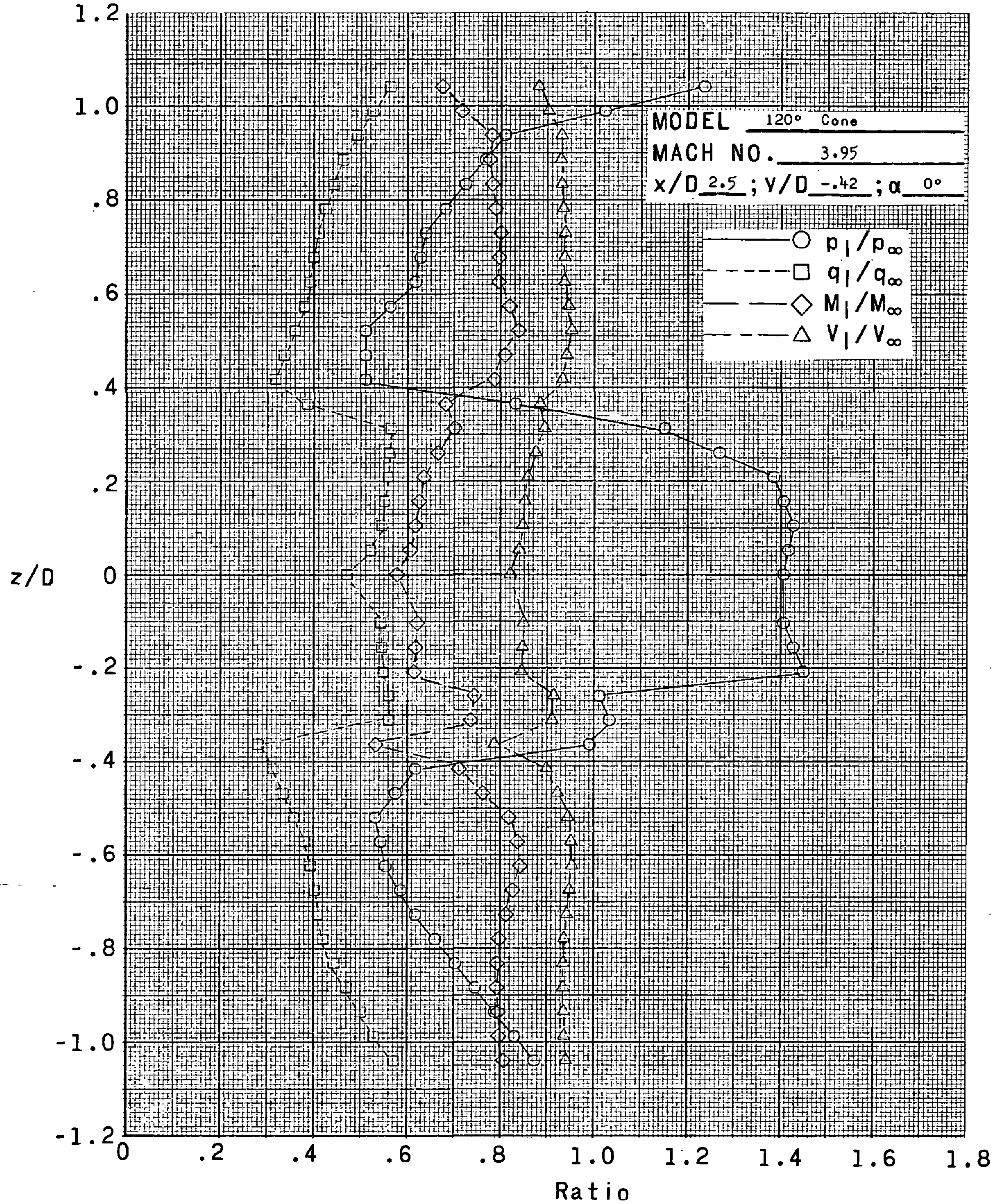
(k) x/D = 2.5; y/D = 0.21; α = 0°.

Figure 9.- Continued.



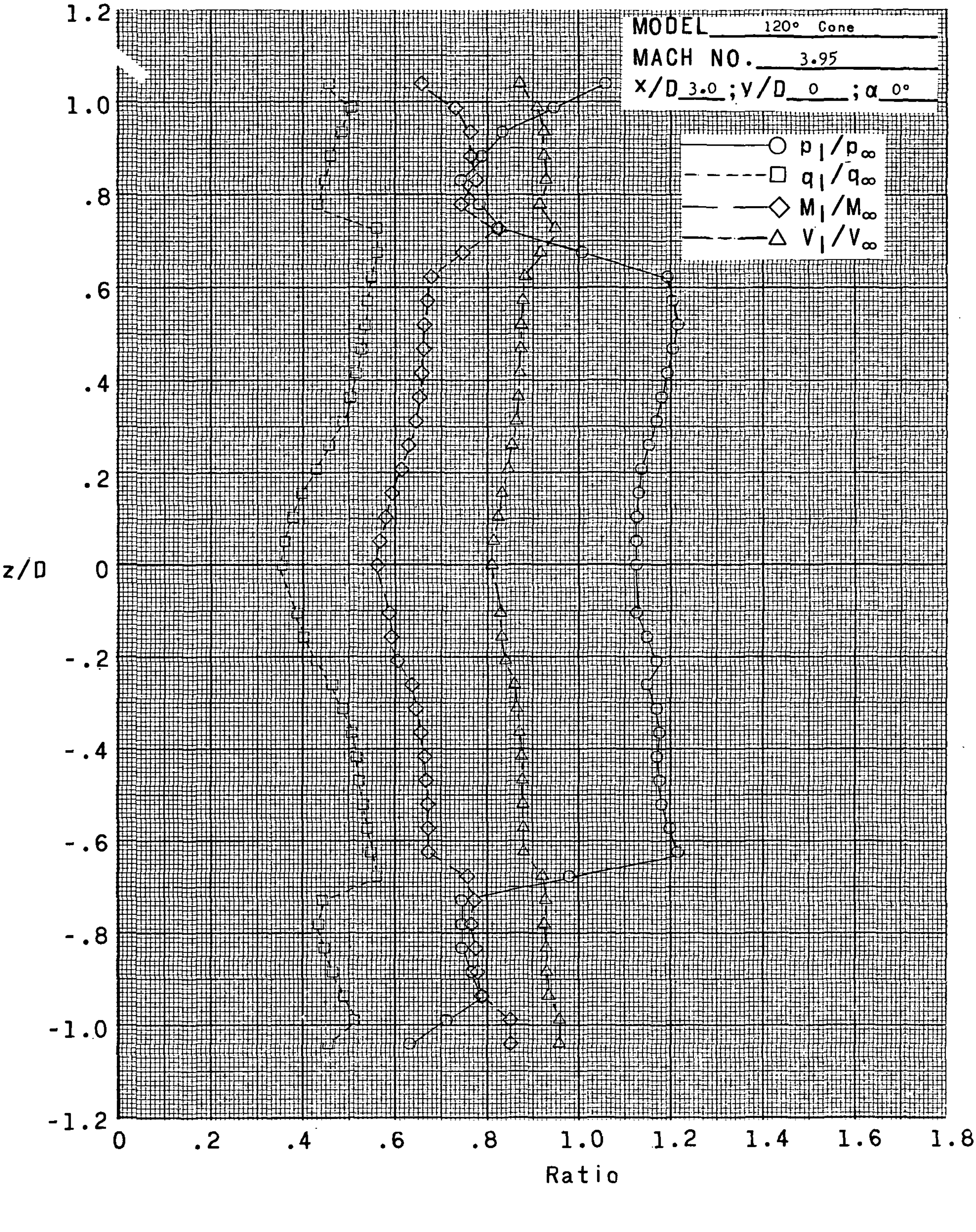
(l) $x/D = 2.5$; $y/D = 0$; $\alpha = 0^0$.

Figure 9.- Continued.



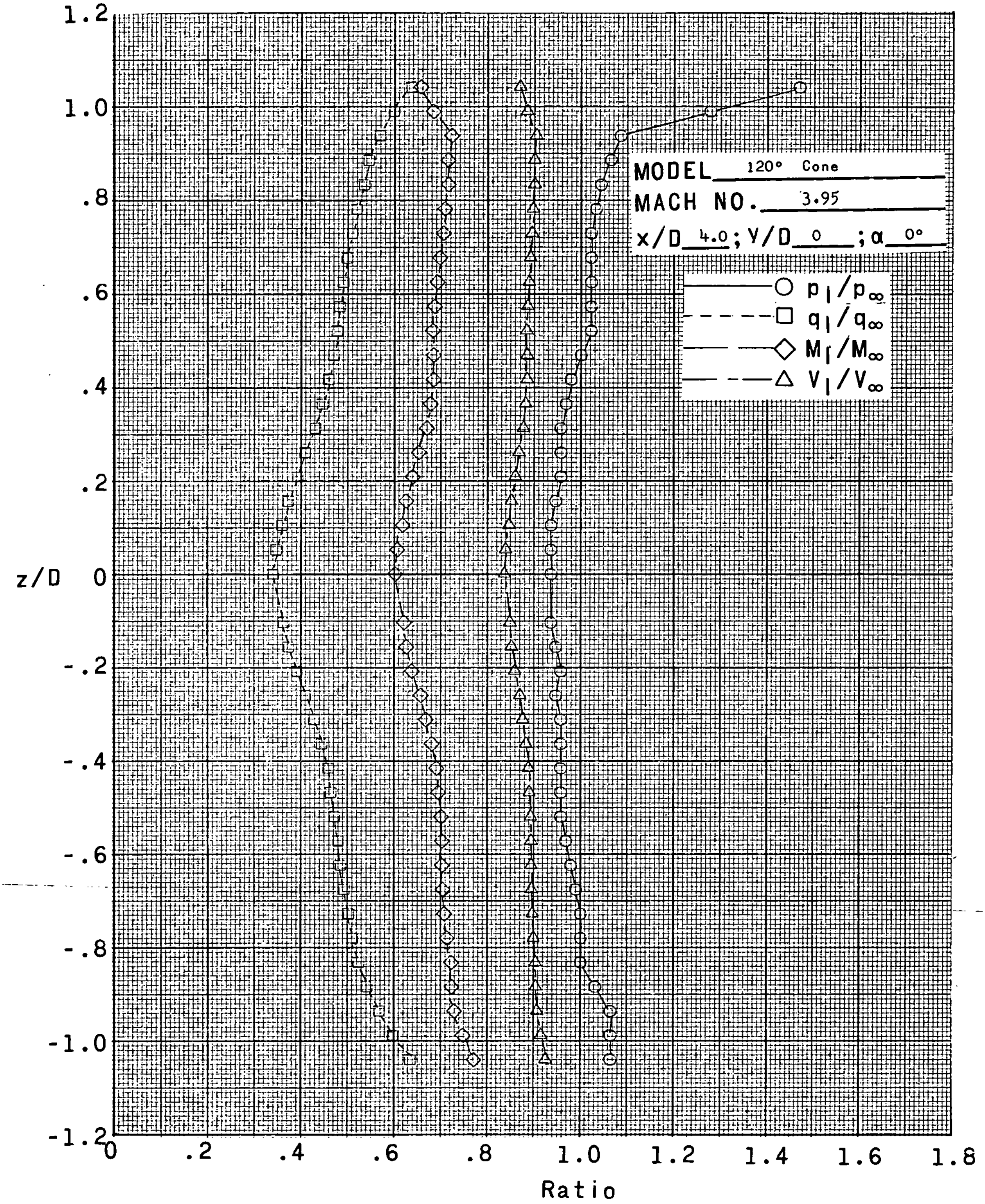
(m) x/D = 2.5; y/D = -0.42; α = 0°.

Figure 9.- Continued.



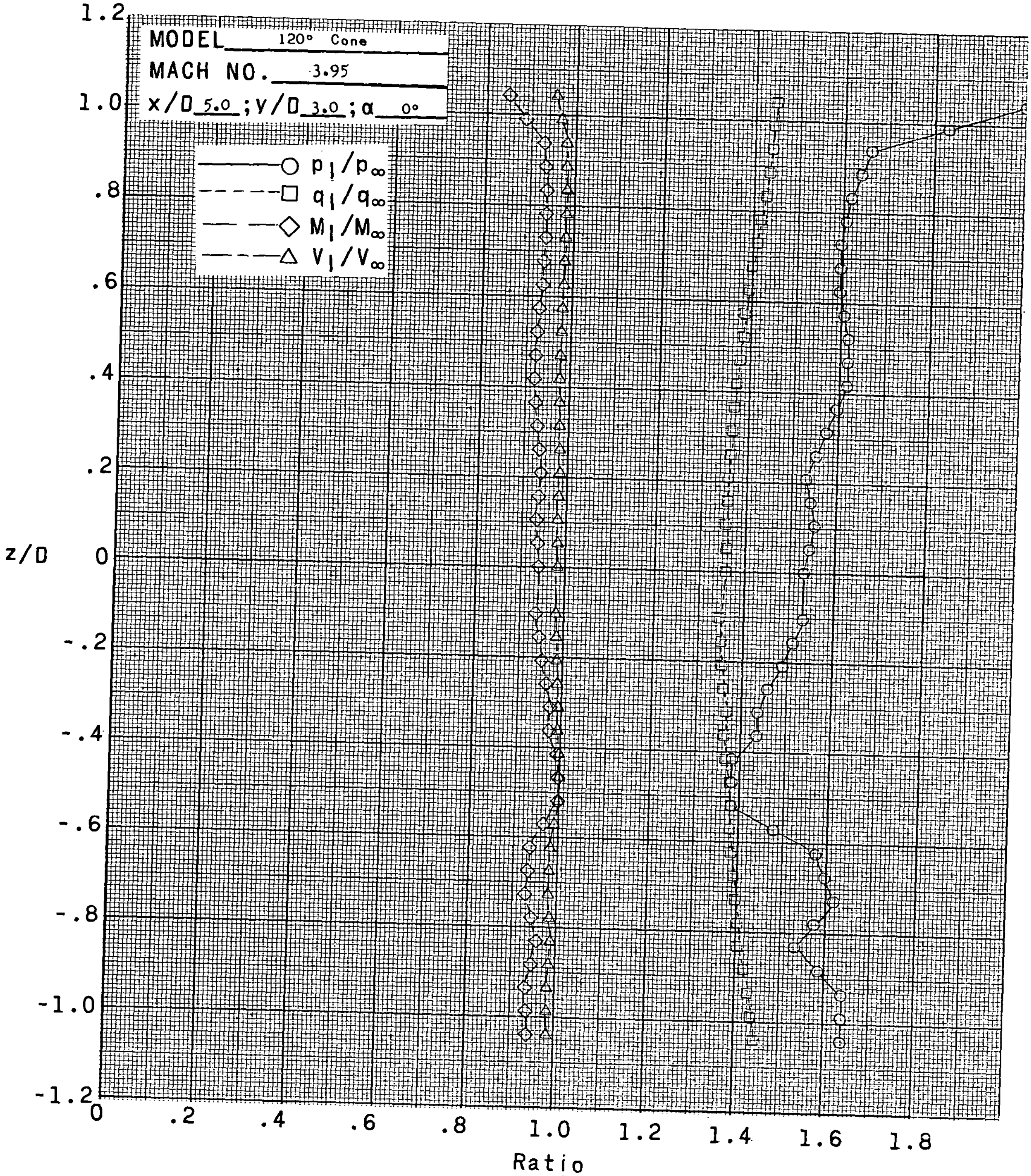
(n) x/D = 3.0; y/D = 0; α = 0°.

Figure 9.- Continued.



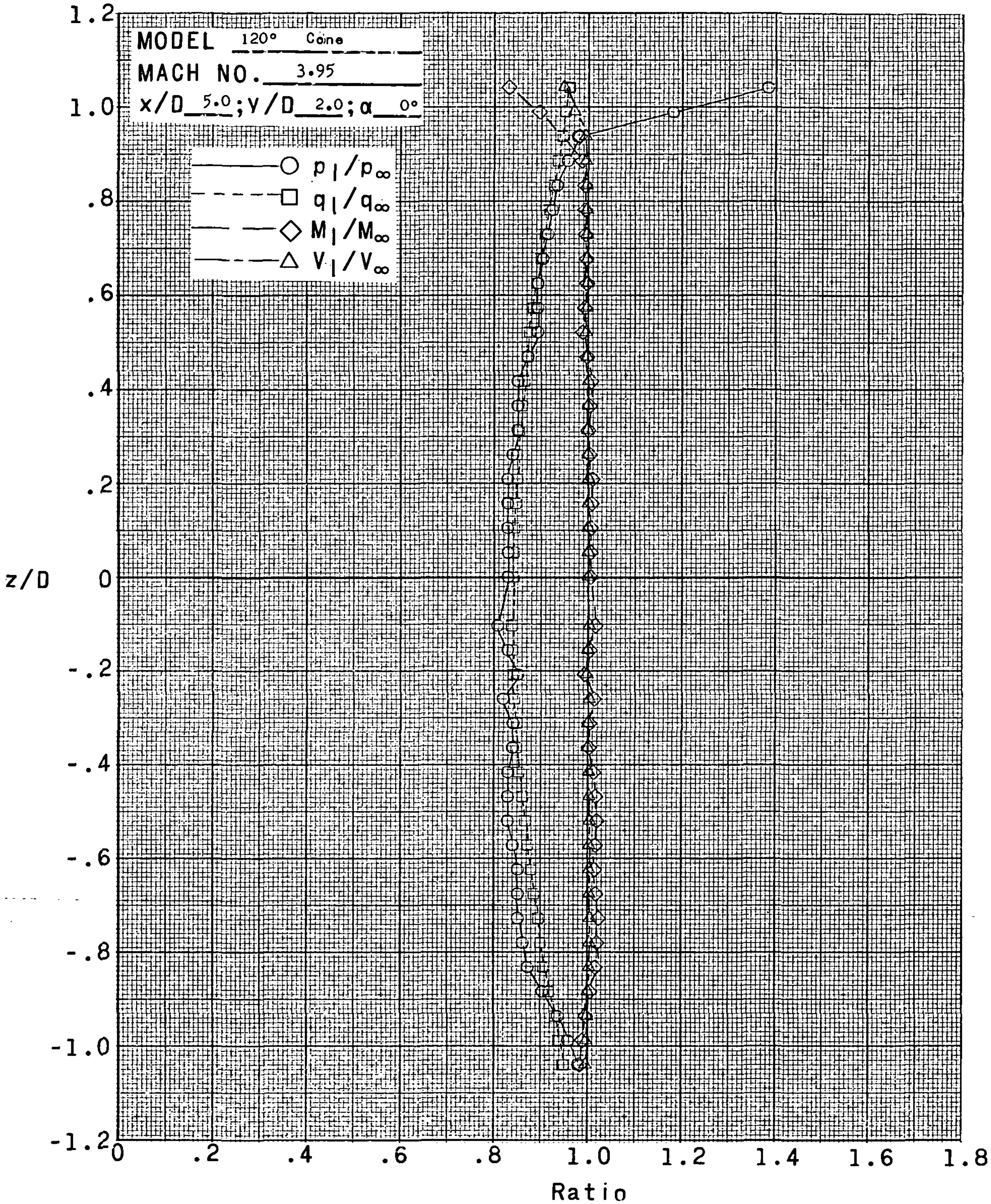
(o) x/D = 4.0; y/D = 0; α = 0°.

Figure 9.- Continued.



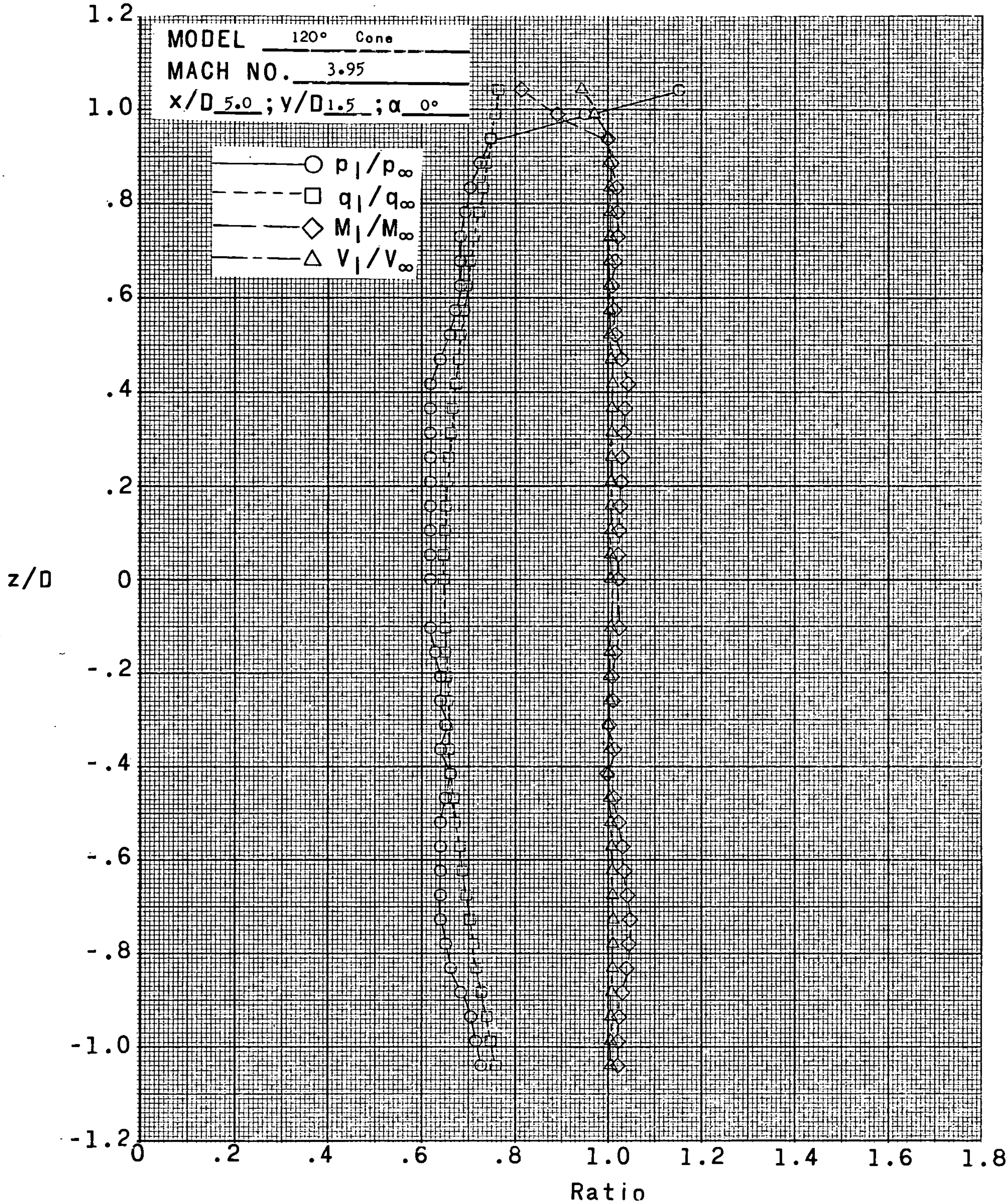
(p) x/D = 5.0; y/D = 3.0; α = 0°.

Figure 9.- Continued.



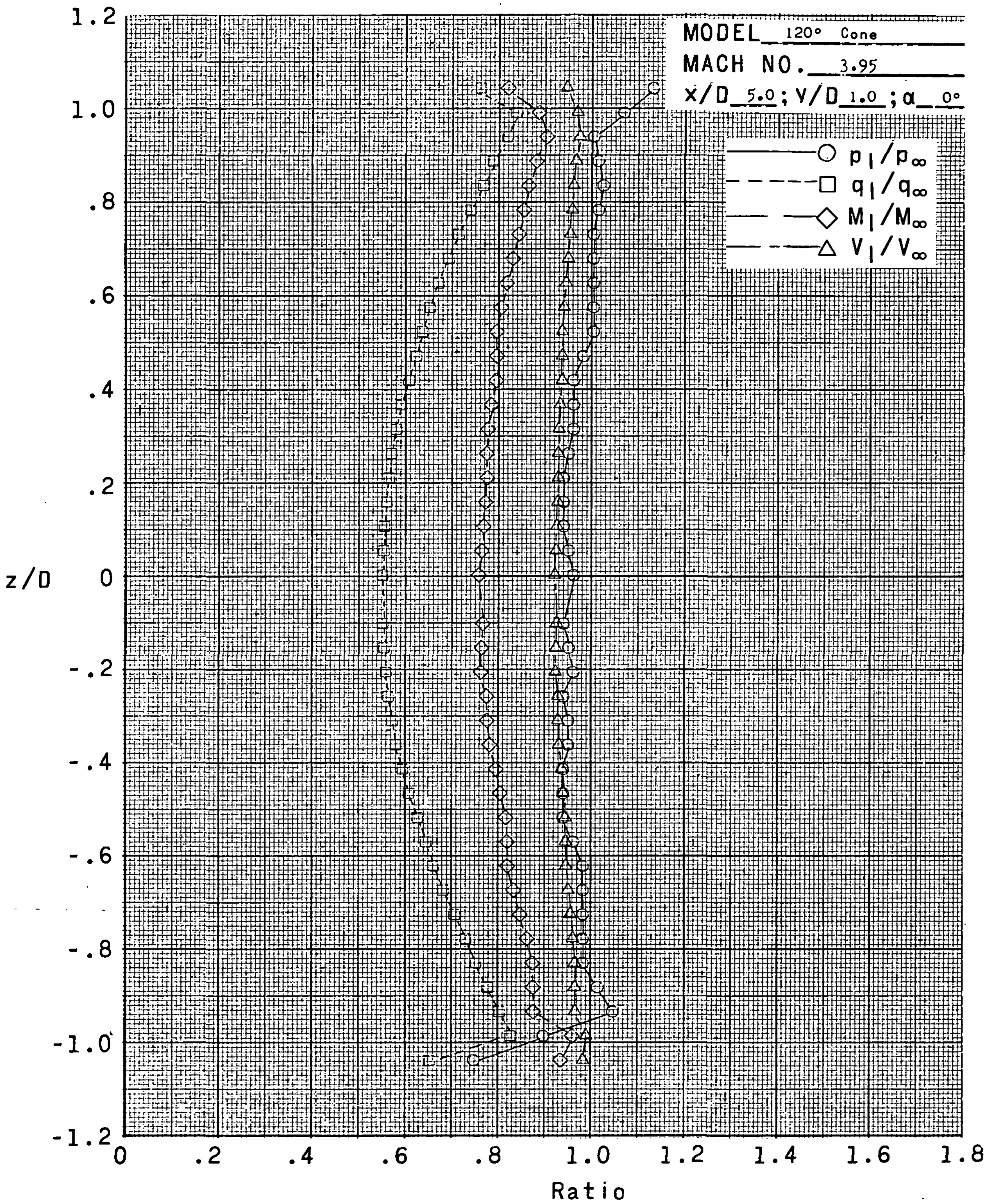
(q) $x/D = 5.0$; $y/D = 2.0$; $\alpha = 0^0$.

Figure 9.- Continued.



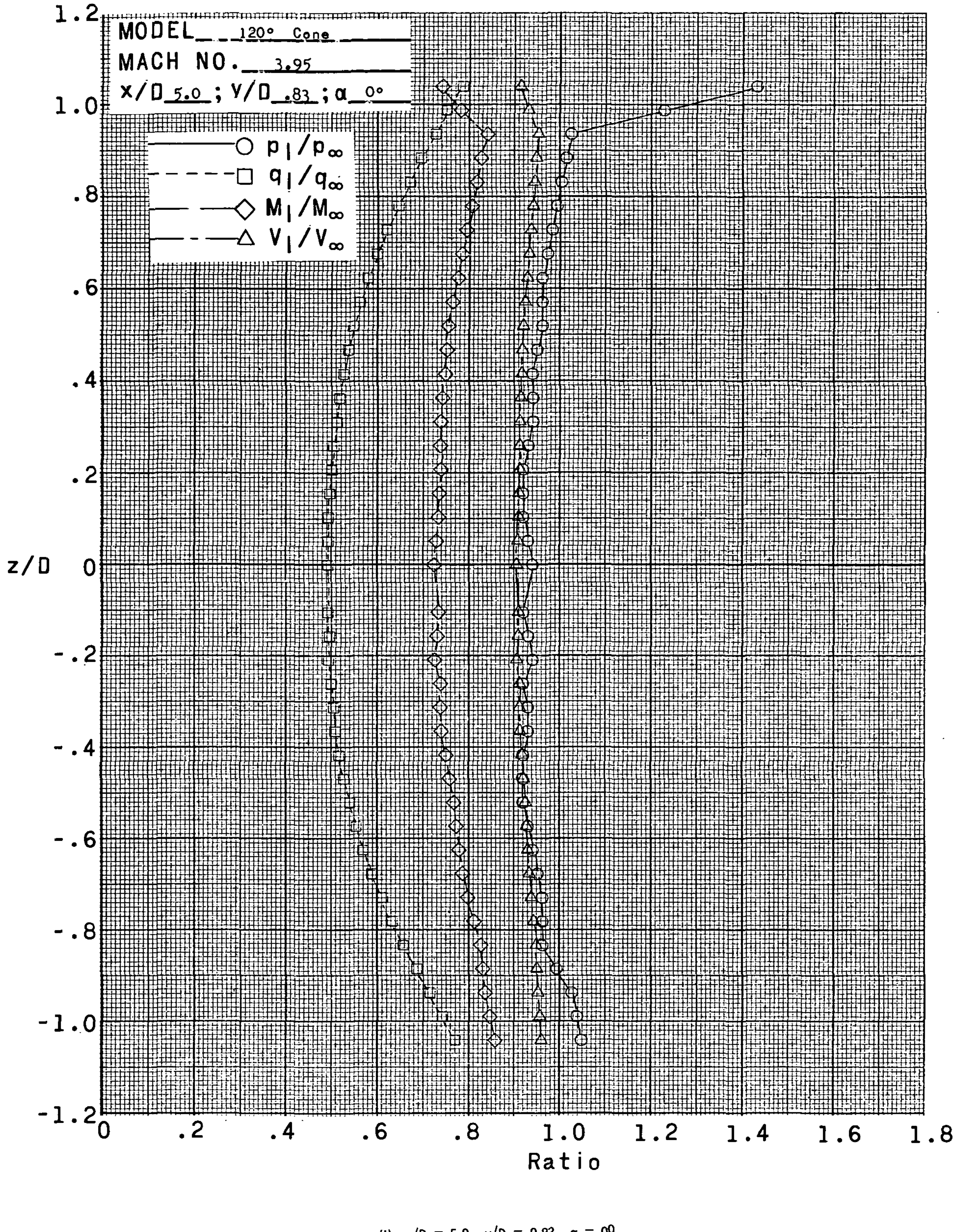
(r) $x/D = 5.0$; $y/D = 1.5$; $\alpha = 0^{0}$.

Figure 9.- Continued.



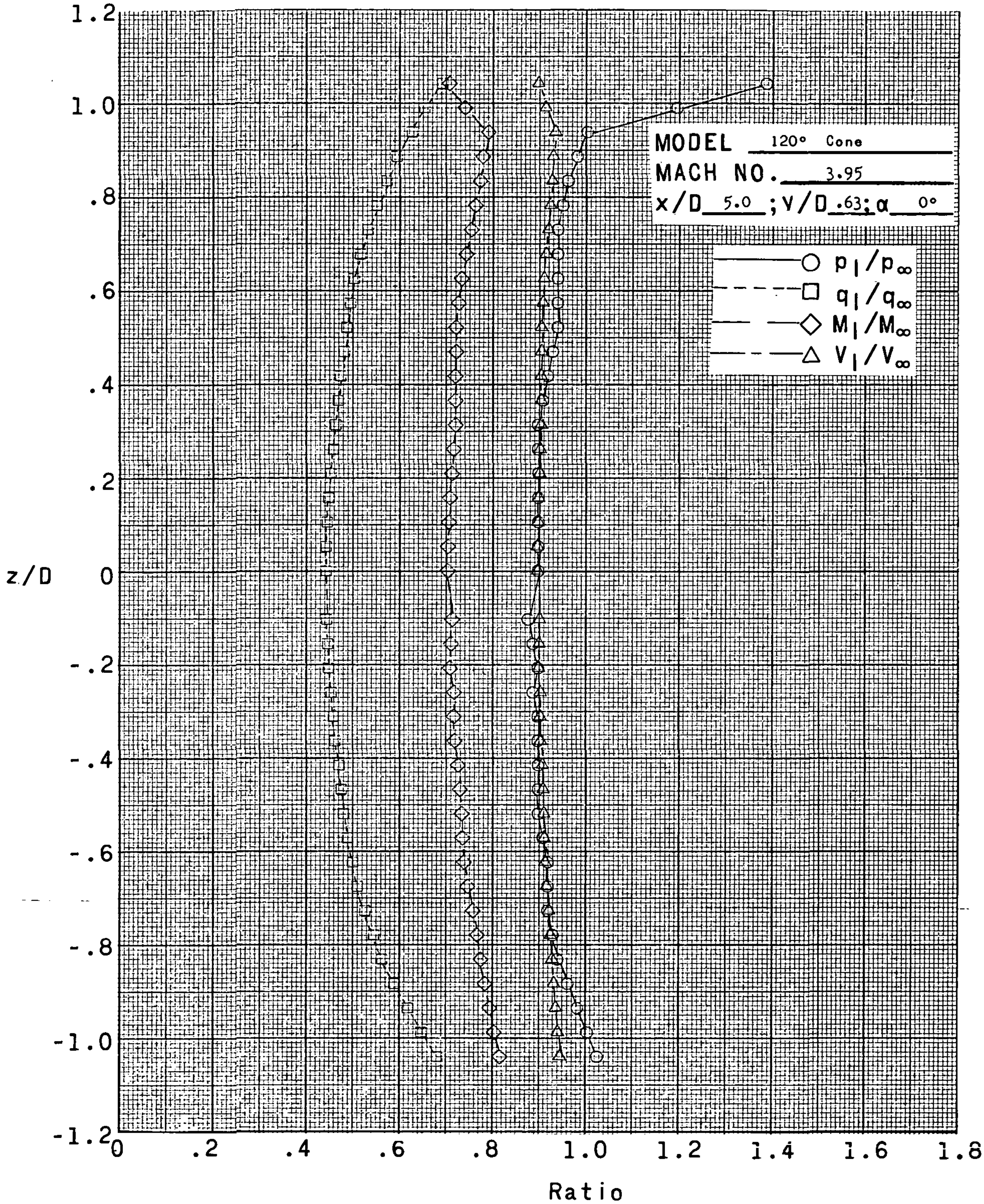
(s) $x/D = 5.0$; $y/D = 1.0$; $\alpha = 0^0$.

Figure 9.- Continued.



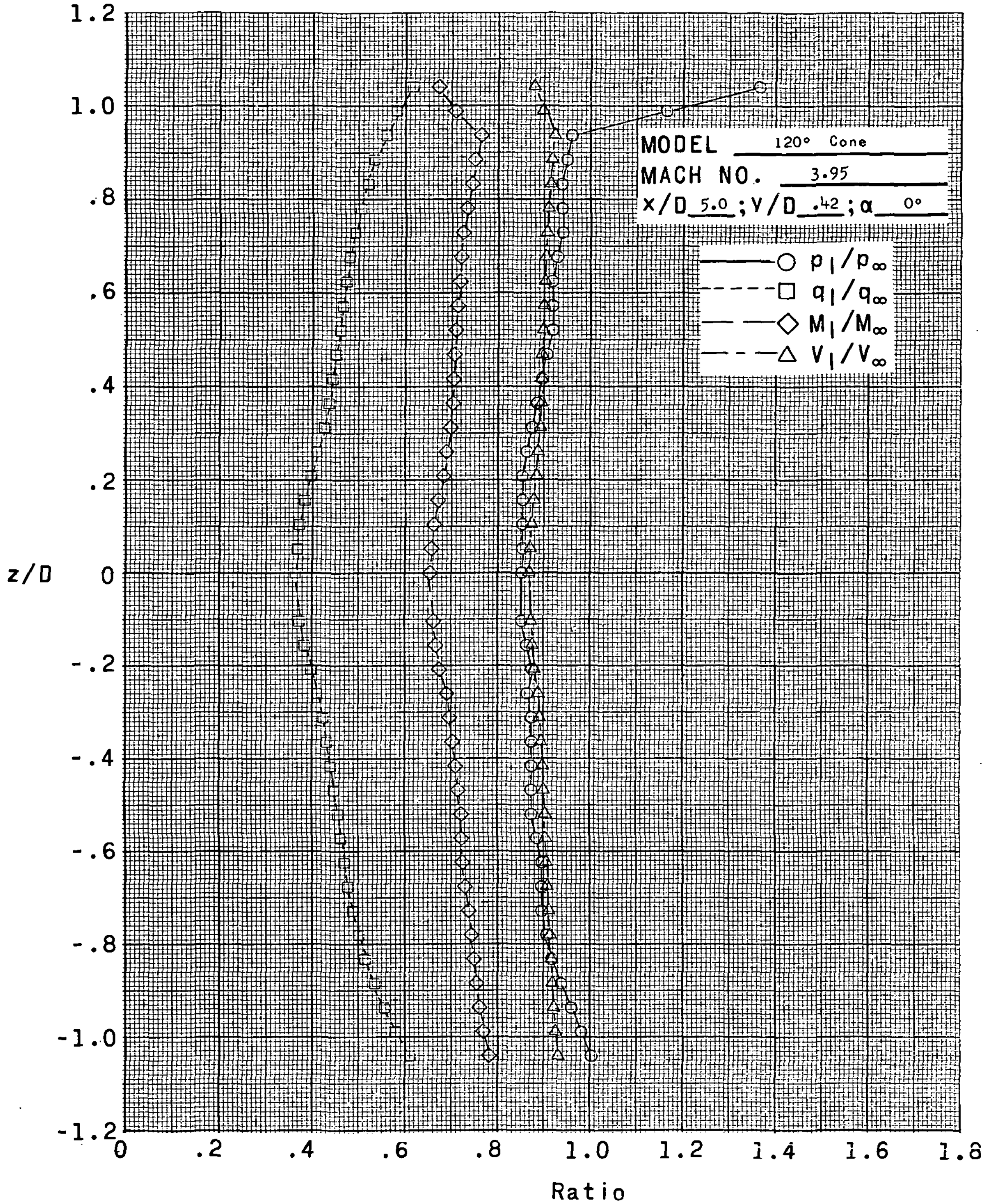
(t) x/D = 5.0; y/D = 0.83; α = 0°.

Figure 9.- Continued.



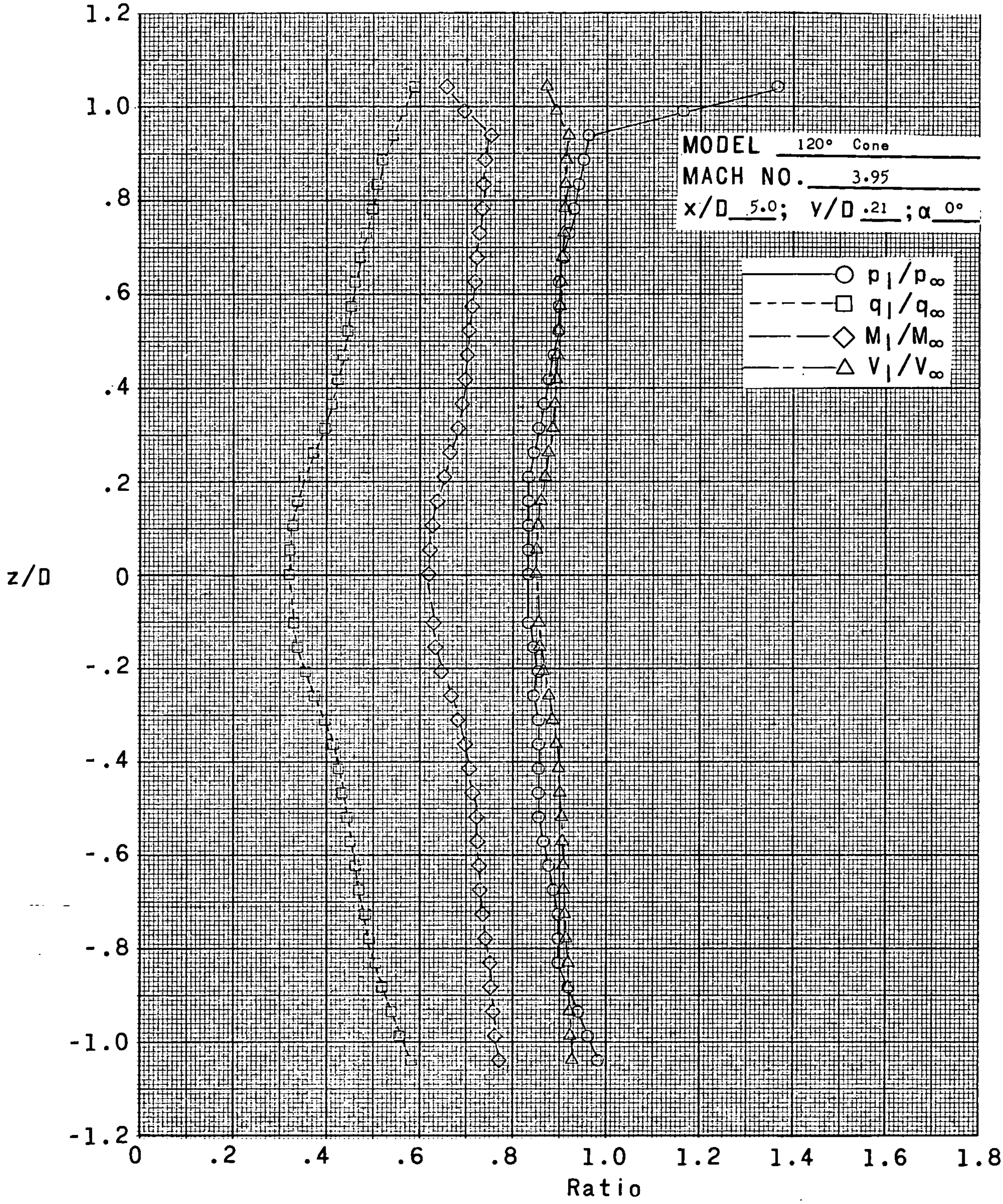
(u) $x/D = 5.0$; $y/D = 0.63$; $\alpha = 0^0$.

Figure 9.- Continued.



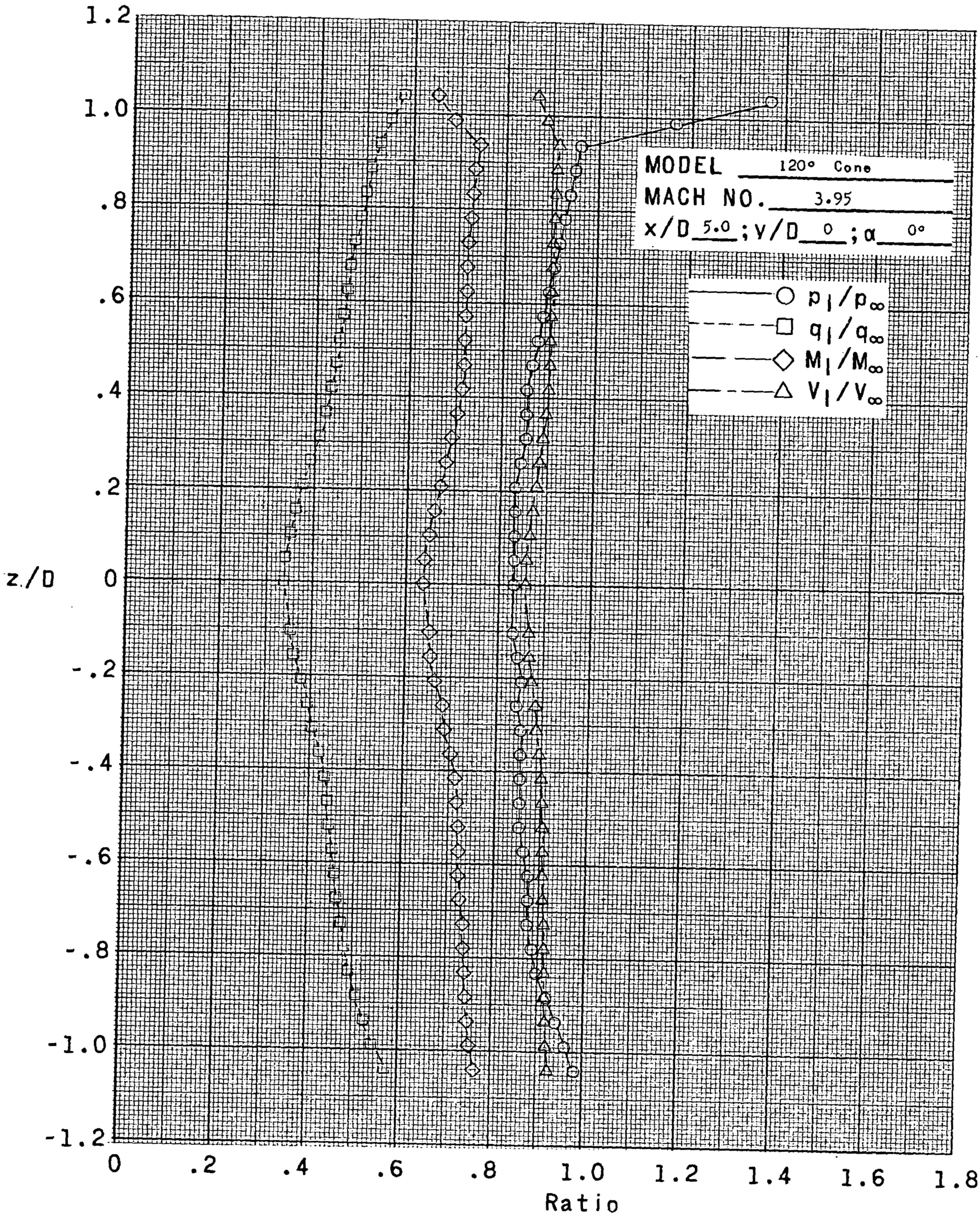
(v) x/D = 5.0; y/D = 0.42; α = 0°.

Figure 9.- Continued.



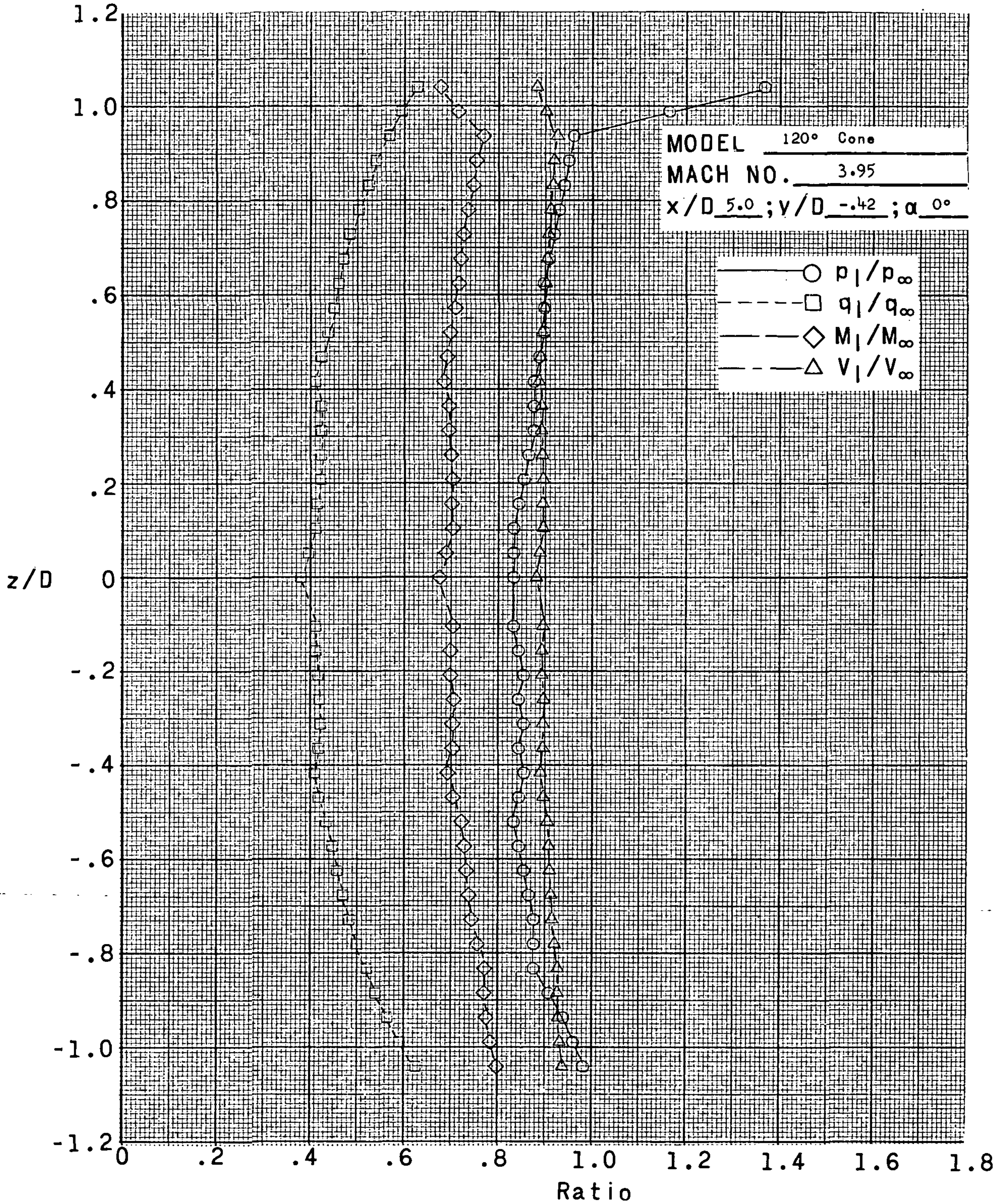
(w) x/D = 5.0; y/D = 0.21; α = 0°.

Figure 9.- Continued.



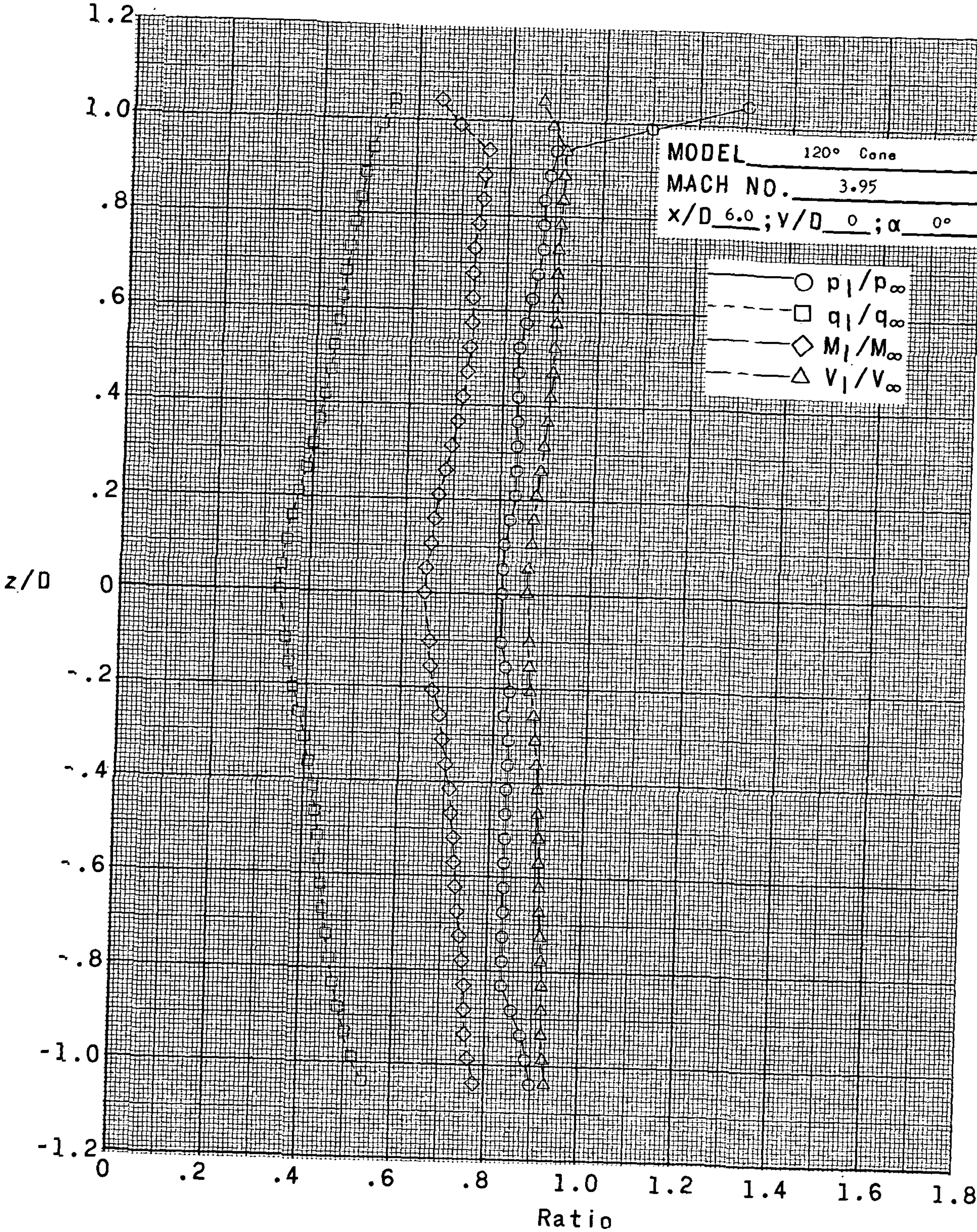
(x) x/D = 5.0; y/D = 0; α = 0°.

Figure 9.- Continued.



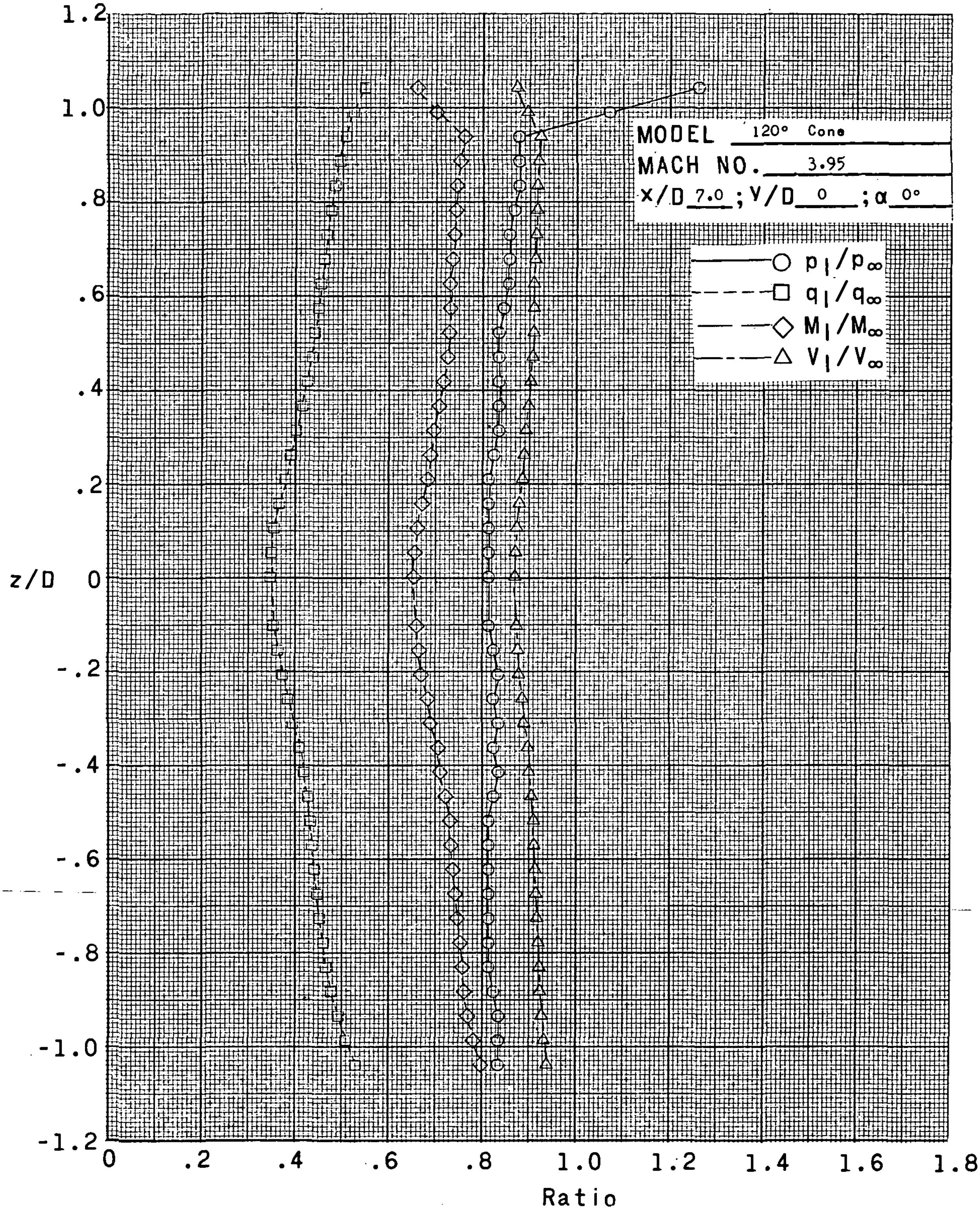
(y) $x/D = 5.0$; $y/D = -0.42$; $\alpha = 0^{0}$.

Figure 9.- Continued.



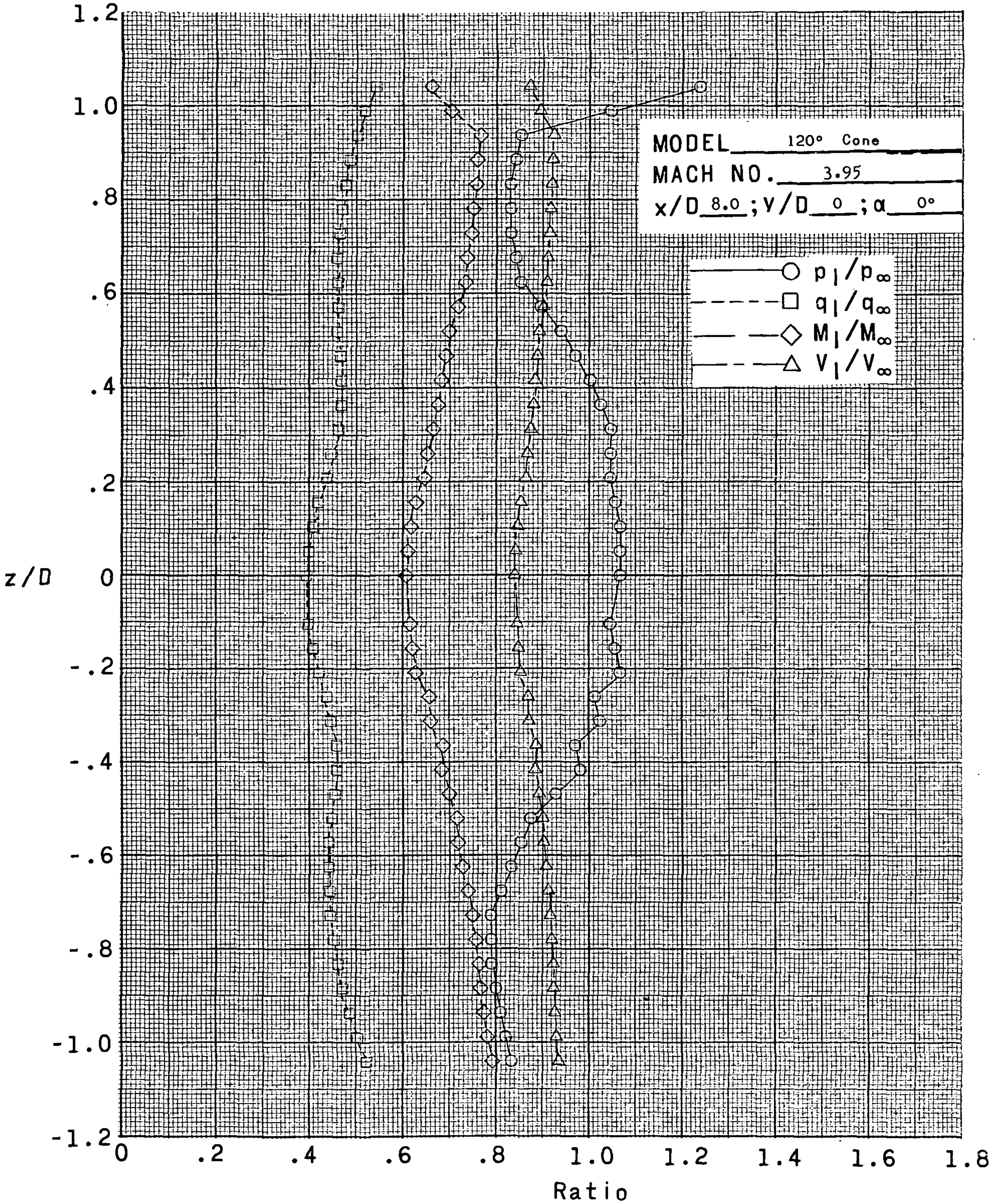
(z) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 9.- Continued.



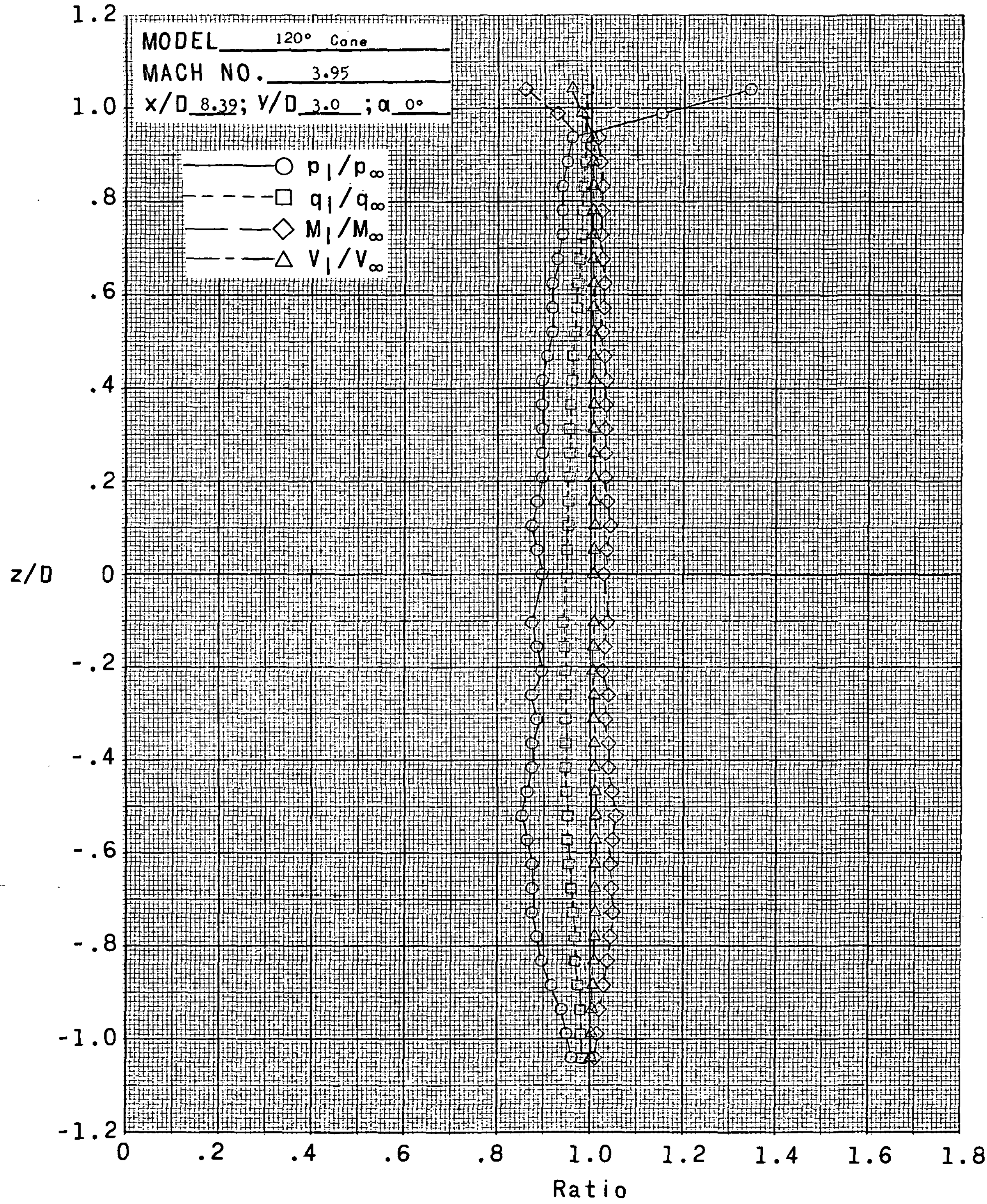
(aa) x/D = 7.0; y/D = 0; α = 0°.

Figure 9.- Continued.



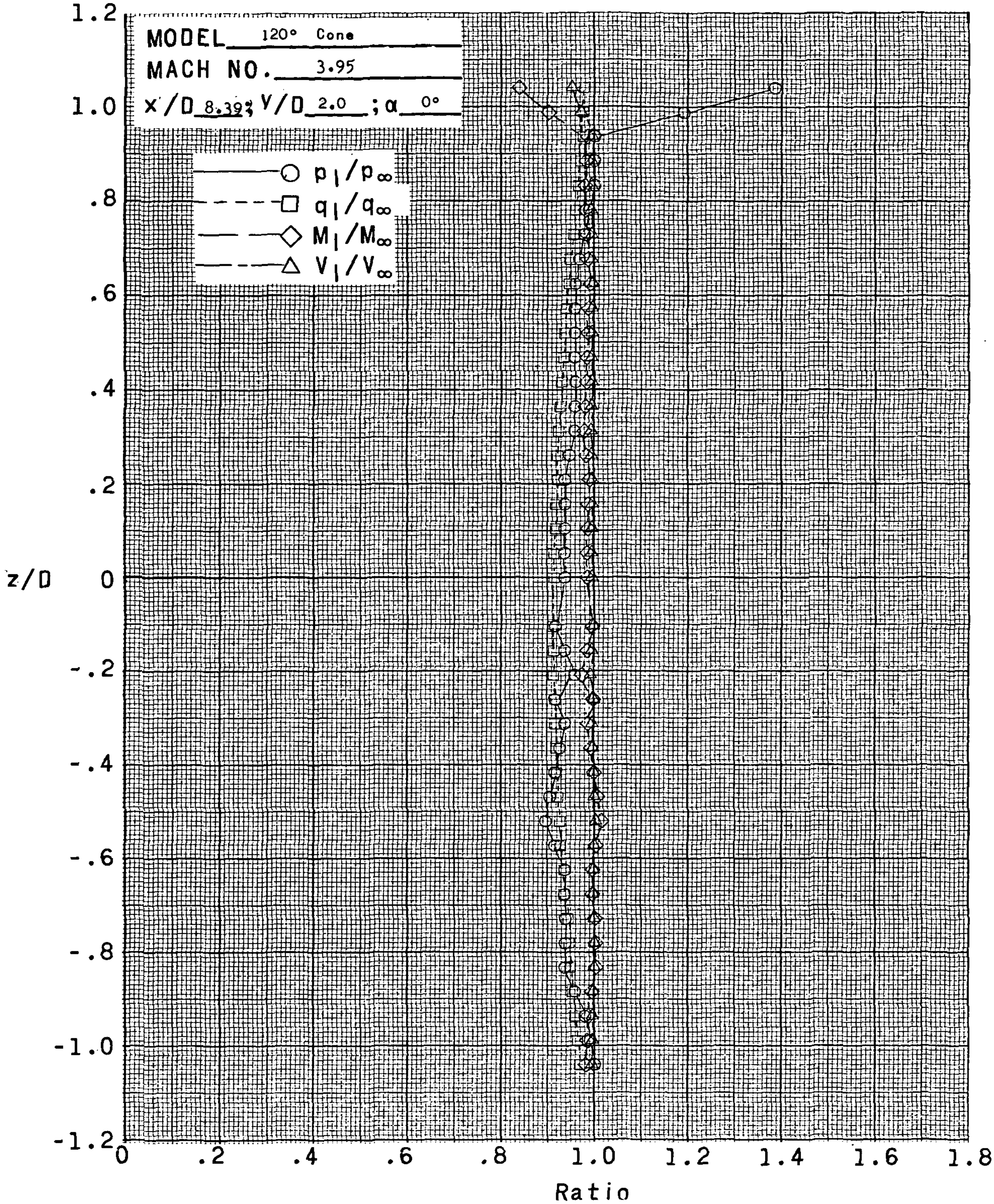
(bb) $x/D = 8.0$; $y/D = 0$; $\alpha = 0^o$.

Figure 9.- Continued.



(cc) $x/D = 8.39$; $y/D = 3.0$; $\alpha = 0^o$.

Figure 9.- Continued.

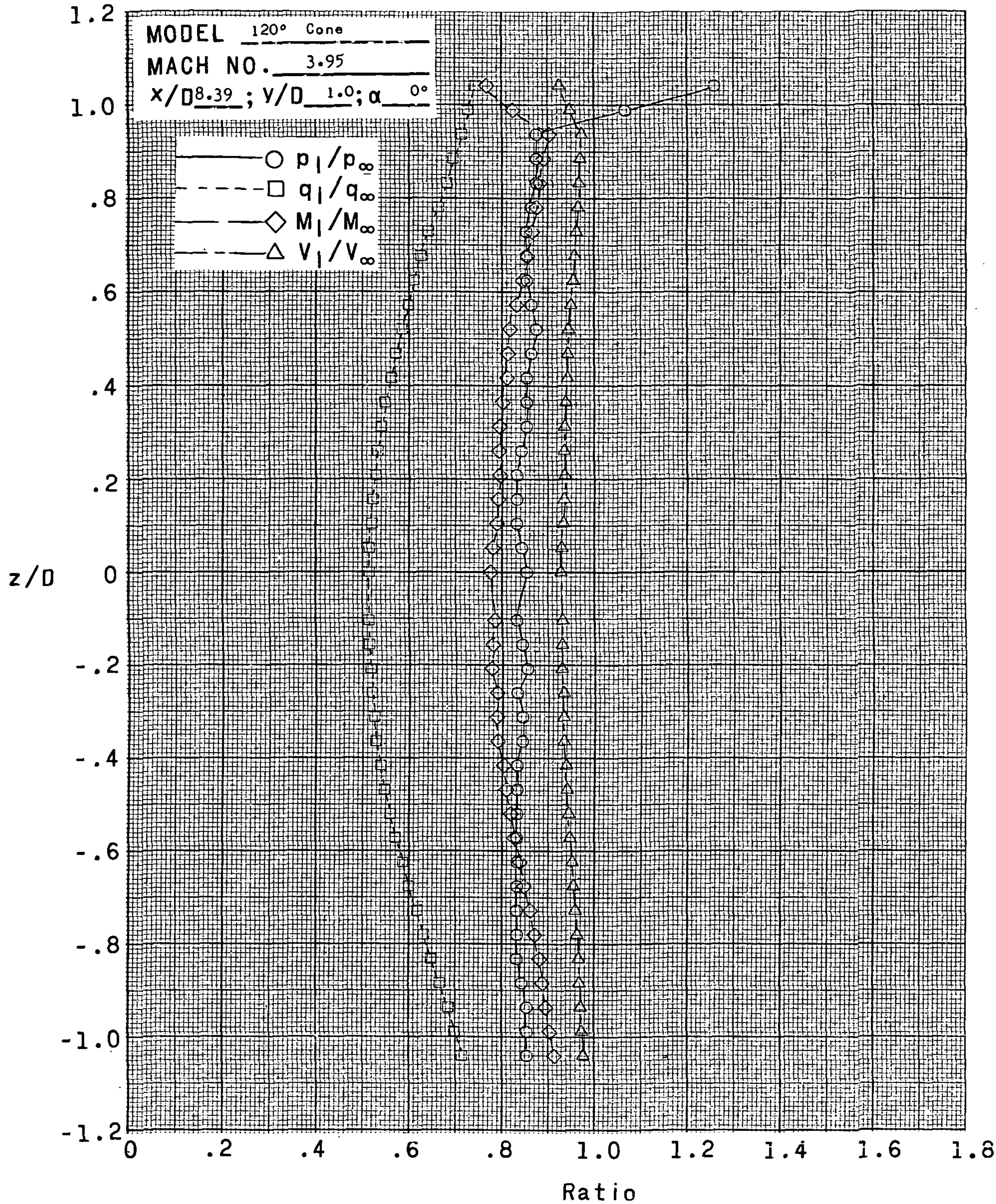


(dd) x/D = 8.39; y/D = 2.0; α = 0°.

Figure 9.- Continued.

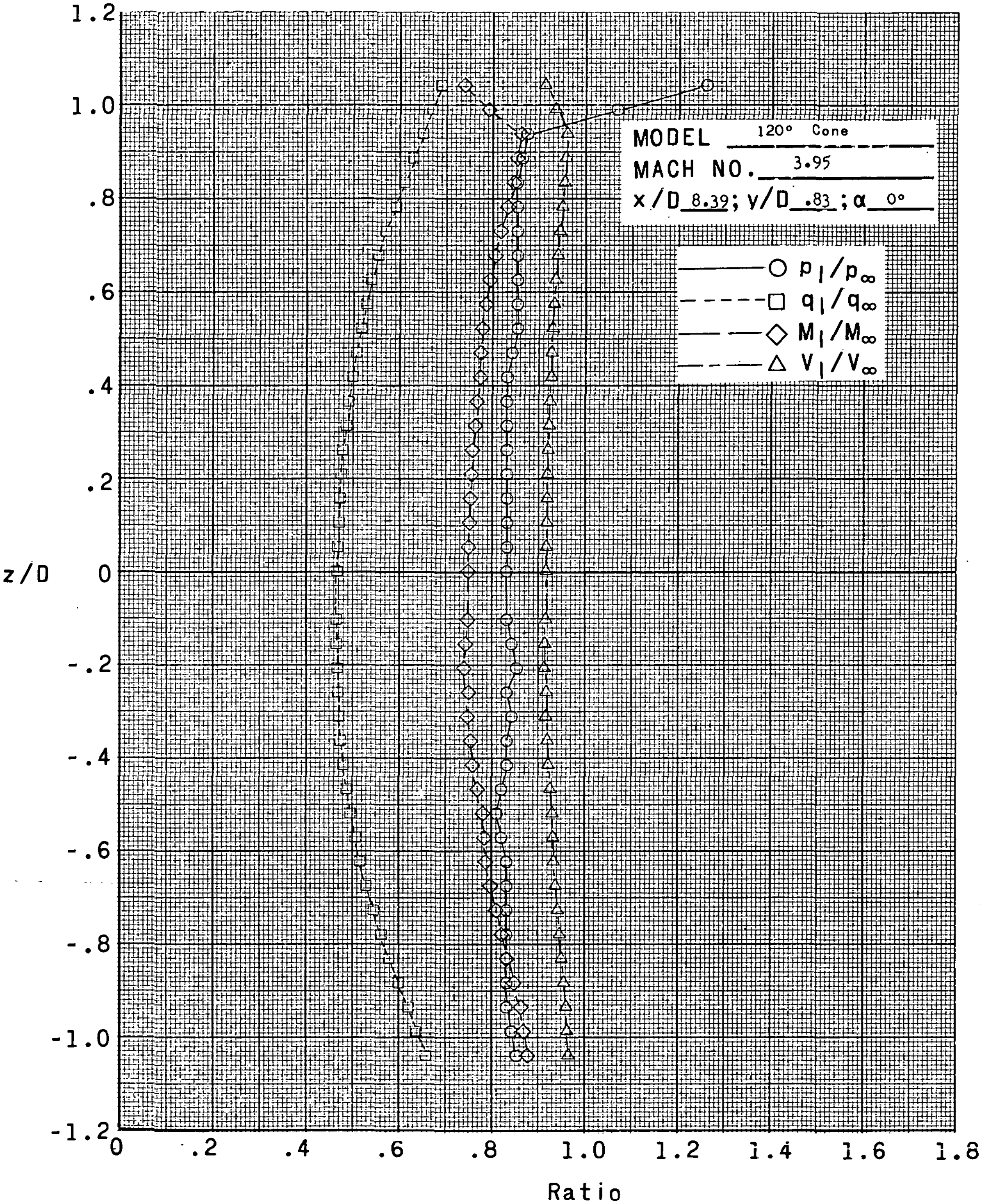
(ee) $x/D = 8.39$; $y/D = 1.5$; $\alpha = 0^\circ$.

Figure 9.- Continued.



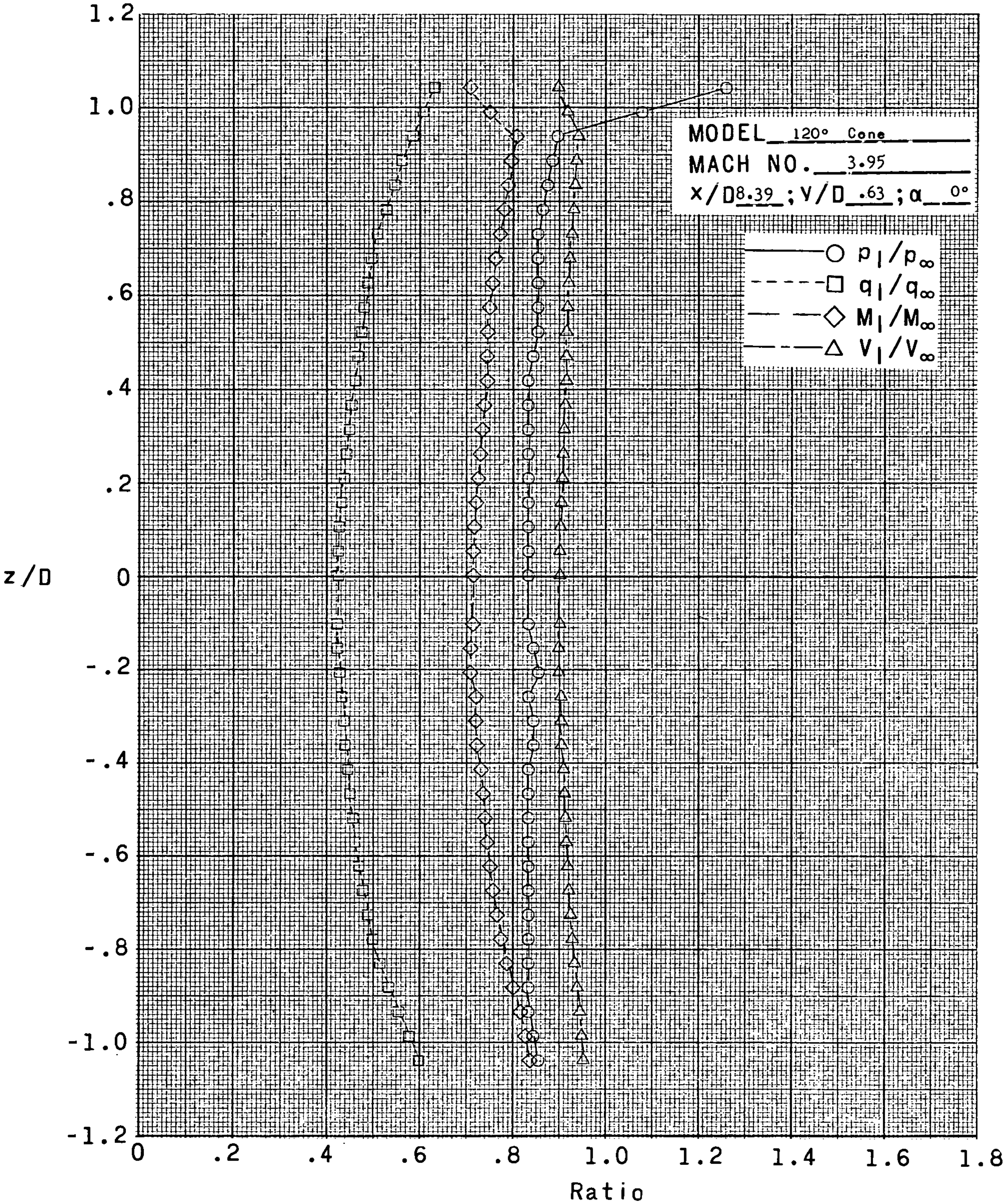
(ff) x/D = 8.39; y/D = 1.0; α = 0°.

Figure 9.- Continued.



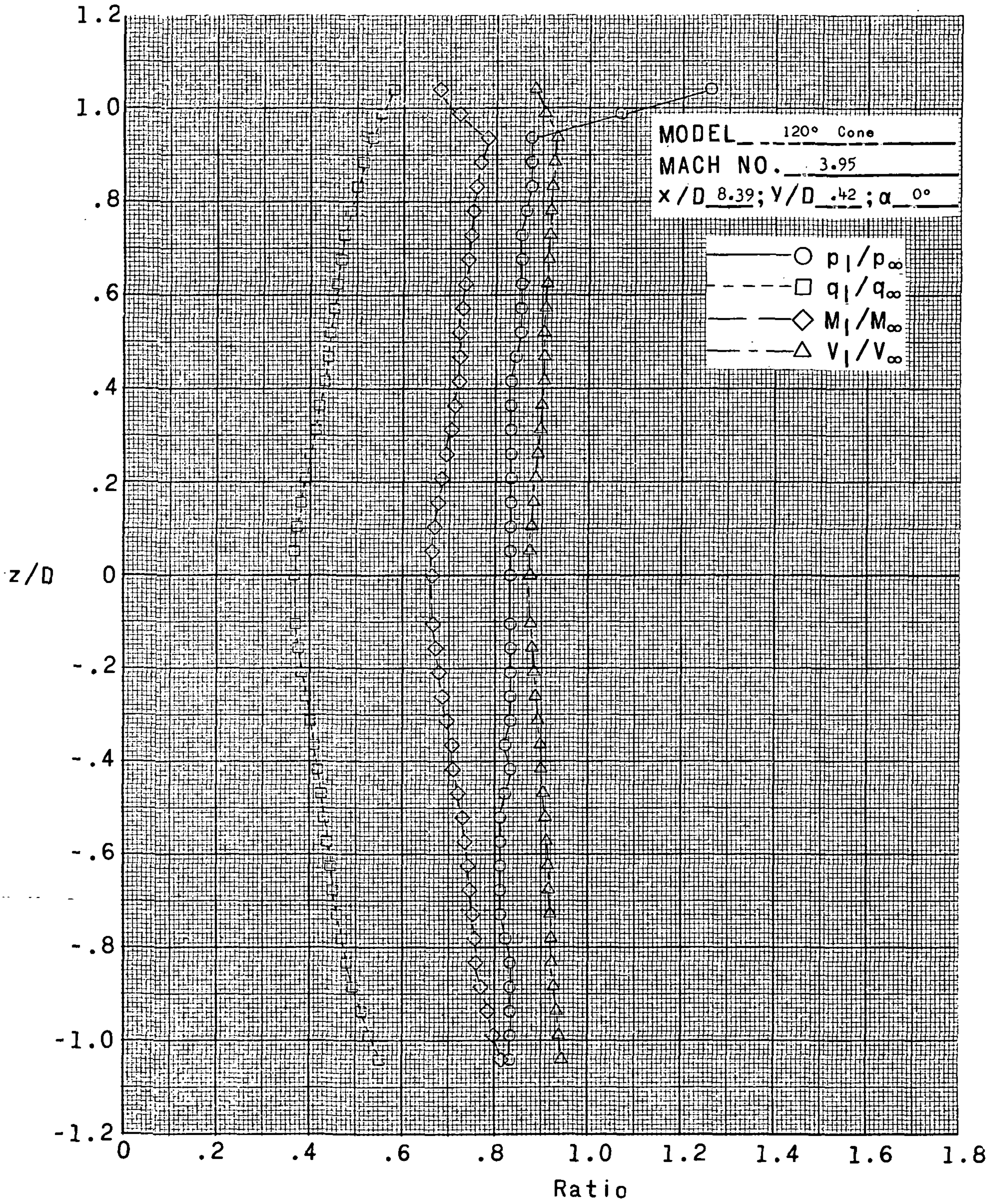
(gg) $x/D = 8.39$; $y/D = 0.83$; $\alpha = 0^0$.

Figure 9.- Continued.



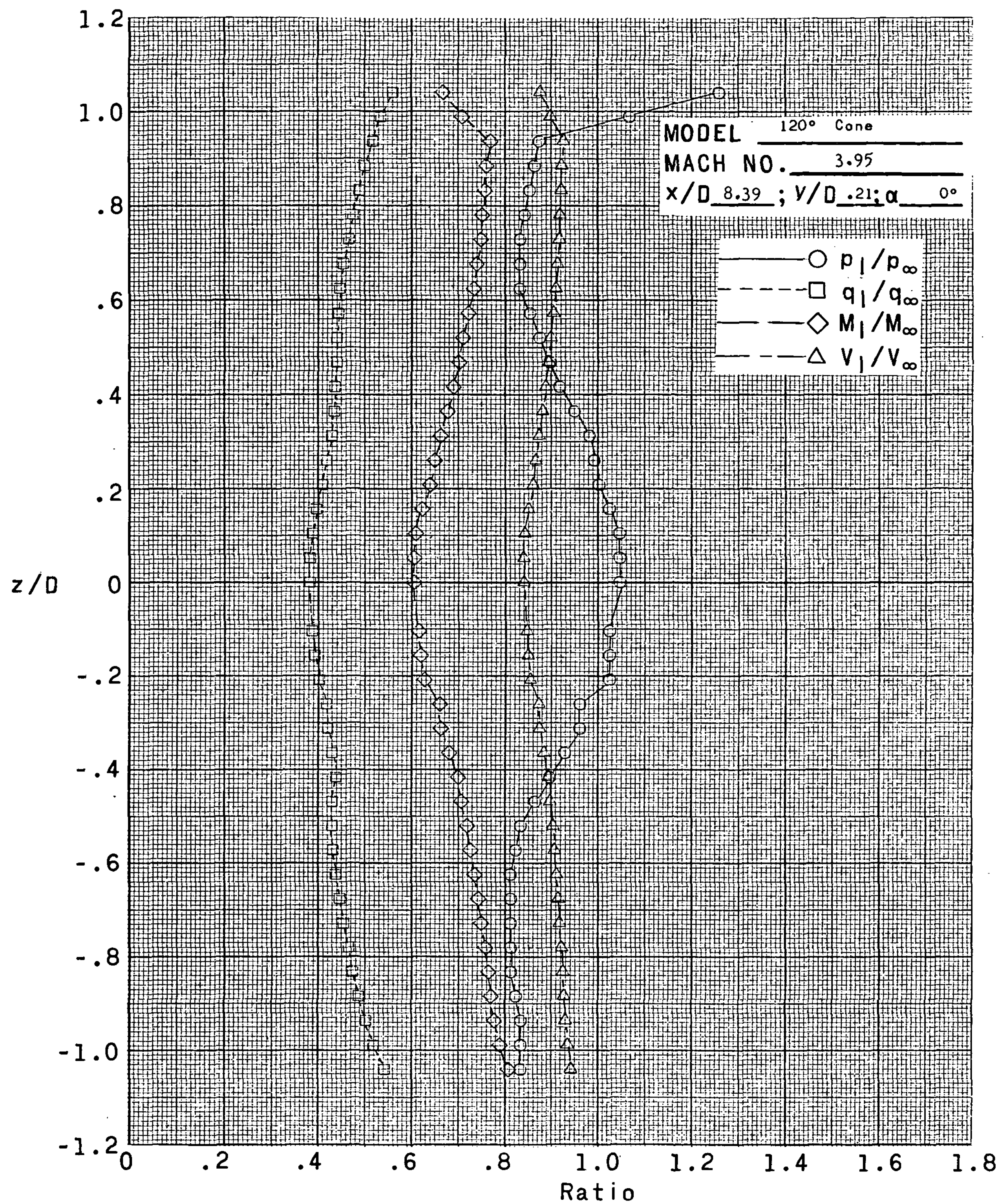
(hh) x/D = 8.39; y/D = 0.63; α = 0°.

Figure 9.- Continued.



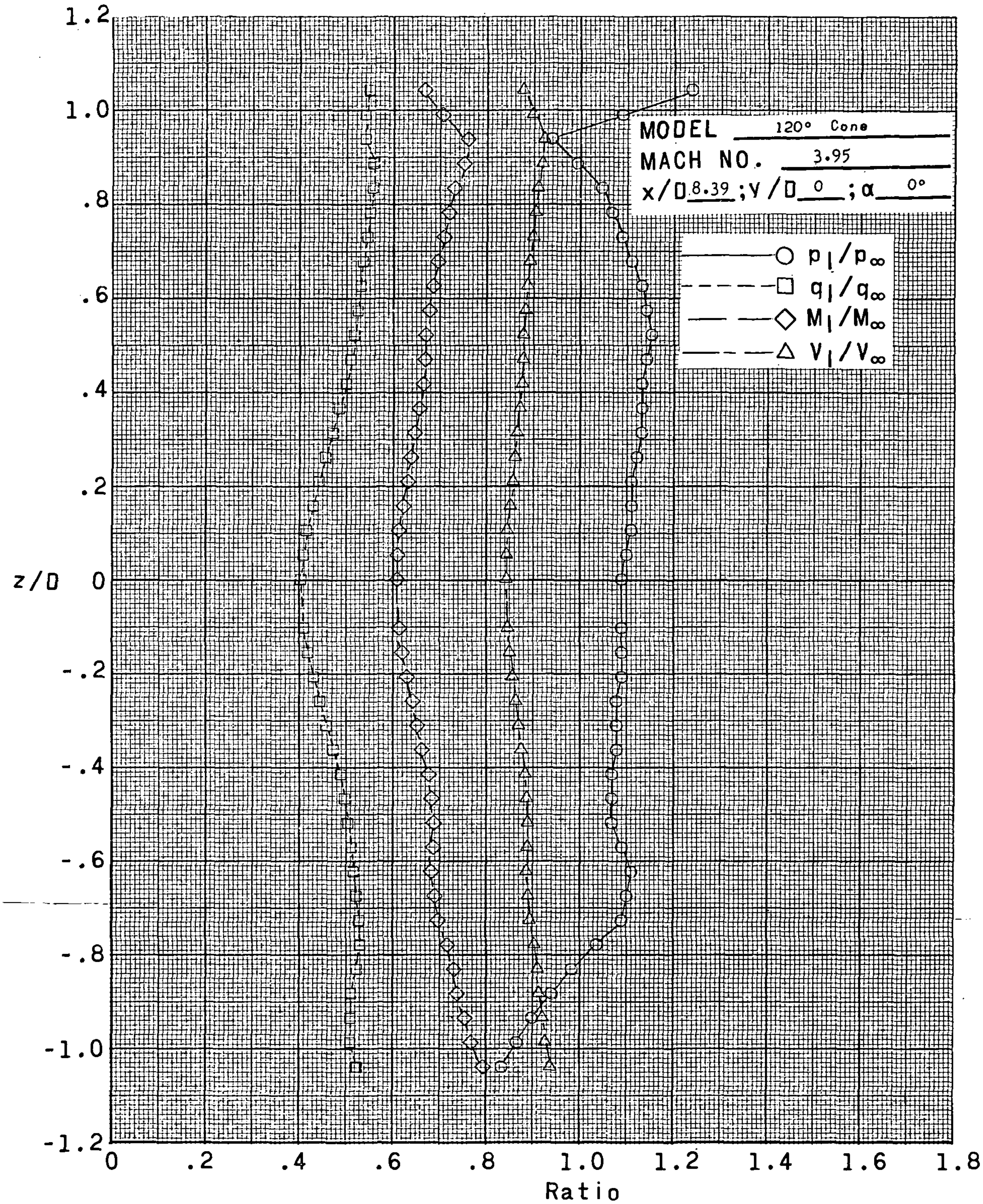
(ii) x/D = 8.39; y/D = 0.42; α = 0°.

Figure 9.- Continued.



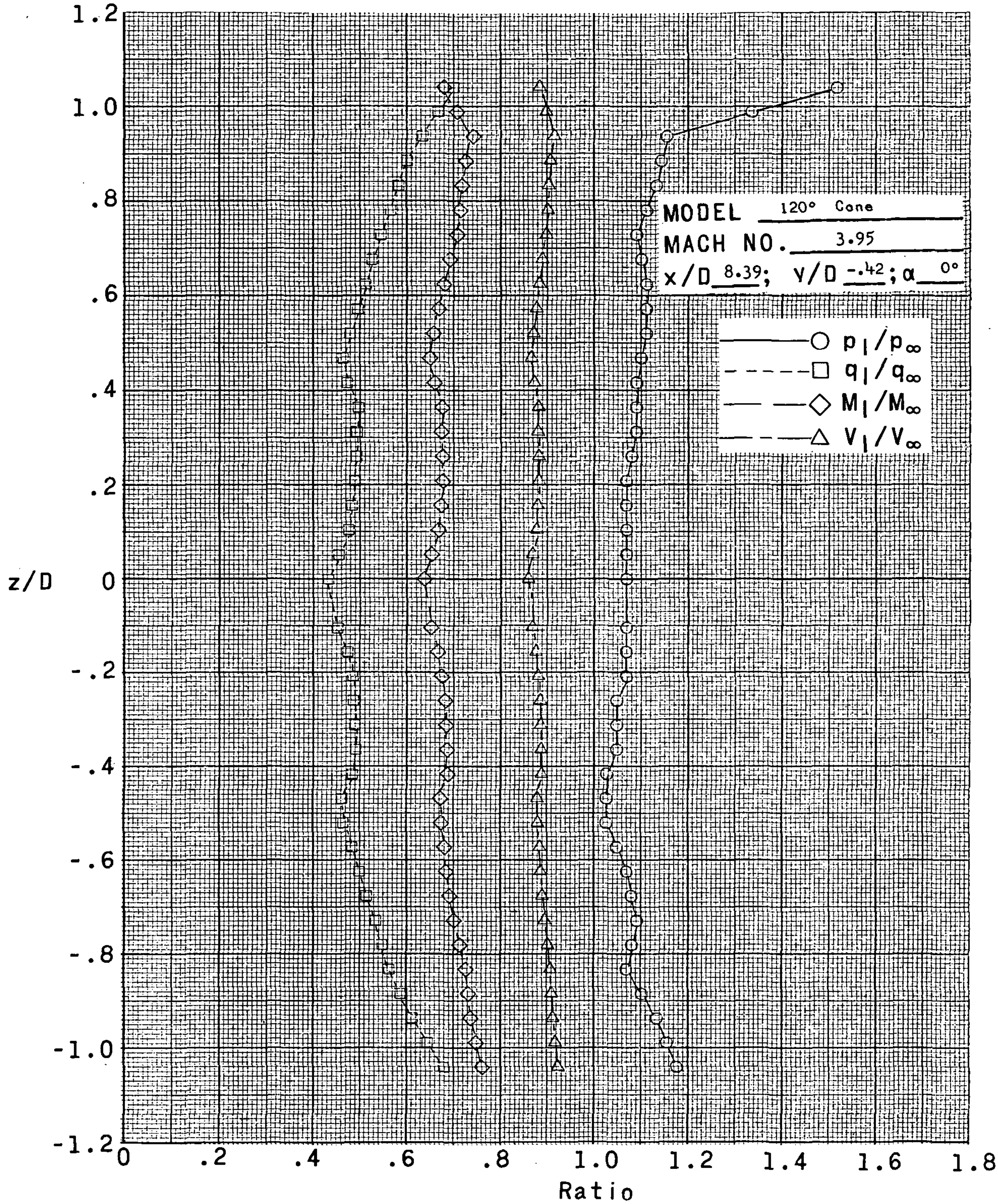
(jj) $x/D = 8.39$; $y/D = 0.21$; $\alpha = 0^0$.

Figure 9.- Continued.



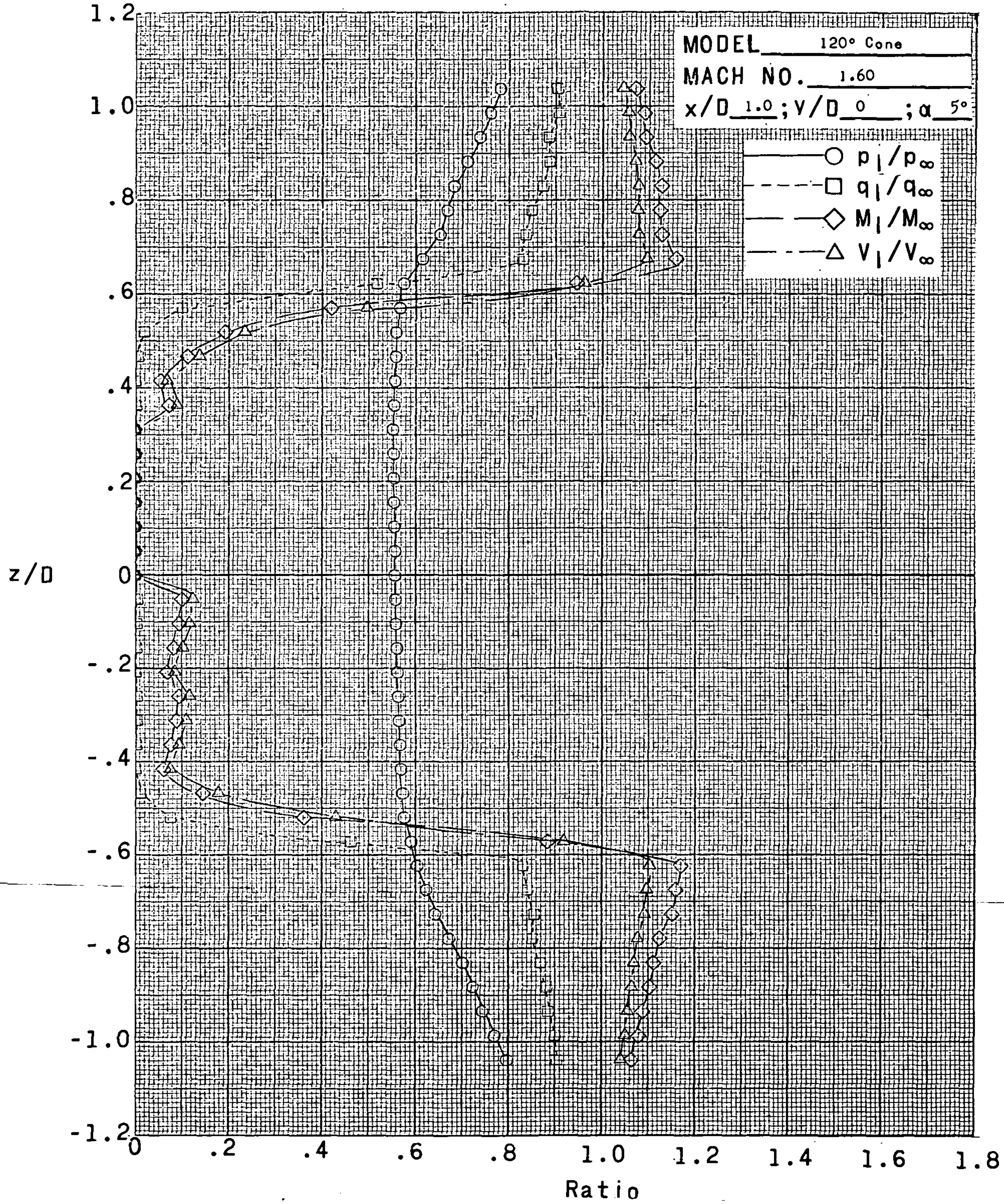
(kk) $x/D = 8.39$; $y/D = 0$; $\alpha = 0^\circ$.

Figure 9.- Continued.



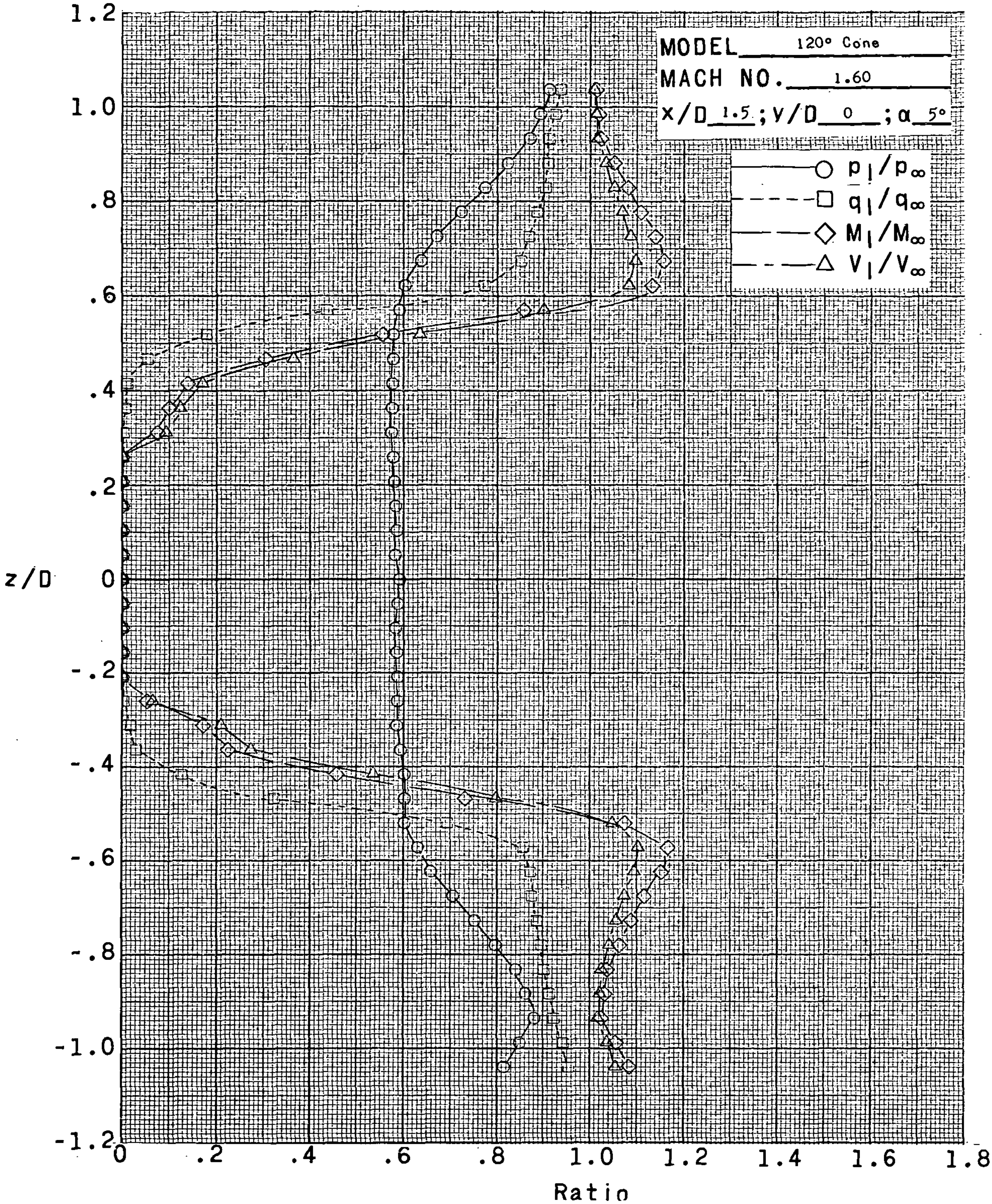
(ll) $x/D = 8.39$; $y/D = -0.42$; $\alpha = 0^0$.

Figure 9.- Concluded.



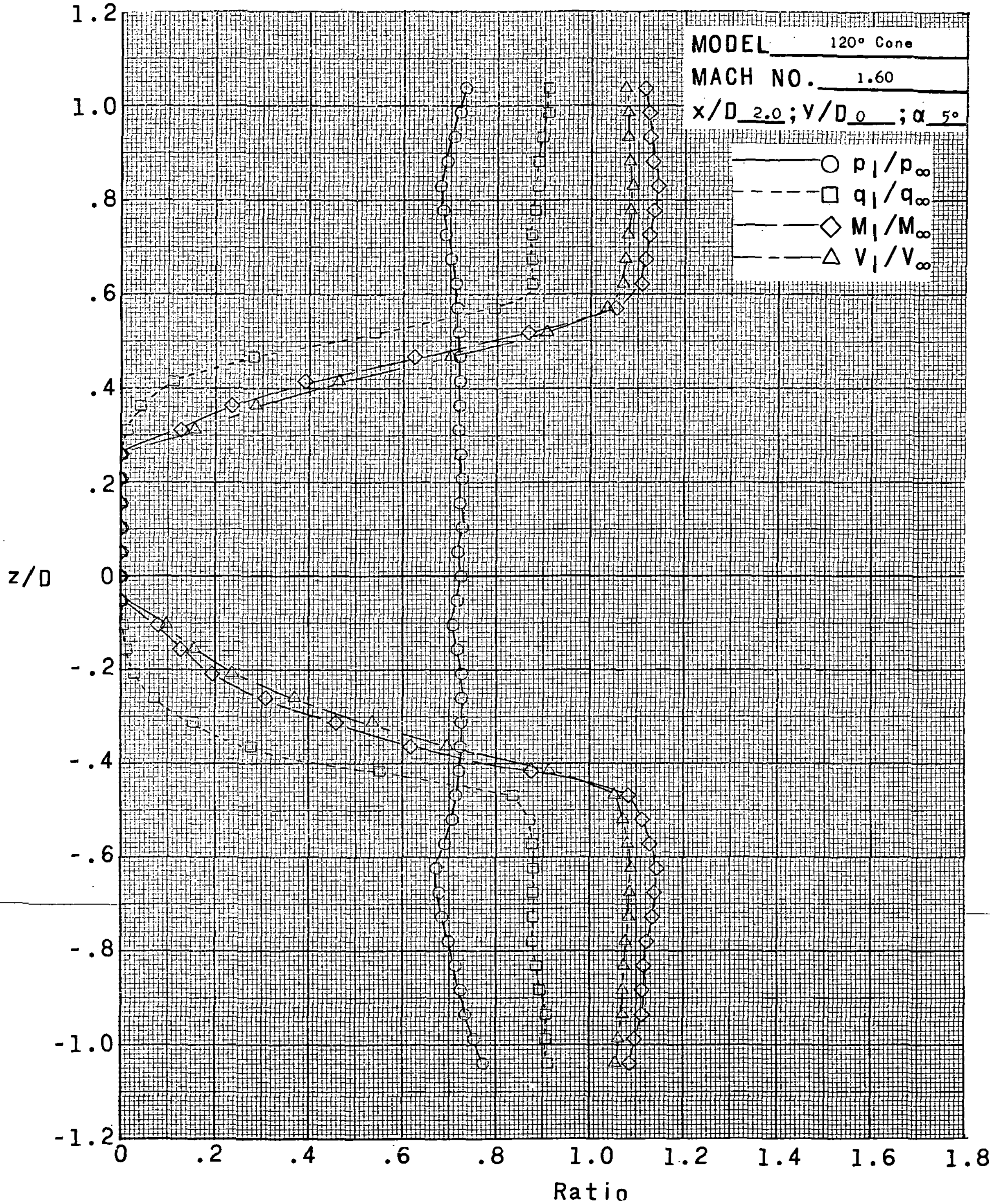
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 10.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D at the center of wake of a 120°-included-angle cone at a Mach number of 160 and a Reynolds number of 1.65×10^6 per foot $(5.42 \times 10^6$ per meter).



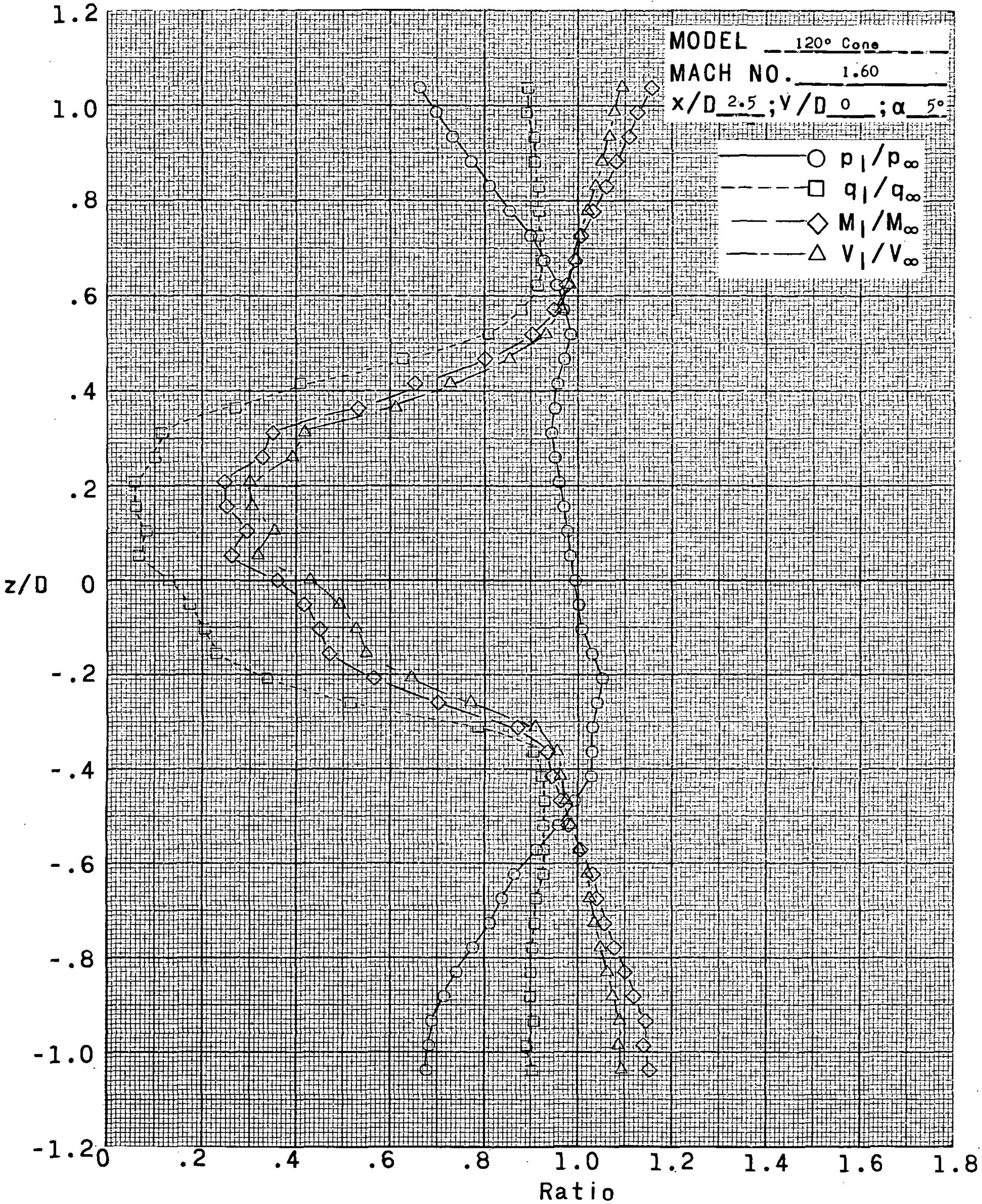
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 10.- Continued.



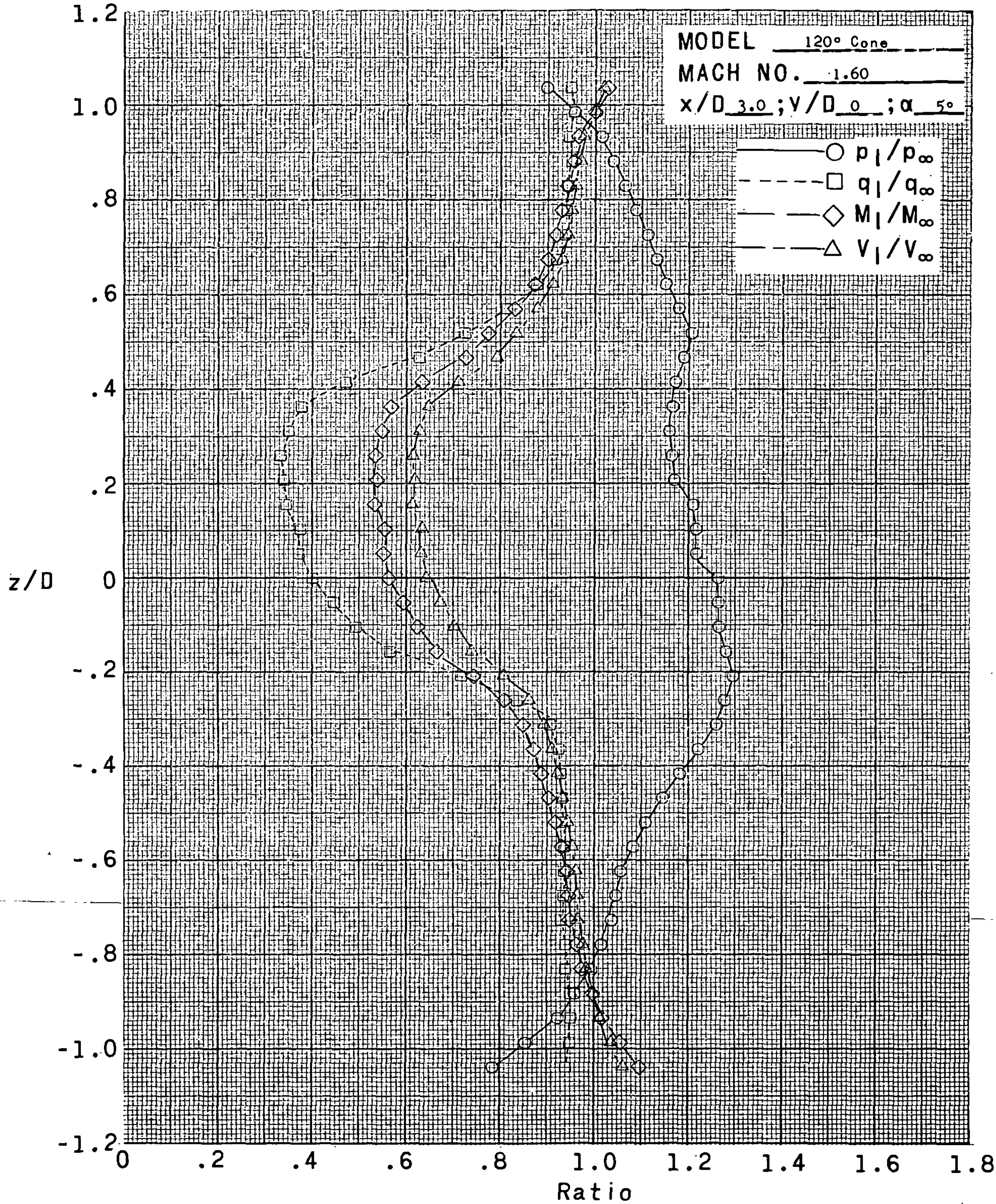
(c) x/D = 2.0; y/D = 0; α = 5°.

Figure 10.- Continued.



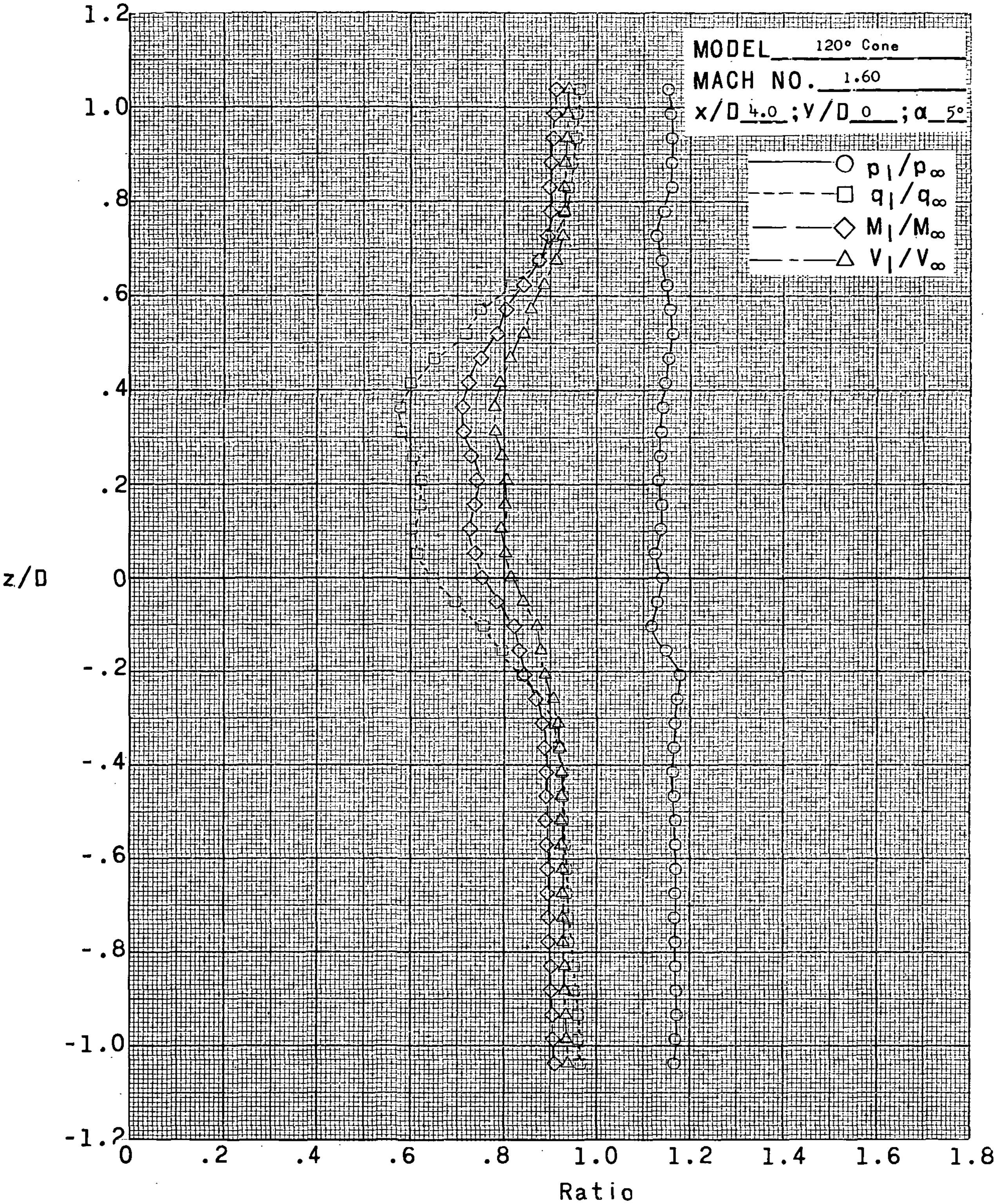
(d) x/D = 2.5; y/D = 0; α = 5°.

Figure 10.- Continued.



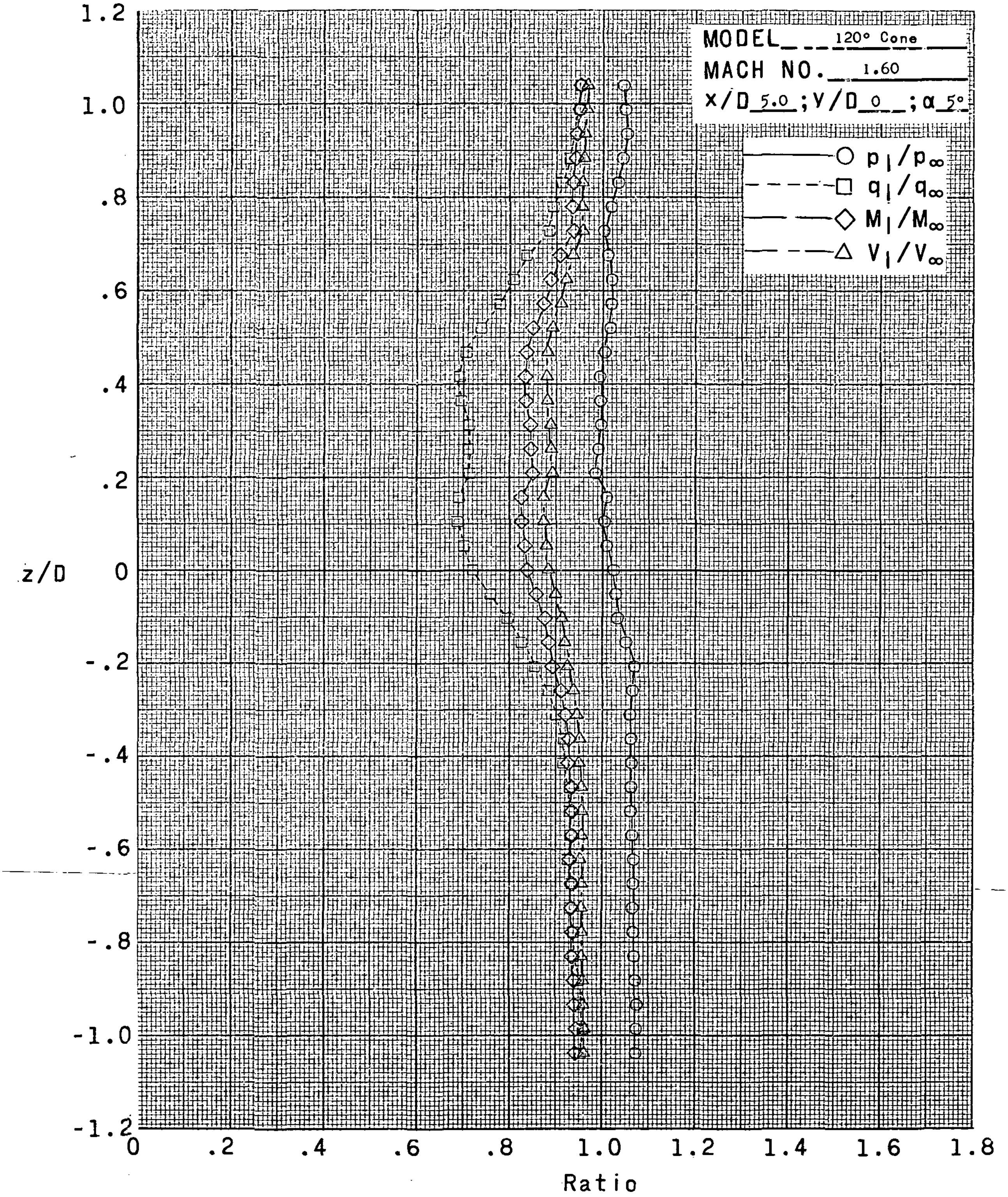
(e) x/D = 3.0; y/D = 0; α = 5°.

Figure 10.- Continued.



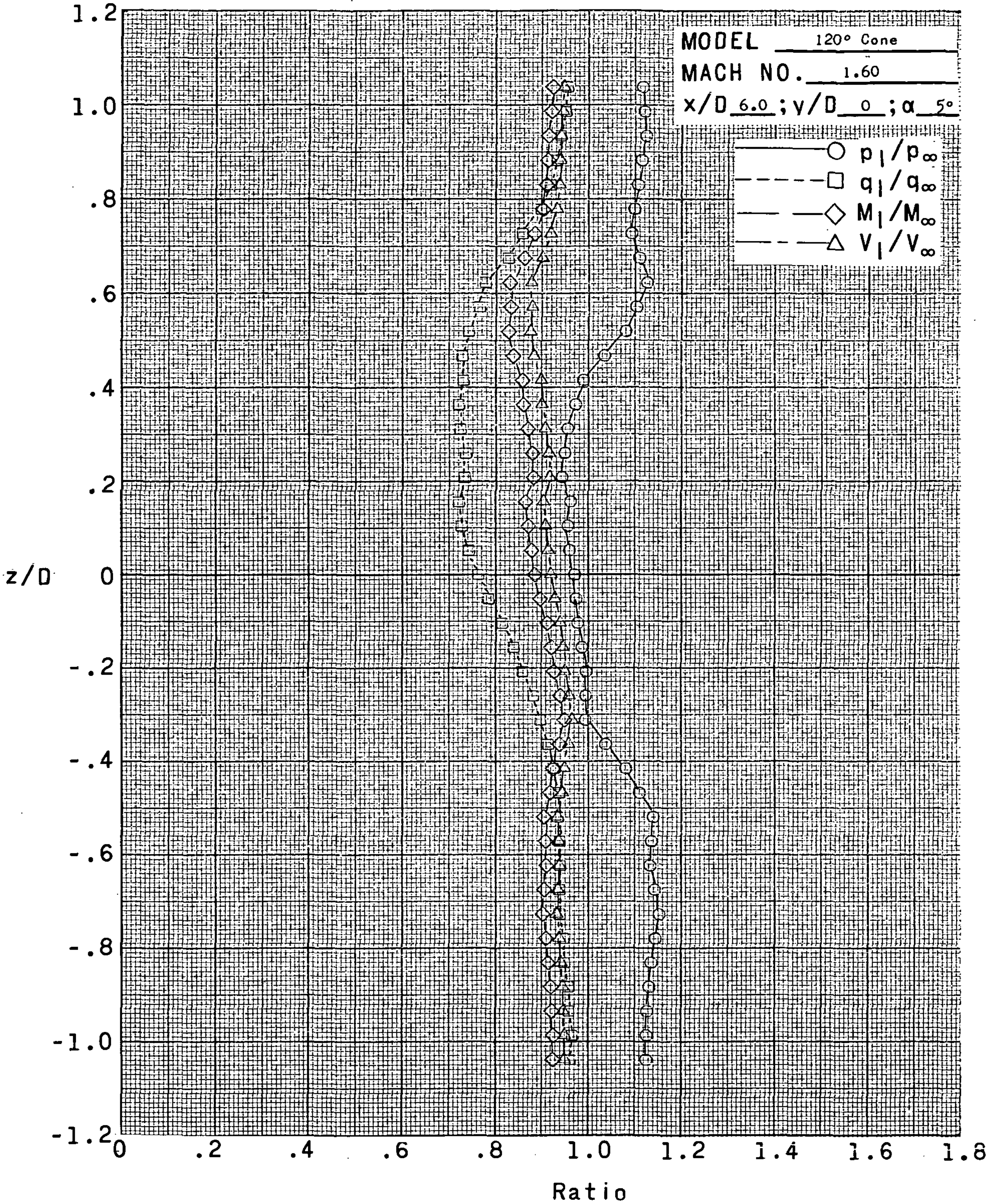
(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 5^\circ$.

Figure 10.- Continued.



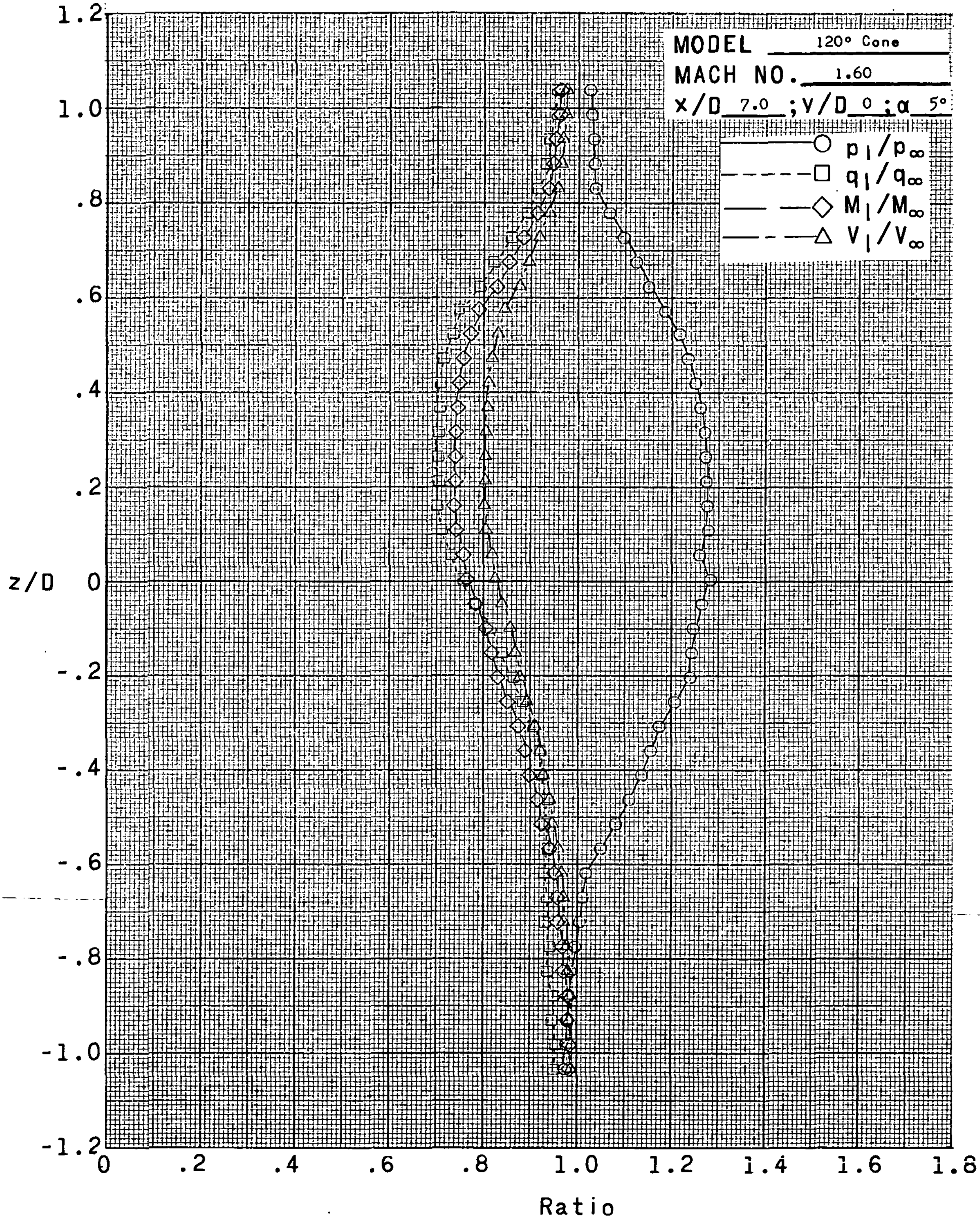
(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 10.- Continued.



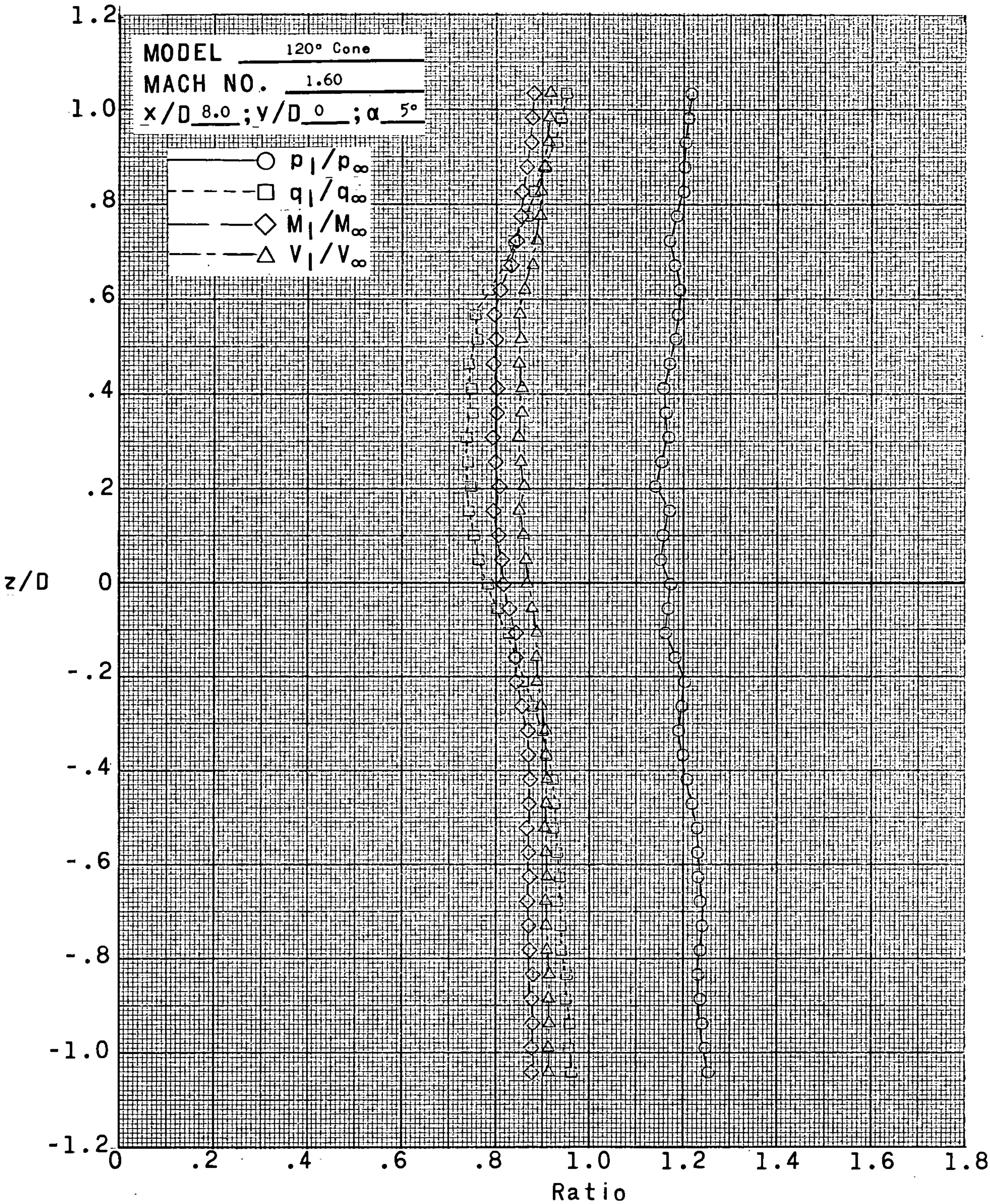
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 10.- Continued.



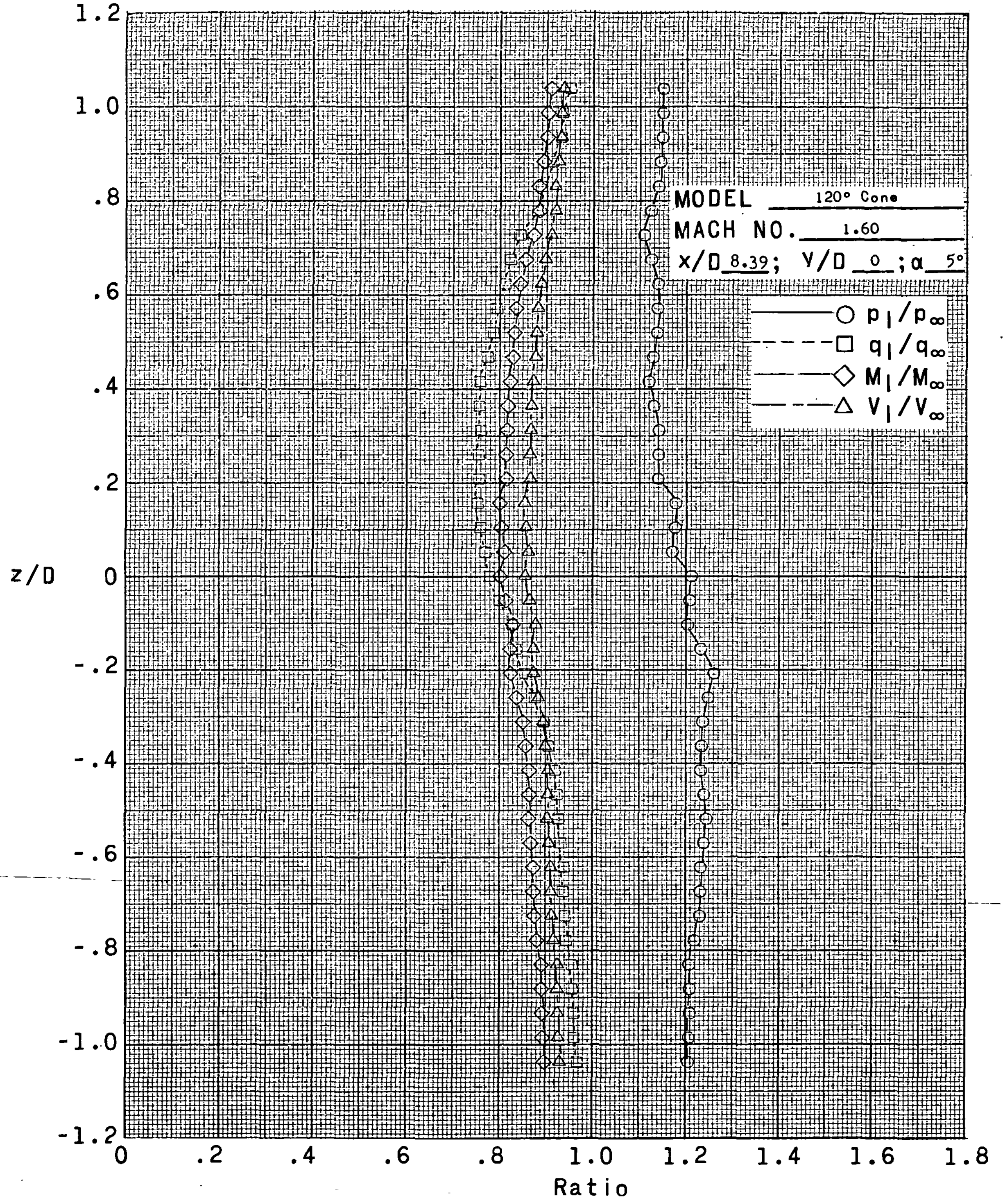
(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 10.- Continued.



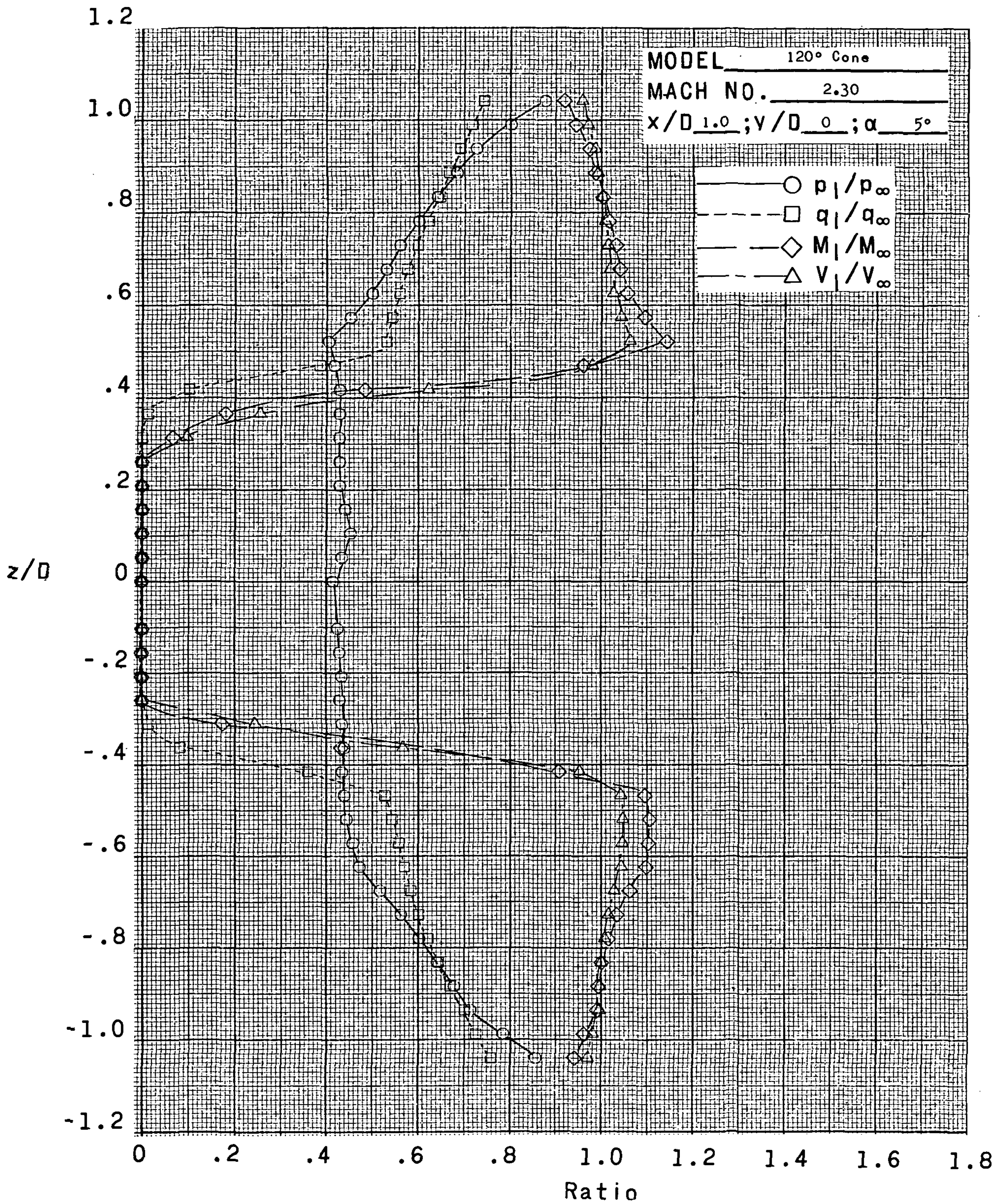
(j) x/D = 8.0; y/D = 0; α = 5°.

Figure 10.- Continued.



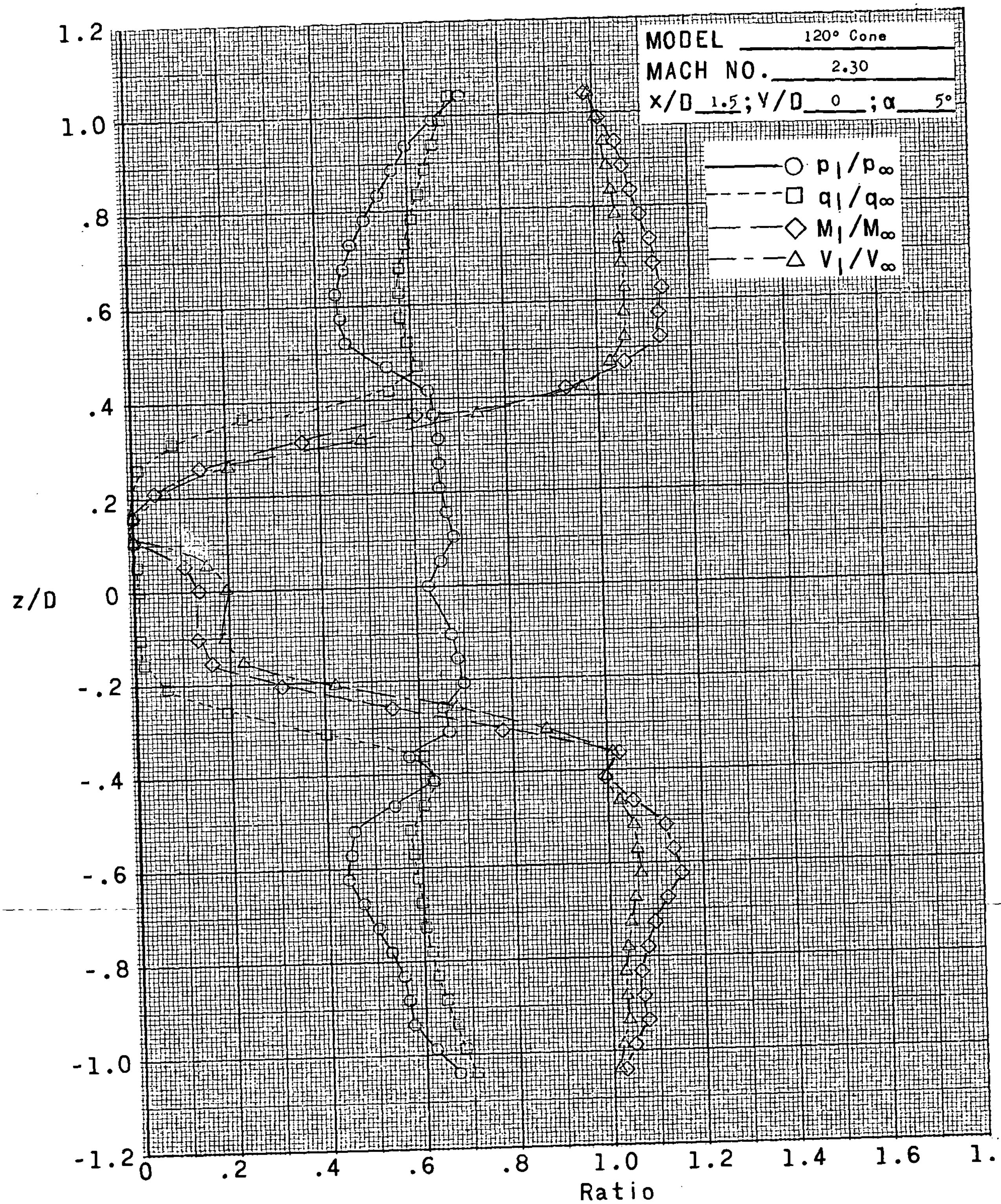
(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 10.- Concluded.



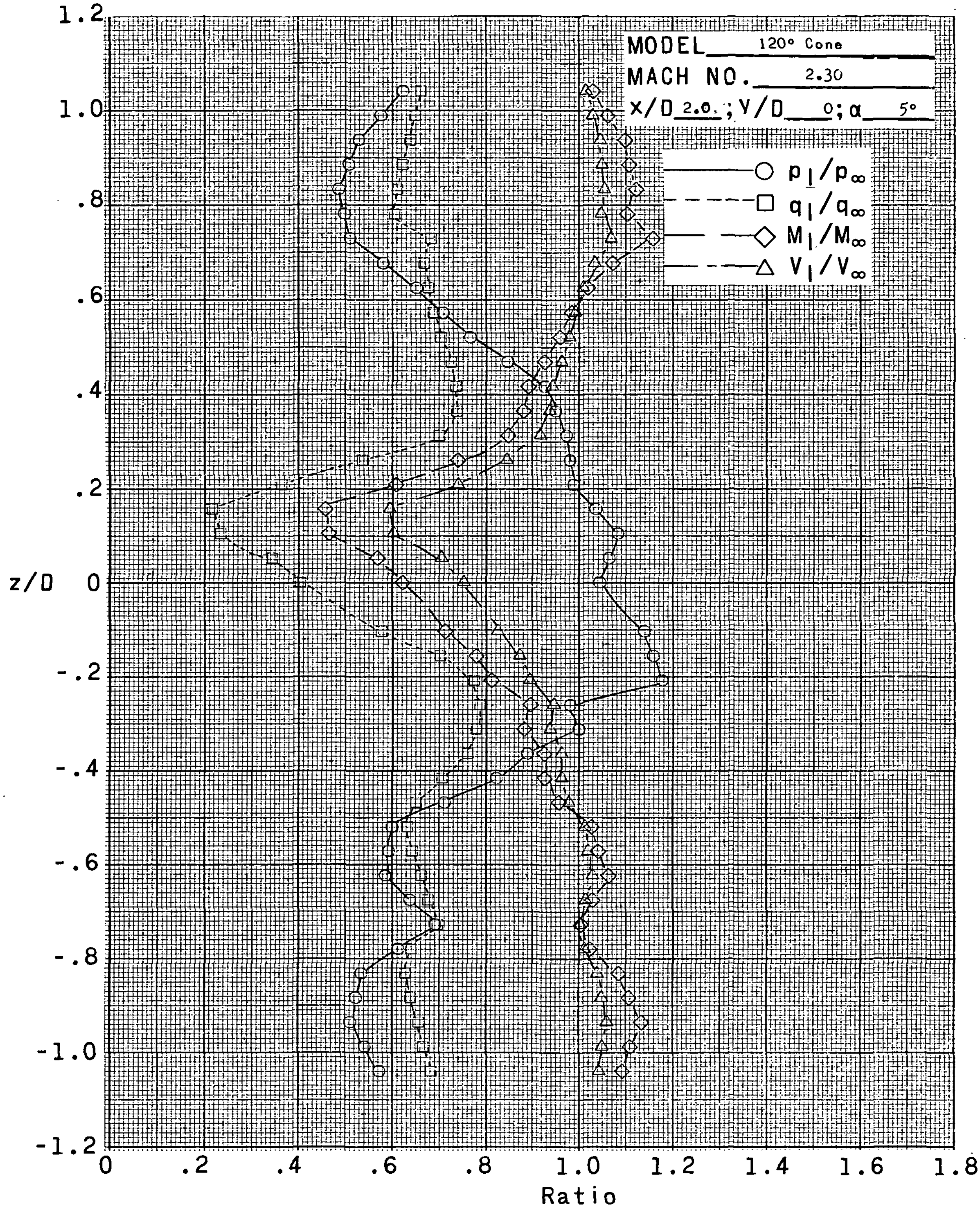
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^\circ$.

Figure 11.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D at the center of wake of a 120°-included-angle cone at a Mach number of 2.30 and a Reynolds number of 1.65×10^6 per foot (5.42×10^6 per meter).



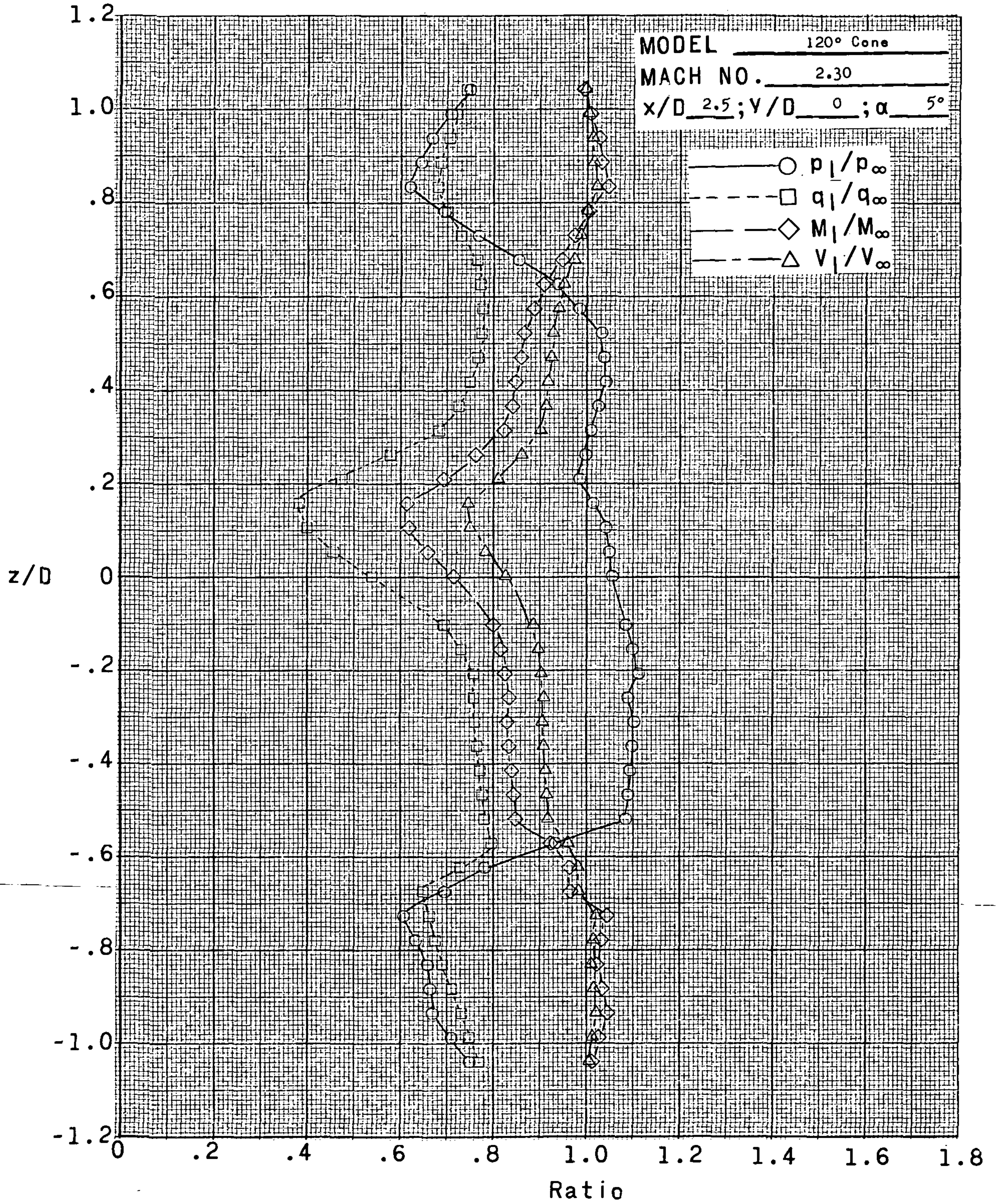
(b) x/D = 1.5; y/D = 0; α = 5°.

Figure 11.- Continued.



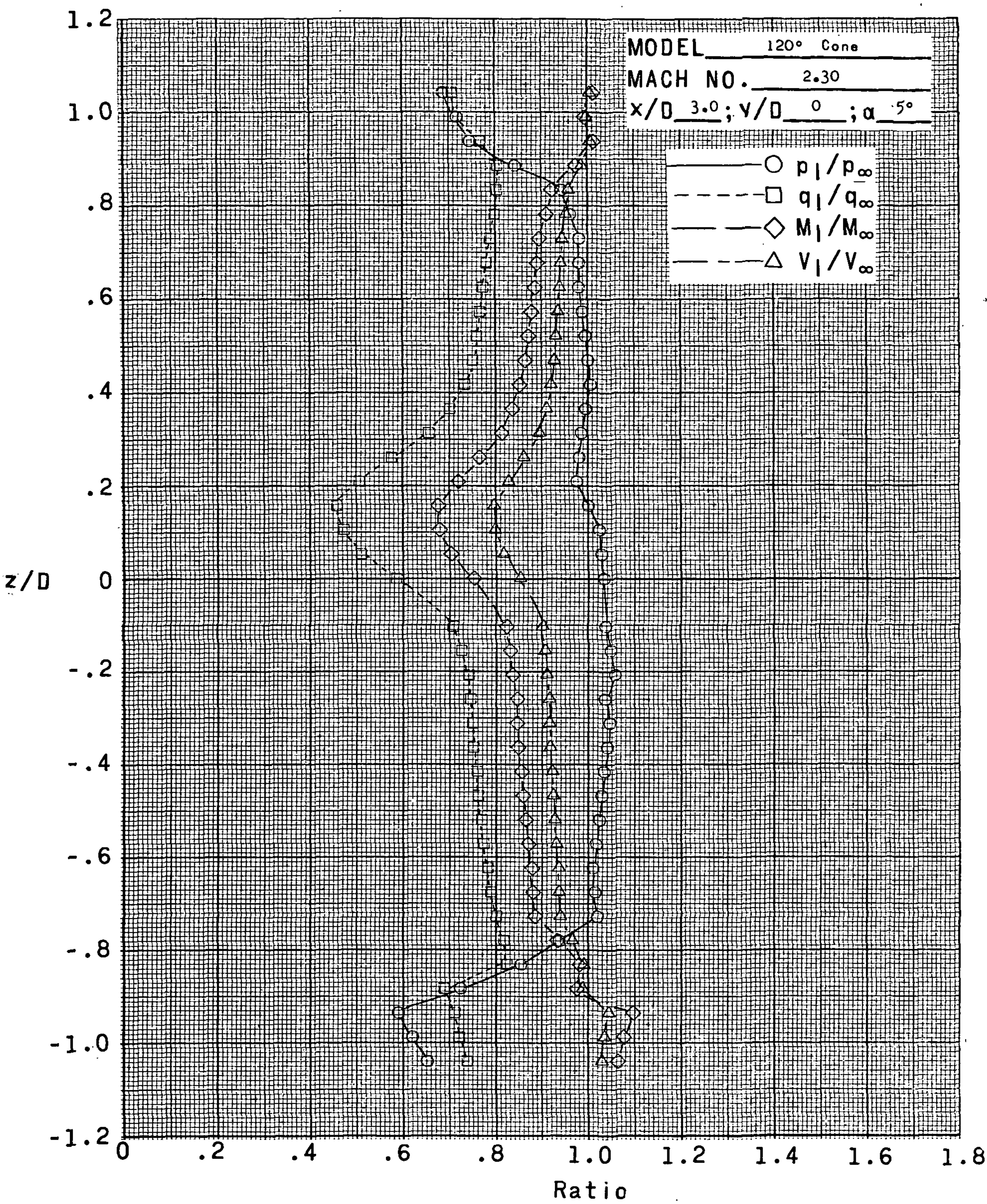
(c) x/D = 2.0; y/D = 0; α = 5°.

Figure 11.- Continued.



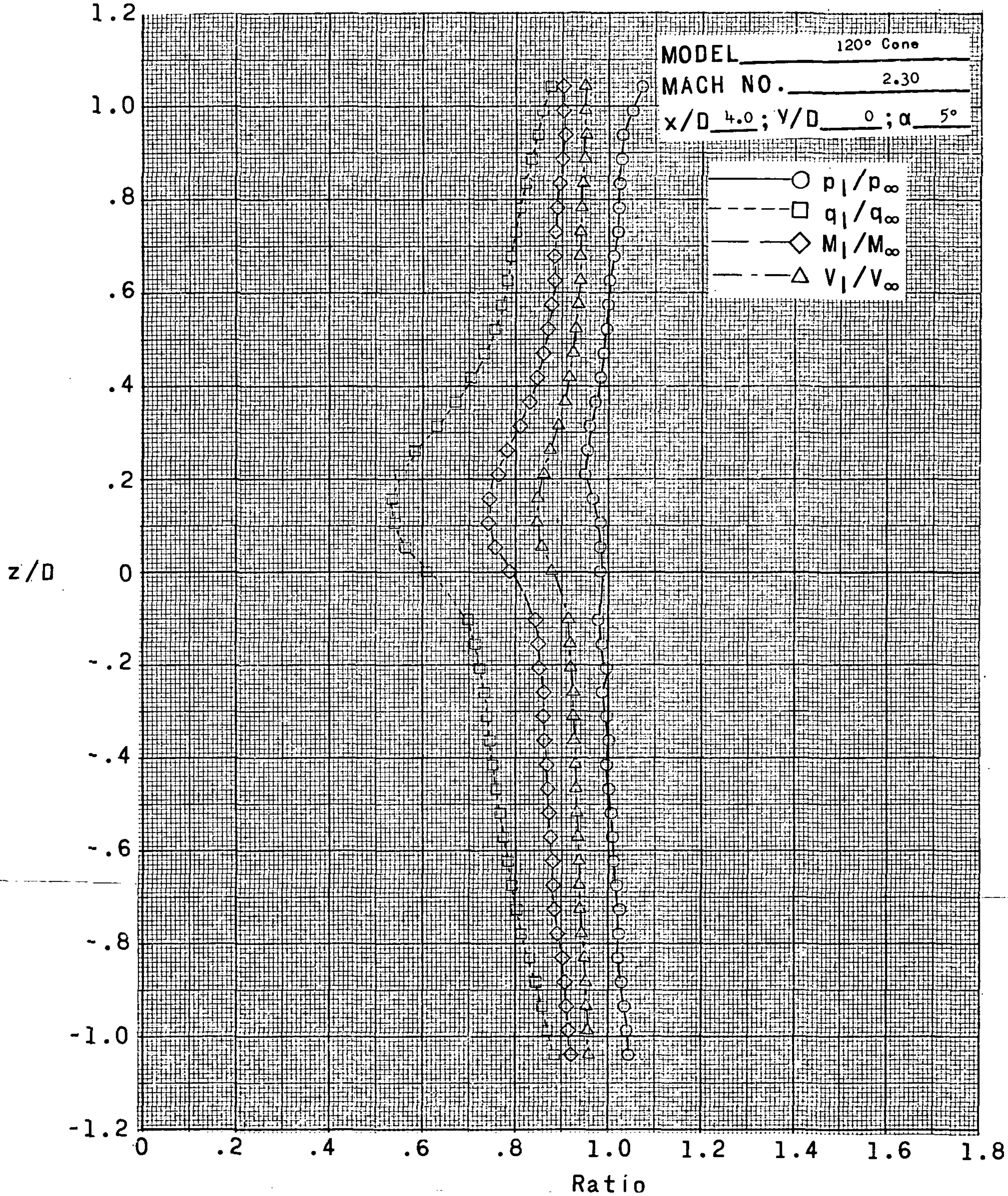
(d) x/D = 2.5; y/D = 0; α = 5°.

Figure 11.- Continued.



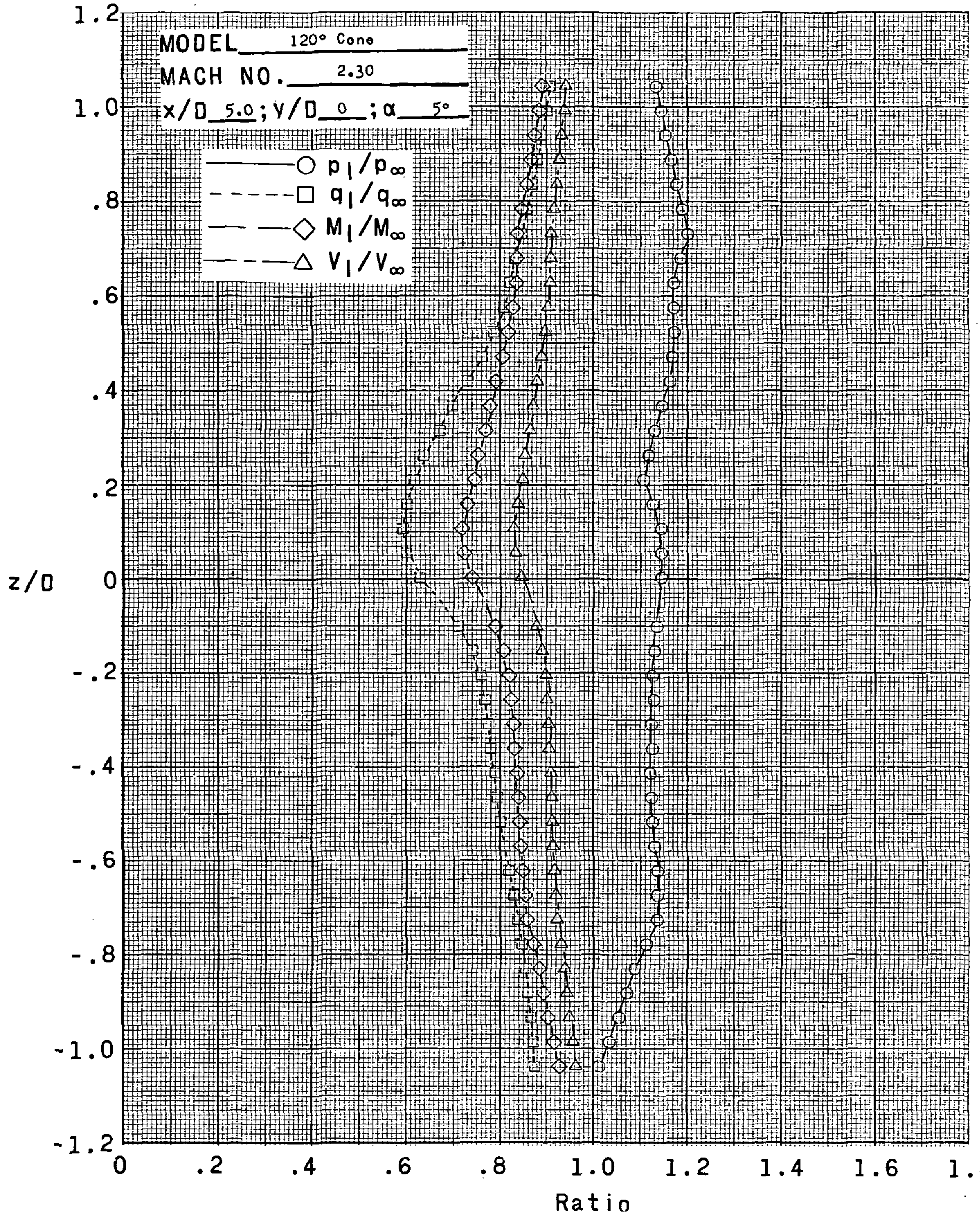
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



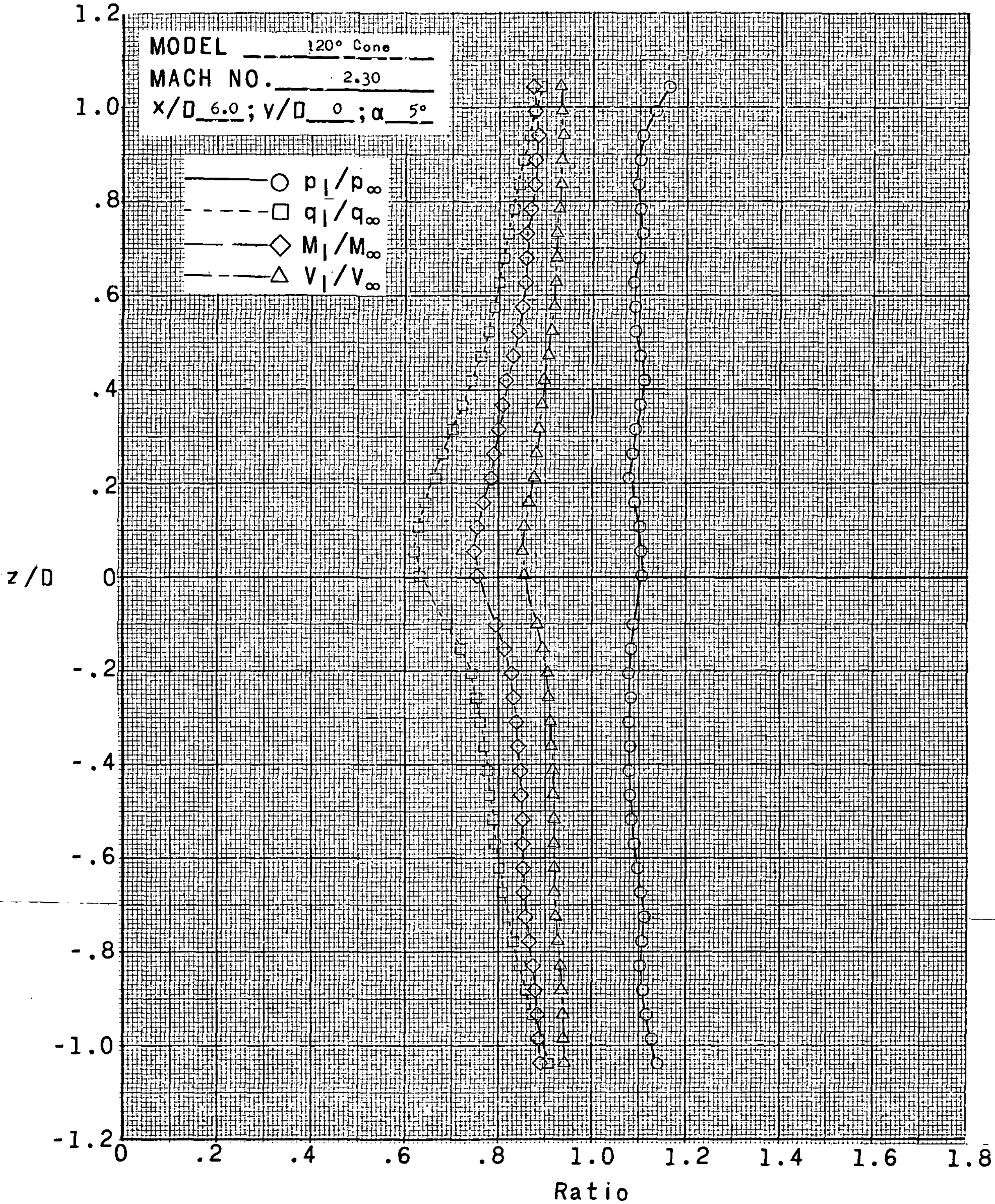
(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



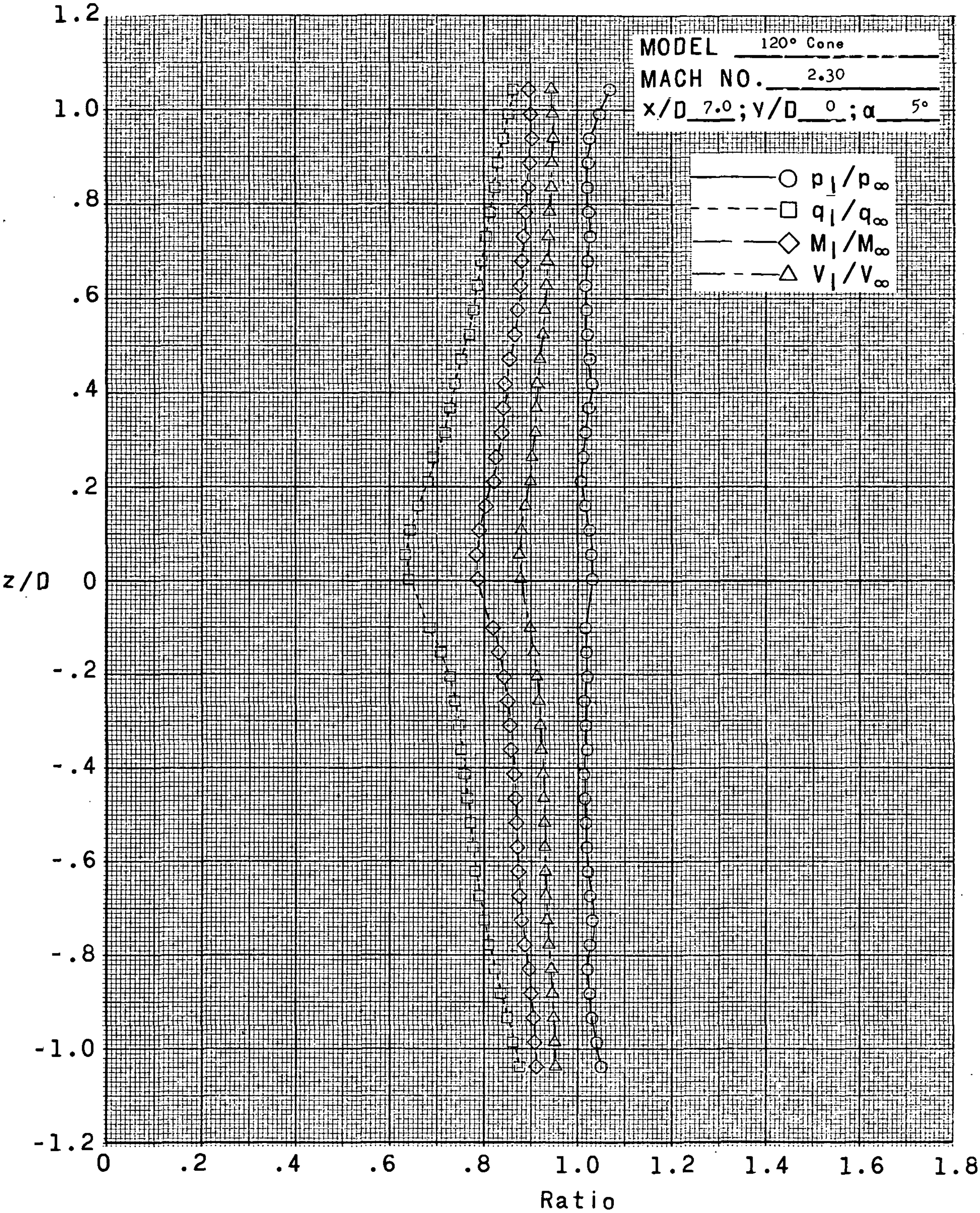
(g) x/D = 5.0; y/D = 0; α = 5°.

Figure 11.- Continued.



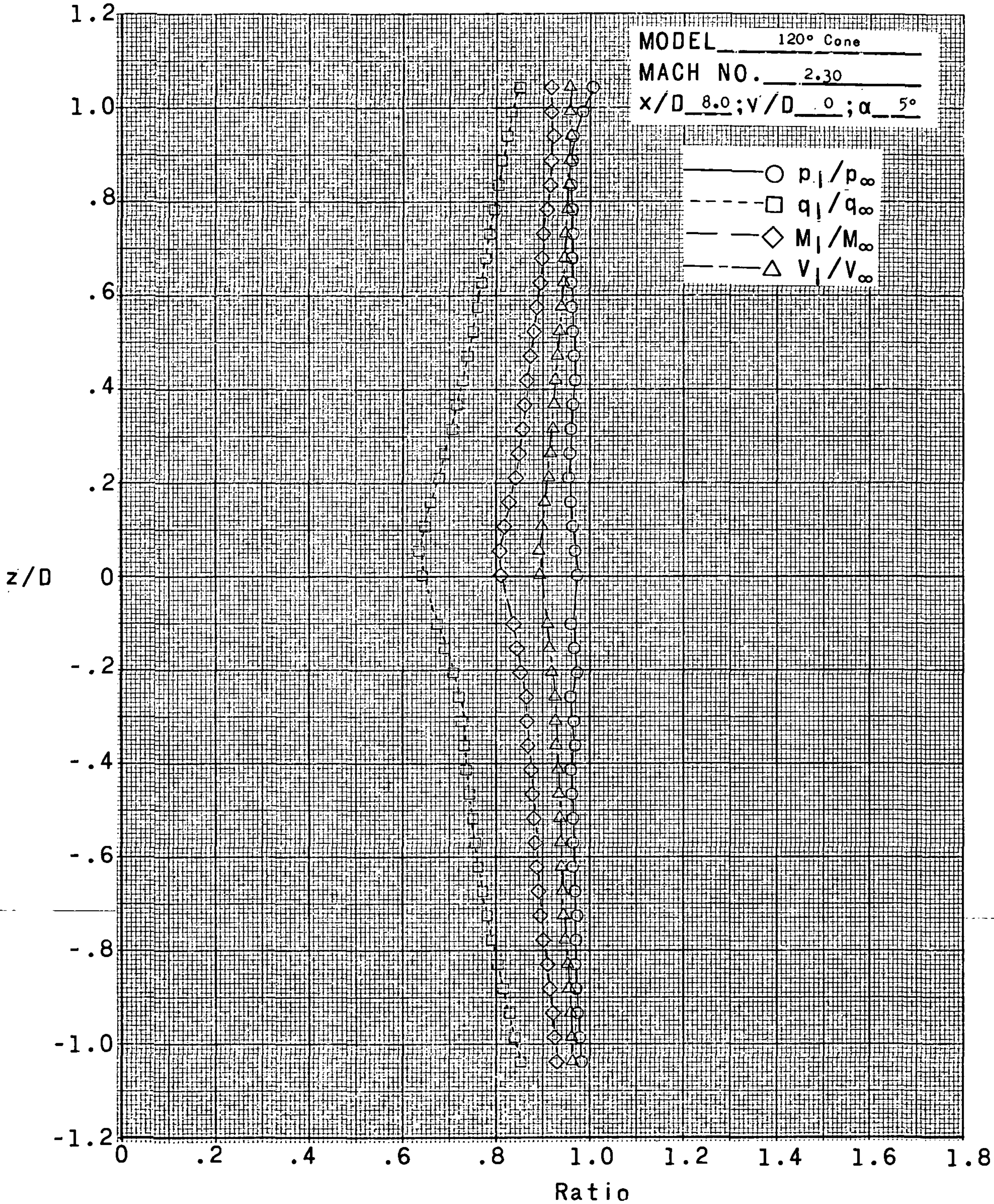
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 11.- Continued.



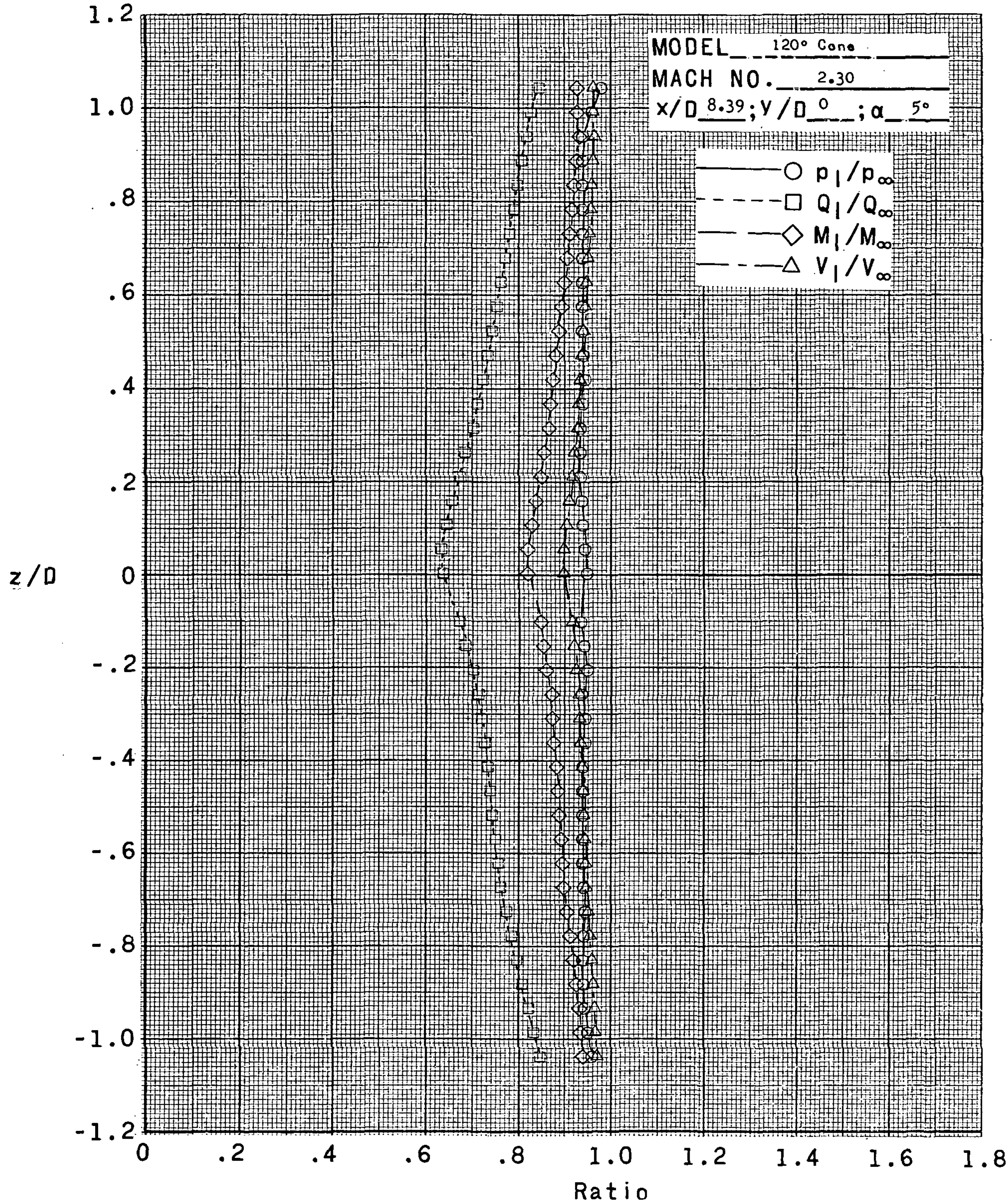
(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



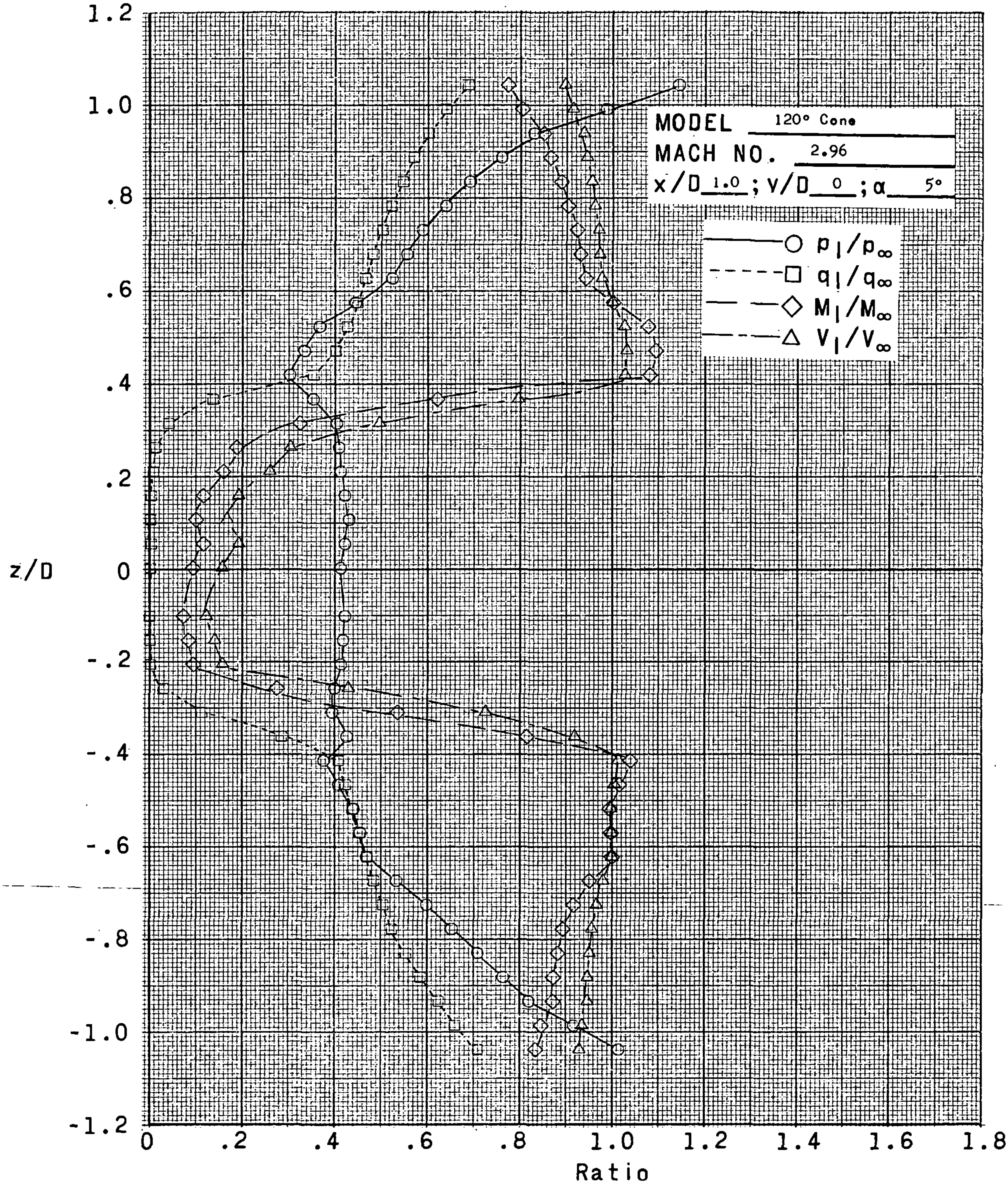
(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Continued.



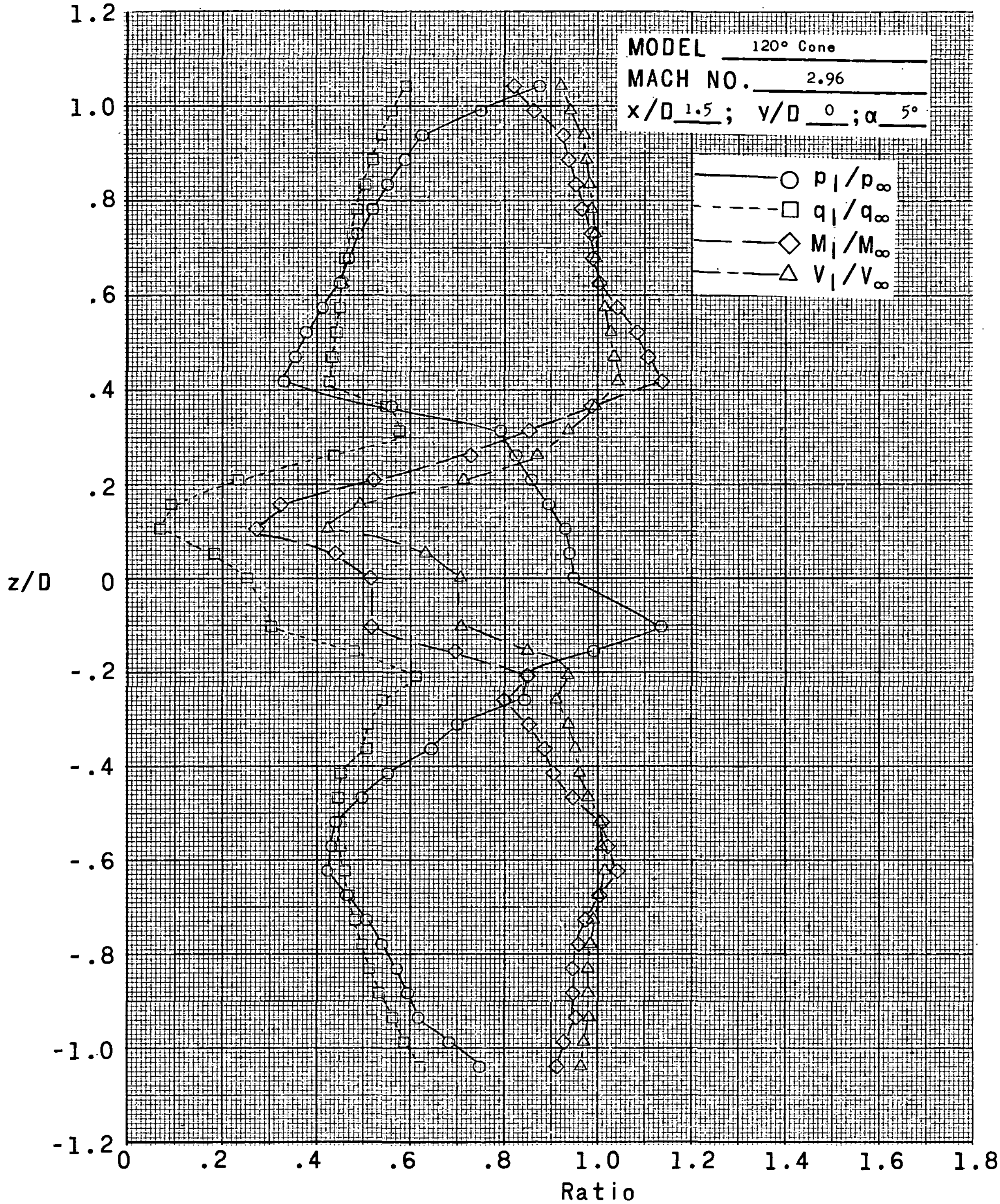
(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^0$.

Figure 11.- Concluded.



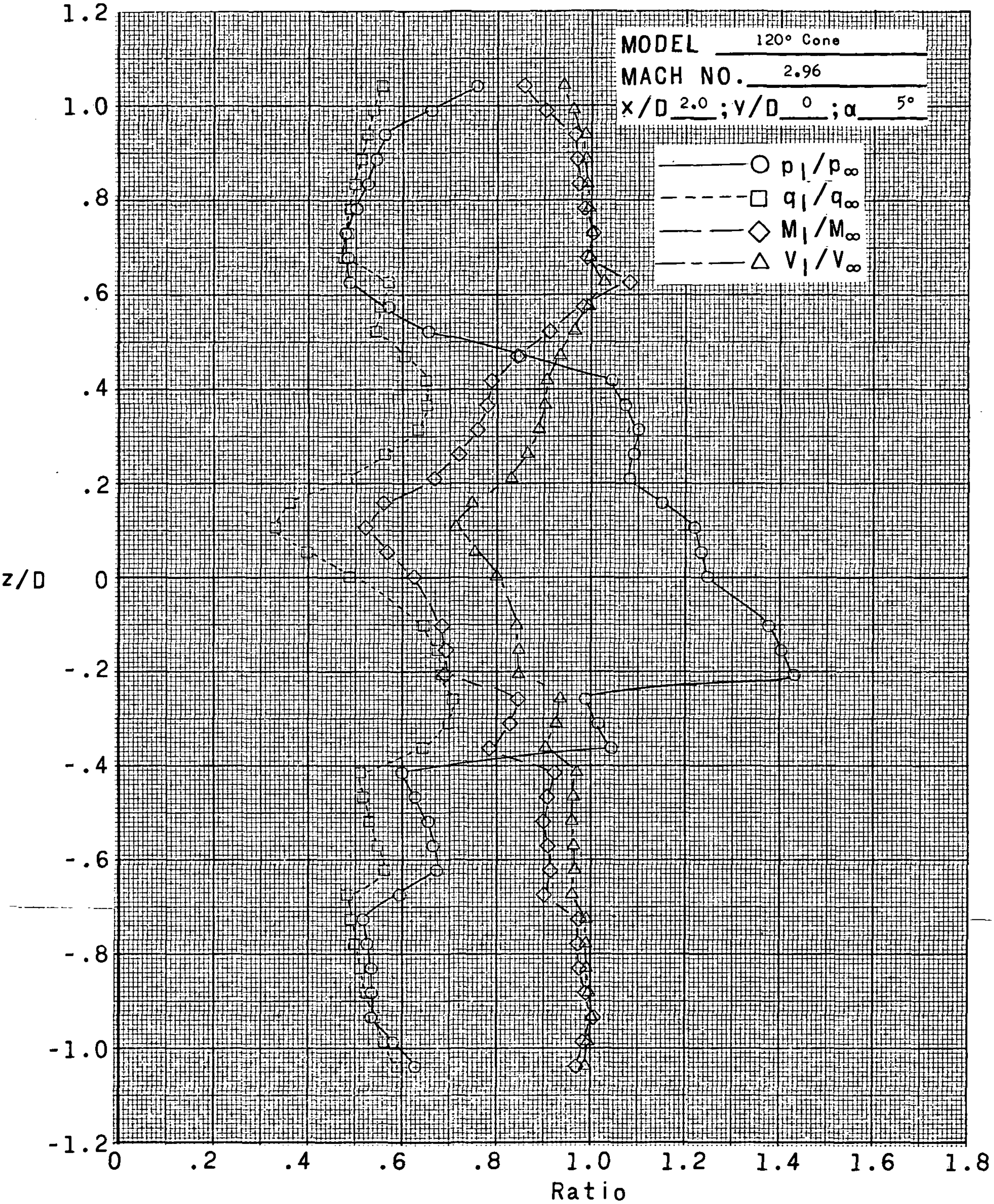
(a) $x/D = 1.0$; $y/D = 0$; $\alpha = 5^\circ$.

Figure 12.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D at the center of wake of a 120°-included-angle cone at a Mach number of 2.96 and a Reynolds number of 1.65×10^6 per foot (5.42×10^6 per meter).



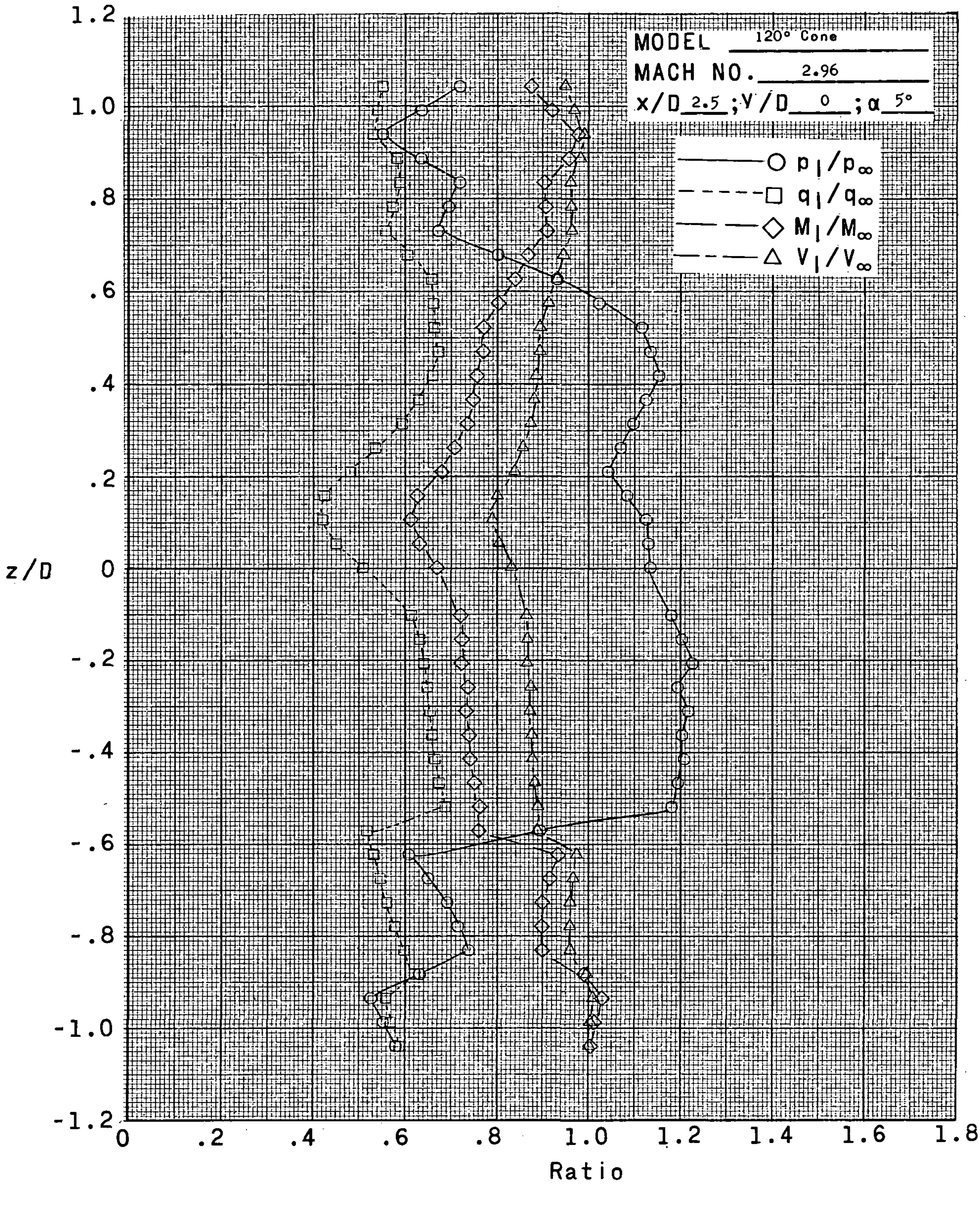
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^{o}$.

Figure 12.- Continued.



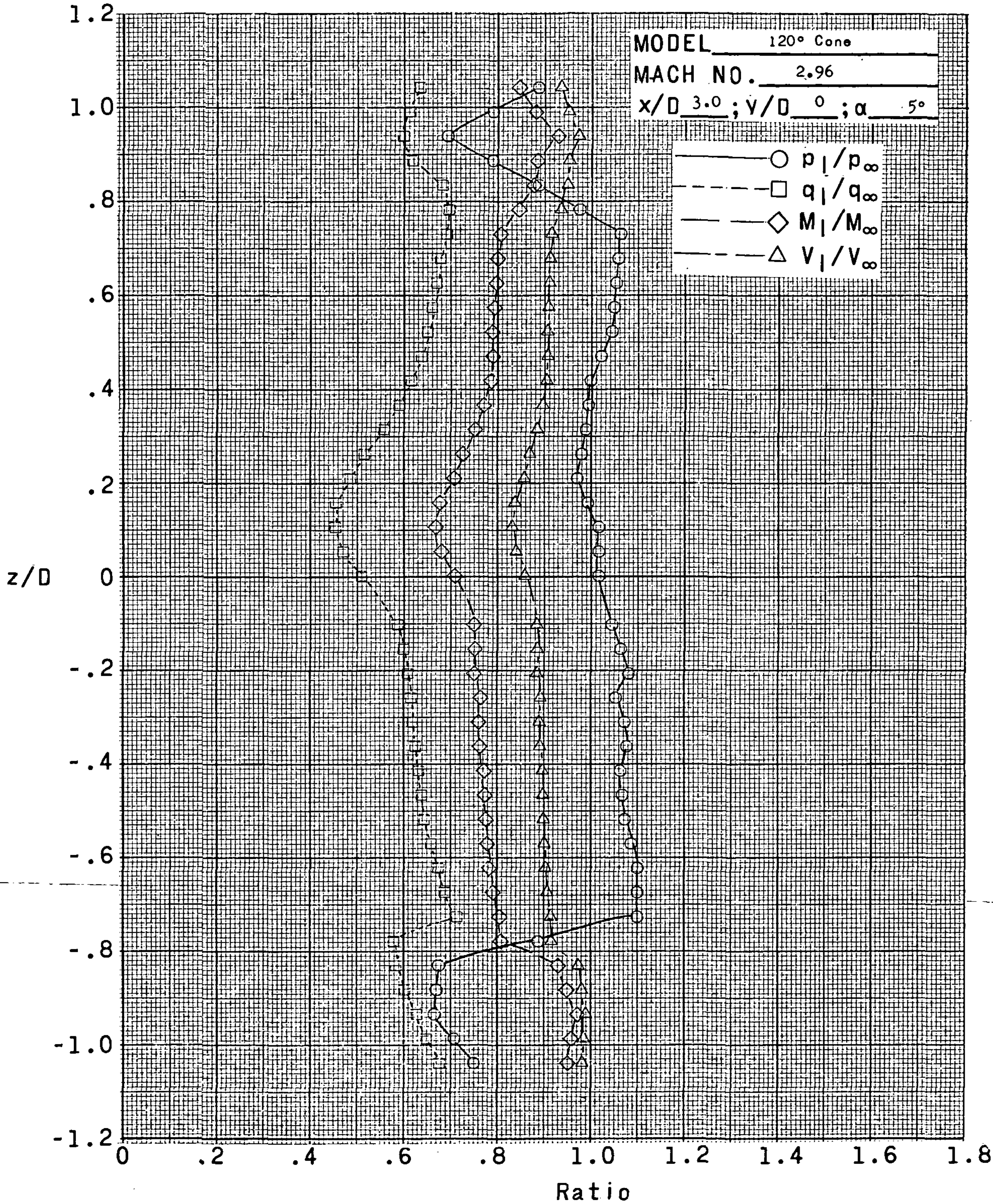
(c) x/D = 2.0; y/D = 0; α = 5°.

Figure 12.- Continued.



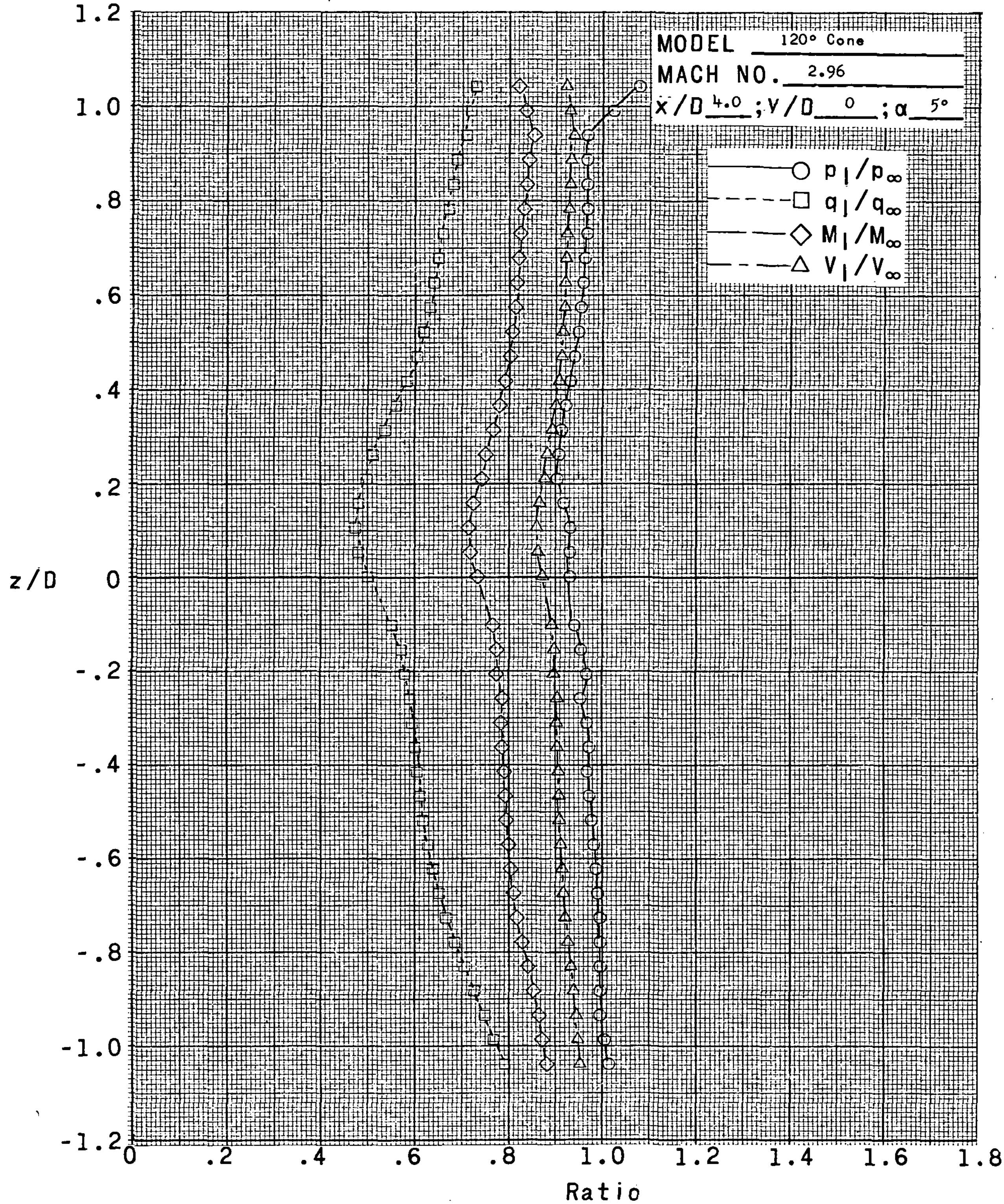
(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 12.- Continued.



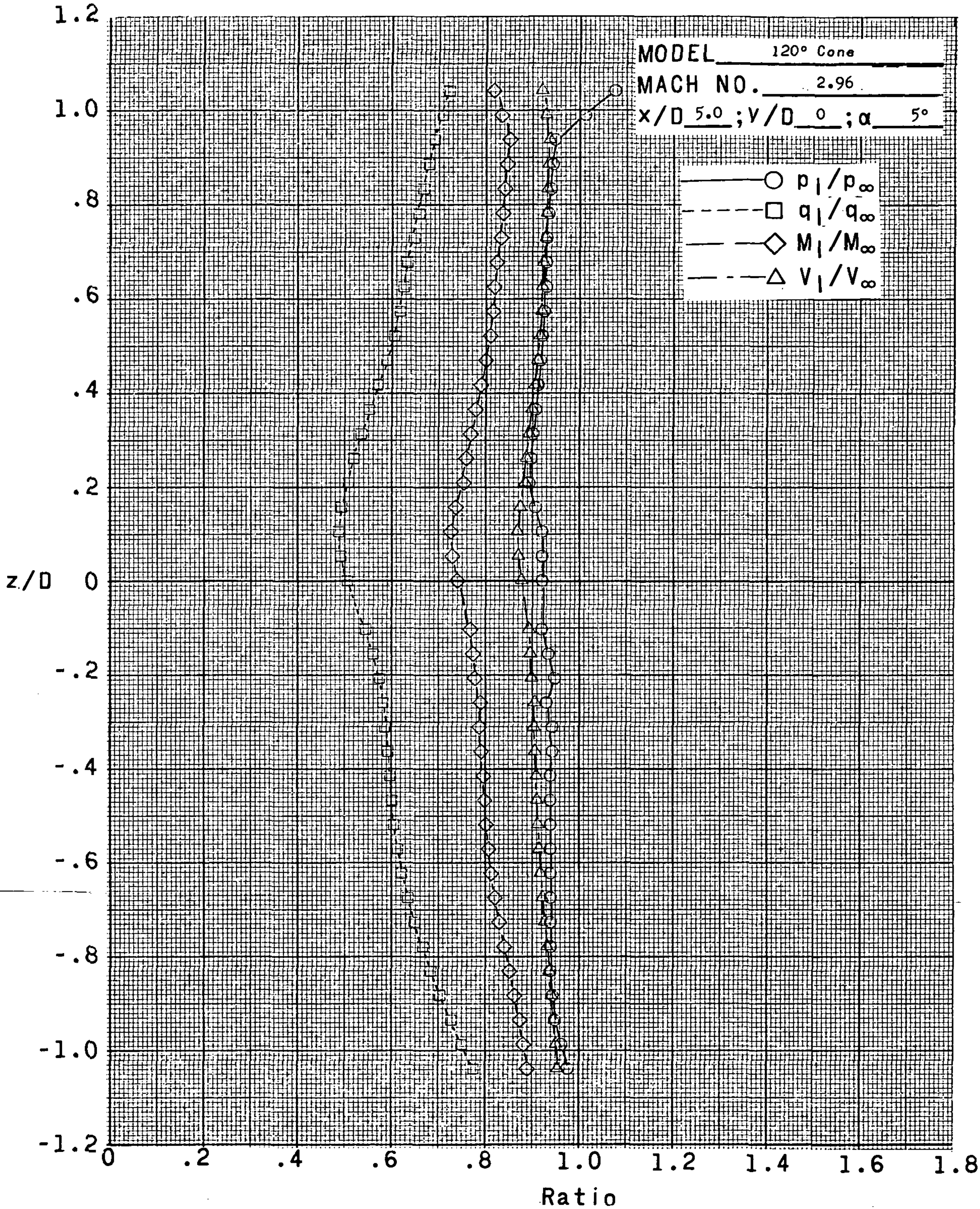
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 12.- Continued.



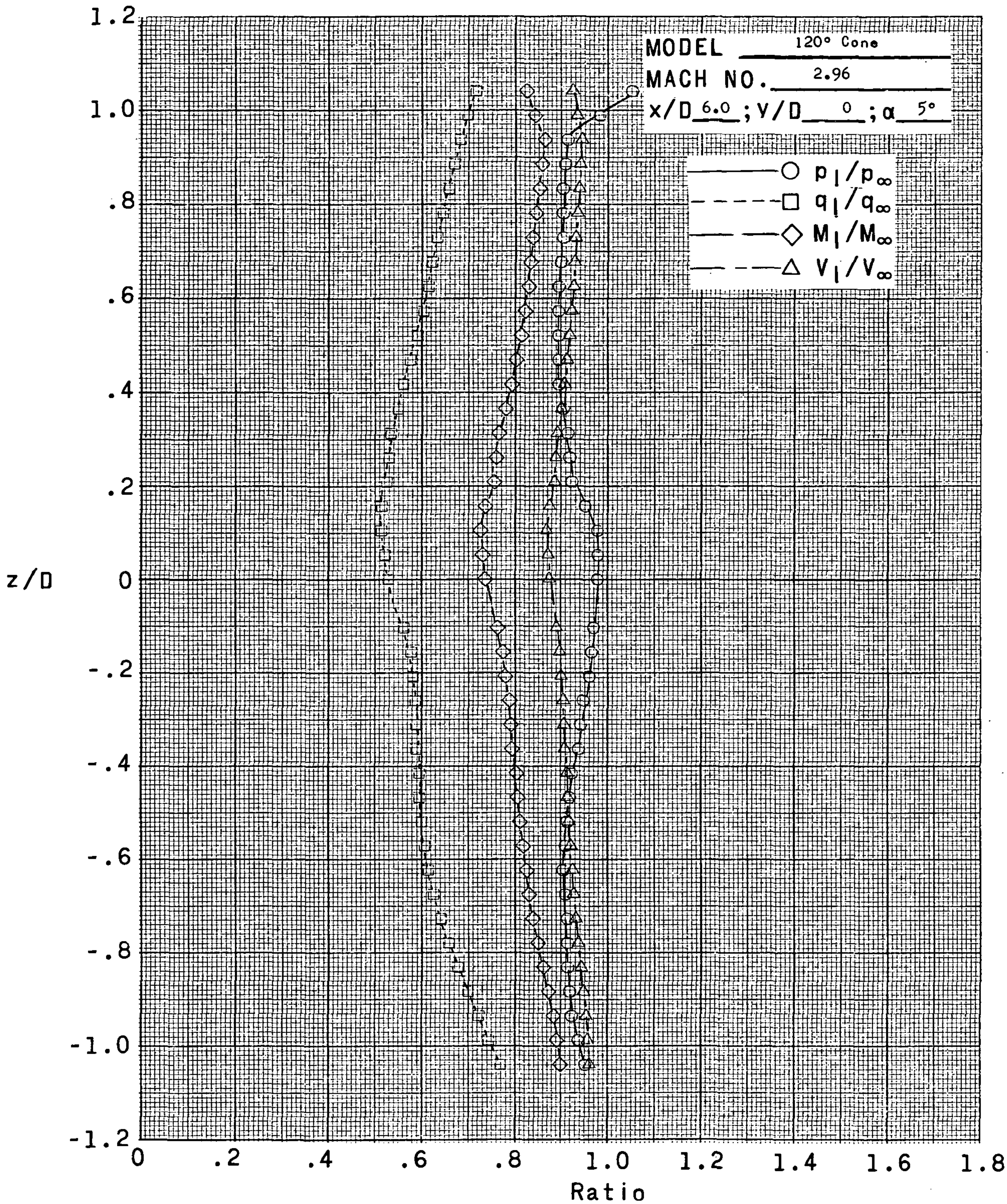
(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 12.- Continued.



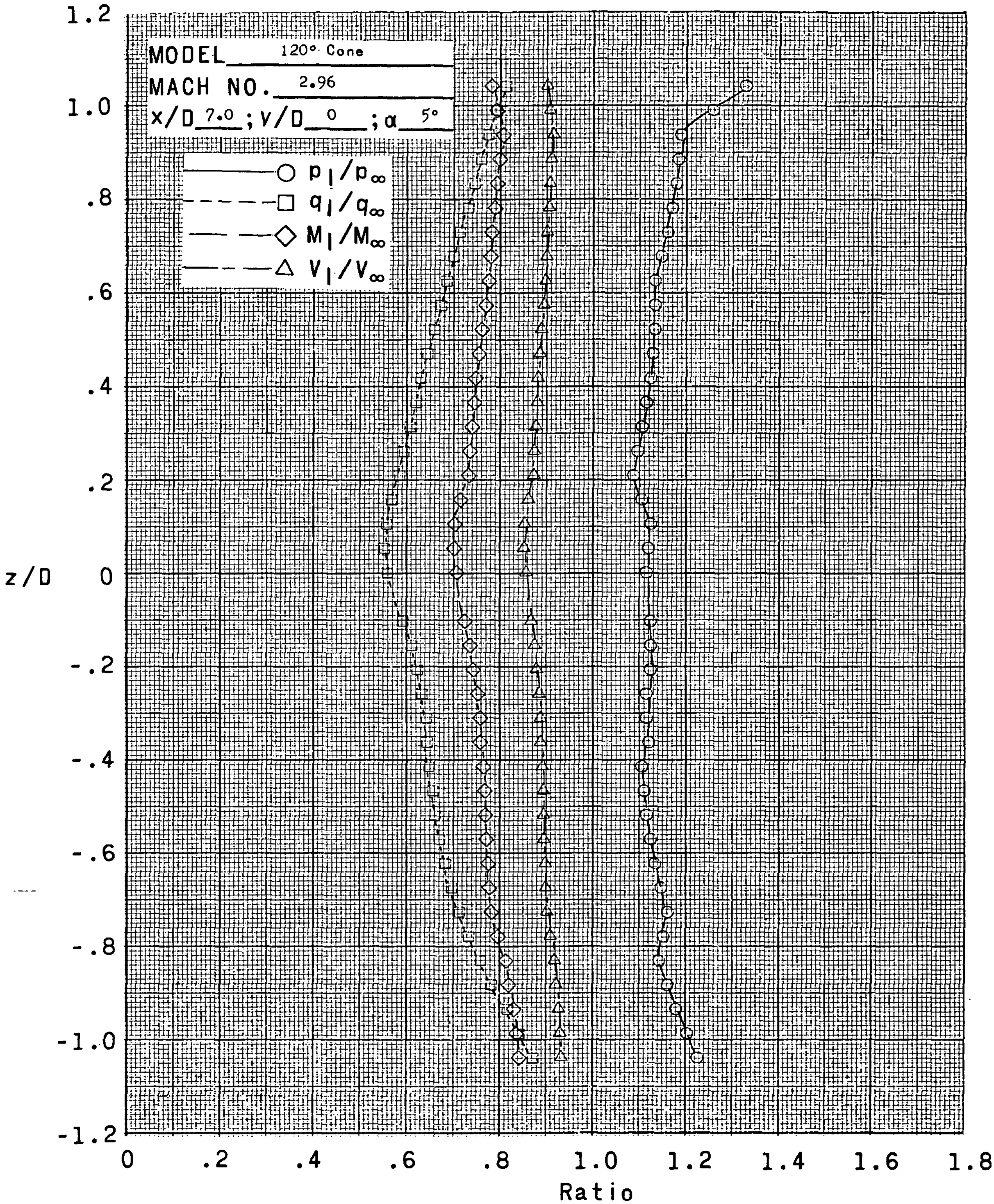
(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 12.- Continued.



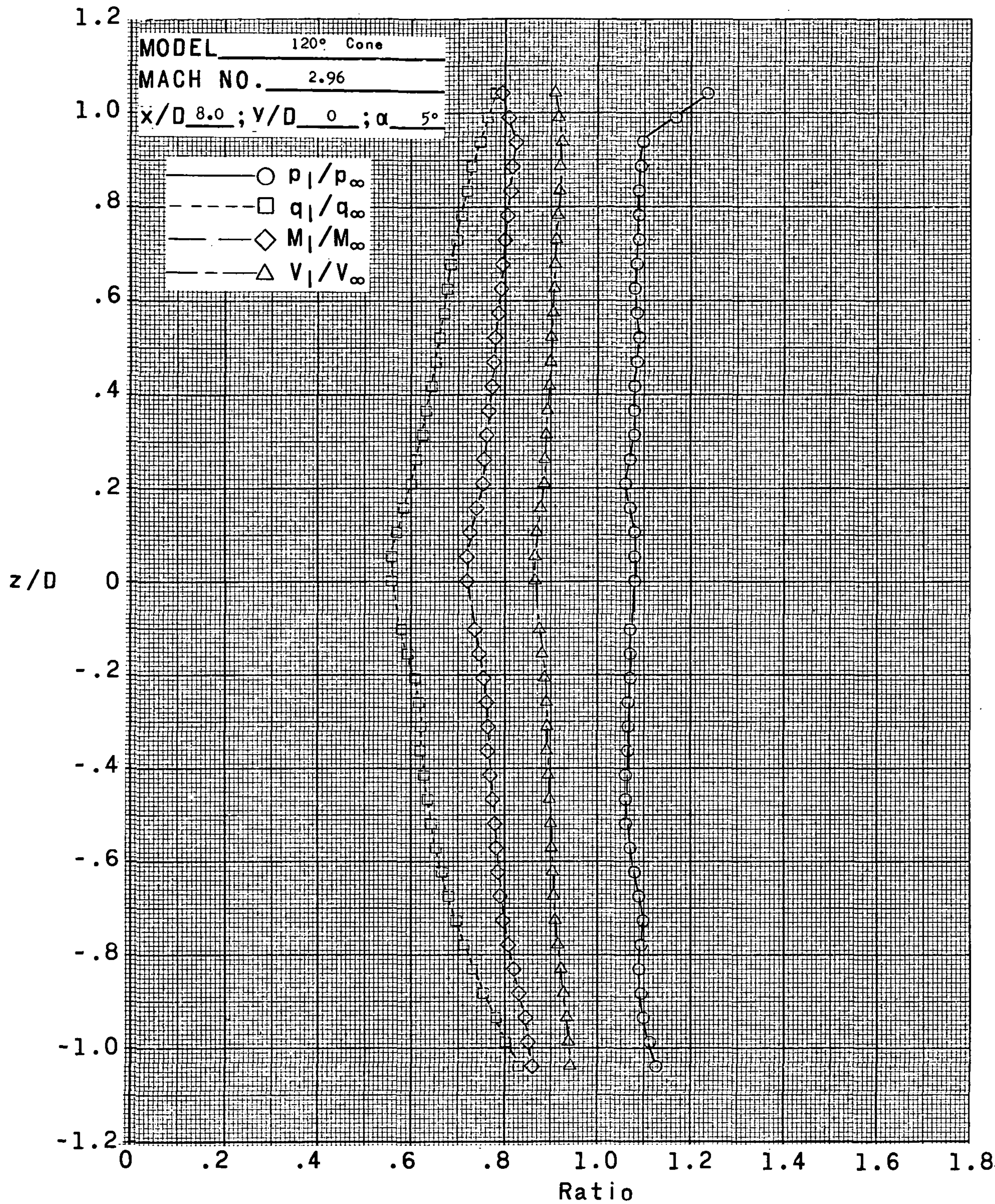
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 12.- Continued.



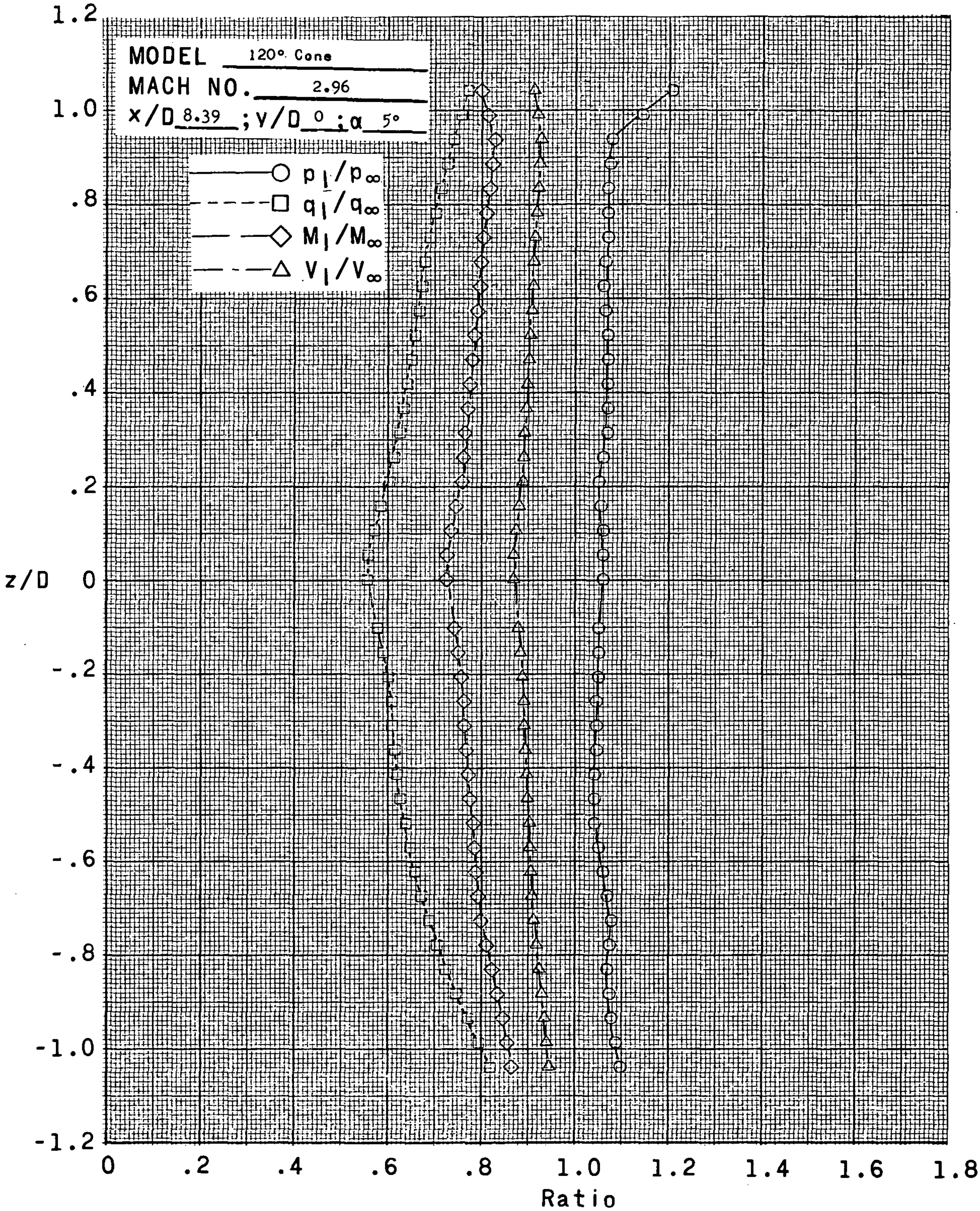
(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 12.- Continued.



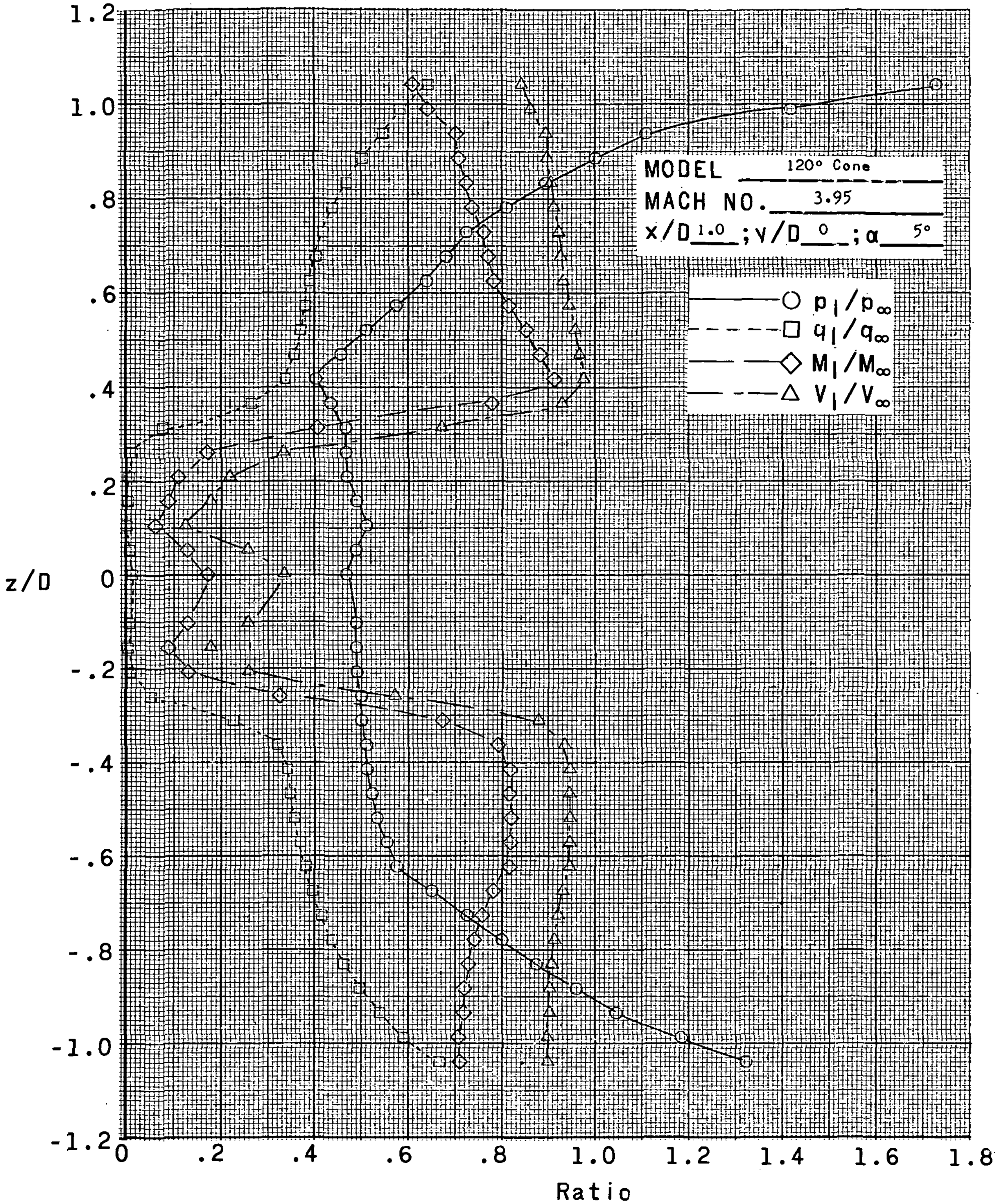
(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^o$.

Figure 12.- Continued.



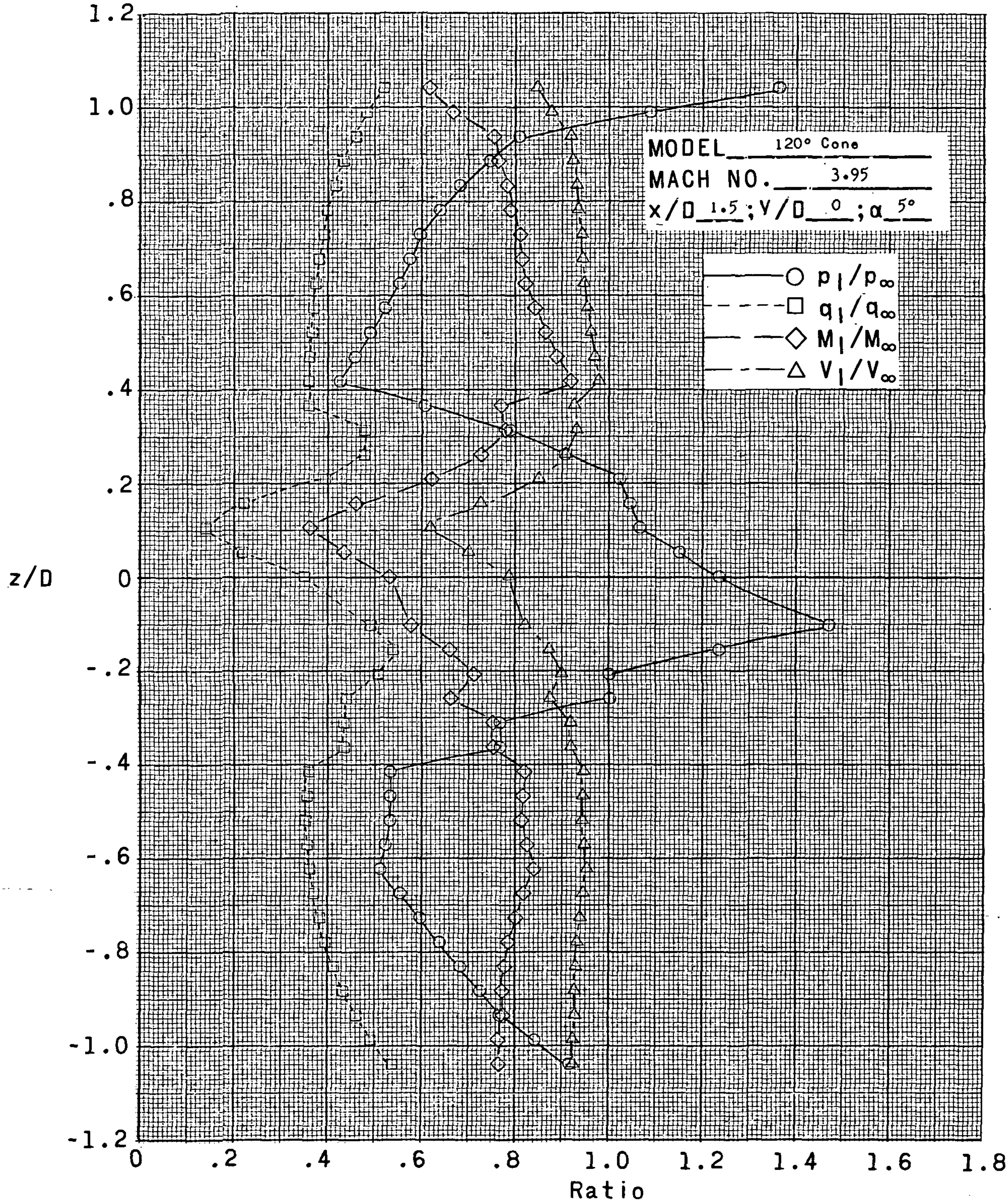
(k) $x/D = 8.39$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 12.- Concluded.



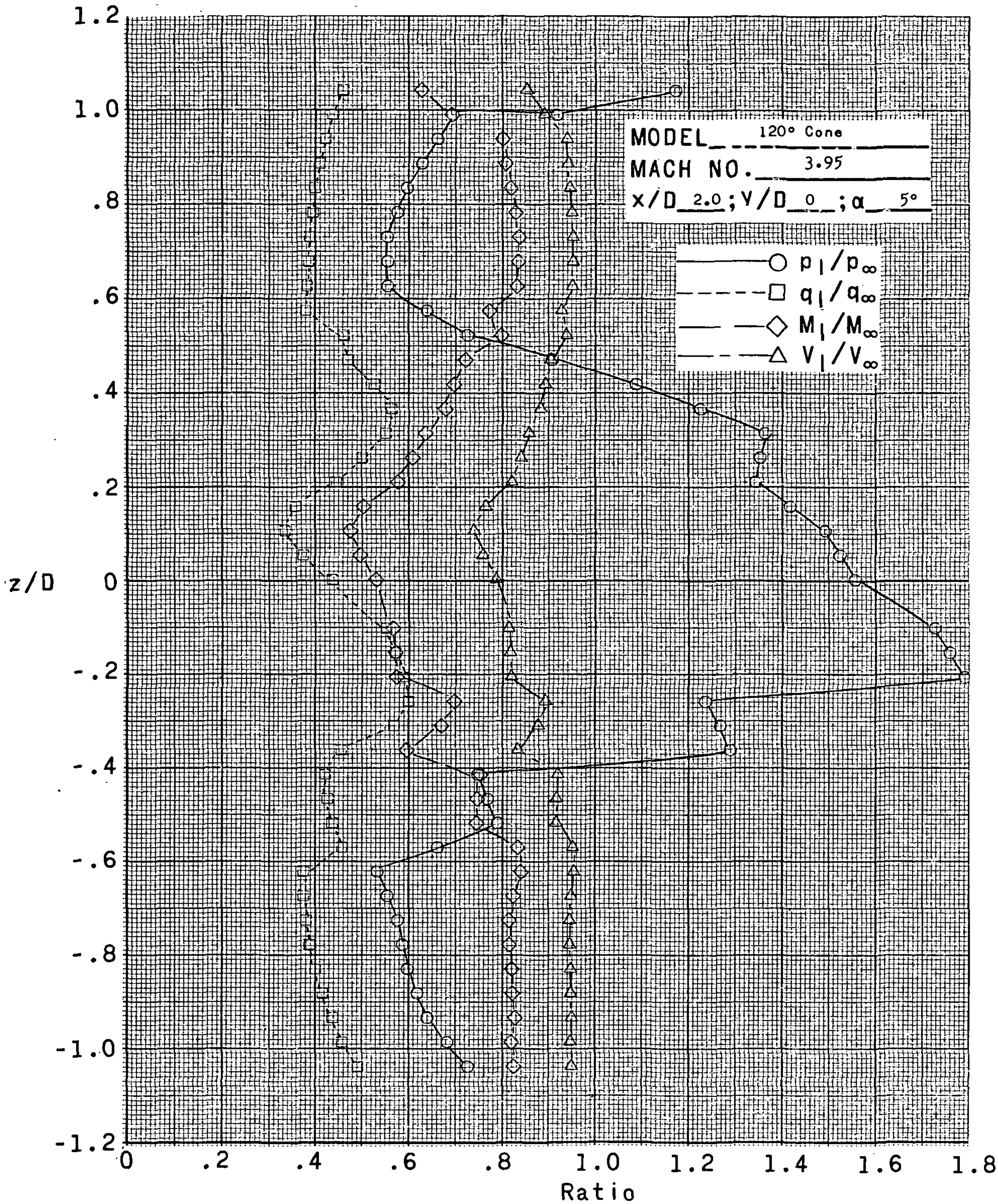
(a) x/D = 1.0; y/D = 0; α = 5°.

Figure 13.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D at the center of wake of a 120°-included-angle cone at a Mach number of 3.95 and a Reynolds number of 1.65×10^6 per foot (5.42×10^6 per meter).



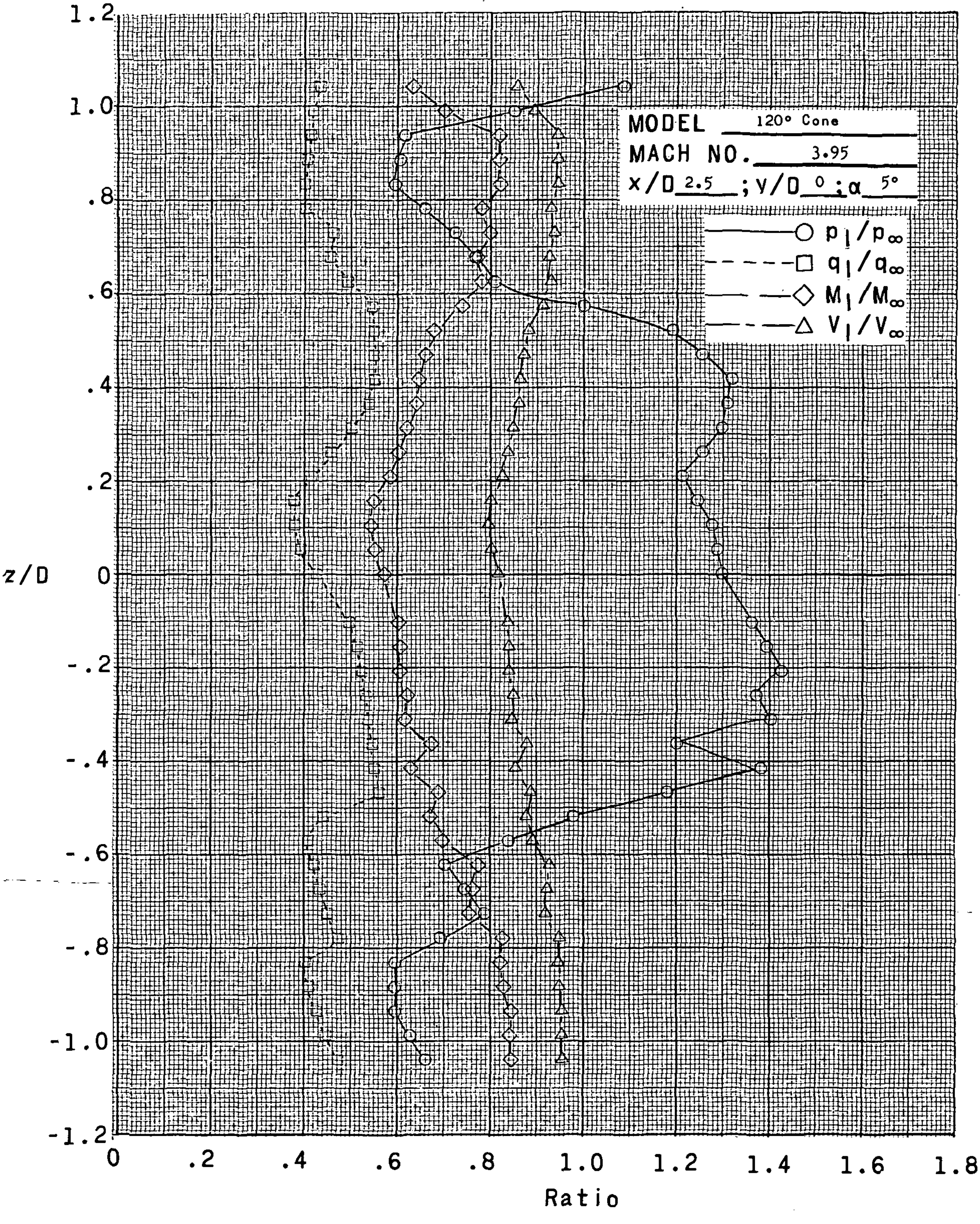
(b) $x/D = 1.5$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 13.- Continued.



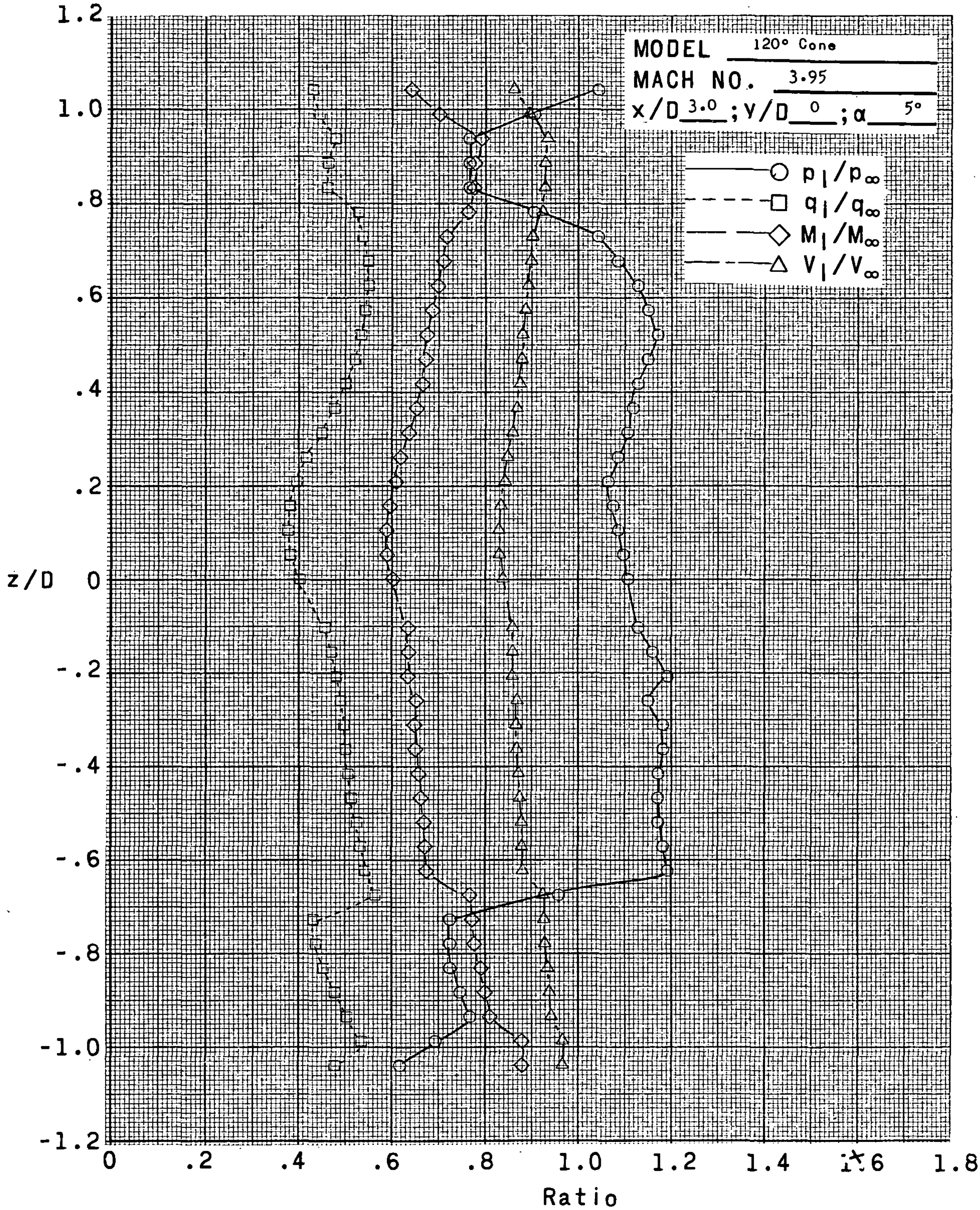
(c) x/D = 2.0; y/D = 0; α = 5°.

Figure 13.- Continued.



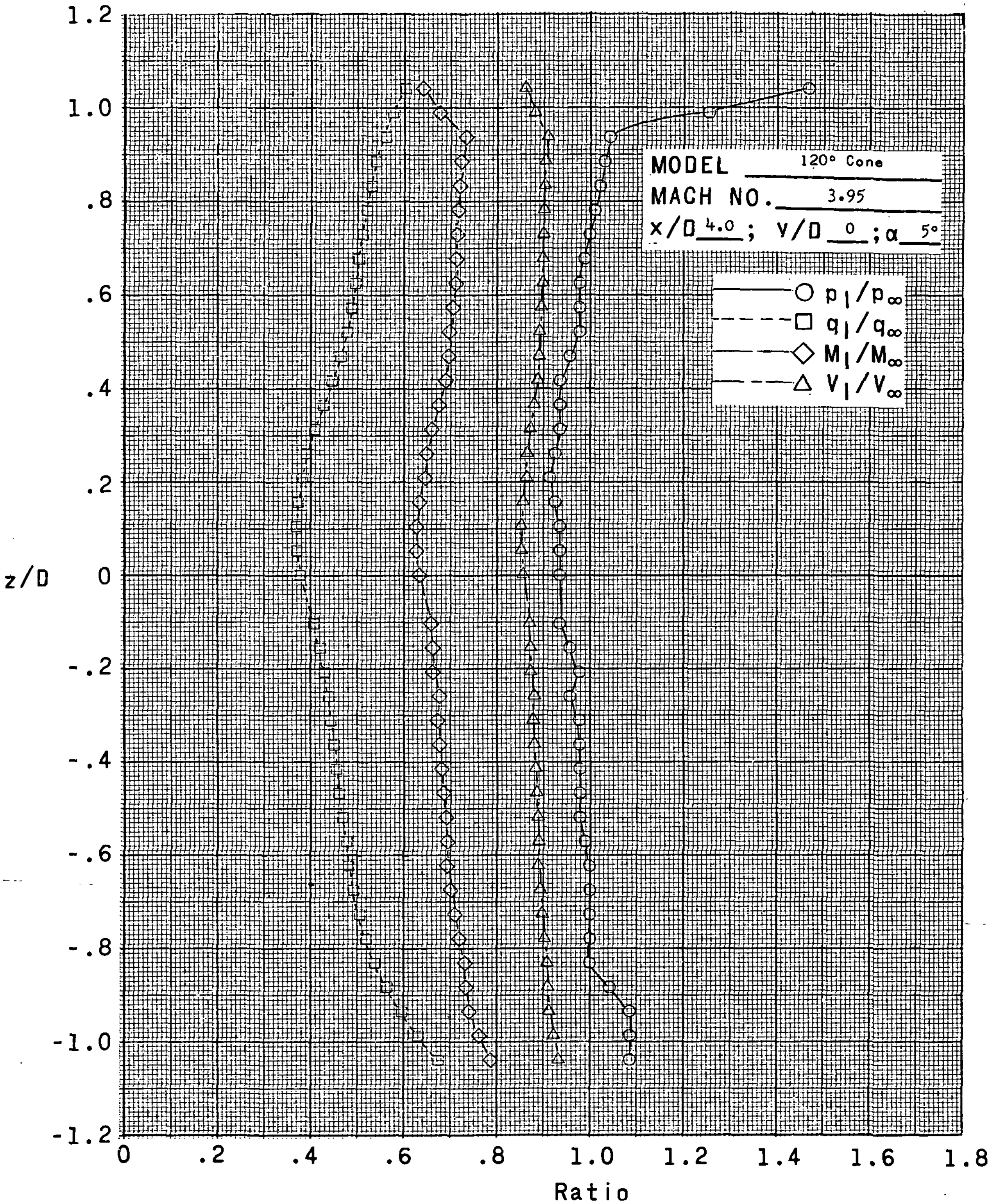
(d) $x/D = 2.5$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 13.- Continued.



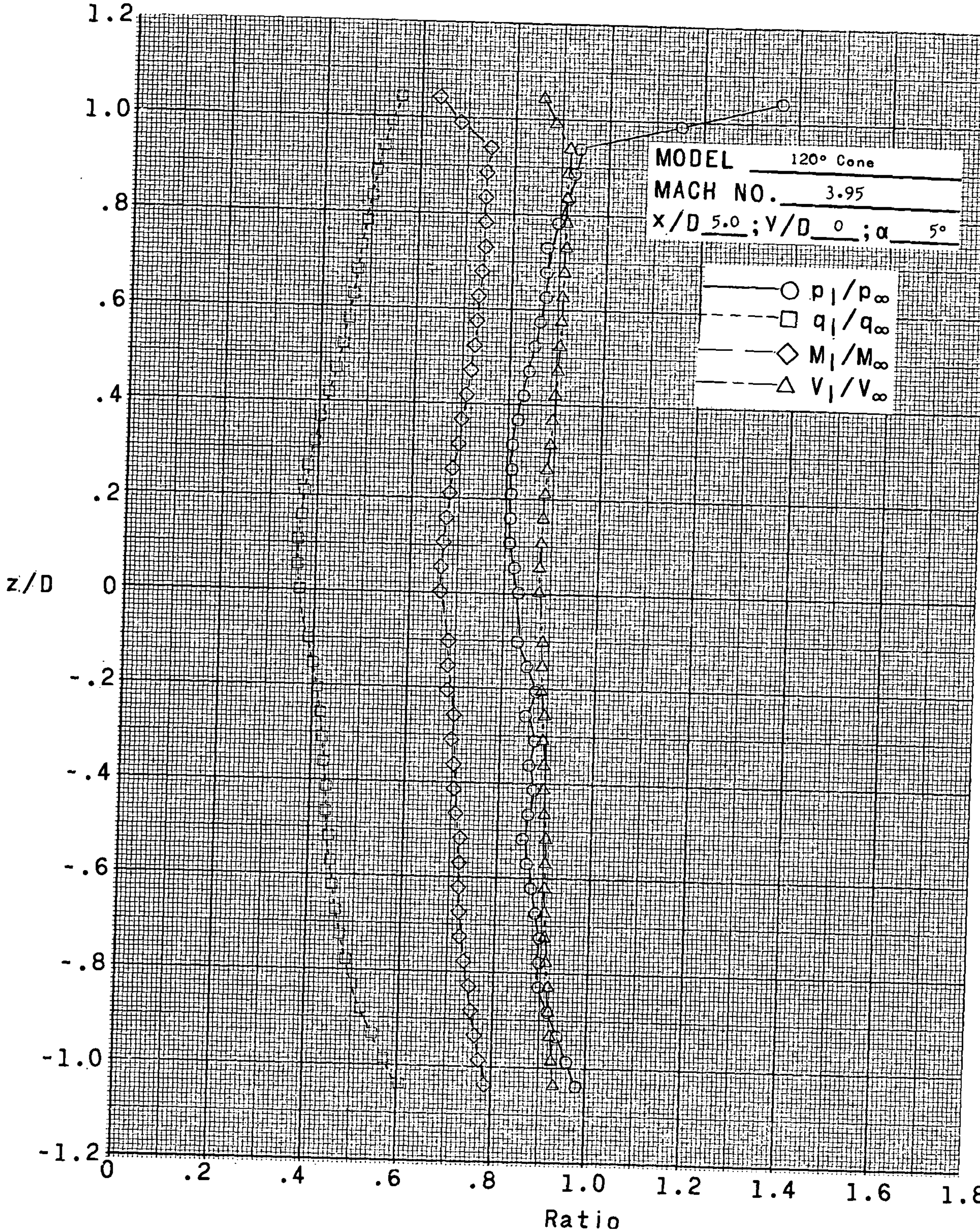
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 5^{0}$.

Figure 13.- Continued.



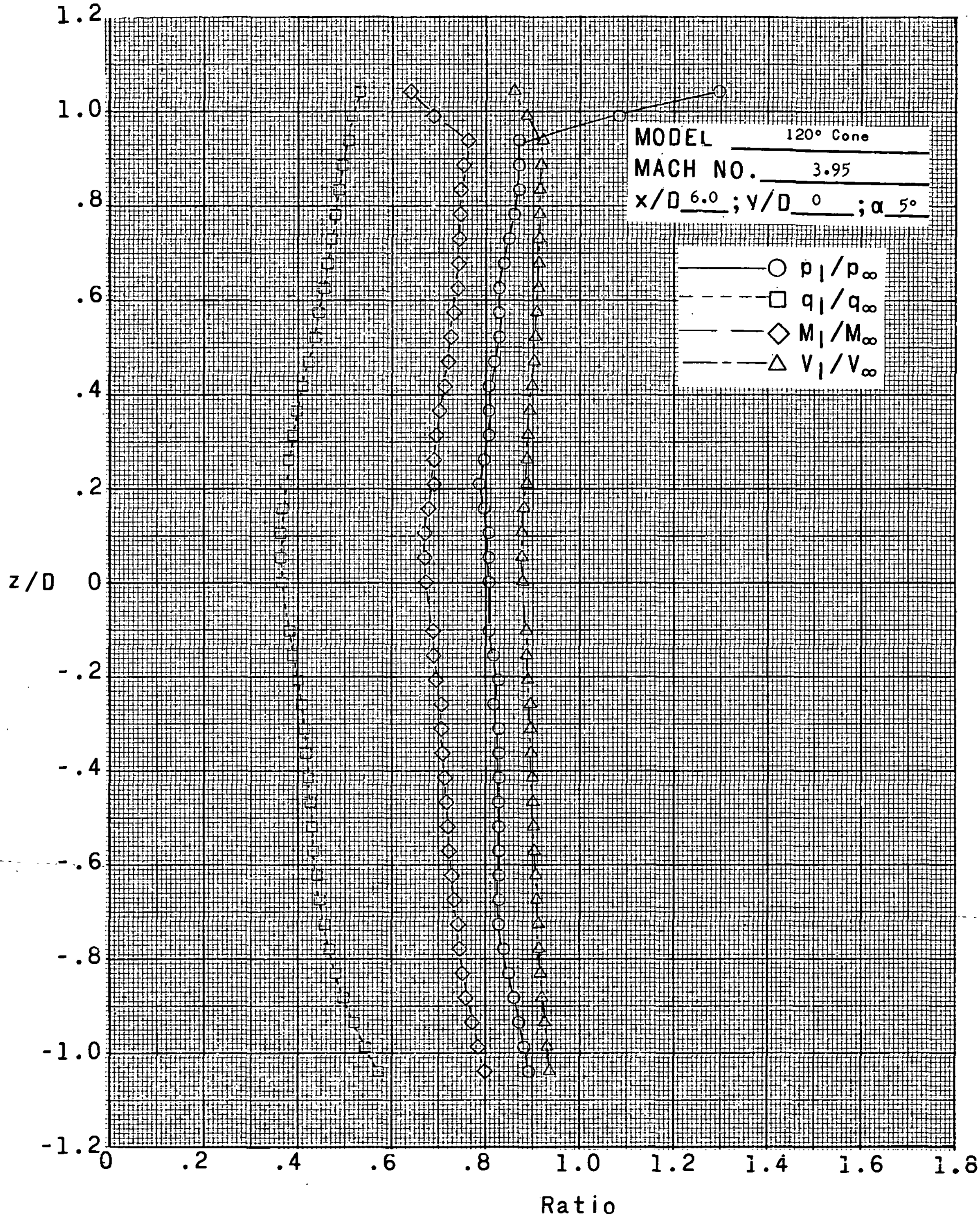
(f) x/D = 4.0; y/D = 0; α = 5°.

Figure 13.- Continued.



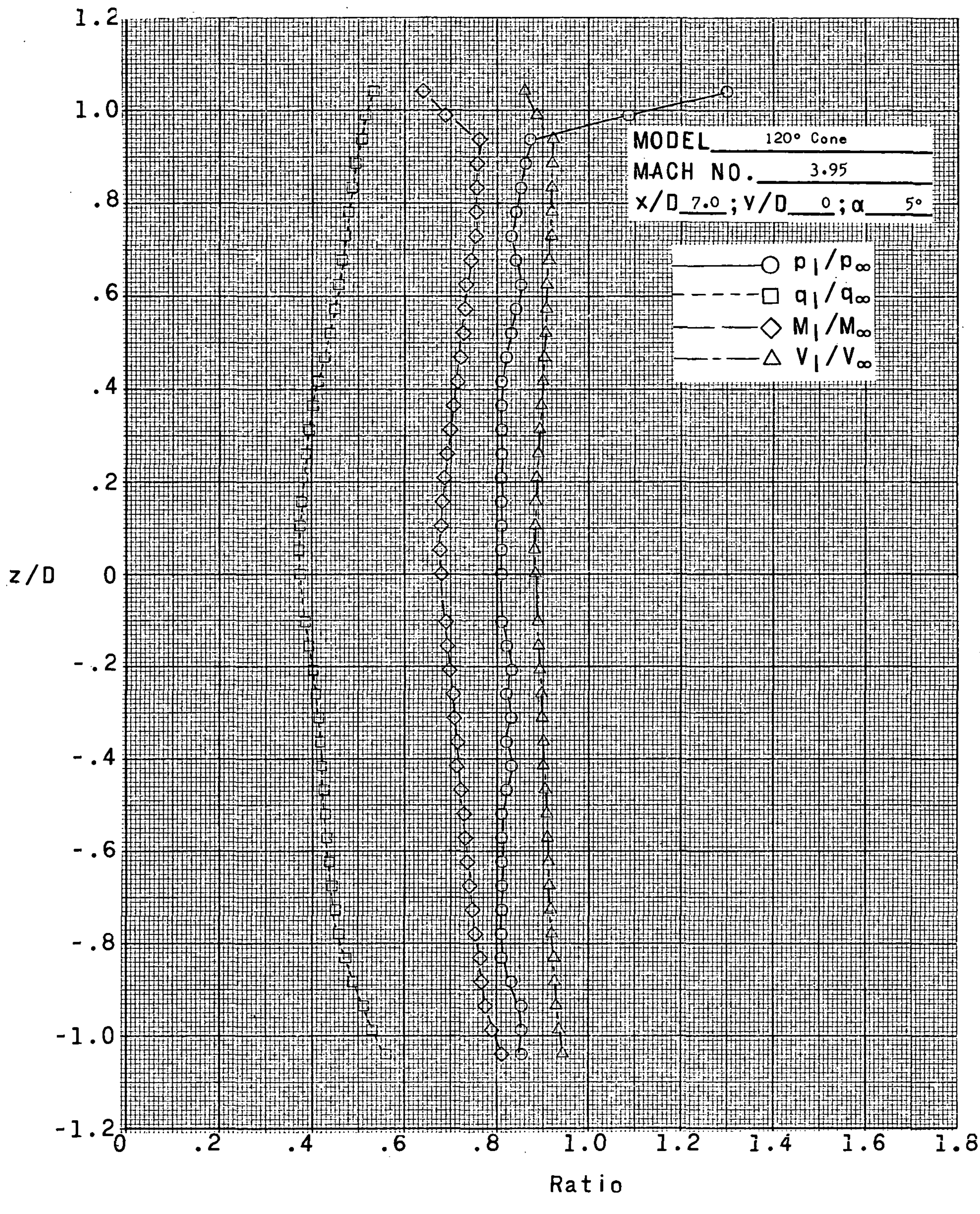
(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 13.- Continued.



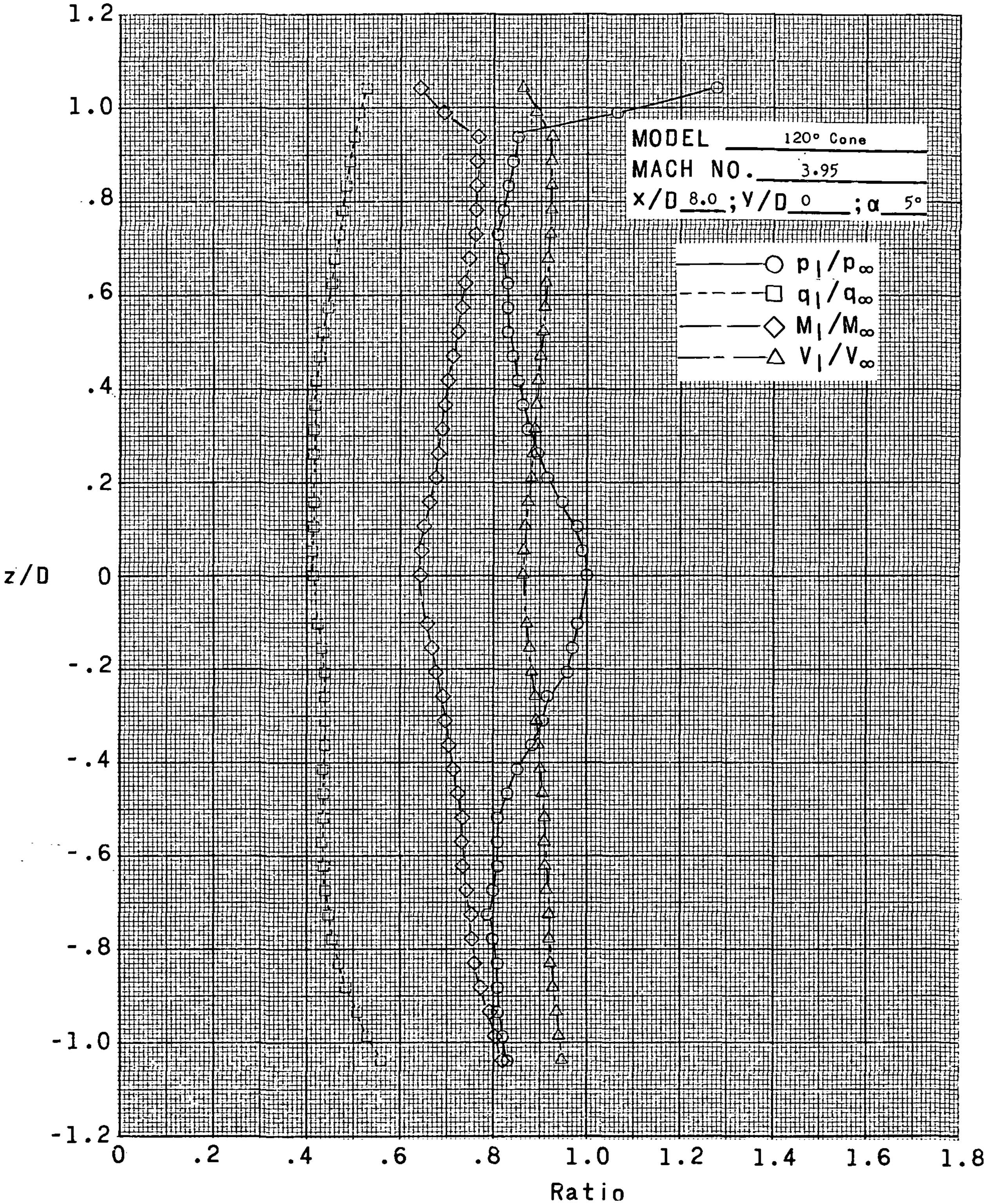
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 13.- Continued.



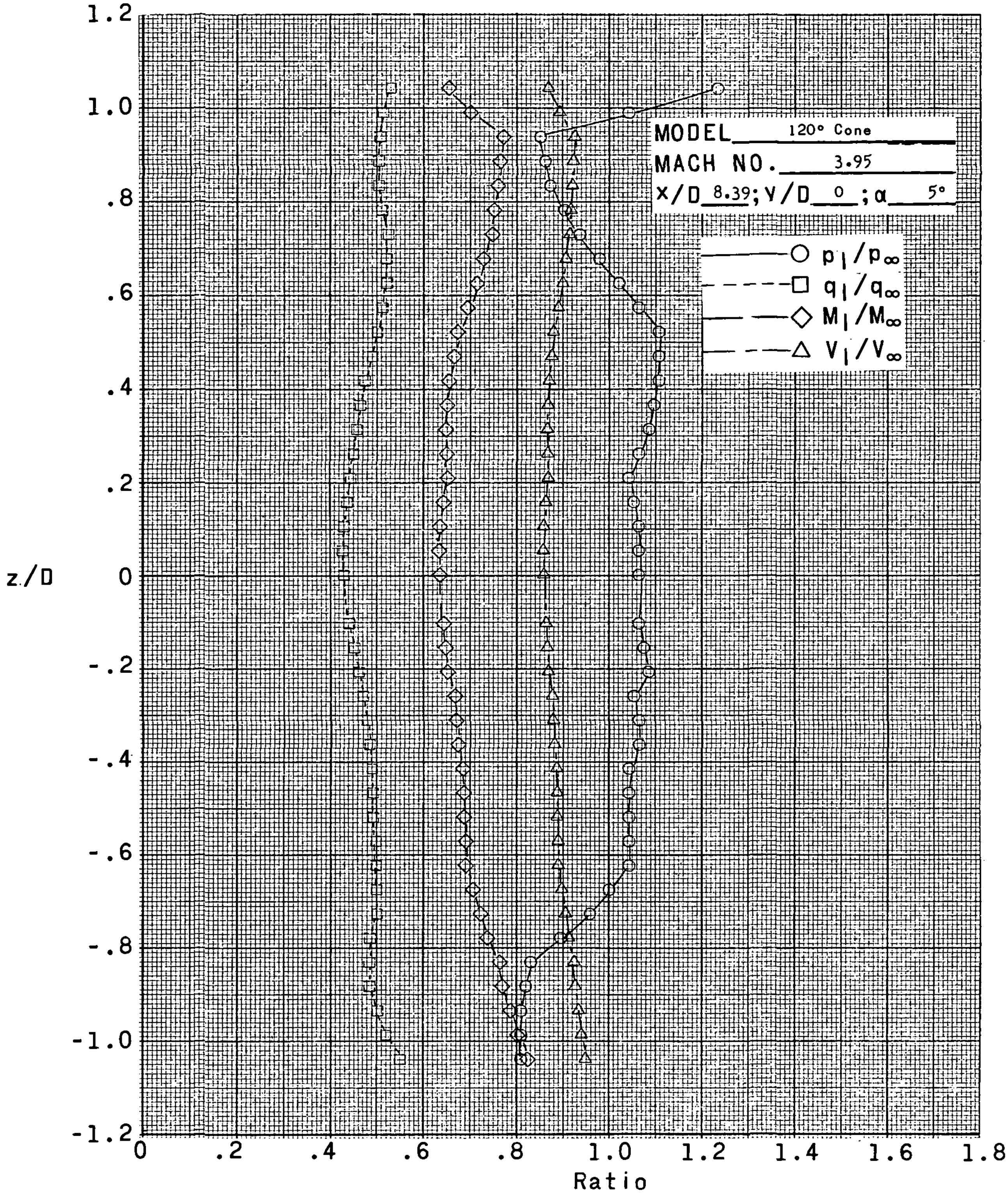
(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 5^{\circ}$.

Figure 13.- Continued.



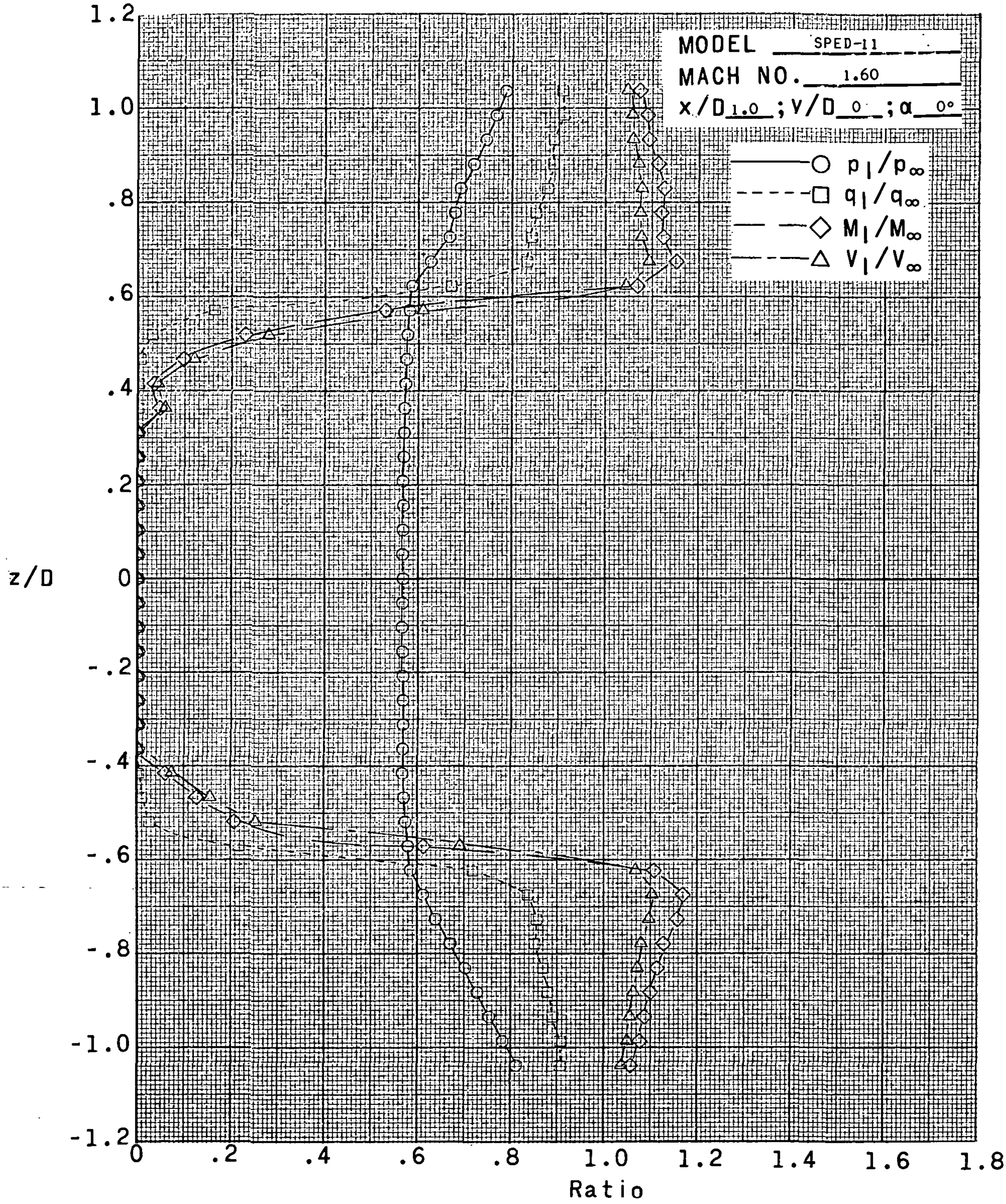
(j) $x/D = 8.0$; $y/D = 0$; $\alpha = 5^0$.

Figure 13.- Continued.



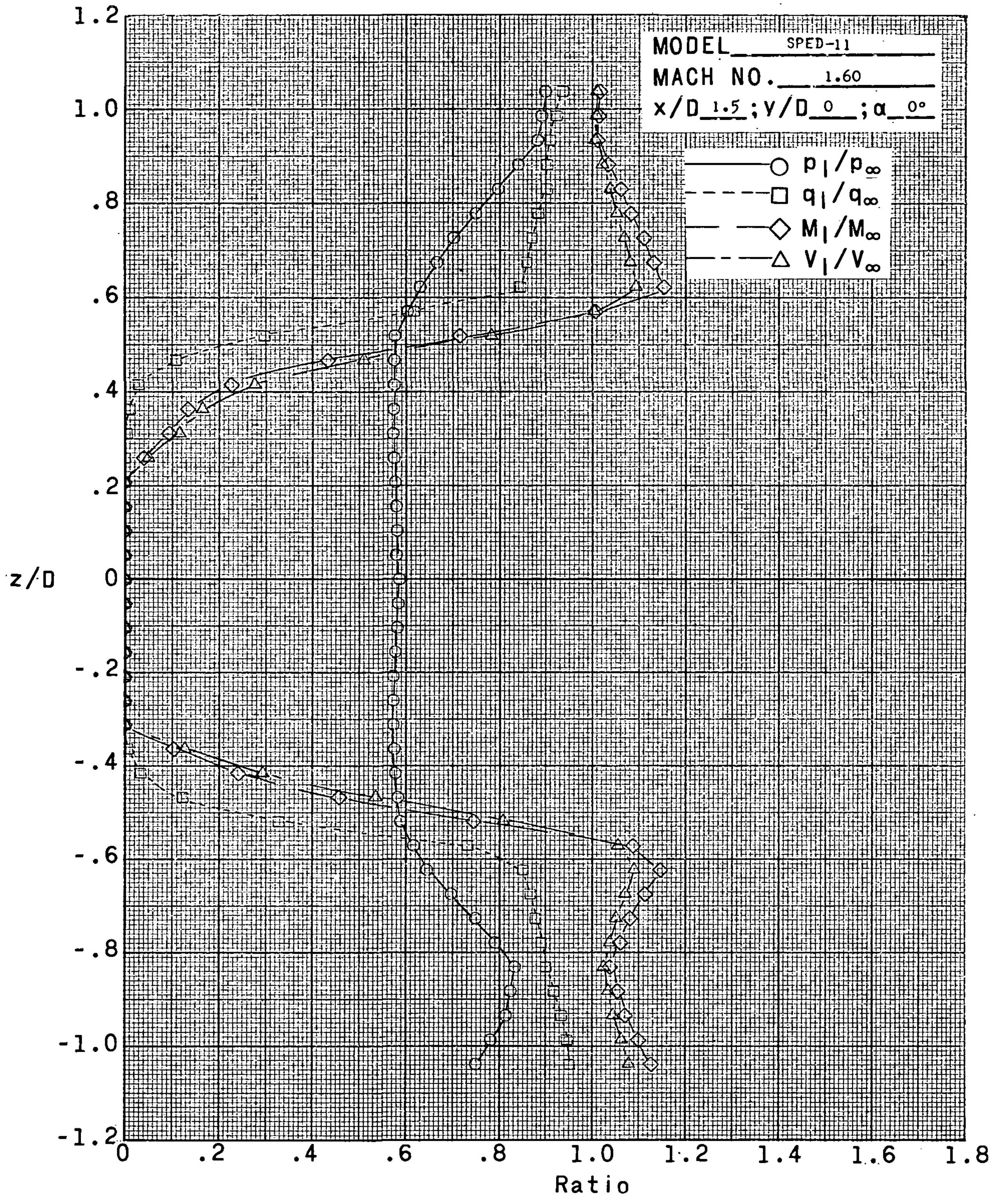
(k) x/D = 8.39; y/D = 0; α = 5°.

Figure 13.- Concluded.



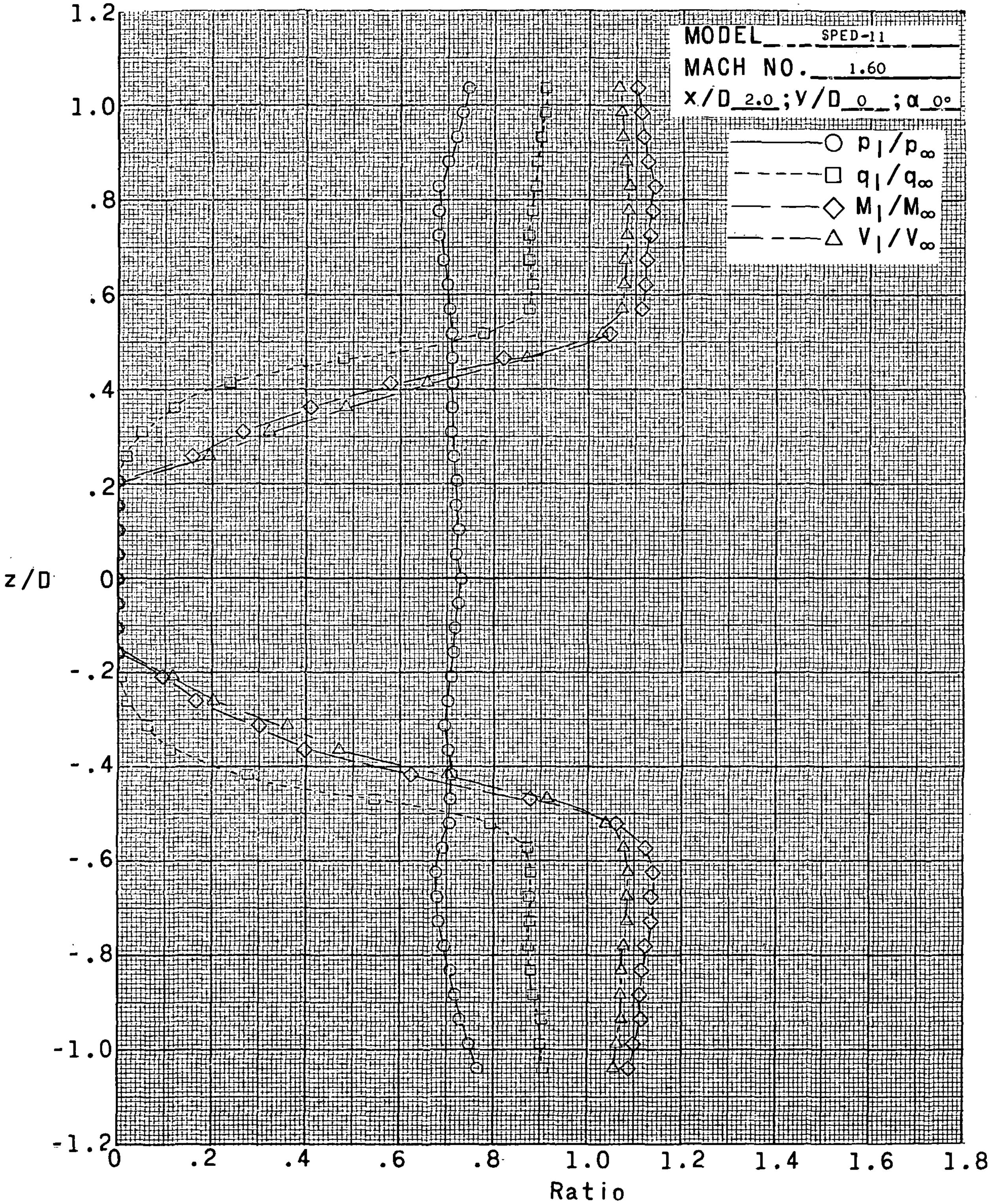
(a) x/D = 1.0; y/D = 0; α = 0°.

Figure 14.- Variation of p_l/p_∞, q_l/q_∞, M_l/M_∞, and V_l/V_∞ with z/D at the center of wake of the SPED-II vehicle at a Mach number of 1.60 and a Reynolds number of 1.65×10^6 per foot (5.42×10^6 per meter).



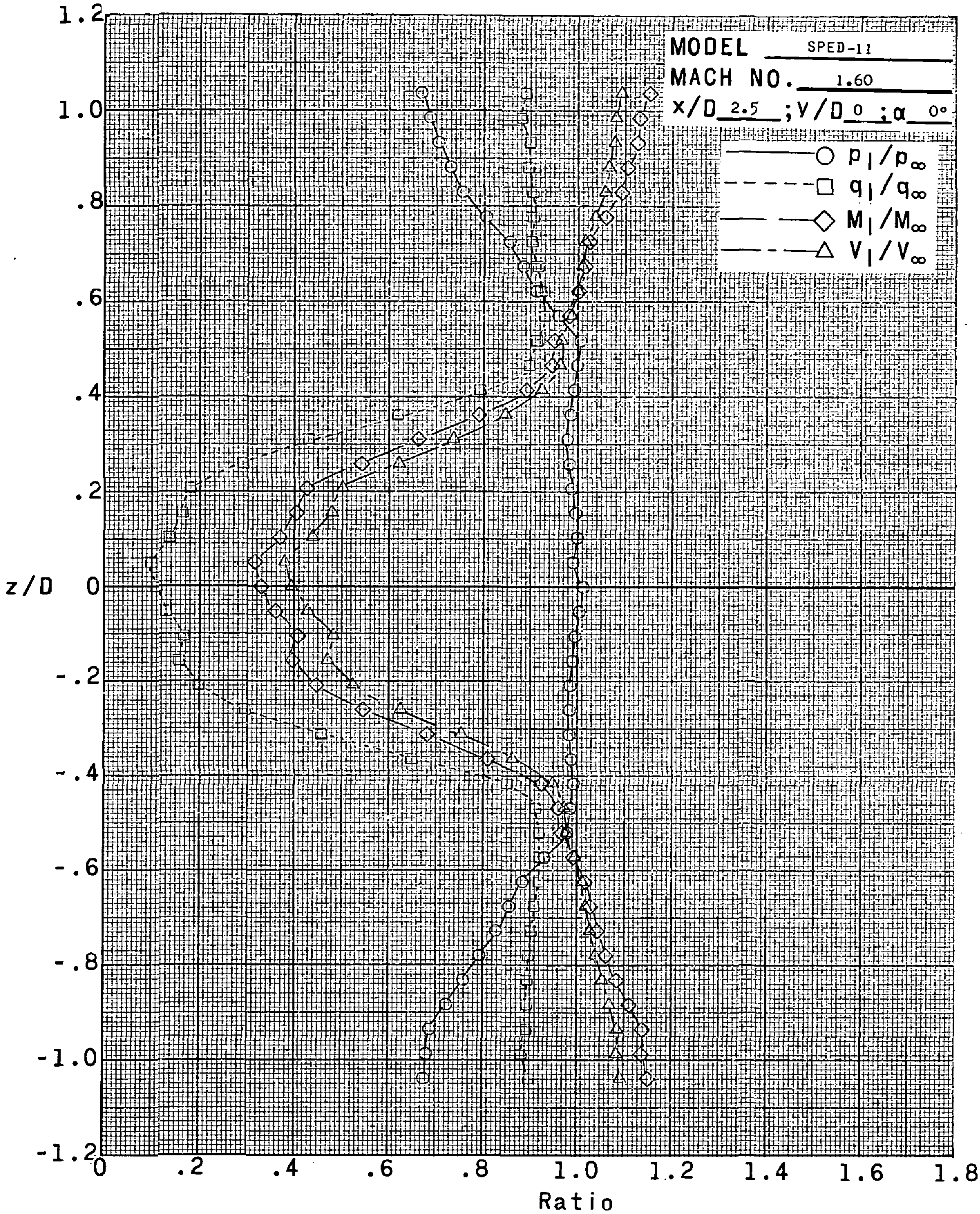
(b) x/D = 1.5; y/D = 0; α = 0°.

Figure 14.- Continued.



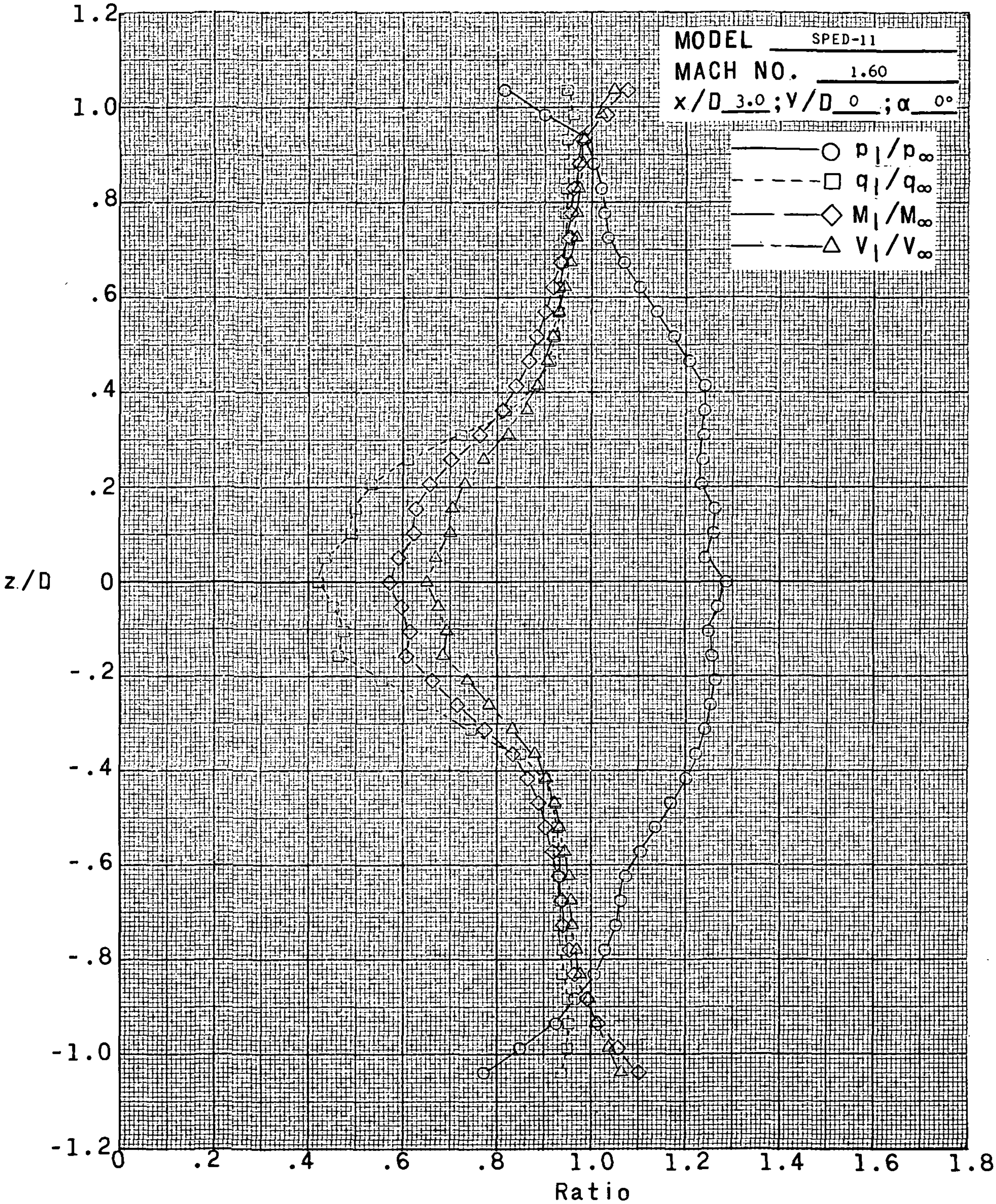
(c) x/D = 2.0; y/D = 0; α = 0°.

Figure 14.- Continued.



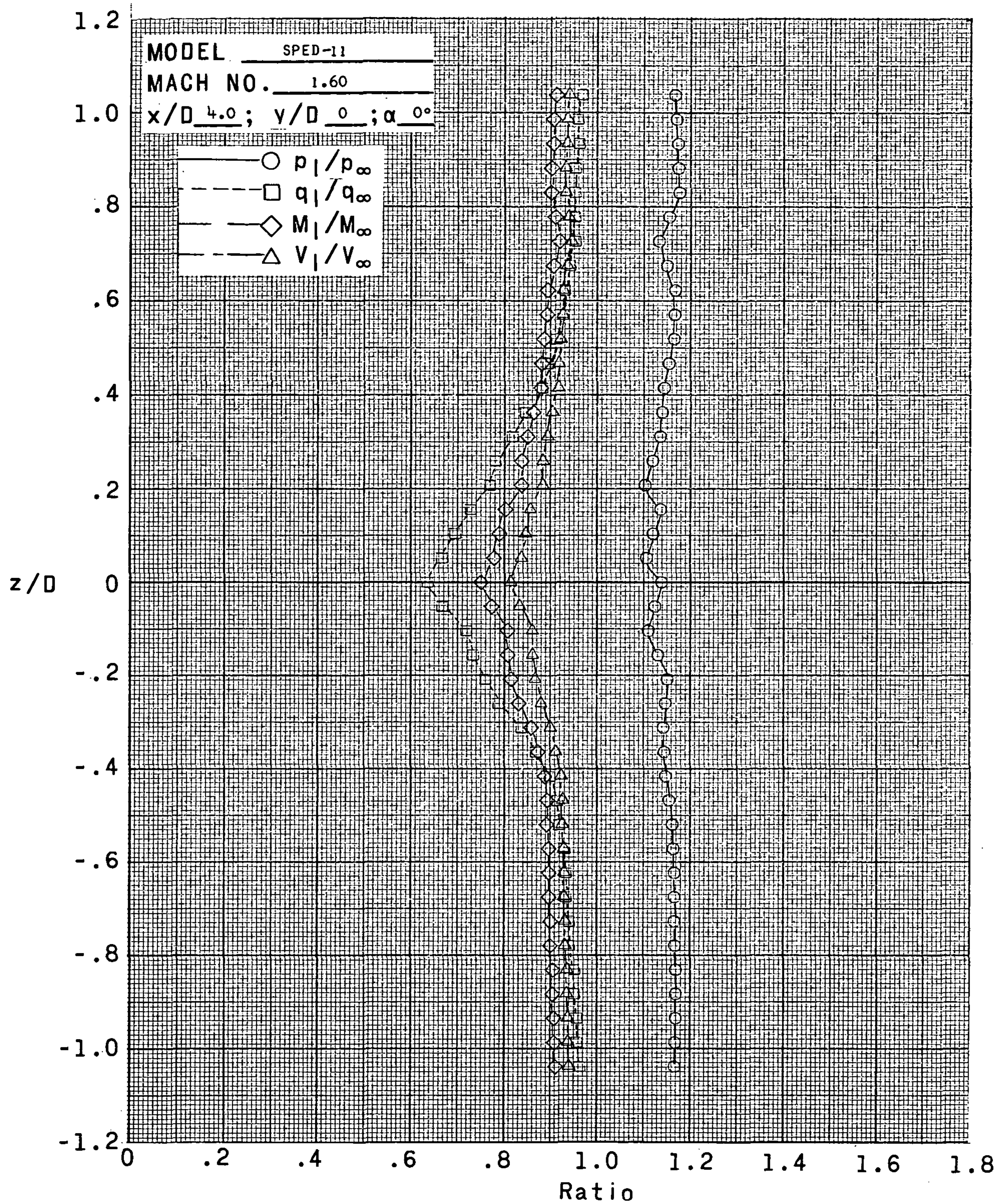
(d) x/D = 2.5; y/D = 0; α = 0°.

Figure 14.- Continued.



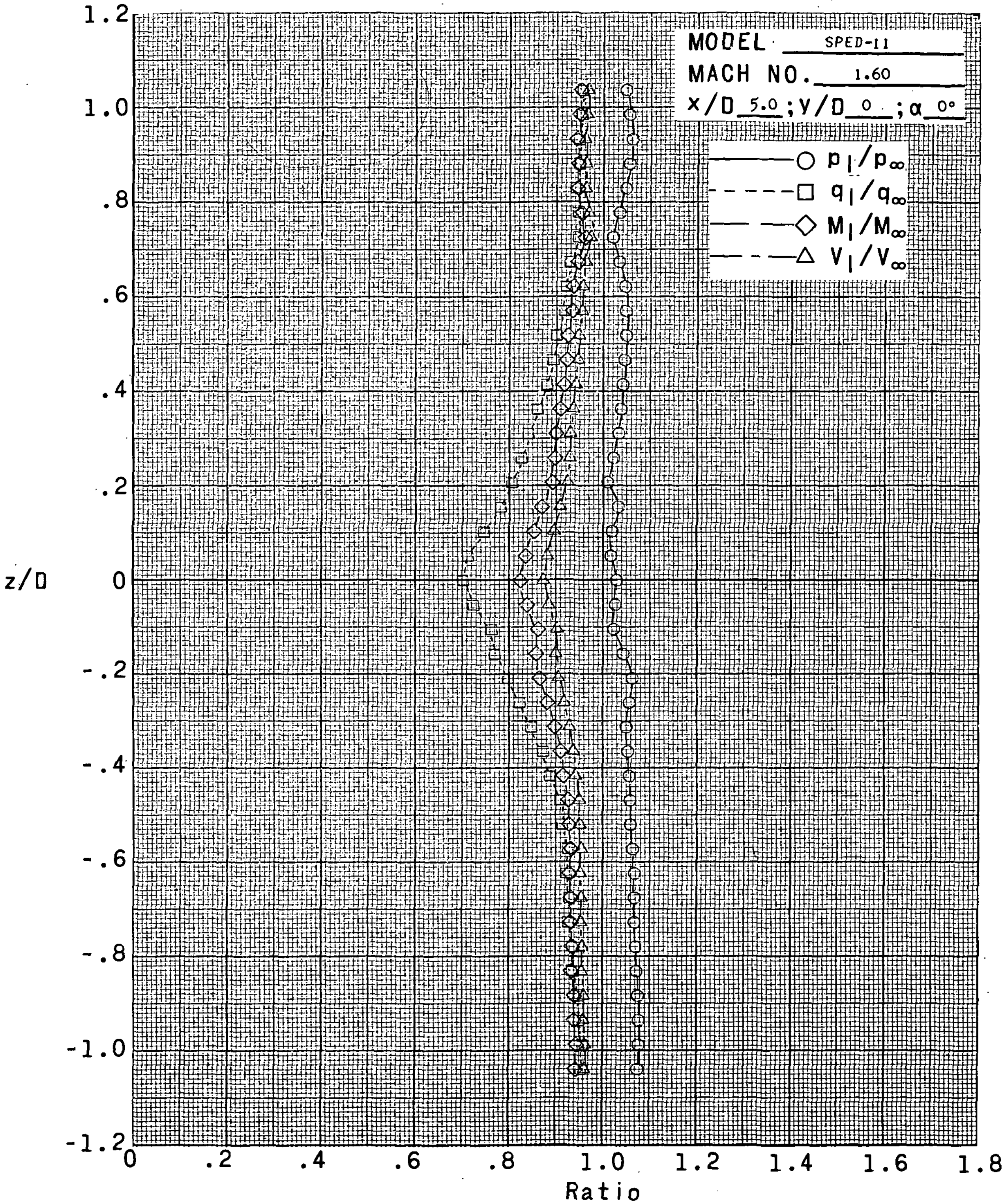
(e) $x/D = 3.0$; $y/D = 0$; $\alpha = 0°$.

Figure 14.- Continued.



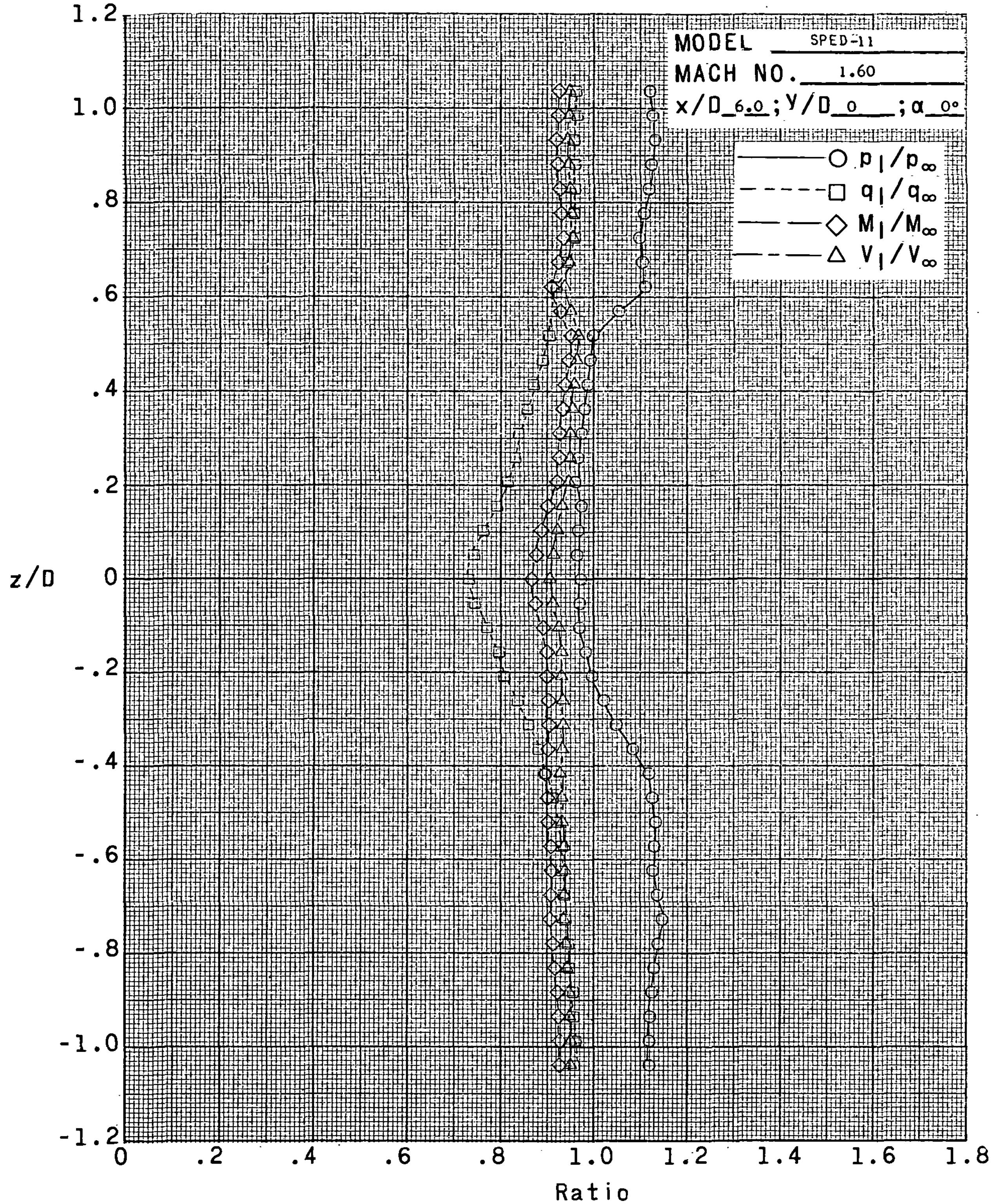
(f) $x/D = 4.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 14.- Continued.



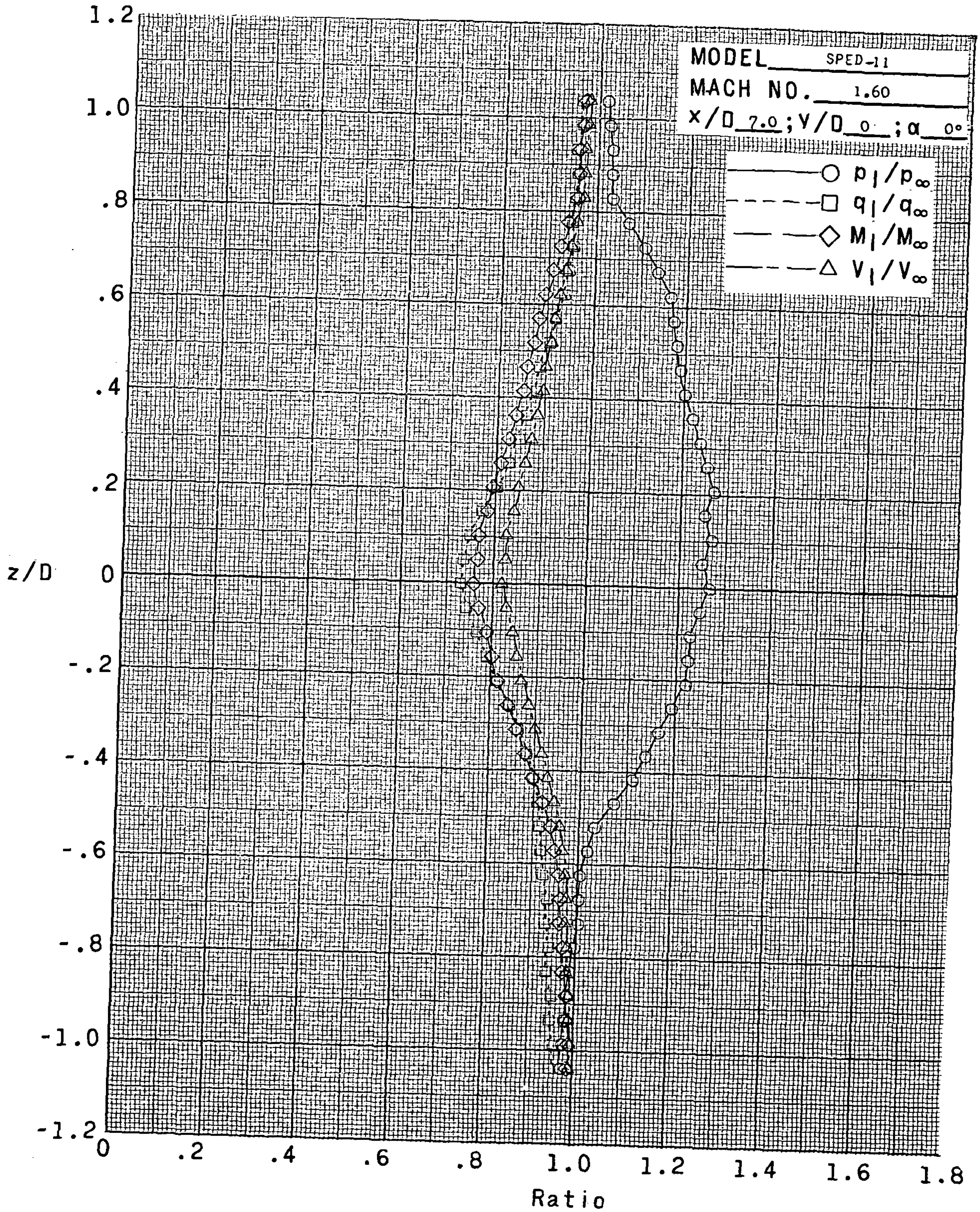
(g) $x/D = 5.0$; $y/D = 0$; $\alpha = 0^0$.

Figure 14.- Continued.



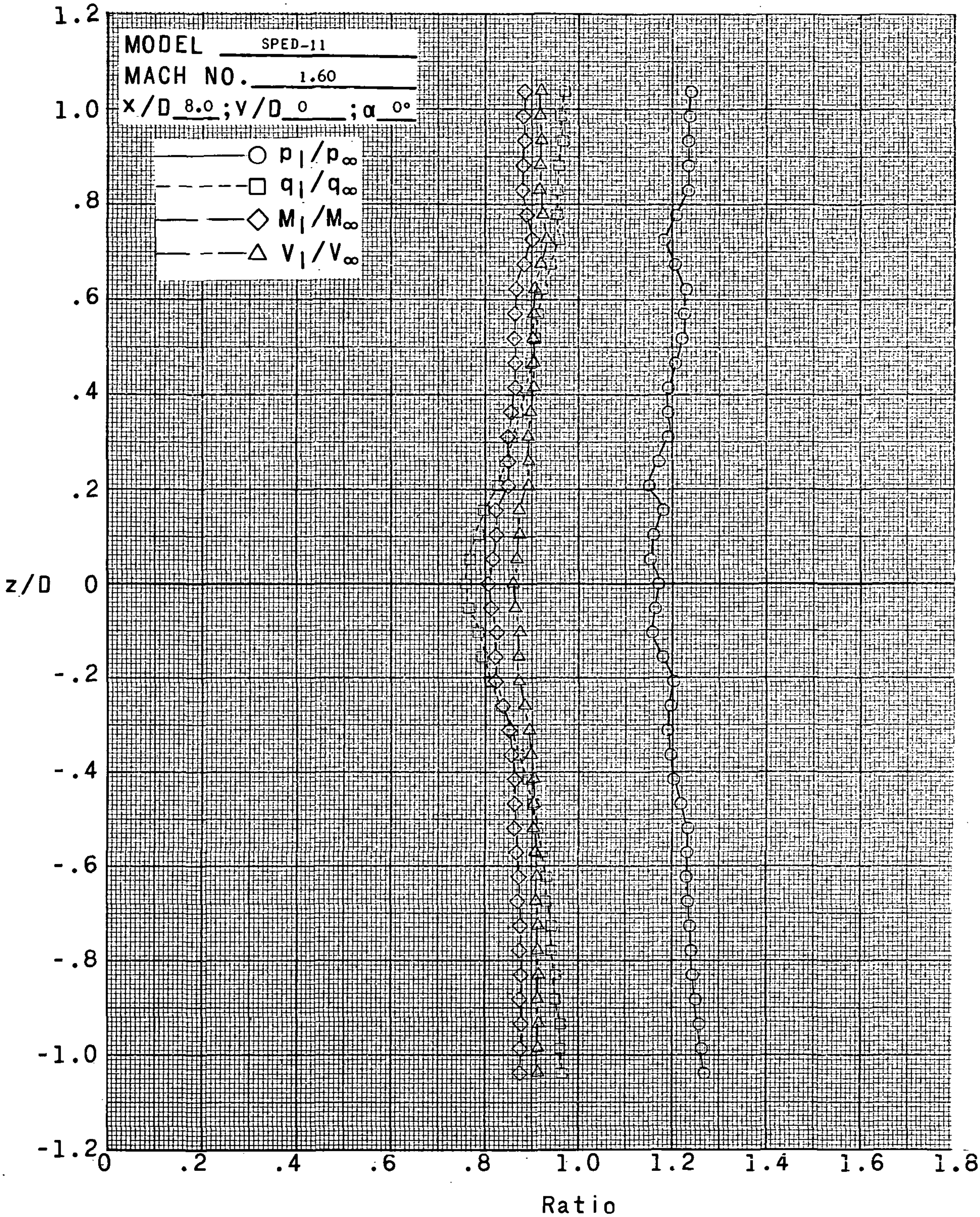
(h) $x/D = 6.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 14.- Continued.



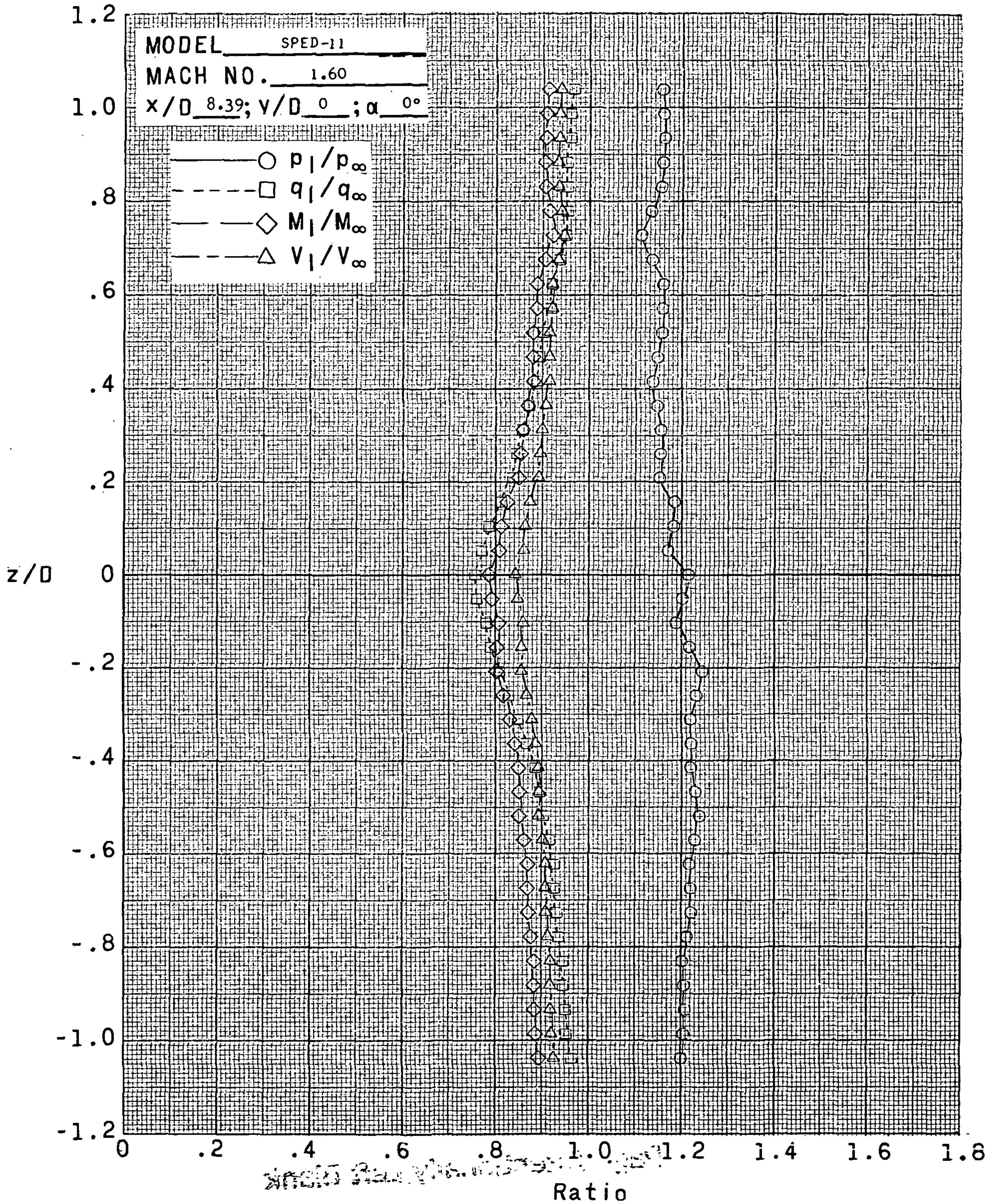
(i) $x/D = 7.0$; $y/D = 0$; $\alpha = 0^{\circ}$.

Figure 14.- Continued.



(j) x/D = 8.0; y/D = 0; $\alpha = 0^0$.

Figure 14.- Continued.



(k) x/D = 8.39; y/D = 0; α = 0°.

Figure 14.- Concluded.

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